

Broadband Outdoor Radiometer Calibration Shortwave

BORCAL-SW 2020-02

Generated by



Radiometer Calibration and Characterization

Customer

NREL-SRRL-BMS

Organization: NREL

Address: BMS, SRRL, Golden, CO 80401 USA

Phone: 303-384-6326

Calibration Facility

Solar Radiation Research Laboratory

Latitude: 39.742°N

Longitude: 105.180°W

Elevation: 1828.8 meters AMSL

Time Zone: -7.0

Calibration date

05/04/2020 to 05/05/2020

Report Date

December 9, 2021



NOTICE

This report was prepared as an account of work sponsored by an agency of the United States government. Neither the United States government nor any agency thereof, nor any of their employees, makes any warranty, express or implied, or assumes any legal liability or responsibility for the accuracy, completeness, or usefulness of any information, apparatus, product, or process disclosed, or represents that its use would not infringe privately owned rights. Reference herein to any specific commercial product, process, or service by trade name, trademark, manufacturer, or otherwise does not necessarily constitute or imply its endorsement, recommendation, or favoring by the United States government or any agency thereof. The views and opinions of authors expressed herein do not necessarily state or reflect those of the United States government or any agency thereof.

Broadband Outdoor Radiometer Calibration Report

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Introduction

This report compiles the calibration results from a Broadband Outdoor Radiometer Calibration (BORCAL). The work was accomplished at the Radiometer Calibration Facility shown on the front of this report. The calibration results reported here are traceable to the International System (SI) Units of Measurement.

This report includes these sections:

- Control Instruments - a group of instruments included in each BORCAL event that provides a measure of process consistency.
- Results Summary - a table of all instruments included in this report summarizing their calibration results and uncertainty.
- Instrument Details - the calibration certificates for each instrument.
- Environmental and Sky Conditions - meteorological conditions and reference irradiance during the calibration event.

BORCAL Notes or Comments

This report has been revised to accommodate updated responsivities given by the calibration provider of the BORCAL reference irradiance instruments. This report replaces the report with an issue date of May 12, 2020. This update affects all responsivities for the devices under test issued in this report by approximately -0.675%. There will also be a very slightly change in reported uncertainties due the reference irradiance instruments' uncertainties changing as well.

Control Instrument History

Figure 1. Eppley NIP Control Instrument History

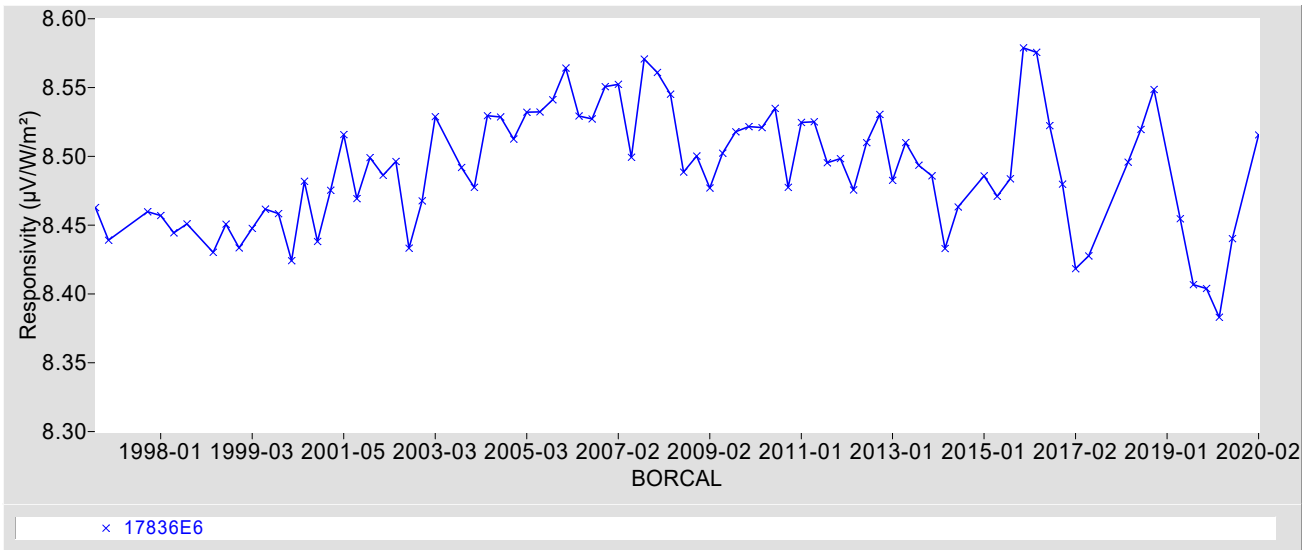
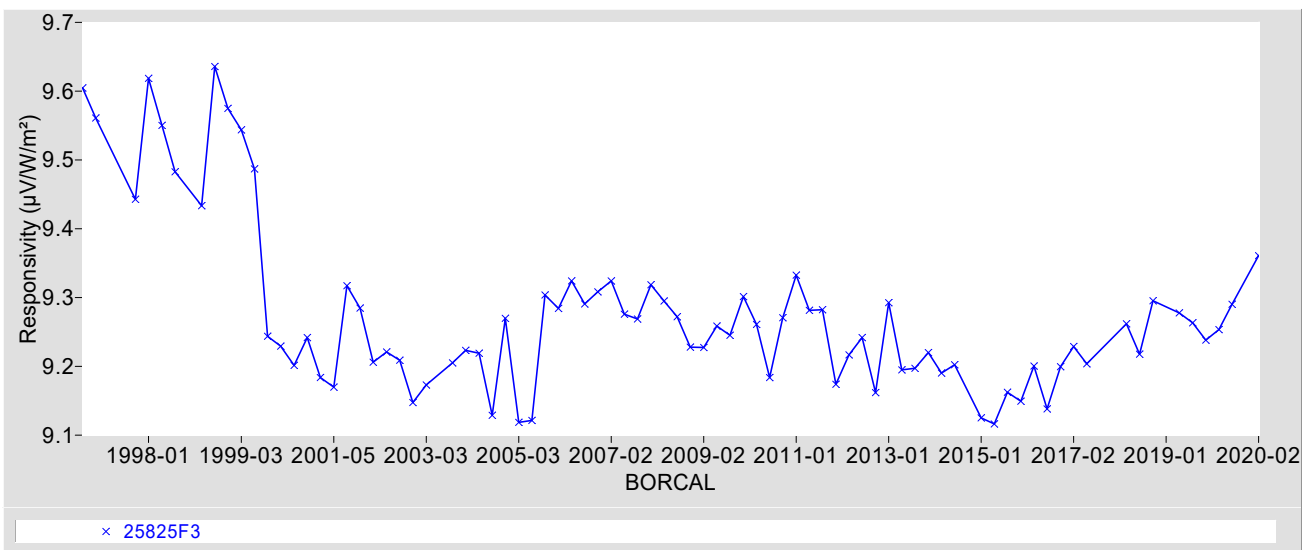


Figure 2. Eppley PSP Control Instrument History



Results Summary

Table 1. Results Summary

| Instrument | R@45 ¹ ($\mu\text{V/W/m}^2$) | CF@45 ¹ ($\text{W/m}^2/\text{mV}$) | U ² (%) | Rnet ³ ($\mu\text{V/W/m}^2$) | Page |
|--------------------------------|--|--|-----------------------|--|--------|
| 010046 Kipp & Zonen CM22 | 9.3651 | 106.78 | +1.5 / -1.2 | 0.087000 | A1-2 |
| 010284-DW-CM3 Kipp & Zonen CM3 | 17.344 | 57.657 | +1.9 / -2.2 | 0.40000 | A1-5 |
| 010995 Kipp & Zonen SP-LITE | 75.850 | 13.184 | +5.1 / -3.3 | 0 | A1-8 |
| 014261 Kipp & Zonen CM3 | 22.577 | 44.293 | +1.2 / -2.2 | 0.40000 | A1-11 |
| 015189 Kipp & Zonen CM6B | 11.069 | 90.340 | +2.0 / -2.5 | 0.30000 | A1-14 |
| 0212-2 Yankee TSP-700 | 3000.1 | 0.33333 | +1.7 / -1.4 | 0 | A1-17 |
| 080009 Kipp & Zonen CHP1 | 7.9207 | 126.25 | +0.83 / -0.75 | 0 | A1-20 |
| 080017 Kipp & Zonen CMP22 | 10.501 | 95.229 | +1.3 / -1.7 | 0.087000 | A1-23 |
| 100174 Kipp & Zonen CMP22 | 9.8524 | 101.50 | +0.88 / -1.1 | 0.087000 | A1-26 |
| 1171 Apogee SP-510 | 53.397 | 18.728 | +2.1 / -4.1 | 2.5000 | A1-29 |
| 140043 Kipp & Zonen CMP22 | 9.0791 | 110.14 | +0.94 / -1.1 | 0.087000 | A1-32 |
| 140108 Kipp & Zonen CHP1 | 8.0747 | 123.84 | +0.78 / -0.70 | 0 | A1-35 |
| 140712 Kipp & Zonen CMP11 | 9.1796 | 108.94 | +1.1 / -2.3 | 0.20500 | A1-38 |
| 140713 Kipp & Zonen CMP11 | 8.6806 | 115.20 | +1.0 / -1.8 | 0.20500 | A1-41 |
| 151027 Kipp & Zonen SP-LITE2 | 69.009 | 14.491 | +2.6 / -2.1 | 0 | A1-44 |
| 160430 Kipp & Zonen CMP22 | 9.8050 | 101.99 | +0.87 / -1.5 | 0.087000 | A1-47 |
| 194362 Kipp & Zonen SP-LITE2 | 72.703 | 13.755 | +2.5 / -2.1 | 0 | A1-50 |
| 21096 Eppley 8-48 | 11.649 | 85.844 | +3.6 / -1.6 | 0 | A1-53 |
| 2530 Hukseflux SR25 | 11.142 | 89.749 | +1.9 / -1.6 | 0.043000 | A1-56 |
| 2543 Hukseflux SR25 | 9.5397 | 104.83 | +1.1 / -1.2 | 0.043000 | A1-59 |
| 28402F3 Eppley PSP | 6.9486 | 143.91 | +2.0 / -2.0 | 0.64000 | A1-62 |
| 31137E6 Eppley NIP | 8.4394 | 118.49 | +1.6 / -0.86 | 0 | A1-65 |
| 34722 Eppley 8-48 | 9.7590 | 102.47 | +3.0 / -1.5 | 0 | A1-68 |
| 37831F3 Eppley GPP | 8.5290 | 117.25 | +1.7 / -2.9 | 0.15000 | A1-71 |
| 37839F3 Eppley SPP | 8.6353 | 115.80 | +1.5 / -1.7 | 0.30000 | A1-74 |
| 37882E6 Eppley sNIP | 8.3611 | 119.60 | +1.0 / -0.77 | 0 | A1-77 |
| 38924F3 Eppley SPP | 7.9068 | 126.47 | +1.8 / -2.4 | 0.22000 | A1-80 |
| 40337 Apogee SP-110 | 181.86 | 5.4986 | +2.0 / -1.8 | 0 | A1-83 |
| 9206 Hukseflux DR02 | 11.020 | 90.746 | +0.80 / -0.74 | 0 | A1-86 |
| 970003 Kipp & Zonen SP-LITE | 81.550 | 12.262 | +4.7 / -3.4 | 0 | A1-89 |
| A360 Delta-T SPN1 | 1019.4 | 0.98097 | +8.8 / -5.0 | 0 | A1-92 |
| F14077R EKO MS-802 | 7.1082 | 140.68 | +1.3 / -2.3 | 0.18000 | A1-95 |
| PY100360 Licor LI200R | 10.757 | 92.960 | +1.4 / -1.1 | 0 | A1-98 |
| PY108623 Licor LI200R | 9.9311 | 100.69 | +1.8 / -1.5 | 0 | A1-101 |
| PY1750 Licor LI200 | 13.157 | 76.007 | +1.3 / -1.3 | 0 | A1-104 |
| PY28257 Licor LI200 | 13.751 | 72.722 | +2.0 / -2.3 | 0 | A1-107 |
| PYHR101 Licor LI201SB | 6.0067 | 166.48 | +3.0 / -1.9 | 0 | A1-110 |
| S13071483 EKO MS-602 | 7.1318 | 140.22 | +1.9 / -4.4 | 0.30000 | A1-113 |
| S13135063 EKO ML-01 | 40.432 | 24.733 | +1.8 / -0.93 | 0 | A1-116 |
| S13144.085R EKO MS-410 | 9.3463 | 106.99 | +1.5 / -1.5 | 0.20000 | A1-119 |
| S17096005 EKO MS-80 | 10.633 | 94.049 | +1.2 / -1.3 | 0.043000 | A1-122 |
| S18015.22 EKO MS-57 | 6.6728 | 149.86 | +0.78 / -0.70 | 0 | A1-125 |

¹ CF = 1000 / R

² See certificate for valid zenith angle range

³ Instrument's Effective Net IR Response

Note: Environmental Conditions for BORCAL starts on page A1-128.

Appendix 1

Instrument Details

Calibration Certificates: 3 pages for each radiometer (4 including Environmental Conditions)

Environmental Conditions for BORCAL: Last Page of a Calibration Certificate. Note: This appears only once, at the end of Appendix 1.



National Renewable Energy Laboratory

Solar Radiation Research Laboratory

Metrology Laboratory

Calibration Certificate



| | | | |
|--------------------------|--------------------------|----------------------------------|--------------|
| Test Instrument: | Pyranometer (Ventilated) | Manufacturer: | Kipp & Zonen |
| Model: | CM22 | Serial Number: | 010046 |
| Calibration Date: | 5/5/2020 | Due Date: | 5/5/2021 |
| Customer: | NREL-SRRL-BMS | Environmental Conditions: | see page 4 |
| Test Dates: | 5/4-5 | | |

This certifies that the above product was calibrated in compliance with ISO/IEC 17025:2017. Measurement uncertainties at the time of calibration are consistent with the Guide to the Expression of Uncertainty in Measurement (GUM) using Reda et al., 2008. All nominal values are traceable to the International System (SI) Units of Measurement.

No statement of compliance with specifications is made or implied on this certificate. However, the estimated uncertainties are the uncertainties of the calibration process; users must add other uncertainties that are relevant to their measuring system, environmental and sky conditions, outdoor set-up, and site location.

The Type-B Standard Uncertainty of using the responsivity at each even zenith angle is reported, and the Expanded Uncertainty of the calibration is reported using two methods:

1. The Expanded Uncertainty of using the responsivity at zenith angle = 45°, within the zenith angle range from 30.0° to 60.0°
2. The Expanded Uncertainty of using Spline Interpolating Functions for the responsivity versus zenith angle.

This certificate applies only to the item identified above and shall not be reproduced other than in full, without specific written approval from the calibration facility. Certificate without signature is not valid.

Table 1. Traceability

| Measurement Type | Instrument | Calibration Date | Calibration Due Date |
|-----------------------|--|------------------|----------------------|
| Beam Irradiance † | Eppley Absolute Cavity Radiometer Model HF, S/N 29219 | 09/27/2019 | 09/27/2020 |
| Diffuse Irradiance † | Hukseflux Pyranometer Model SR25, S/N 2541 | 04/17/2020 | 04/17/2021 |
| Diffuse Irradiance † | Hukseflux Pyranometer Model SR25, S/N 2542 | 04/17/2020 | 04/17/2021 |
| Data Acquisition | NREL Data Acquisition System Model RAP-DAQ, S/N 2005-998 | 02/14/2019 | 02/14/2021 |
| Data Acquisition | NREL Data Acquisition System Model RAP-DAQ, S/N 2005-999 | 02/14/2019 | 02/14/2021 |
| Infrared Irradiance ‡ | Kipp & Zonen Pyrgeometer Model CGR4, S/N 140021 | 04/02/2019 | 04/02/2023 |

† Through the World Radiometric Reference (WRR)

‡ Through the World Infrared Standard Group (WISG)

Number of pages of certificate: 4

Calibration Procedure: BORCAL-P00-Calibration and QA Procedure; available upon request.

Setup: Radiometers are calibrated outdoors, using the sun as the source. Pyranometers and pyrgeometers are installed for horizontal measurements, with their signal connectors oriented north, if their design permits.

The shading disk for the reference diffuse subtends a solid angle of 5°. Pyrheliometers are installed on solar trackers.

Calibrated by: Afshin Andreas, Ibrahim Reda, Peter Gotseff, and RCC

Ibrahim Reda, Technical Manager

Date

For questions or comments, please contact the technical manager at:

ibrahim.reda@nrel.gov; 303-384-6385; 15013 Denver West Parkway, Golden, CO 80401, USA

Calibration Results

010046 Kipp & Zonen CM22

The responsivity (R , $\mu\text{V}/\text{W}/\text{m}^2$) of the test instrument during calibration is calculated using this Measurement Equation:

$$R = (V - R_{net} * W_{net}) / I \tag{1}$$

where,

- V = radiometer output voltage (microvolts),
 - R_{net} = radiometer net infrared responsivity ($\mu\text{V}/\text{W}/\text{m}^2$), see Table 4,
 - W_{net} = effective net infrared measured by pyrgeometer (W/m^2),
 - = $W_{in} - W_{out} = W_{in} - \sigma * T_c^4$
 - where, W_{in} = incoming infrared (W/m^2), $\sigma = 5.6704\text{e-}8 \text{ W}\cdot\text{m}^{-2}\cdot\text{K}^{-4}$,
 - T_c = case temperature of pyrgeometer (K).
- I = reference irradiance (W/m^2), beam (B) or global (G)
 - where, $G = B * \text{COS}(Z) + D$,
 - Z = zenith angle (degrees),
 - D = reference diffuse irradiance (W/m^2).

Figure 1. Responsivity vs Zenith Angle

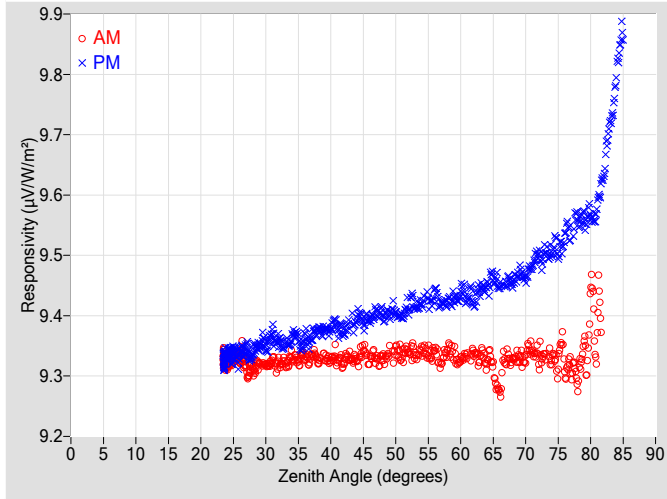


Figure 2. Responsivity vs Local Standard Time

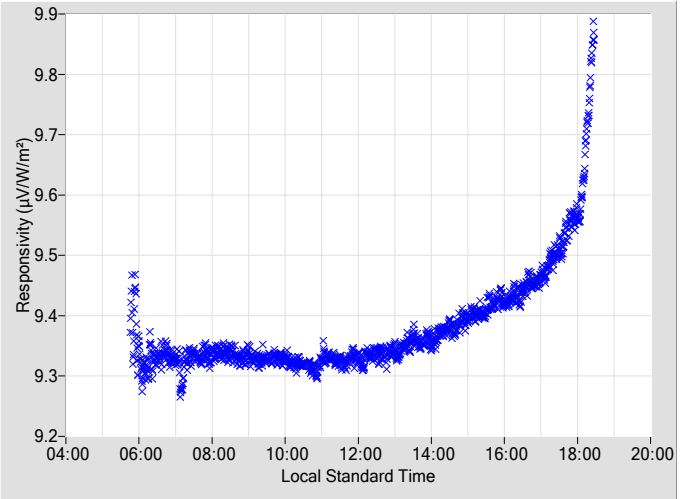


Table 2. Instrument Responsivity (R) and Calibration Type-B Standard Uncertainty, u(B)

| Zenith Angle (deg.) | R ($\mu\text{V}/\text{W}/\text{m}^2$) | u(B) \pm (%) | Azimuth Angle | R ($\mu\text{V}/\text{W}/\text{m}^2$) | u(B) \pm (%) | Azimuth Angle | Zenith Angle (deg.) | R ($\mu\text{V}/\text{W}/\text{m}^2$) | u(B) \pm (%) | Azimuth Angle | R ($\mu\text{V}/\text{W}/\text{m}^2$) | u(B) \pm (%) | Azimuth Angle |
|---------------------|---|----------------|---------------|---|----------------|---------------|---------------------|---|----------------|---------------|---|----------------|---------------|
| 0 | N/A | N/A | N/A | N/A | N/A | N/A | 46 | 9.3255 | 0.31 | 106.78 | 9.3930 | 0.31 | 252.84 |
| 2 | N/A | N/A | N/A | N/A | N/A | N/A | 48 | 9.3292 | 0.33 | 104.51 | 9.4011 | 0.31 | 255.09 |
| 4 | N/A | N/A | N/A | N/A | N/A | N/A | 50 | 9.3421 | 0.32 | 102.43 | 9.4034 | 0.33 | 257.25 |
| 6 | N/A | N/A | N/A | N/A | N/A | N/A | 52 | 9.3388 | 0.32 | 100.39 | 9.4154 | 0.32 | 259.31 |
| 8 | N/A | N/A | N/A | N/A | N/A | N/A | 54 | 9.3432 | 0.35 | 98.42 | 9.4209 | 0.33 | 261.24 |
| 10 | N/A | N/A | N/A | N/A | N/A | N/A | 56 | 9.3425 | 0.37 | 96.60 | 9.4413 | 0.33 | 263.12 |
| 12 | N/A | N/A | N/A | N/A | N/A | N/A | 58 | 9.3438 | 0.36 | 94.81 | 9.4244 | 0.34 | 264.93 |
| 14 | N/A | N/A | N/A | N/A | N/A | N/A | 60 | 9.3267 | 0.35 | 93.07 | 9.4412 | 0.37 | 266.68 |
| 16 | N/A | N/A | N/A | N/A | N/A | N/A | 62 | 9.3386 | 0.35 | 91.36 | 9.4220 | 0.36 | 268.41 |
| 18 | N/A | N/A | N/A | N/A | N/A | N/A | 64 | 9.3211 | 0.37 | 89.69 | 9.4495 | 0.37 | 270.06 |
| 20 | N/A | N/A | N/A | N/A | N/A | N/A | 66 | 9.2752 | 0.38 | 88.05 | 9.4489 | 0.38 | 271.73 |
| 22 | N/A | N/A | N/A | N/A | N/A | N/A | 68 | 9.3275 | 0.43 | 86.39 | 9.4534 | 0.40 | 273.37 |
| 24 | 9.3229 | 0.31 | 166.80 | 9.3349 | 0.31 | 192.80 | 70 | 9.3310 | 0.42 | 84.79 | 9.4625 | 0.43 | 275.00 |
| 26 | 9.3316 | 0.33 | 150.95 | 9.3385 | 0.31 | 209.24 | 72 | 9.3350 | 0.45 | 83.20 | 9.5000 | 0.46 | 276.61 |
| 28 | 9.3126 | 0.33 | 140.77 | 9.3380 | 0.31 | 217.98 | 74 | 9.3301 | 0.50 | 81.62 | 9.5046 | 0.50 | 278.21 |
| 30 | 9.3187 | 0.32 | 134.34 | 9.3465 | 0.30 | 224.76 | 76 | 9.3158 | 0.55 | 80.00 | 9.5296 | 0.56 | 279.80 |
| 32 | 9.3199 | 0.33 | 129.28 | 9.3586 | 0.32 | 229.99 | 78 | 9.2952 | 0.62 | 78.40 | 9.5608 | N/A | 281.41 |
| 34 | 9.3303 | 0.33 | 124.77 | 9.3620 | 0.33 | 234.46 | 80 | 9.4253 | N/A | 76.76 | 9.5674 | N/A | 283.06 |
| 36 | 9.3320 | 0.31 | 121.03 | 9.3656 | 0.31 | 238.43 | 82 | N/A | N/A | N/A | 9.6327 | N/A | 284.71 |
| 38 | 9.3257 | 0.32 | 117.59 | 9.3762 | 0.31 | 241.85 | 84 | N/A | N/A | N/A | 9.8036 | N/A | 286.40 |
| 40 | 9.3273 | 0.31 | 114.53 | 9.3788 | 0.34 | 245.02 | 86 | N/A | N/A | N/A | N/A | N/A | N/A |
| 42 | 9.3221 | 0.32 | 111.70 | 9.3704 | 0.32 | 247.83 | 88 | N/A | N/A | N/A | N/A | N/A | N/A |
| 44 | 9.3255 | 0.32 | 109.17 | 9.3968 | 0.31 | 250.47 | 90 | N/A | N/A | N/A | N/A | N/A | N/A |

N/A - Not Available

Figure 3. Type-B Standard Uncertainty vs Zenith Angle

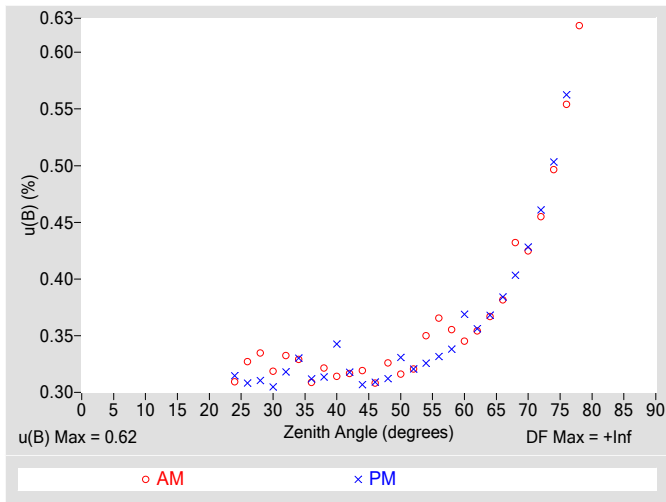


Figure 4. Residuals from Spline Interpolation

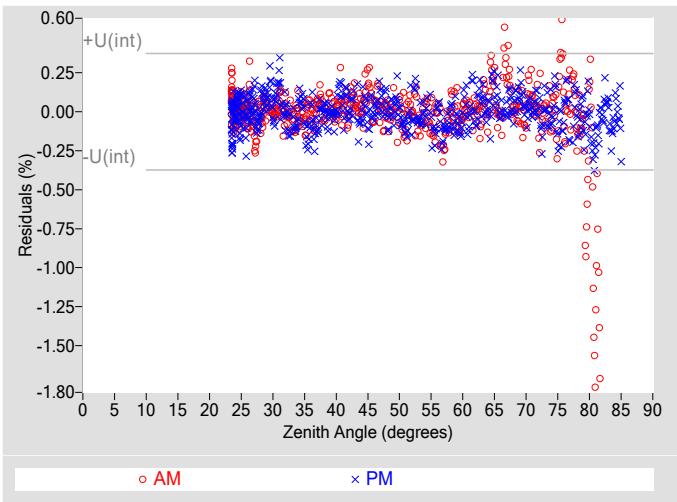


Table 3. Uncertainty using Spline Interpolation ‡

| | |
|---|------------|
| Type-B Standard Uncertainty, $u(B)$ (%) | ± 0.62 |
| Type-A Interpolating Function, $u(int)$ (%) | ± 0.19 |
| Combined Standard Uncertainty, $u(c)$ (%) | ± 0.65 |
| Effective degrees of freedom, $DF(c)$ | 169568 |
| Coverage factor, k | 1.96 |
| Expanded Uncertainty, U_{95} (%) | ± 1.3 |
| AM Valid zenith angle range | 24° to 78° |
| PM Valid zenith angle range | 24° to 76° |

‡ An illustration for how to reduce the uncertainty in calculating the irradiance using a function rather than $R@45^\circ$. Not accredited.

Table 4. Calibration Label Values

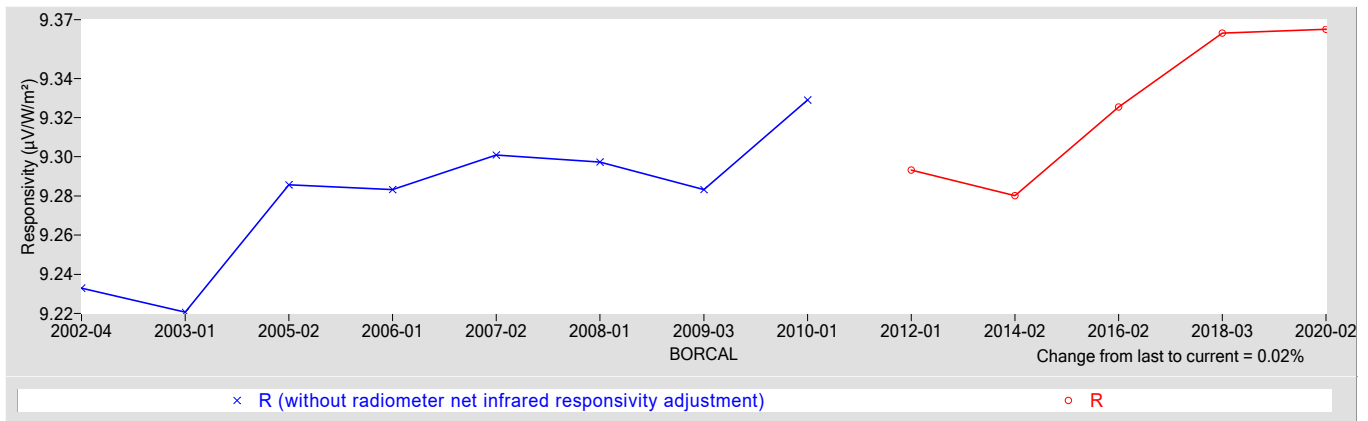
| | |
|----------------------------------|-------------------------------|
| $R @ 45^\circ$ ($\mu V/W/m^2$) | R_{net} ($\mu V/W/m^2$) † |
| 9.3651 | 0.087000 |

† R_{net} determination date: Estimated

Table 5. Uncertainty using $R @ 45^\circ$

| | |
|---|----------------|
| Type-B Expanded Uncertainty, $U(B)$ (%) | ± 0.72 |
| Offset Uncertainty, $U(off)$ (%) | +0.81 / -0.50 |
| Expanded Uncertainty, U (%) | +1.5 / -1.2 |
| Effective degrees of freedom, DF | +Inf |
| Coverage factor, k | 1.96 |
| Valid zenith angle range | 30.0° to 60.0° |

Figure 5. History of instrument at Zenith Angle = 45°



References:

[1] Reda, I.; Hickey, J.; Long, C.; Myers, D.; Stoffel, T.; Wilcox, S.; Michalsky, J. J.; Dutton, E. G.; Nelson, D. (2005). "Using a Blackbody to Calculate Net Longwave Responsivity of Shortwave Solar Pyranometers to Correct for Their Thermal Offset Error During Outdoor Calibration Using the Component Sum Method." *Journal of Atmospheric and Oceanic Technology*, 2005; pp. 1531-1540; NREL Report No. JA-560-36646. doi:10.1175/JTECH1782.1

[2] Reda, I.; Myers, D.; Stoffel, T. (2008). "Uncertainty Estimate for the Outdoor Calibration of Solar Pyranometers: A Metrologist Perspective." *Measure*. (NCSLI *Journal of Measurement Science*). Vol. 3(4), December 2008; pp. 58-66; NREL Report No. JA-581-4137

[3] Reda, I.; Andreas, A. (2004). "Solar Position Algorithm for Solar Radiation Applications." *Solar Energy*. Vol. 76(5), 2004; pp. 577-589; NREL Report No. JA-560-35518. doi:10.1016/j.solener.2003.12.003

[4] Stoffel, T.; Reda, I. (2009). "NREL Pyrheliometer Comparisons: 22 September - 3 October 2008 (NPC-2008)." 54 pp.; NREL Report No. TP-550-45016.

[5] Reda, I.; Stoffel, T.; Myers, D. (2003). "Method to Calibrate a Solar Pyranometer for Measuring Reference Diffuse Irradiance." *Solar Energy*. Vol. 74, 2003; pp. 103-112; NREL Report No. JA-560-35025. doi:10.1016/S0038-092X(03)00124-5

[6] Reda, I. (1996). *Calibration of a Solar Absolute Cavity Radiometer with Traceability to the World Radiometric Reference*. 79 pp.; NREL Report No. TP-463-20619.

[7] Reda, I.; Gröbner, J.; Stoffel, T.; Myers, D.; Forgan, B. (2008). *Improvements in the Blackbody Calibration of Pyrgometers*. ARM 2008 Science Team Meeting (Poster).



National Renewable Energy Laboratory

Solar Radiation Research Laboratory

Metrology Laboratory

Calibration Certificate



| | | | |
|--------------------------|---------------|----------------------------------|---------------|
| Test Instrument: | Pyranometer | Manufacturer: | Kipp & Zonen |
| Model: | CM3 | Serial Number: | 010284-DW-CM3 |
| Calibration Date: | 5/5/2020 | Due Date: | 5/5/2021 |
| Customer: | NREL-SRRL-BMS | Environmental Conditions: | see page 4 |
| Test Dates: | 5/4-5 | | |

This certifies that the above product was calibrated in compliance with ISO/IEC 17025:2017. Measurement uncertainties at the time of calibration are consistent with the Guide to the Expression of Uncertainty in Measurement (GUM) using Reda et al., 2008. All nominal values are traceable to the International System (SI) Units of Measurement.

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2. The Expanded Uncertainty of using Spline Interpolating Functions for the responsivity versus zenith angle.

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Table 1. Traceability

| Measurement Type | Instrument | Calibration Date | Calibration Due Date |
|-----------------------|--|------------------|----------------------|
| Beam Irradiance † | Eppley Absolute Cavity Radiometer Model HF, S/N 29219 | 09/27/2019 | 09/27/2020 |
| Diffuse Irradiance † | Hukseflux Pyranometer Model SR25, S/N 2541 | 04/17/2020 | 04/17/2021 |
| Diffuse Irradiance † | Hukseflux Pyranometer Model SR25, S/N 2542 | 04/17/2020 | 04/17/2021 |
| Data Acquisition | NREL Data Acquisition System Model RAP-DAQ, S/N 2005-998 | 02/14/2019 | 02/14/2021 |
| Data Acquisition | NREL Data Acquisition System Model RAP-DAQ, S/N 2005-999 | 02/14/2019 | 02/14/2021 |
| Infrared Irradiance ‡ | Kipp & Zonen Pyrgeometer Model CG4, S/N FT002 | 04/16/2018 | 04/16/2022 |

† Through the World Radiometric Reference (WRR)

‡ Through the World Infrared Standard Group (WISG)

Number of pages of certificate: 4

Calibration Procedure: BORCAL-P00-Calibration and QA Procedure; available upon request.

Setup: Radiometers are calibrated outdoors, using the sun as the source. Pyranometers and pyrgeometers are installed for horizontal measurements, with their signal connectors oriented north, if their design permits.

The shading disk for the reference diffuse subtends a solid angle of 5°. Pyrheliometers are installed on solar trackers.

Calibrated by: Afshin Andreas, Ibrahim Reda, Peter Gotseff, and RCC

Ibrahim Reda, Technical Manager

Date

For questions or comments, please contact the technical manager at:
ibrahim.reda@nrel.gov; 303-384-6385; 15013 Denver West Parkway, Golden, CO 80401, USA

Calibration Results

010284-DW-CM3 Kipp & Zonen CM3

The responsivity (R , $\mu\text{V}/\text{W}/\text{m}^2$) of the test instrument during calibration is calculated using this Measurement Equation:

$$R = (V - R_{net} * W_{net}) / I \tag{1}$$

where,

- V = radiometer output voltage (microvolts),
 - R_{net} = radiometer net infrared responsivity ($\mu\text{V}/\text{W}/\text{m}^2$), see Table 4,
 - W_{net} = effective net infrared measured by pyrgeometer (W/m^2),
 - = $W_{in} - W_{out} = W_{in} - \sigma * T_c^4$
 - where, W_{in} = incoming infrared (W/m^2), $\sigma = 5.6704\text{e-}8 \text{ W}\cdot\text{m}^{-2}\cdot\text{K}^{-4}$,
 - T_c = case temperature of pyrgeometer (K).
- I = reference irradiance (W/m^2), beam (B) or global (G)
 - where, $G = B * \text{COS}(Z) + D$,
 - Z = zenith angle (degrees),
 - D = reference diffuse irradiance (W/m^2).

Figure 1. Responsivity vs Zenith Angle

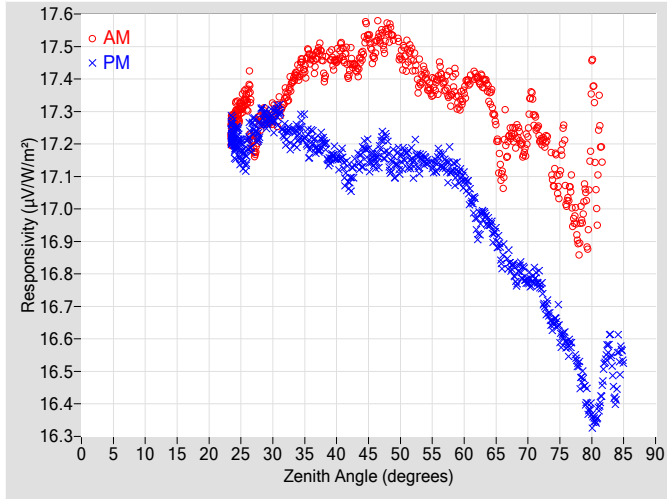


Figure 2. Responsivity vs Local Standard Time

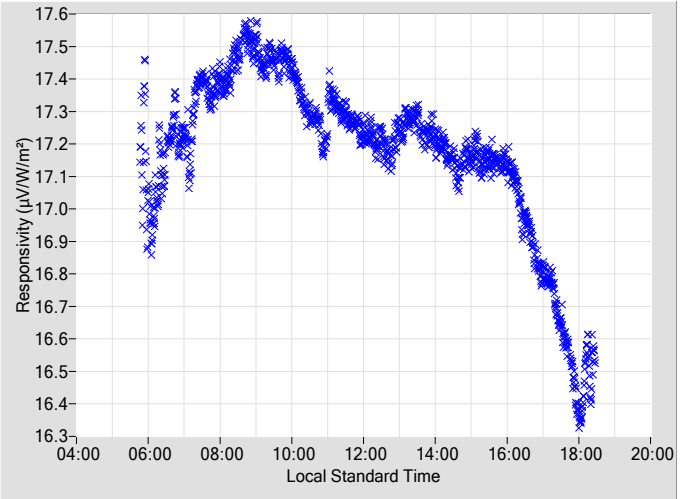


Table 2. Instrument Responsivity (R) and Calibration Type-B Standard Uncertainty, $u(B)$

| Zenith Angle (deg.) | R ($\mu\text{V}/\text{W}/\text{m}^2$) | AM $u(B)$ \pm (%) | Azimuth Angle | R ($\mu\text{V}/\text{W}/\text{m}^2$) | PM $u(B)$ \pm (%) | Azimuth Angle | Zenith Angle (deg.) | R ($\mu\text{V}/\text{W}/\text{m}^2$) | AM $u(B)$ \pm (%) | Azimuth Angle | R ($\mu\text{V}/\text{W}/\text{m}^2$) | PM $u(B)$ \pm (%) | Azimuth Angle |
|---------------------|---|---------------------|---------------|---|---------------------|---------------|---------------------|---|---------------------|---------------|---|---------------------|---------------|
| 0 | N/A | N/A | N/A | N/A | N/A | N/A | 46 | 17.489 | 0.33 | 106.78 | 17.144 | 0.31 | 252.83 |
| 2 | N/A | N/A | N/A | N/A | N/A | N/A | 48 | 17.547 | 0.33 | 104.56 | 17.182 | 0.31 | 255.09 |
| 4 | N/A | N/A | N/A | N/A | N/A | N/A | 50 | 17.476 | 0.33 | 102.42 | 17.140 | 0.32 | 257.24 |
| 6 | N/A | N/A | N/A | N/A | N/A | N/A | 52 | 17.464 | 0.37 | 100.42 | 17.144 | 0.32 | 259.25 |
| 8 | N/A | N/A | N/A | N/A | N/A | N/A | 54 | 17.404 | 0.35 | 98.46 | 17.147 | 0.33 | 261.24 |
| 10 | N/A | N/A | N/A | N/A | N/A | N/A | 56 | 17.410 | 0.36 | 96.59 | 17.163 | 0.34 | 263.11 |
| 12 | N/A | N/A | N/A | N/A | N/A | N/A | 58 | 17.355 | 0.34 | 94.81 | 17.115 | 0.34 | 264.92 |
| 14 | N/A | N/A | N/A | N/A | N/A | N/A | 60 | 17.354 | 0.37 | 93.06 | 17.089 | 0.35 | 266.68 |
| 16 | N/A | N/A | N/A | N/A | N/A | N/A | 62 | 17.407 | 0.36 | 91.36 | 16.941 | 0.36 | 268.40 |
| 18 | N/A | N/A | N/A | N/A | N/A | N/A | 64 | 17.350 | 0.42 | 89.69 | 16.958 | 0.37 | 270.10 |
| 20 | N/A | N/A | N/A | N/A | N/A | N/A | 66 | 17.095 | 0.42 | 88.04 | 16.848 | 0.39 | 271.68 |
| 22 | N/A | N/A | N/A | N/A | N/A | N/A | 68 | 17.225 | 0.41 | 86.39 | 16.788 | 0.41 | 273.37 |
| 24 | 17.279 | 0.31 | 167.00 | 17.207 | 0.31 | 193.21 | 70 | 17.256 | 0.46 | 84.79 | 16.783 | 0.44 | 275.00 |
| 26 | 17.343 | 0.30 | 150.94 | 17.184 | 0.33 | 209.12 | 72 | 17.211 | 0.56 | 83.19 | 16.767 | 0.47 | 276.61 |
| 28 | 17.271 | 0.30 | 140.94 | 17.259 | 0.33 | 217.97 | 74 | 17.092 | 0.59 | 81.62 | 16.647 | 0.52 | 278.21 |
| 30 | 17.291 | 0.32 | 134.56 | 17.277 | 0.35 | 224.64 | 76 | 17.061 | 0.57 | 80.00 | 16.589 | 0.58 | 279.80 |
| 32 | 17.345 | 0.32 | 129.13 | 17.229 | 0.31 | 230.09 | 78 | 16.901 | 0.64 | 78.40 | 16.502 | N/A | 281.41 |
| 34 | 17.417 | 0.31 | 124.85 | 17.223 | 0.33 | 234.55 | 80 | 17.329 | N/A | 76.80 | 16.363 | N/A | 283.06 |
| 36 | 17.463 | 0.31 | 121.04 | 17.204 | 0.32 | 238.43 | 82 | N/A | N/A | N/A | 16.520 | N/A | 284.70 |
| 38 | 17.425 | 0.33 | 117.59 | 17.203 | 0.32 | 241.92 | 84 | N/A | N/A | N/A | 16.498 | N/A | 286.35 |
| 40 | 17.462 | 0.34 | 114.59 | 17.156 | 0.30 | 244.94 | 86 | N/A | N/A | N/A | N/A | N/A | N/A |
| 42 | 17.432 | 0.32 | 111.76 | 17.085 | 0.32 | 247.76 | 88 | N/A | N/A | N/A | N/A | N/A | N/A |
| 44 | 17.469 | 0.32 | 109.23 | 17.158 | 0.32 | 250.40 | 90 | N/A | N/A | N/A | N/A | N/A | N/A |

N/A - Not Available

Figure 3. Type-B Standard Uncertainty vs Zenith Angle

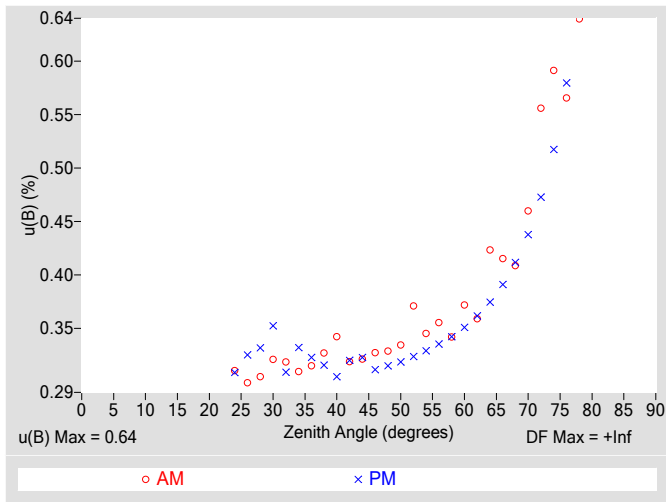


Figure 4. Residuals from Spline Interpolation

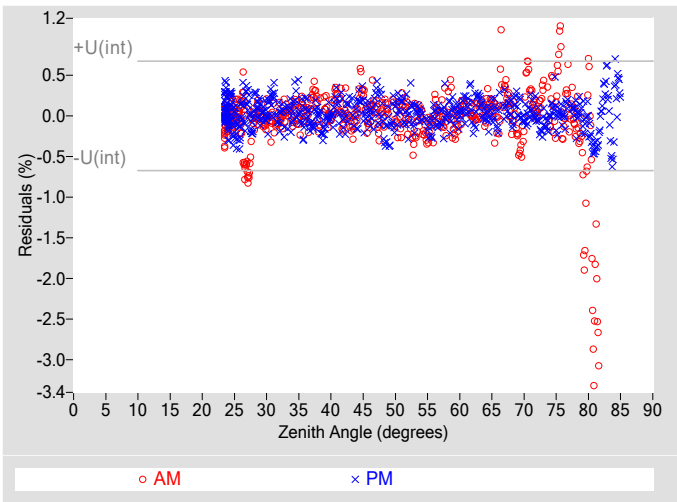


Table 3. Uncertainty using Spline Interpolation ‡

| | |
|---|------------|
| Type-B Standard Uncertainty, $u(B)$ (%) | ± 0.64 |
| Type-A Interpolating Function, $u(int)$ (%) | ± 0.34 |
| Combined Standard Uncertainty, $u(c)$ (%) | ± 0.72 |
| Effective degrees of freedom, $DF(c)$ | 24271 |
| Coverage factor, k | 1.96 |
| Expanded Uncertainty, U_{95} (%) | ± 1.4 |
| AM Valid zenith angle range | 24° to 78° |
| PM Valid zenith angle range | 24° to 76° |

‡ An illustration for how to reduce the uncertainty in calculating the irradiance using a function rather than $R@45^\circ$. Not accredited.

Table 4. Calibration Label Values

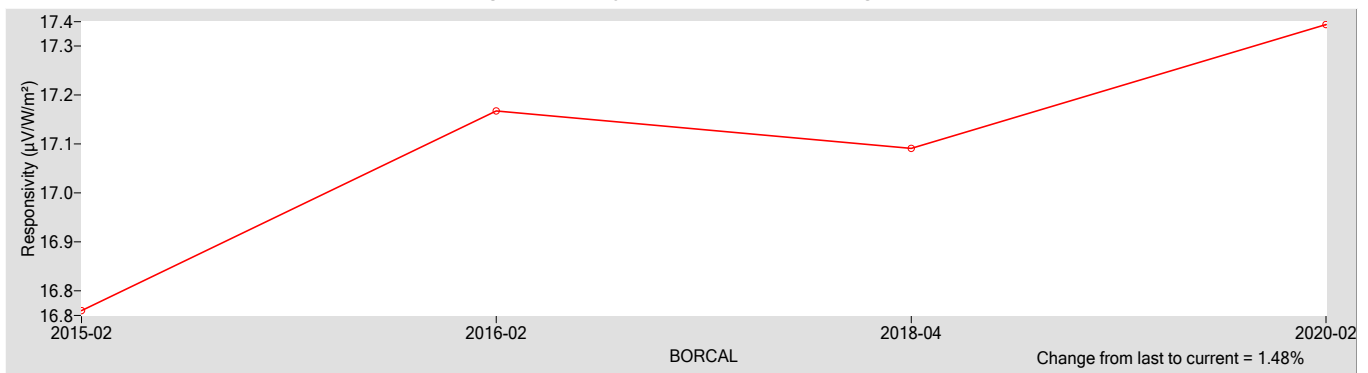
| | |
|----------------------------------|-------------------------------|
| $R @ 45^\circ$ ($\mu V/W/m^2$) | R_{net} ($\mu V/W/m^2$) † |
| 17.344 | 0.40000 |

† R_{net} determination date: Estimated

Table 5. Uncertainty using $R @ 45^\circ$

| | |
|---|----------------|
| Type-B Expanded Uncertainty, $U(B)$ (%) | ± 0.73 |
| Offset Uncertainty, $U(off)$ (%) | +1.2 / -1.5 |
| Expanded Uncertainty, U (%) | +1.9 / -2.2 |
| Effective degrees of freedom, DF | +Inf |
| Coverage factor, k | 1.96 |
| Valid zenith angle range | 30.0° to 60.0° |

Figure 5. History of instrument at Zenith Angle = 45°



References:

[1] Reda, I.; Hickey, J.; Long, C.; Myers, D.; Stoffel, T.; Wilcox, S.; Michalsky, J. J.; Dutton, E. G.; Nelson, D. (2005). "Using a Blackbody to Calculate Net Longwave Responsivity of Shortwave Solar Pyranometers to Correct for Their Thermal Offset Error During Outdoor Calibration Using the Component Sum Method." *Journal of Atmospheric and Oceanic Technology*, 2005; pp. 1531-1540; NREL Report No. JA-560-36646. doi:10.1175/JTECH1782.1

[2] Reda, I.; Myers, D.; Stoffel, T. (2008). "Uncertainty Estimate for the Outdoor Calibration of Solar Pyranometers: A Metrologist Perspective." *Measure*. (NCSLI Journal of Measurement Science). Vol. 3(4), December 2008; pp. 58-66; NREL Report No. JA-581-4137

[3] Reda, I.; Andreas, A. (2004). "Solar Position Algorithm for Solar Radiation Applications." *Solar Energy*. Vol. 76(5), 2004; pp. 577-589; NREL Report No. JA-560-35518. doi:10.1016/j.solener.2003.12.003

[4] Stoffel, T.; Reda, I. (2009). "NREL Pyrheliometer Comparisons: 22 September - 3 October 2008 (NPC-2008)." 54 pp.; NREL Report No. TP-550-45016.

[5] Reda, I.; Stoffel, T.; Myers, D. (2003). "Method to Calibrate a Solar Pyranometer for Measuring Reference Diffuse Irradiance." *Solar Energy*. Vol. 74, 2003; pp. 103-112; NREL Report No. JA-560-35025. doi:10.1016/S0038-092X(03)00124-5

[6] Reda, I. (1996). Calibration of a Solar Absolute Cavity Radiometer with Traceability to the World Radiometric Reference. 79 pp.; NREL Report No. TP-463-20619.

[7] Reda, I.; Gröbner, J.; Stoffel, T.; Myers, D.; Forgan, B. (2008). Improvements in the Blackbody Calibration of Pyrgometers. ARM 2008 Science Team Meeting (Poster).



National Renewable Energy Laboratory

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Metrology Laboratory

Calibration Certificate



| | | | |
|--------------------------|---------------------|----------------------------------|--------------|
| Test Instrument: | Silicon Pyranometer | Manufacturer: | Kipp & Zonen |
| Model: | SP-LITE | Serial Number: | 010995 |
| Calibration Date: | 5/5/2020 | Due Date: | 5/5/2021 |
| Customer: | NREL-SRRL-BMS | Environmental Conditions: | see page 4 |
| Test Dates: | 5/4-5 | | |

This certifies that the above product was calibrated in compliance with ISO/IEC 17025:2017. Measurement uncertainties at the time of calibration are consistent with the Guide to the Expression of Uncertainty in Measurement (GUM) using Reda et al., 2008. All nominal values are traceable to the International System (SI) Units of Measurement.

No statement of compliance with specifications is made or implied on this certificate. However, the estimated uncertainties are the uncertainties of the calibration process; users must add other uncertainties that are relevant to their measuring system, environmental and sky conditions, outdoor set-up, and site location.

The Type-B Standard Uncertainty of using the responsivity at each even zenith angle is reported, and the Expanded Uncertainty of the calibration is reported using two methods:

1. The Expanded Uncertainty of using the responsivity at zenith angle = 45°, within the zenith angle range from 30.0° to 60.0°
2. The Expanded Uncertainty of using Spline Interpolating Functions for the responsivity versus zenith angle.

This certificate applies only to the item identified above and shall not be reproduced other than in full, without specific written approval from the calibration facility. Certificate without signature is not valid.

Table 1. Traceability

| Measurement Type | Instrument | Calibration Date | Calibration Due Date |
|----------------------|--|------------------|----------------------|
| Beam Irradiance † | Eppley Absolute Cavity Radiometer Model HF, S/N 29219 | 09/27/2019 | 09/27/2020 |
| Diffuse Irradiance † | Hukseflux Pyranometer Model SR25, S/N 2541 | 04/17/2020 | 04/17/2021 |
| Diffuse Irradiance † | Hukseflux Pyranometer Model SR25, S/N 2542 | 04/17/2020 | 04/17/2021 |
| Data Acquisition | NREL Data Acquisition System Model RAP-DAQ, S/N 2005-998 | 02/14/2019 | 02/14/2021 |
| Data Acquisition | NREL Data Acquisition System Model RAP-DAQ, S/N 2005-999 | 02/14/2019 | 02/14/2021 |

† Through the World Radiometric Reference (WRR)

Number of pages of certificate: 4

Calibration Procedure: BORCAL-P00-Calibration and QA Procedure; available upon request.

Setup: Radiometers are calibrated outdoors, using the sun as the source. Pyranometers and pyrgeometers are installed for horizontal measurements, with their signal connectors oriented north, if their design permits.

The shading disk for the reference diffuse subtends a solid angle of 5°. Pyrheliometers are installed on solar trackers.

Calibrated by: Afshin Andreas, Ibrahim Reda, Peter Gotseff, and RCC

Ibrahim Reda, Technical Manager

Date

For questions or comments, please contact the technical manager at:

ibrahim.reda@nrel.gov; 303-384-6385; 15013 Denver West Parkway, Golden, CO 80401, USA

Calibration Results

010995 Kipp & Zonen SP-LITE

The responsivity (R , $\mu\text{V}/\text{W}/\text{m}^2$) of the test instrument during calibration is calculated using this Measurement Equation:

$$R = (V - R_{net} * W_{net}) / I \tag{1}$$

where,

- V = radiometer output voltage (microvolts),
 - R_{net} = radiometer net infrared responsivity ($\mu\text{V}/\text{W}/\text{m}^2$), see Table 4,
 - W_{net} = effective net infrared measured by pyrgeometer (W/m^2),
 - = $W_{in} - W_{out} = W_{in} - \sigma * T_c^4$
 - where, W_{in} = incoming infrared (W/m^2), $\sigma = 5.6704\text{e-}8 \text{ W}\cdot\text{m}^{-2}\cdot\text{K}^{-4}$,
 - T_c = case temperature of pyrgeometer (K).
- I = reference irradiance (W/m^2), beam (B) or global (G)
 - where, $G = B * \text{COS}(Z) + D$,
 - Z = zenith angle (degrees),
 - D = reference diffuse irradiance (W/m^2).

Figure 1. Responsivity vs Zenith Angle

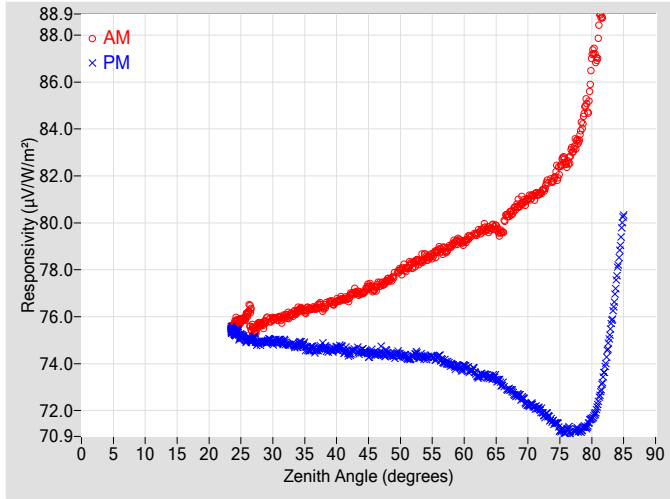


Figure 2. Responsivity vs Local Standard Time

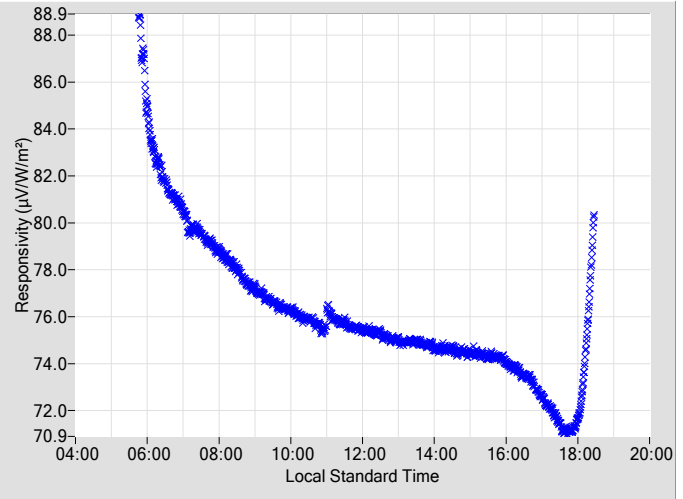


Table 2. Instrument Responsivity (R) and Calibration Type-B Standard Uncertainty, $u(B)$

| Zenith Angle (deg.) | R ($\mu\text{V}/\text{W}/\text{m}^2$) | AM $u(B)$ \pm (%) | Azimuth Angle | R ($\mu\text{V}/\text{W}/\text{m}^2$) | PM $u(B)$ \pm (%) | Azimuth Angle | Zenith Angle (deg.) | R ($\mu\text{V}/\text{W}/\text{m}^2$) | AM $u(B)$ \pm (%) | Azimuth Angle | R ($\mu\text{V}/\text{W}/\text{m}^2$) | PM $u(B)$ \pm (%) | Azimuth Angle |
|---------------------|---|---------------------|---------------|---|---------------------|---------------|---------------------|---|---------------------|---------------|---|---------------------|---------------|
| 0 | N/A | N/A | N/A | N/A | N/A | N/A | 46 | 77.163 | 0.31 | 106.77 | 74.408 | 0.32 | 252.82 |
| 2 | N/A | N/A | N/A | N/A | N/A | N/A | 48 | 77.562 | 0.31 | 104.55 | 74.475 | 0.32 | 255.08 |
| 4 | N/A | N/A | N/A | N/A | N/A | N/A | 50 | 77.942 | 0.33 | 102.41 | 74.366 | 0.33 | 257.23 |
| 6 | N/A | N/A | N/A | N/A | N/A | N/A | 52 | 78.197 | 0.35 | 100.38 | 74.333 | 0.32 | 259.29 |
| 8 | N/A | N/A | N/A | N/A | N/A | N/A | 54 | 78.570 | 0.34 | 98.45 | 74.282 | 0.32 | 261.22 |
| 10 | N/A | N/A | N/A | N/A | N/A | N/A | 56 | 78.847 | 0.36 | 96.58 | 74.320 | 0.33 | 263.10 |
| 12 | N/A | N/A | N/A | N/A | N/A | N/A | 58 | 79.038 | 0.38 | 94.75 | 73.952 | 0.33 | 264.91 |
| 14 | N/A | N/A | N/A | N/A | N/A | N/A | 60 | 79.176 | 0.34 | 93.05 | 73.873 | 0.34 | 266.67 |
| 16 | N/A | N/A | N/A | N/A | N/A | N/A | 62 | 79.551 | 0.35 | 91.35 | 73.483 | 0.35 | 268.39 |
| 18 | N/A | N/A | N/A | N/A | N/A | N/A | 64 | 79.729 | 0.36 | 89.68 | 73.424 | 0.36 | 270.09 |
| 20 | N/A | N/A | N/A | N/A | N/A | N/A | 66 | 79.700 | 0.40 | 88.03 | 73.085 | 0.38 | 271.72 |
| 22 | N/A | N/A | N/A | N/A | N/A | N/A | 68 | 80.638 | 0.39 | 86.42 | 72.642 | 0.40 | 273.36 |
| 24 | 75.628 | 0.31 | 167.16 | 75.329 | 0.31 | 193.01 | 70 | 81.025 | 0.42 | 84.82 | 72.230 | 0.42 | 274.99 |
| 26 | 76.108 | 0.32 | 151.05 | 75.017 | 0.31 | 209.06 | 72 | 81.286 | 0.45 | 83.18 | 71.991 | 0.45 | 276.60 |
| 28 | 75.682 | 0.33 | 140.91 | 74.898 | 0.31 | 218.07 | 74 | 81.841 | 0.49 | 81.61 | 71.496 | 0.49 | 278.20 |
| 30 | 75.885 | 0.31 | 134.42 | 74.904 | 0.29 | 224.61 | 76 | 82.521 | 0.54 | 79.99 | 71.129 | 0.55 | 279.83 |
| 32 | 76.001 | 0.30 | 129.21 | 74.898 | 0.32 | 230.02 | 78 | 83.601 | 0.61 | 78.39 | 71.136 | N/A | 281.44 |
| 34 | 76.290 | 0.31 | 124.83 | 74.819 | 0.32 | 234.61 | 80 | 86.858 | N/A | 76.74 | 71.688 | N/A | 283.09 |
| 36 | 76.327 | 0.31 | 121.06 | 74.664 | 0.31 | 238.40 | 82 | N/A | N/A | N/A | 73.812 | N/A | 284.73 |
| 38 | 76.355 | 0.31 | 117.65 | 74.724 | 0.31 | 241.82 | 84 | N/A | N/A | N/A | 77.895 | N/A | 286.39 |
| 40 | 76.675 | 0.32 | 114.46 | 74.651 | 0.33 | 244.99 | 86 | N/A | N/A | N/A | N/A | N/A | N/A |
| 42 | 76.815 | 0.31 | 111.82 | 74.413 | 0.33 | 247.81 | 88 | N/A | N/A | N/A | N/A | N/A | N/A |
| 44 | 76.999 | 0.30 | 109.15 | 74.538 | 0.36 | 250.45 | 90 | N/A | N/A | N/A | N/A | N/A | N/A |

N/A - Not Available

Figure 3. Type-B Standard Uncertainty vs Zenith Angle

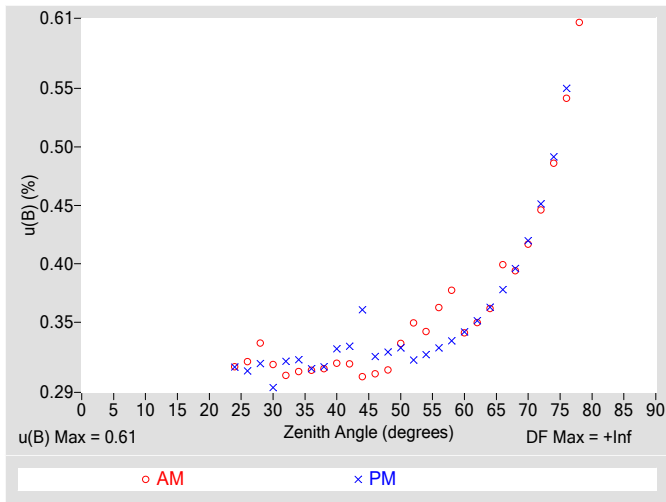


Figure 4. Residuals from Spline Interpolation

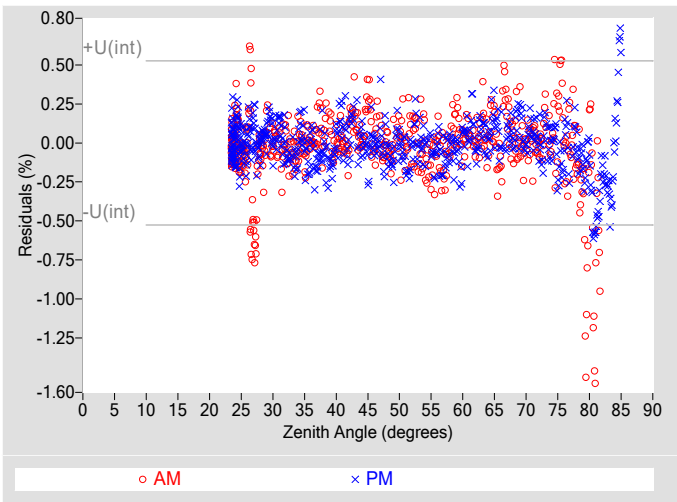


Table 3. Uncertainty using Spline Interpolation ‡

| | |
|---|------------|
| Type-B Standard Uncertainty, $u(B)$ (%) | ± 0.61 |
| Type-A Interpolating Function, $u(int)$ (%) | ± 0.26 |
| Combined Standard Uncertainty, $u(c)$ (%) | ± 0.66 |
| Effective degrees of freedom, $DF(c)$ | 45857 |
| Coverage factor, k | 1.96 |
| Expanded Uncertainty, $U95$ (%) | ± 1.3 |
| AM Valid zenith angle range | 24° to 78° |
| PM Valid zenith angle range | 24° to 76° |

‡ An illustration for how to reduce the uncertainty in calculating the irradiance using a function rather than $R@45^\circ$. Not accredited.

Table 4. Calibration Label Values

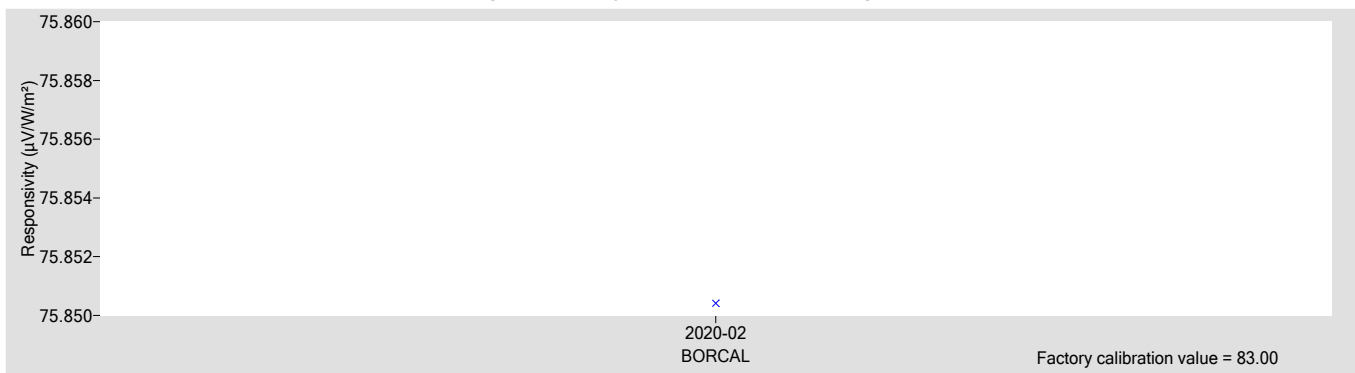
| | |
|----------------------------------|-------------------------------|
| $R @ 45^\circ$ ($\mu V/W/m^2$) | R_{net} ($\mu V/W/m^2$) † |
| 75.850 | 0 |

† R_{net} determination date: N/A

Table 5. Uncertainty using $R @ 45^\circ$

| | |
|---|----------------|
| Type-B Expanded Uncertainty, $U(B)$ (%) | ± 0.74 |
| Offset Uncertainty, $U(off)$ (%) | +4.4 / -2.6 |
| Expanded Uncertainty, U (%) | +5.1 / -3.3 |
| Effective degrees of freedom, DF | +Inf |
| Coverage factor, k | 1.96 |
| Valid zenith angle range | 30.0° to 60.0° |

Figure 5. History of instrument at Zenith Angle = 45°



References:

[1] Reda, I.; Hickey, J.; Long, C.; Myers, D.; Stoffel, T.; Wilcox, S.; Michalsky, J. J.; Dutton, E. G.; Nelson, D. (2005). "Using a Blackbody to Calculate Net Longwave Responsivity of Shortwave Solar Pyranometers to Correct for Their Thermal Offset Error During Outdoor Calibration Using the Component Sum Method." *Journal of Atmospheric and Oceanic Technology*, 2005; pp. 1531-1540; NREL Report No. JA-560-36646. doi:10.1175/JTECH1782.1

[2] Reda, I.; Myers, D.; Stoffel, T. (2008). "Uncertainty Estimate for the Outdoor Calibration of Solar Pyranometers: A Metrologist Perspective." *Measure*. (NCSLI *Journal of Measurement Science*). Vol. 3(4), December 2008; pp. 58-66; NREL Report No. JA-581-4137

[3] Reda, I.; Andreas, A. (2004). "Solar Position Algorithm for Solar Radiation Applications." *Solar Energy*. Vol. 76(5), 2004; pp. 577-589; NREL Report No. JA-560-35518. doi:10.1016/j.solener.2003.12.003

[4] Stoffel, T.; Reda, I. (2009). "NREL Pyrheliometer Comparisons: 22 September - 3 October 2008 (NPC-2008)." 54 pp.; NREL Report No. TP-550-45016.

[5] Reda, I.; Stoffel, T.; Myers, D. (2003). "Method to Calibrate a Solar Pyranometer for Measuring Reference Diffuse Irradiance." *Solar Energy*. Vol. 74, 2003; pp. 103-112; NREL Report No. JA-560-35025. doi:10.1016/S0038-092X(03)00124-5

[6] Reda, I. (1996). *Calibration of a Solar Absolute Cavity Radiometer with Traceability to the World Radiometric Reference*. 79 pp.; NREL Report No. TP-463-20619.

[7] Reda, I.; Gröbner, J.; Stoffel, T.; Myers, D.; Forgan, B. (2008). *Improvements in the Blackbody Calibration of Pyrgometers*. ARM 2008 Science Team Meeting (Poster).



National Renewable Energy Laboratory

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Calibration Certificate



| | | | |
|--------------------------|---------------|----------------------------------|--------------|
| Test Instrument: | Pyranometer | Manufacturer: | Kipp & Zonen |
| Model: | CM3 | Serial Number: | 014261 |
| Calibration Date: | 5/5/2020 | Due Date: | 5/5/2021 |
| Customer: | NREL-SRRL-BMS | Environmental Conditions: | see page 4 |
| Test Dates: | 5/4-5 | | |

This certifies that the above product was calibrated in compliance with ISO/IEC 17025:2017. Measurement uncertainties at the time of calibration are consistent with the Guide to the Expression of Uncertainty in Measurement (GUM) using Reda et al., 2008. All nominal values are traceable to the International System (SI) Units of Measurement.

No statement of compliance with specifications is made or implied on this certificate. However, the estimated uncertainties are the uncertainties of the calibration process; users must add other uncertainties that are relevant to their measuring system, environmental and sky conditions, outdoor set-up, and site location.

The Type-B Standard Uncertainty of using the responsivity at each even zenith angle is reported, and the Expanded Uncertainty of the calibration is reported using two methods:

1. The Expanded Uncertainty of using the responsivity at zenith angle = 45°, within the zenith angle range from 30.0° to 60.0°
2. The Expanded Uncertainty of using Spline Interpolating Functions for the responsivity versus zenith angle.

This certificate applies only to the item identified above and shall not be reproduced other than in full, without specific written approval from the calibration facility. Certificate without signature is not valid.

Table 1. Traceability

| Measurement Type | Instrument | Calibration Date | Calibration Due Date |
|-----------------------|--|------------------|----------------------|
| Beam Irradiance † | Eppley Absolute Cavity Radiometer Model HF, S/N 29219 | 09/27/2019 | 09/27/2020 |
| Diffuse Irradiance † | Hukseflux Pyranometer Model SR25, S/N 2541 | 04/17/2020 | 04/17/2021 |
| Diffuse Irradiance † | Hukseflux Pyranometer Model SR25, S/N 2542 | 04/17/2020 | 04/17/2021 |
| Data Acquisition | NREL Data Acquisition System Model RAP-DAQ, S/N 2005-998 | 02/14/2019 | 02/14/2021 |
| Data Acquisition | NREL Data Acquisition System Model RAP-DAQ, S/N 2005-999 | 02/14/2019 | 02/14/2021 |
| Infrared Irradiance ‡ | Kipp & Zonen Pyrgeometer Model CG4, S/N FT002 | 04/16/2018 | 04/16/2022 |

† Through the World Radiometric Reference (WRR)

‡ Through the World Infrared Standard Group (WISG)

Number of pages of certificate: 4

Calibration Procedure: BORCAL-P00-Calibration and QA Procedure; available upon request.

Setup: Radiometers are calibrated outdoors, using the sun as the source. Pyranometers and pyrgeometers are installed for horizontal measurements, with their signal connectors oriented north, if their design permits.

The shading disk for the reference diffuse subtends a solid angle of 5°. Pyrheliometers are installed on solar trackers.

Calibrated by: Afshin Andreas, Ibrahim Reda, Peter Gotseff, and RCC

Ibrahim Reda, Technical Manager

Date

For questions or comments, please contact the technical manager at:

ibrahim.reda@nrel.gov; 303-384-6385; 15013 Denver West Parkway, Golden, CO 80401, USA

Calibration Results

014261 Kipp & Zonen CM3

The responsivity (R , $\mu\text{V}/\text{W}/\text{m}^2$) of the test instrument during calibration is calculated using this Measurement Equation:

$$R = (V - R_{net} * W_{net}) / I \tag{1}$$

where,

- V = radiometer output voltage (microvolts),
 - R_{net} = radiometer net infrared responsivity ($\mu\text{V}/\text{W}/\text{m}^2$), see Table 4,
 - W_{net} = effective net infrared measured by pyrgeometer (W/m^2),
 - = $W_{in} - W_{out} = W_{in} - \sigma * T_c^4$
 - where, W_{in} = incoming infrared (W/m^2), $\sigma = 5.6704\text{e-}8 \text{ W}\cdot\text{m}^{-2}\cdot\text{K}^{-4}$,
 - T_c = case temperature of pyrgeometer (K).
- I = reference irradiance (W/m^2), beam (B) or global (G)
 - where, $G = B * \text{COS}(Z) + D$,
 - Z = zenith angle (degrees),
 - D = reference diffuse irradiance (W/m^2).

Figure 1. Responsivity vs Zenith Angle

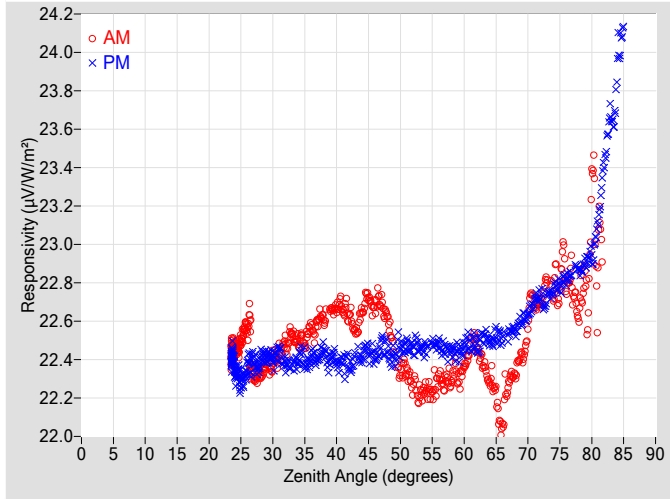


Figure 2. Responsivity vs Local Standard Time

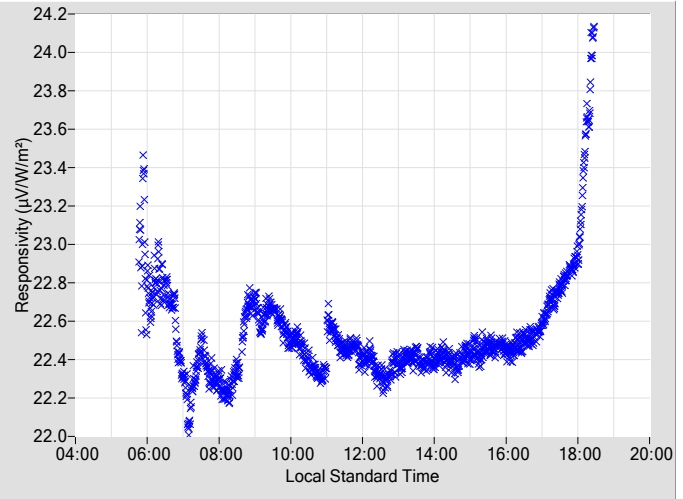


Table 2. Instrument Responsivity (R) and Calibration Type-B Standard Uncertainty, u(B)

| Zenith | | | AM | | | PM | | | Zenith | | | AM | | | PM | | |
|--------|---------------------------------------|-------|---------|---------------------------------------|-------|---------|--------|---------------------------------------|--------|---------|---------------------------------------|-------|---------|---------------------------------------|-------|---------|--|
| Angle | R | u(B) | Azimuth | R | u(B) | Azimuth | Angle | R | u(B) | Azimuth | R | u(B) | Azimuth | R | u(B) | Azimuth | |
| (deg.) | ($\mu\text{V}/\text{W}/\text{m}^2$) | ± (%) | Angle | ($\mu\text{V}/\text{W}/\text{m}^2$) | ± (%) | Angle | (deg.) | ($\mu\text{V}/\text{W}/\text{m}^2$) | ± (%) | Angle | ($\mu\text{V}/\text{W}/\text{m}^2$) | ± (%) | Angle | ($\mu\text{V}/\text{W}/\text{m}^2$) | ± (%) | Angle | |
| 0 | N/A | N/A | N/A | N/A | N/A | N/A | 46 | 22.681 | 0.33 | 106.78 | 22.403 | 0.31 | 252.83 | | | | |
| 2 | N/A | N/A | N/A | N/A | N/A | N/A | 48 | 22.612 | 0.33 | 104.56 | 22.453 | 0.31 | 255.09 | | | | |
| 4 | N/A | N/A | N/A | N/A | N/A | N/A | 50 | 22.338 | 0.33 | 102.42 | 22.459 | 0.32 | 257.24 | | | | |
| 6 | N/A | N/A | N/A | N/A | N/A | N/A | 52 | 22.264 | 0.37 | 100.42 | 22.459 | 0.32 | 259.25 | | | | |
| 8 | N/A | N/A | N/A | N/A | N/A | N/A | 54 | 22.236 | 0.34 | 98.46 | 22.458 | 0.33 | 261.24 | | | | |
| 10 | N/A | N/A | N/A | N/A | N/A | N/A | 56 | 22.305 | 0.35 | 96.59 | 22.481 | 0.33 | 263.11 | | | | |
| 12 | N/A | N/A | N/A | N/A | N/A | N/A | 58 | 22.285 | 0.34 | 94.81 | 22.440 | 0.34 | 264.92 | | | | |
| 14 | N/A | N/A | N/A | N/A | N/A | N/A | 60 | 22.361 | 0.37 | 93.06 | 22.472 | 0.35 | 266.68 | | | | |
| 16 | N/A | N/A | N/A | N/A | N/A | N/A | 62 | 22.478 | 0.36 | 91.36 | 22.452 | 0.36 | 268.40 | | | | |
| 18 | N/A | N/A | N/A | N/A | N/A | N/A | 64 | 22.285 | 0.42 | 89.69 | 22.498 | 0.37 | 270.10 | | | | |
| 20 | N/A | N/A | N/A | N/A | N/A | N/A | 66 | 22.045 | 0.41 | 88.04 | 22.507 | 0.39 | 271.68 | | | | |
| 22 | N/A | N/A | N/A | N/A | N/A | N/A | 68 | 22.328 | 0.40 | 86.39 | 22.549 | 0.40 | 273.37 | | | | |
| 24 | 22.459 | 0.31 | 167.00 | 22.366 | 0.31 | 193.21 | 70 | 22.589 | 0.45 | 84.79 | 22.641 | 0.43 | 275.00 | | | | |
| 26 | 22.571 | 0.30 | 150.94 | 22.362 | 0.32 | 209.12 | 72 | 22.691 | 0.55 | 83.19 | 22.731 | 0.46 | 276.61 | | | | |
| 28 | 22.322 | 0.30 | 140.94 | 22.392 | 0.33 | 217.97 | 74 | 22.754 | 0.58 | 81.62 | 22.766 | 0.51 | 278.21 | | | | |
| 30 | 22.382 | 0.32 | 134.56 | 22.399 | 0.35 | 224.64 | 76 | 22.809 | 0.56 | 80.00 | 22.822 | 0.57 | 279.80 | | | | |
| 32 | 22.473 | 0.32 | 129.13 | 22.375 | 0.31 | 230.09 | 78 | 22.645 | 0.63 | 78.40 | 22.864 | N/A | 281.41 | | | | |
| 34 | 22.490 | 0.31 | 124.85 | 22.393 | 0.33 | 234.55 | 80 | 23.223 | N/A | 76.80 | 22.935 | N/A | 283.06 | | | | |
| 36 | 22.568 | 0.31 | 121.04 | 22.411 | 0.32 | 238.43 | 82 | N/A | N/A | N/A | 23.435 | N/A | 284.70 | | | | |
| 38 | 22.607 | 0.33 | 117.59 | 22.446 | 0.31 | 241.92 | 84 | N/A | N/A | N/A | 23.898 | N/A | 286.35 | | | | |
| 40 | 22.670 | 0.34 | 114.59 | 22.381 | 0.30 | 244.94 | 86 | N/A | N/A | N/A | N/A | N/A | N/A | | | | |
| 42 | 22.629 | 0.32 | 111.76 | 22.370 | 0.32 | 247.76 | 88 | N/A | N/A | N/A | N/A | N/A | N/A | | | | |
| 44 | 22.642 | 0.32 | 109.23 | 22.412 | 0.32 | 250.40 | 90 | N/A | N/A | N/A | N/A | N/A | N/A | | | | |

N/A - Not Available

Figure 3. Type-B Standard Uncertainty vs Zenith Angle

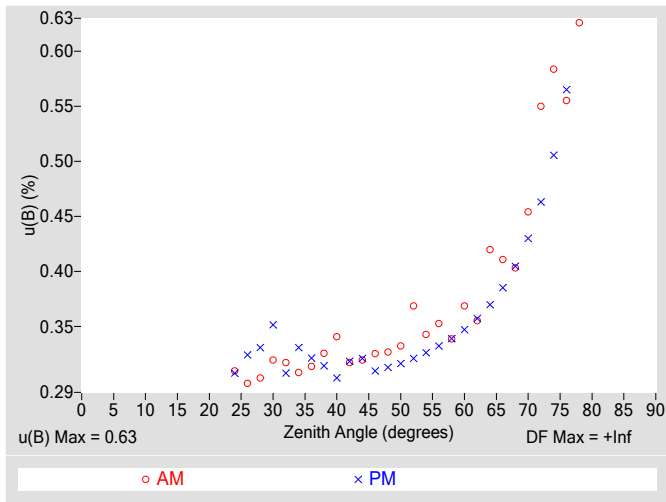


Figure 4. Residuals from Spline Interpolation

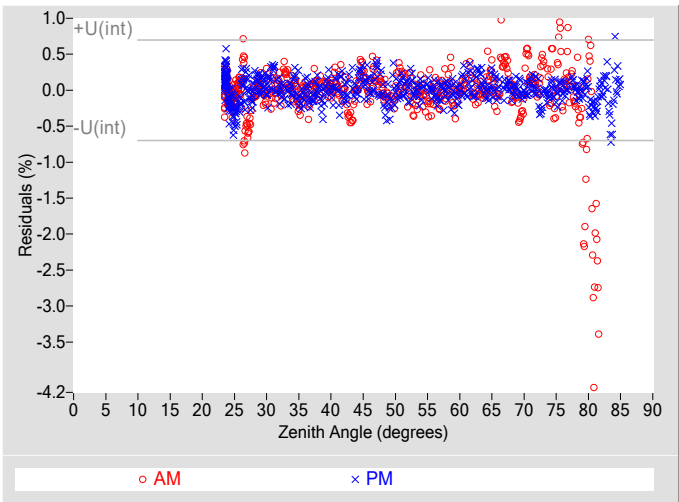


Table 3. Uncertainty using Spline Interpolation ‡

| | |
|---|------------|
| Type-B Standard Uncertainty, $u(B)$ (%) | ± 0.63 |
| Type-A Interpolating Function, $u(int)$ (%) | ± 0.35 |
| Combined Standard Uncertainty, $u(c)$ (%) | ± 0.72 |
| Effective degrees of freedom, $DF(c)$ | 20128 |
| Coverage factor, k | 1.96 |
| Expanded Uncertainty, U_{95} (%) | ± 1.4 |
| AM Valid zenith angle range | 24° to 78° |
| PM Valid zenith angle range | 24° to 76° |

‡ An illustration for how to reduce the uncertainty in calculating the irradiance using a function rather than $R@45^\circ$. Not accredited.

Table 4. Calibration Label Values

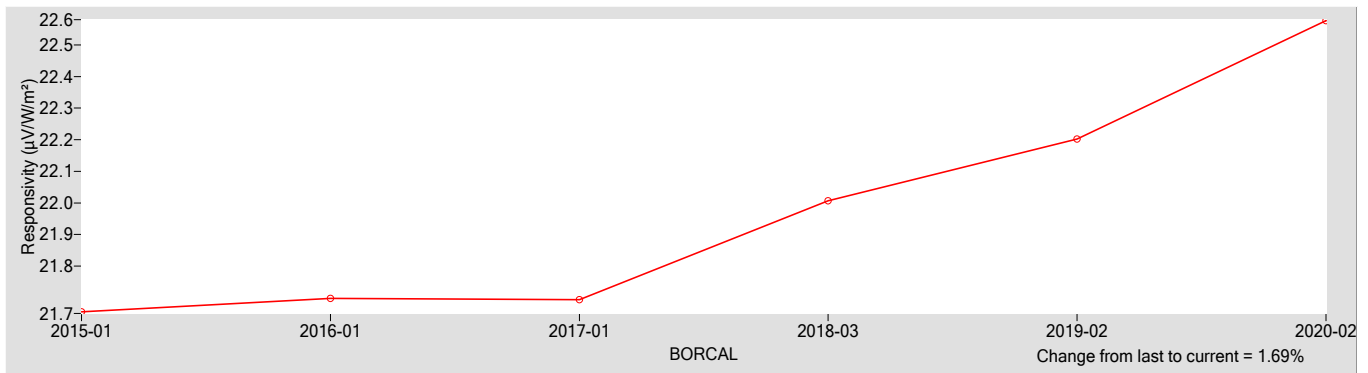
| | |
|----------------------------------|-------------------------------|
| $R @ 45^\circ$ ($\mu V/W/m^2$) | R_{net} ($\mu V/W/m^2$) † |
| 22.577 | 0.40000 |

† R_{net} determination date: Estimated

Table 5. Uncertainty using $R @ 45^\circ$

| | |
|---|----------------|
| Type-B Expanded Uncertainty, $U(B)$ (%) | ± 0.72 |
| Offset Uncertainty, $U(off)$ (%) | +0.46 / -1.5 |
| Expanded Uncertainty, U (%) | +1.2 / -2.2 |
| Effective degrees of freedom, DF | +Inf |
| Coverage factor, k | 1.96 |
| Valid zenith angle range | 30.0° to 60.0° |

Figure 5. History of instrument at Zenith Angle = 45°



References:

- [1] Reda, I.; Hickey, J.; Long, C.; Myers, D.; Stoffel, T.; Wilcox, S.; Michalsky, J. J.; Dutton, E. G.; Nelson, D. (2005). "Using a Blackbody to Calculate Net Longwave Responsivity of Shortwave Solar Pyranometers to Correct for Their Thermal Offset Error During Outdoor Calibration Using the Component Sum Method." *Journal of Atmospheric and Oceanic Technology*, 2005; pp. 1531-1540; NREL Report No. JA-560-36646. doi:10.1175/JTECH1782.1
- [2] Reda, I.; Myers, D.; Stoffel, T. (2008). "Uncertainty Estimate for the Outdoor Calibration of Solar Pyranometers: A Metrologist Perspective." *Measure*. (NCSLI Journal of Measurement Science). Vol. 3(4), December 2008; pp. 58-66; NREL Report No. JA-581-4137
- [3] Reda, I.; Andreas, A. (2004). "Solar Position Algorithm for Solar Radiation Applications." *Solar Energy*. Vol. 76(5), 2004; pp. 577-589; NREL Report No. JA-560-35518. doi:10.1016/j.solener.2003.12.003
- [4] Stoffel, T.; Reda, I. (2009). "NREL Pyrheliometer Comparisons: 22 September - 3 October 2008 (NPC-2008)." 54 pp.; NREL Report No. TP-550-45016.
- [5] Reda, I.; Stoffel, T.; Myers, D. (2003). "Method to Calibrate a Solar Pyranometer for Measuring Reference Diffuse Irradiance." *Solar Energy*. Vol. 74, 2003; pp. 103-112; NREL Report No. JA-560-35025. doi:10.1016/S0038-092X(03)00124-5
- [6] Reda, I. (1996). Calibration of a Solar Absolute Cavity Radiometer with Traceability to the World Radiometric Reference. 79 pp.; NREL Report No. TP-463-20619.
- [7] Reda, I.; Gröbner, J.; Stoffel, T.; Myers, D.; Forgan, B. (2008). Improvements in the Blackbody Calibration of Pyrgometers. ARM 2008 Science Team Meeting (Poster).



National Renewable Energy Laboratory

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Calibration Certificate



| | | | |
|--------------------------|---------------|----------------------------------|--------------|
| Test Instrument: | Pyranometer | Manufacturer: | Kipp & Zonen |
| Model: | CM6B | Serial Number: | 015189 |
| Calibration Date: | 5/5/2020 | Due Date: | 5/5/2021 |
| Customer: | NREL-SRRL-BMS | Environmental Conditions: | see page 4 |
| Test Dates: | 5/4-5 | | |

This certifies that the above product was calibrated in compliance with ISO/IEC 17025:2017. Measurement uncertainties at the time of calibration are consistent with the Guide to the Expression of Uncertainty in Measurement (GUM) using Reda et al., 2008. All nominal values are traceable to the International System (SI) Units of Measurement.

No statement of compliance with specifications is made or implied on this certificate. However, the estimated uncertainties are the uncertainties of the calibration process; users must add other uncertainties that are relevant to their measuring system, environmental and sky conditions, outdoor set-up, and site location.

The Type-B Standard Uncertainty of using the responsivity at each even zenith angle is reported, and the Expanded Uncertainty of the calibration is reported using two methods:

1. The Expanded Uncertainty of using the responsivity at zenith angle = 45°, within the zenith angle range from 30.0° to 60.0°
2. The Expanded Uncertainty of using Spline Interpolating Functions for the responsivity versus zenith angle.

This certificate applies only to the item identified above and shall not be reproduced other than in full, without specific written approval from the calibration facility. Certificate without signature is not valid.

Table 1. Traceability

| Measurement Type | Instrument | Calibration Date | Calibration Due Date |
|-----------------------|--|------------------|----------------------|
| Beam Irradiance † | Eppley Absolute Cavity Radiometer Model HF, S/N 29219 | 09/27/2019 | 09/27/2020 |
| Diffuse Irradiance † | Hukseflux Pyranometer Model SR25, S/N 2541 | 04/17/2020 | 04/17/2021 |
| Diffuse Irradiance † | Hukseflux Pyranometer Model SR25, S/N 2542 | 04/17/2020 | 04/17/2021 |
| Data Acquisition | NREL Data Acquisition System Model RAP-DAQ, S/N 2005-998 | 02/14/2019 | 02/14/2021 |
| Data Acquisition | NREL Data Acquisition System Model RAP-DAQ, S/N 2005-999 | 02/14/2019 | 02/14/2021 |
| Infrared Irradiance ‡ | Kipp & Zonen Pyrgeometer Model CG4, S/N FT002 | 04/16/2018 | 04/16/2022 |

† Through the World Radiometric Reference (WRR)

‡ Through the World Infrared Standard Group (WISG)

Number of pages of certificate: 4

Calibration Procedure: BORCAL-P00-Calibration and QA Procedure; available upon request.

Setup: Radiometers are calibrated outdoors, using the sun as the source. Pyranometers and pyrgeometers are installed for horizontal measurements, with their signal connectors oriented north, if their design permits.

The shading disk for the reference diffuse subtends a solid angle of 5°. Pyrheliometers are installed on solar trackers.

Calibrated by: Afshin Andreas, Ibrahim Reda, Peter Gotseff, and RCC

Ibrahim Reda, Technical Manager

Date

For questions or comments, please contact the technical manager at:

ibrahim.reda@nrel.gov; 303-384-6385; 15013 Denver West Parkway, Golden, CO 80401, USA

Calibration Results

015189 Kipp & Zonen CM6B

The responsivity (R , $\mu\text{V}/\text{W}/\text{m}^2$) of the test instrument during calibration is calculated using this Measurement Equation:

$$R = (V - R_{net} * W_{net}) / I \tag{1}$$

where,

- V = radiometer output voltage (microvolts),
 - R_{net} = radiometer net infrared responsivity ($\mu\text{V}/\text{W}/\text{m}^2$), see Table 4,
 - W_{net} = effective net infrared measured by pyrgeometer (W/m^2),
 - = $W_{in} - W_{out} = W_{in} - \sigma * T_c^4$
 - where, W_{in} = incoming infrared (W/m^2), $\sigma = 5.6704\text{e-}8 \text{ W}\cdot\text{m}^{-2}\cdot\text{K}^{-4}$,
 - T_c = case temperature of pyrgeometer (K).
- I = reference irradiance (W/m^2), beam (B) or global (G)
 - where, $G = B * \text{COS}(Z) + D$,
 - Z = zenith angle (degrees),
 - D = reference diffuse irradiance (W/m^2).

Figure 1. Responsivity vs Zenith Angle

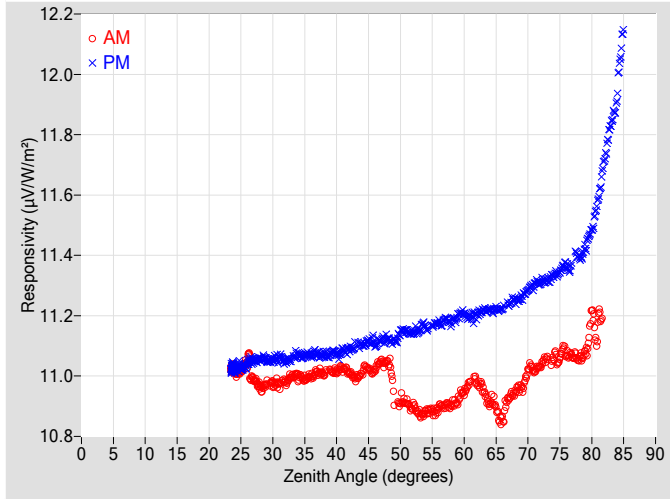


Figure 2. Responsivity vs Local Standard Time

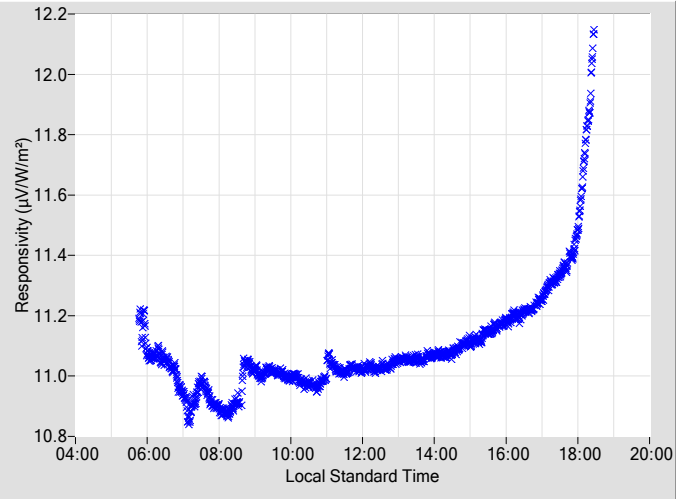


Table 2. Instrument Responsivity (R) and Calibration Type-B Standard Uncertainty, $u(B)$

| Zenith Angle (deg.) | R ($\mu\text{V}/\text{W}/\text{m}^2$) | AM $u(B)$ \pm (%) | Azimuth Angle | R ($\mu\text{V}/\text{W}/\text{m}^2$) | PM $u(B)$ \pm (%) | Azimuth Angle | Zenith Angle (deg.) | R ($\mu\text{V}/\text{W}/\text{m}^2$) | AM $u(B)$ \pm (%) | Azimuth Angle | R ($\mu\text{V}/\text{W}/\text{m}^2$) | PM $u(B)$ \pm (%) | Azimuth Angle |
|---------------------|---|---------------------|---------------|---|---------------------|---------------|---------------------|---|---------------------|---------------|---|---------------------|---------------|
| 0 | N/A | N/A | N/A | N/A | N/A | N/A | 46 | 11.021 | 0.31 | 106.78 | 11.103 | 0.33 | 252.84 |
| 2 | N/A | N/A | N/A | N/A | N/A | N/A | 48 | 11.044 | 0.33 | 104.57 | 11.127 | 0.33 | 255.09 |
| 4 | N/A | N/A | N/A | N/A | N/A | N/A | 50 | 10.908 | 0.38 | 102.46 | 11.146 | 0.32 | 257.25 |
| 6 | N/A | N/A | N/A | N/A | N/A | N/A | 52 | 10.900 | 0.36 | 100.39 | 11.144 | 0.34 | 259.26 |
| 8 | N/A | N/A | N/A | N/A | N/A | N/A | 54 | 10.881 | 0.33 | 98.47 | 11.159 | 0.35 | 261.24 |
| 10 | N/A | N/A | N/A | N/A | N/A | N/A | 56 | 10.896 | 0.36 | 96.60 | 11.177 | 0.36 | 263.12 |
| 12 | N/A | N/A | N/A | N/A | N/A | N/A | 58 | 10.904 | 0.39 | 94.81 | 11.179 | 0.35 | 264.93 |
| 14 | N/A | N/A | N/A | N/A | N/A | N/A | 60 | 10.947 | 0.35 | 93.06 | 11.207 | 0.35 | 266.69 |
| 16 | N/A | N/A | N/A | N/A | N/A | N/A | 62 | 10.980 | 0.36 | 91.36 | 11.201 | 0.37 | 268.41 |
| 18 | N/A | N/A | N/A | N/A | N/A | N/A | 64 | 10.908 | 0.43 | 89.69 | 11.221 | 0.38 | 270.10 |
| 20 | N/A | N/A | N/A | N/A | N/A | N/A | 66 | 10.853 | 0.39 | 88.05 | 11.225 | 0.40 | 271.69 |
| 22 | N/A | N/A | N/A | N/A | N/A | N/A | 68 | 10.948 | 0.44 | 86.39 | 11.253 | 0.42 | 273.37 |
| 24 | 11.023 | 0.32 | 167.23 | 11.026 | 0.32 | 193.22 | 70 | 11.018 | 0.47 | 84.79 | 11.286 | 0.44 | 275.00 |
| 26 | 11.051 | 0.31 | 150.95 | 11.039 | 0.32 | 209.17 | 72 | 11.035 | 0.47 | 83.20 | 11.312 | 0.48 | 276.61 |
| 28 | 10.963 | 0.32 | 140.82 | 11.058 | 0.31 | 217.98 | 74 | 11.060 | 0.52 | 81.62 | 11.335 | 0.52 | 278.17 |
| 30 | 10.976 | 0.32 | 134.42 | 11.056 | 0.33 | 224.65 | 76 | 11.075 | 0.58 | 80.00 | 11.367 | 0.59 | 279.80 |
| 32 | 10.980 | 0.33 | 129.14 | 11.049 | 0.30 | 230.09 | 78 | 11.057 | 0.65 | 78.40 | 11.393 | N/A | 281.42 |
| 34 | 10.999 | 0.33 | 124.86 | 11.068 | 0.31 | 234.55 | 80 | 11.202 | N/A | 76.76 | 11.485 | N/A | 283.06 |
| 36 | 10.998 | 0.31 | 121.03 | 11.069 | 0.32 | 238.43 | 82 | N/A | N/A | N/A | 11.719 | N/A | 284.70 |
| 38 | 11.007 | 0.32 | 117.60 | 11.072 | 0.32 | 241.92 | 84 | N/A | N/A | N/A | 11.940 | N/A | 286.36 |
| 40 | 11.016 | 0.33 | 114.60 | 11.074 | 0.35 | 244.95 | 86 | N/A | N/A | N/A | N/A | N/A | N/A |
| 42 | 11.010 | 0.31 | 111.77 | 11.091 | 0.31 | 247.76 | 88 | N/A | N/A | N/A | N/A | N/A | N/A |
| 44 | 11.008 | 0.31 | 109.25 | 11.104 | 0.32 | 250.40 | 90 | N/A | N/A | N/A | N/A | N/A | N/A |

N/A - Not Available

Figure 3. Type-B Standard Uncertainty vs Zenith Angle

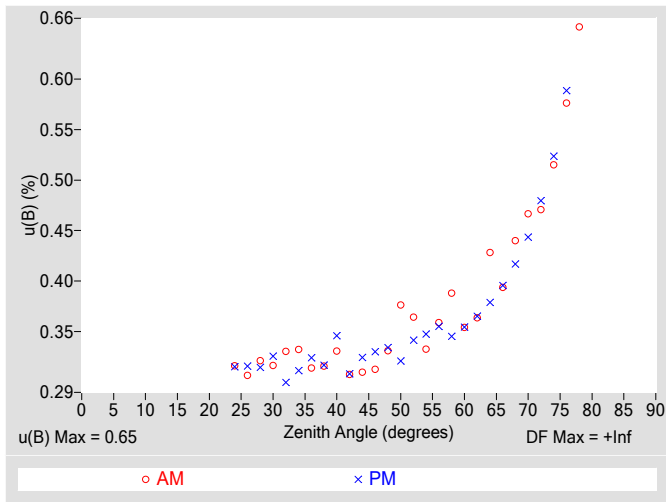


Figure 4. Residuals from Spline Interpolation

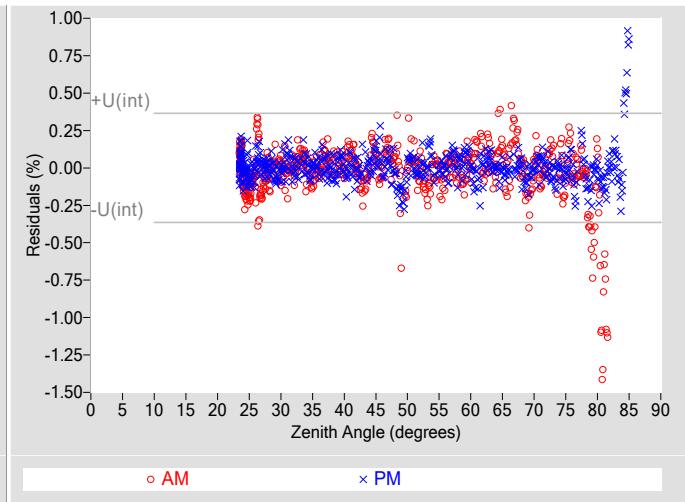


Table 3. Uncertainty using Spline Interpolation ‡

| | |
|---|------------|
| Type-B Standard Uncertainty, $u(B)$ (%) | ± 0.65 |
| Type-A Interpolating Function, $u(int)$ (%) | ± 0.18 |
| Combined Standard Uncertainty, $u(c)$ (%) | ± 0.68 |
| Effective degrees of freedom, $DF(c)$ | 218287 |
| Coverage factor, k | 1.96 |
| Expanded Uncertainty, $U95$ (%) | ± 1.3 |
| AM Valid zenith angle range | 24° to 78° |
| PM Valid zenith angle range | 24° to 76° |

‡ An illustration for how to reduce the uncertainty in calculating the irradiance using a function rather than $R@45^\circ$. Not accredited.

Table 4. Calibration Label Values

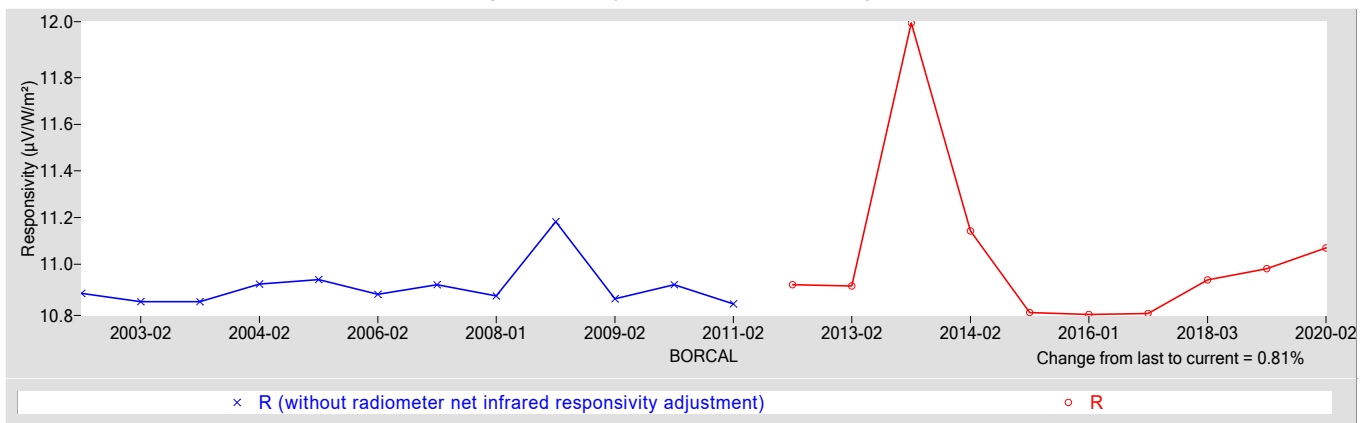
| | |
|----------------------------------|-------------------------------|
| $R @ 45^\circ$ ($\mu V/W/m^2$) | R_{net} ($\mu V/W/m^2$) † |
| 11.069 | 0.30000 |

† R_{net} determination date: Estimated

Table 5. Uncertainty using $R @ 45^\circ$

| | |
|---|----------------|
| Type-B Expanded Uncertainty, $U(B)$ (%) | ± 0.76 |
| Offset Uncertainty, $U(off)$ (%) | +1.2 / -1.7 |
| Expanded Uncertainty, U (%) | +2.0 / -2.5 |
| Effective degrees of freedom, DF | +Inf |
| Coverage factor, k | 1.96 |
| Valid zenith angle range | 30.0° to 60.0° |

Figure 5. History of instrument at Zenith Angle = 45°



References:

[1] Reda, I.; Hickey, J.; Long, C.; Myers, D.; Stoffel, T.; Wilcox, S.; Michalsky, J. J.; Dutton, E. G.; Nelson, D. (2005). "Using a Blackbody to Calculate Net Longwave Responsivity of Shortwave Solar Pyranometers to Correct for Their Thermal Offset Error During Outdoor Calibration Using the Component Sum Method." *Journal of Atmospheric and Oceanic Technology*, 2005; pp. 1531-1540; NREL Report No. JA-560-36646. doi:10.1175/JTECH1782.1

[2] Reda, I.; Myers, D.; Stoffel, T. (2008). "Uncertainty Estimate for the Outdoor Calibration of Solar Pyranometers: A Metrologist Perspective." *Measure*. (NCSLI Journal of Measurement Science). Vol. 3(4), December 2008; pp. 58-66; NREL Report No. JA-581-4137

[3] Reda, I.; Andreas, A. (2004). "Solar Position Algorithm for Solar Radiation Applications." *Solar Energy*. Vol. 76(5), 2004; pp. 577-589; NREL Report No. JA-560-35518. doi:10.1016/j.solener.2003.12.003

[4] Stoffel, T.; Reda, I. (2009). "NREL Pyrheliometer Comparisons: 22 September - 3 October 2008 (NPC-2008)." 54 pp.; NREL Report No. TP-550-45016.

[5] Reda, I.; Stoffel, T.; Myers, D. (2003). "Method to Calibrate a Solar Pyranometer for Measuring Reference Diffuse Irradiance." *Solar Energy*. Vol. 74, 2003; pp. 103-112; NREL Report No. JA-560-35025. doi:10.1016/S0038-092X(03)00124-5

[6] Reda, I. (1996). Calibration of a Solar Absolute Cavity Radiometer with Traceability to the World Radiometric Reference. 79 pp.; NREL Report No. TP-463-20619.

[7] Reda, I.; Gröbner, J.; Stoffel, T.; Myers, D.; Forgan, B. (2008). Improvements in the Blackbody Calibration of Pyrgeometers. ARM 2008 Science Team Meeting (Poster).



National Renewable Energy Laboratory

Solar Radiation Research Laboratory

Metrology Laboratory

Calibration Certificate



| | | | |
|--------------------------|--------------------------|----------------------------------|------------|
| Test Instrument: | Pyranometer (Ventilated) | Manufacturer: | Yankee |
| Model: | TSP-700 | Serial Number: | 0212-2 |
| Calibration Date: | 5/5/2020 | Due Date: | 5/5/2021 |
| Customer: | NREL-SRRL-BMS | Environmental Conditions: | see page 4 |
| Test Dates: | 5/4-5 | | |

This certifies that the above product was calibrated in compliance with ISO/IEC 17025:2017. Measurement uncertainties at the time of calibration are consistent with the Guide to the Expression of Uncertainty in Measurement (GUM) using Reda et al., 2008. All nominal values are traceable to the International System (SI) Units of Measurement.

No statement of compliance with specifications is made or implied on this certificate. However, the estimated uncertainties are the uncertainties of the calibration process; users must add other uncertainties that are relevant to their measuring system, environmental and sky conditions, outdoor set-up, and site location.

The Type-B Standard Uncertainty of using the responsivity at each even zenith angle is reported, and the Expanded Uncertainty of the calibration is reported using two methods:

1. The Expanded Uncertainty of using the responsivity at zenith angle = 45°, within the zenith angle range from 30.0° to 60.0°
2. The Expanded Uncertainty of using Spline Interpolating Functions for the responsivity versus zenith angle.

This certificate applies only to the item identified above and shall not be reproduced other than in full, without specific written approval from the calibration facility. Certificate without signature is not valid.

Table 1. Traceability

| Measurement Type | Instrument | Calibration Date | Calibration Due Date |
|----------------------|--|------------------|----------------------|
| Beam Irradiance † | Eppley Absolute Cavity Radiometer Model HF, S/N 29219 | 09/27/2019 | 09/27/2020 |
| Diffuse Irradiance † | Hukseflux Pyranometer Model SR25, S/N 2541 | 04/17/2020 | 04/17/2021 |
| Diffuse Irradiance † | Hukseflux Pyranometer Model SR25, S/N 2542 | 04/17/2020 | 04/17/2021 |
| Data Acquisition | NREL Data Acquisition System Model RAP-DAQ, S/N 2005-998 | 02/14/2019 | 02/14/2021 |
| Data Acquisition | NREL Data Acquisition System Model RAP-DAQ, S/N 2005-999 | 02/14/2019 | 02/14/2021 |

† Through the World Radiometric Reference (WRR)

Number of pages of certificate: 4

Calibration Procedure: BORCAL-P00-Calibration and QA Procedure; available upon request.

Setup: Radiometers are calibrated outdoors, using the sun as the source. Pyranometers and pyrgeometers are installed for horizontal measurements, with their signal connectors oriented north, if their design permits.

The shading disk for the reference diffuse subtends a solid angle of 5°. Pyrheliometers are installed on solar trackers.

Calibrated by: Afshin Andreas, Ibrahim Reda, Peter Gotseff, and RCC

Ibrahim Reda, Technical Manager

Date

For questions or comments, please contact the technical manager at:

ibrahim.reda@nrel.gov; 303-384-6385; 15013 Denver West Parkway, Golden, CO 80401, USA

Calibration Results

0212-2 Yankee TSP-700

The responsivity (R , $\mu\text{V}/\text{W}/\text{m}^2$) of the test instrument during calibration is calculated using this Measurement Equation:

$$R = (V - R_{net} * W_{net}) / I \quad [1]$$

where,

- V = radiometer output voltage (microvolts),
 - R_{net} = radiometer net infrared responsivity ($\mu\text{V}/\text{W}/\text{m}^2$), see Table 4,
 - W_{net} = effective net infrared measured by pyrgeometer (W/m^2),
 - = $W_{in} - W_{out} = W_{in} - \sigma * T_c^4$
 - where, W_{in} = incoming infrared (W/m^2), $\sigma = 5.6704\text{e-}8 \text{ W}\cdot\text{m}^{-2}\cdot\text{K}^{-4}$,
 - T_c = case temperature of pyrgeometer (K).
- I = reference irradiance (W/m^2), beam (B) or global (G)
 where, $G = B * \text{COS}(Z) + D$,
 Z = zenith angle (degrees),
 D = reference diffuse irradiance (W/m^2).

Figure 1. Responsivity vs Zenith Angle

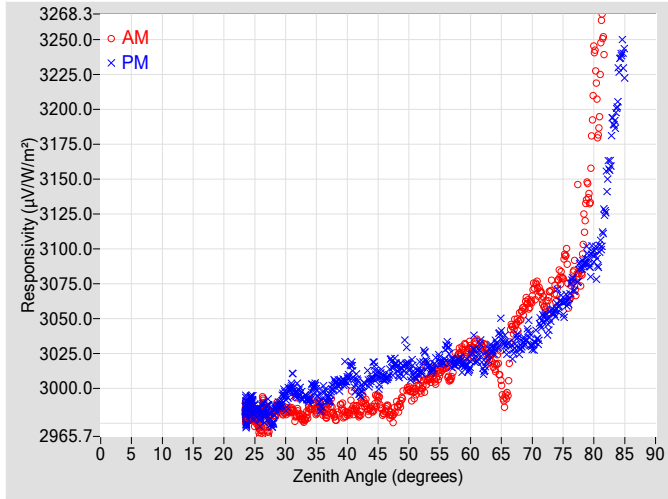


Figure 2. Responsivity vs Local Standard Time

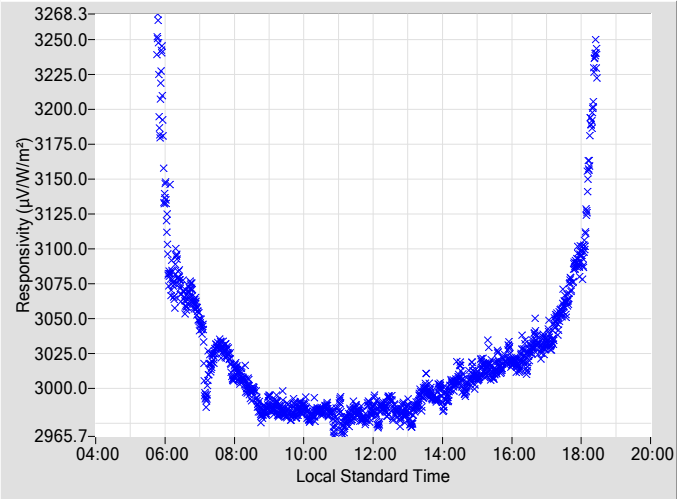


Table 2. Instrument Responsivity (R) and Calibration Type-B Standard Uncertainty, $u(B)$

| Zenith Angle (deg.) | R ($\mu\text{V}/\text{W}/\text{m}^2$) | $u(B)$ \pm (%) | Azimuth Angle | R ($\mu\text{V}/\text{W}/\text{m}^2$) | $u(B)$ \pm (%) | Azimuth Angle | Zenith Angle (deg.) | R ($\mu\text{V}/\text{W}/\text{m}^2$) | $u(B)$ \pm (%) | Azimuth Angle | R ($\mu\text{V}/\text{W}/\text{m}^2$) | $u(B)$ \pm (%) | Azimuth Angle |
|---------------------|---|------------------|---------------|---|------------------|---------------|---------------------|---|------------------|---------------|---|------------------|---------------|
| 0 | N/A | N/A | N/A | N/A | N/A | N/A | 46 | 2982.9 | 0.31 | 106.78 | 3007.2 | 0.31 | 252.83 |
| 2 | N/A | N/A | N/A | N/A | N/A | N/A | 48 | 2986.9 | 0.31 | 104.53 | 3015.9 | 0.31 | 255.09 |
| 4 | N/A | N/A | N/A | N/A | N/A | N/A | 50 | 2999.7 | 0.33 | 102.42 | 3014.3 | 0.33 | 257.24 |
| 6 | N/A | N/A | N/A | N/A | N/A | N/A | 52 | 2999.8 | 0.35 | 100.39 | 3014.2 | 0.32 | 259.30 |
| 8 | N/A | N/A | N/A | N/A | N/A | N/A | 54 | 3009.2 | 0.34 | 98.46 | 3015.5 | 0.34 | 261.23 |
| 10 | N/A | N/A | N/A | N/A | N/A | N/A | 56 | 3014.8 | 0.34 | 96.59 | 3028.9 | 0.33 | 263.11 |
| 12 | N/A | N/A | N/A | N/A | N/A | N/A | 58 | 3024.3 | 0.39 | 94.80 | 3020.2 | 0.33 | 264.92 |
| 14 | N/A | N/A | N/A | N/A | N/A | N/A | 60 | 3029.4 | 0.34 | 93.06 | 3019.5 | 0.34 | 266.68 |
| 16 | N/A | N/A | N/A | N/A | N/A | N/A | 62 | 3031.2 | 0.35 | 91.36 | 3015.3 | 0.35 | 268.40 |
| 18 | N/A | N/A | N/A | N/A | N/A | N/A | 64 | 3015.6 | 0.36 | 89.69 | 3030.9 | 0.36 | 270.10 |
| 20 | N/A | N/A | N/A | N/A | N/A | N/A | 66 | 3000.7 | 0.42 | 88.04 | 3029.8 | 0.38 | 271.73 |
| 22 | N/A | N/A | N/A | N/A | N/A | N/A | 68 | 3049.5 | 0.39 | 86.43 | 3028.3 | 0.40 | 273.37 |
| 24 | 2982.4 | 0.31 | 167.09 | 2986.7 | 0.30 | 193.04 | 70 | 3067.4 | 0.42 | 84.79 | 3029.8 | 0.42 | 274.99 |
| 26 | 2974.9 | 0.30 | 151.05 | 2981.9 | 0.31 | 209.11 | 72 | 3060.4 | 0.45 | 83.19 | 3051.0 | 0.49 | 276.61 |
| 28 | 2983.1 | 0.33 | 140.76 | 2977.1 | 0.31 | 217.97 | 74 | 3071.8 | 0.49 | 81.61 | 3059.0 | 0.49 | 278.20 |
| 30 | 2984.1 | 0.33 | 134.40 | 2992.1 | 0.30 | 224.64 | 76 | 3065.7 | 0.54 | 80.00 | 3066.3 | 0.55 | 279.80 |
| 32 | 2981.9 | 0.31 | 129.23 | 2997.6 | 0.33 | 229.98 | 78 | 3086.8 | 0.75 | 78.39 | 3088.5 | N/A | 281.45 |
| 34 | 2987.3 | 0.32 | 124.85 | 2994.5 | 0.34 | 234.45 | 80 | 3226.4 | N/A | 76.75 | 3095.6 | N/A | 283.05 |
| 36 | 2984.4 | 0.31 | 121.02 | 2992.7 | 0.31 | 238.34 | 82 | N/A | N/A | N/A | 3140.0 | N/A | 284.70 |
| 38 | 2979.8 | 0.33 | 117.58 | 3004.0 | 0.31 | 241.76 | 84 | N/A | N/A | N/A | 3222.8 | N/A | 286.39 |
| 40 | 2981.8 | 0.33 | 114.47 | 3007.0 | 0.31 | 245.01 | 86 | N/A | N/A | N/A | N/A | N/A | N/A |
| 42 | 2981.1 | 0.33 | 111.76 | 2997.0 | 0.32 | 247.82 | 88 | N/A | N/A | N/A | N/A | N/A | N/A |
| 44 | 2984.8 | 0.32 | 109.17 | 3011.0 | 0.33 | 250.46 | 90 | N/A | N/A | N/A | N/A | N/A | N/A |

N/A - Not Available

Figure 3. Type-B Standard Uncertainty vs Zenith Angle

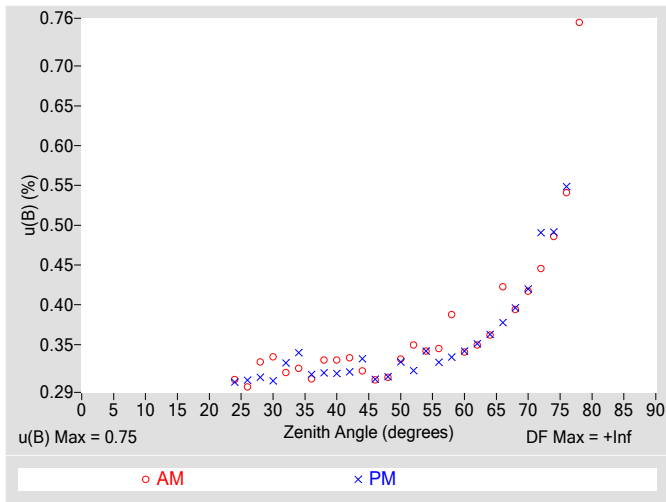


Figure 4. Residuals from Spline Interpolation

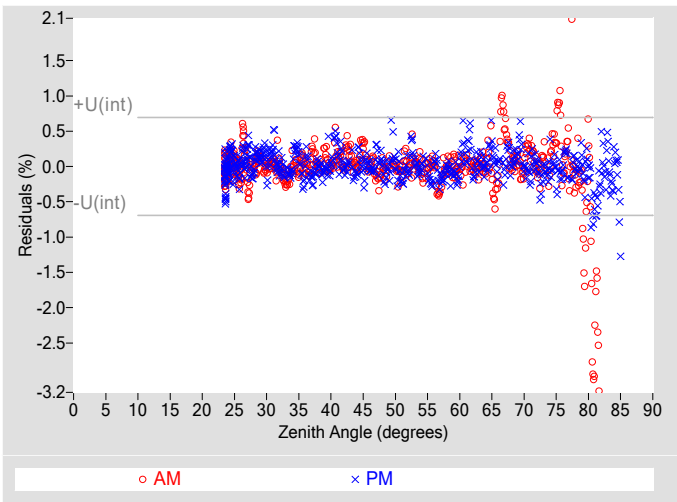


Table 3. Uncertainty using Spline Interpolation ‡

| | |
|---|------------|
| Type-B Standard Uncertainty, $u(B)$ (%) | ± 0.75 |
| Type-A Interpolating Function, $u(int)$ (%) | ± 0.35 |
| Combined Standard Uncertainty, $u(c)$ (%) | ± 0.83 |
| Effective degrees of freedom, $DF(c)$ | 37479 |
| Coverage factor, k | 1.96 |
| Expanded Uncertainty, $U95$ (%) | ± 1.6 |
| AM Valid zenith angle range | 24° to 78° |
| PM Valid zenith angle range | 24° to 76° |

‡ An illustration for how to reduce the uncertainty in calculating the irradiance using a function rather than $R@45^\circ$. Not accredited.

Table 4. Calibration Label Values

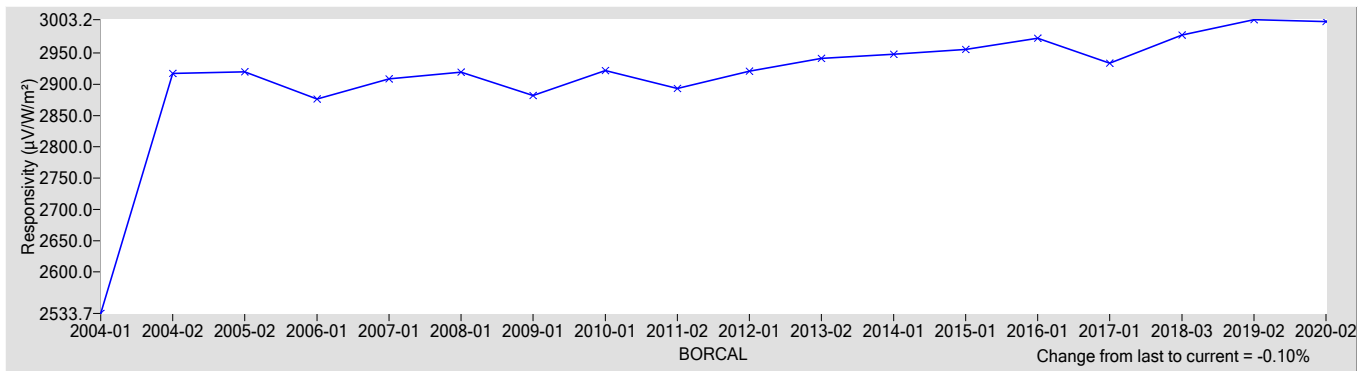
| | |
|----------------------------------|-------------------------------|
| $R @ 45^\circ$ ($\mu V/W/m^2$) | R_{net} ($\mu V/W/m^2$) † |
| 3000.1 | 0 |

† R_{net} determination date: N/A

Table 5. Uncertainty using $R @ 45^\circ$

| | |
|---|----------------|
| Type-B Expanded Uncertainty, $U(B)$ (%) | ± 0.76 |
| Offset Uncertainty, $U(off)$ (%) | +0.98 / -0.68 |
| Expanded Uncertainty, U (%) | +1.7 / -1.4 |
| Effective degrees of freedom, DF | +Inf |
| Coverage factor, k | 1.96 |
| Valid zenith angle range | 30.0° to 60.0° |

Figure 5. History of instrument at Zenith Angle = 45°



References:

[1] Reda, I.; Hickey, J.; Long, C.; Myers, D.; Stoffel, T.; Wilcox, S.; Michalsky, J. J.; Dutton, E. G.; Nelson, D. (2005). "Using a Blackbody to Calculate Net Longwave Responsivity of Shortwave Solar Pyranometers to Correct for Their Thermal Offset Error During Outdoor Calibration Using the Component Sum Method." Journal of Atmospheric and Oceanic Technology. , 2005; pp. 1531-1540; NREL Report No. JA-560-36646. doi:10.1175/JTECH1782.1

[2] Reda, I.; Myers, D.; Stoffel, T. (2008). "Uncertainty Estimate for the Outdoor Calibration of Solar Pyranometers: A Metrologist Perspective." Measure. (NCSLI Journal of Measurement Science). Vol. 3(4), December 2008; pp. 58-66; NREL Report No. JA-581-4137

[3] Reda, I.; Andreas, A. (2004). "Solar Position Algorithm for Solar Radiation Applications." Solar Energy. Vol. 76(5), 2004; pp. 577-589; NREL Report No. JA-560-35518. doi:10.1016/j.solener.2003.12.003

[4] Stoffel, T.; Reda, I. (2009). "NREL Pyrheliometer Comparisons: 22 September - 3 October 2008 (NPC-2008)." 54 pp.; NREL Report No. TP-550-45016.

[5] Reda, I.; Stoffel, T.; Myers, D. (2003). "Method to Calibrate a Solar Pyranometer for Measuring Reference Diffuse Irradiance." Solar Energy. Vol. 74, 2003; pp. 103-112; NREL Report No. JA-560-35025. doi:10.1016/S0038-092X(03)00124-5

[6] Reda, I. (1996). Calibration of a Solar Absolute Cavity Radiometer with Traceability to the World Radiometric Reference. 79 pp.; NREL Report No. TP-463-20619.

[7] Reda, I.; Gröbner, J.; Stoffel, T.; Myers, D.; Forgan, B. (2008). Improvements in the Blackbody Calibration of Pyrgometers. ARM 2008 Science Team Meeting (Poster).



National Renewable Energy Laboratory

Solar Radiation Research Laboratory

Metrology Laboratory

Calibration Certificate



| | | | |
|--------------------------|---------------|----------------------------------|--------------|
| Test Instrument: | Pyrheliometer | Manufacturer: | Kipp & Zonen |
| Model: | CHP1 | Serial Number: | 080009 |
| Calibration Date: | 5/5/2020 | Due Date: | 5/5/2021 |
| Customer: | NREL-SRRL-BMS | Environmental Conditions: | see page 4 |
| Test Dates: | 5/4-5 | | |

This certifies that the above product was calibrated in compliance with ISO/IEC 17025:2017. Measurement uncertainties at the time of calibration are consistent with the Guide to the Expression of Uncertainty in Measurement (GUM) using Reda et al., 2008. All nominal values are traceable to the International System (SI) Units of Measurement.

No statement of compliance with specifications is made or implied on this certificate. However, the estimated uncertainties are the uncertainties of the calibration process; users must add other uncertainties that are relevant to their measuring system, environmental and sky conditions, outdoor set-up, and site location.

The Type-B Standard Uncertainty of using the responsivity at each even zenith angle is reported, and the Expanded Uncertainty of the calibration is reported using two methods:

1. The Expanded Uncertainty of using the responsivity at zenith angle = 45°, within the zenith angle range from 30.0° to 60.0°
2. The Expanded Uncertainty of using Spline Interpolating Functions for the responsivity versus zenith angle.

This certificate applies only to the item identified above and shall not be reproduced other than in full, without specific written approval from the calibration facility. Certificate without signature is not valid.

Table 1. Traceability

| Measurement Type | Instrument | Calibration Date | Calibration Due Date |
|----------------------|--|------------------|----------------------|
| Beam Irradiance † | Eppley Absolute Cavity Radiometer Model HF, S/N 29219 | 09/27/2019 | 09/27/2020 |
| Diffuse Irradiance † | Hukseflux Pyranometer Model SR25, S/N 2541 | 04/17/2020 | 04/17/2021 |
| Diffuse Irradiance † | Hukseflux Pyranometer Model SR25, S/N 2542 | 04/17/2020 | 04/17/2021 |
| Data Acquisition | NREL Data Acquisition System Model RAP-DAQ, S/N 2005-998 | 02/14/2019 | 02/14/2021 |
| Data Acquisition | NREL Data Acquisition System Model RAP-DAQ, S/N 2005-999 | 02/14/2019 | 02/14/2021 |

† Through the World Radiometric Reference (WRR)

Number of pages of certificate: 4

Calibration Procedure: BORCAL-P00-Calibration and QA Procedure; available upon request.

Setup: Radiometers are calibrated outdoors, using the sun as the source. Pyranometers and pyrgeometers are installed for horizontal measurements, with their signal connectors oriented north, if their design permits.
The shading disk for the reference diffuse subtends a solid angle of 5°. Pyrhemometers are installed on solar trackers.

Calibrated by: Afshin Andreas, Ibrahim Reda, Peter Gotseff, and RCC

Ibrahim Reda, Technical Manager

Date

For questions or comments, please contact the technical manager at:
ibrahim.reda@nrel.gov; 303-384-6385; 15013 Denver West Parkway, Golden, CO 80401, USA

Calibration Results

080009 Kipp & Zonen CHP1

The responsivity (R , $\mu\text{V}/\text{W}/\text{m}^2$) of the test instrument during calibration is calculated using this Measurement Equation:

$$R = (V - R_{net} * W_{net}) / I \tag{1}$$

where,

- V = radiometer output voltage (microvolts),
- R_{net} = radiometer net infrared responsivity ($\mu\text{V}/\text{W}/\text{m}^2$), see Table 4,
- W_{net} = effective net infrared measured by pyrgeometer (W/m^2),
- $= W_{in} - W_{out} = W_{in} - \sigma * T_c^4$
- where, W_{in} = incoming infrared (W/m^2), $\sigma = 5.6704\text{e-}8 \text{ W}\cdot\text{m}^{-2}\cdot\text{K}^{-4}$,
- T_c = case temperature of pyrgeometer (K).
- I = reference irradiance (W/m^2), beam (B) or global (G)
- where, $G = B * \text{COS}(Z) + D$,
- Z = zenith angle (degrees),
- D = reference diffuse irradiance (W/m^2).

Figure 1. Responsivity vs Zenith Angle

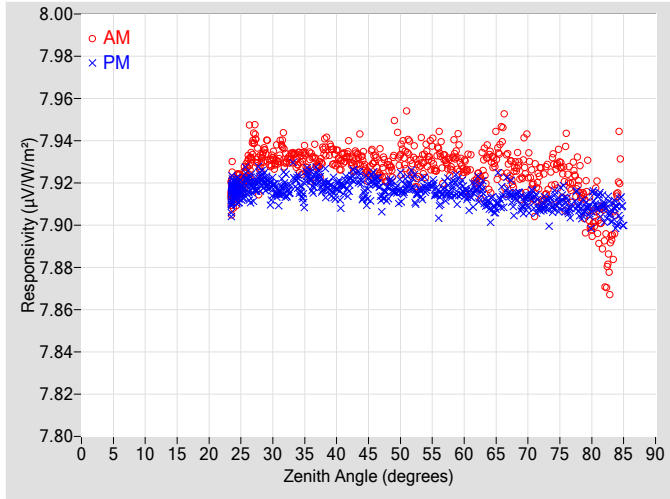


Figure 2. Responsivity vs Local Standard Time

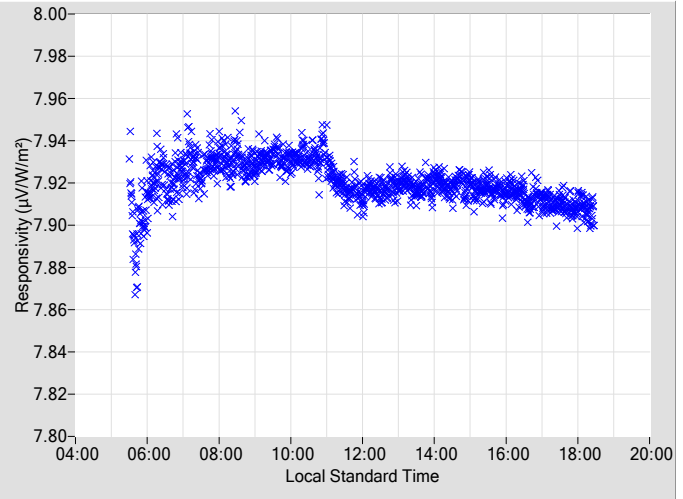


Table 2. Instrument Responsivity (R) and Calibration Type-B Standard Uncertainty, u(B)

| Zenith | | | AM | | | PM | | | Zenith | | | AM | | | PM | | |
|--------|---------------------------------------|-------|---------|---------------------------------------|-------|---------|--------|---------------------------------------|--------|---------|---------------------------------------|-------|---------|---------------------------------------|-------|---------|--|
| Angle | R | u(B) | Azimuth | R | u(B) | Azimuth | Angle | R | u(B) | Azimuth | R | u(B) | Azimuth | R | u(B) | Azimuth | |
| (deg.) | ($\mu\text{V}/\text{W}/\text{m}^2$) | ± (%) | Angle | ($\mu\text{V}/\text{W}/\text{m}^2$) | ± (%) | Angle | (deg.) | ($\mu\text{V}/\text{W}/\text{m}^2$) | ± (%) | Angle | ($\mu\text{V}/\text{W}/\text{m}^2$) | ± (%) | Angle | ($\mu\text{V}/\text{W}/\text{m}^2$) | ± (%) | Angle | |
| 0 | N/A | N/A | N/A | N/A | N/A | N/A | 46 | 7.9308 | 0.29 | 106.76 | 7.9211 | 0.29 | 252.81 | | | | |
| 2 | N/A | N/A | N/A | N/A | N/A | N/A | 48 | 7.9252 | 0.30 | 104.54 | 7.9162 | 0.29 | 255.07 | | | | |
| 4 | N/A | N/A | N/A | N/A | N/A | N/A | 50 | 7.9314 | 0.30 | 102.41 | 7.9167 | 0.29 | 257.23 | | | | |
| 6 | N/A | N/A | N/A | N/A | N/A | N/A | 52 | 7.9276 | 0.31 | 100.37 | 7.9196 | 0.29 | 259.29 | | | | |
| 8 | N/A | N/A | N/A | N/A | N/A | N/A | 54 | 7.9311 | 0.32 | 98.50 | 7.9183 | 0.30 | 261.27 | | | | |
| 10 | N/A | N/A | N/A | N/A | N/A | N/A | 56 | 7.9362 | 0.30 | 96.58 | 7.9114 | 0.29 | 263.10 | | | | |
| 12 | N/A | N/A | N/A | N/A | N/A | N/A | 58 | 7.9280 | 0.30 | 94.79 | 7.9166 | 0.29 | 264.91 | | | | |
| 14 | N/A | N/A | N/A | N/A | N/A | N/A | 60 | 7.9271 | 0.30 | 93.05 | 7.9162 | 0.30 | 266.71 | | | | |
| 16 | N/A | N/A | N/A | N/A | N/A | N/A | 62 | 7.9214 | 0.31 | 91.35 | 7.9175 | 0.30 | 268.39 | | | | |
| 18 | N/A | N/A | N/A | N/A | N/A | N/A | 64 | 7.9271 | 0.30 | 89.68 | 7.9089 | 0.30 | 270.09 | | | | |
| 20 | N/A | N/A | N/A | N/A | N/A | N/A | 66 | 7.9388 | 0.32 | 88.03 | 7.9126 | 0.30 | 271.72 | | | | |
| 22 | N/A | N/A | N/A | N/A | N/A | N/A | 68 | 7.9255 | 0.31 | 86.42 | 7.9121 | 0.30 | 273.36 | | | | |
| 24 | 7.9152 | 0.30 | 167.15 | 7.9170 | 0.30 | 192.94 | 70 | 7.9261 | 0.30 | 84.82 | 7.9109 | 0.30 | 274.98 | | | | |
| 26 | 7.9267 | 0.31 | 151.04 | 7.9198 | 0.29 | 209.08 | 72 | 7.9197 | 0.30 | 83.18 | 7.9084 | 0.31 | 276.59 | | | | |
| 28 | 7.9270 | 0.31 | 140.90 | 7.9225 | 0.31 | 218.19 | 74 | 7.9237 | 0.33 | 81.60 | 7.9103 | 0.31 | 278.20 | | | | |
| 30 | 7.9311 | 0.30 | 134.49 | 7.9179 | 0.32 | 224.72 | 76 | 7.9249 | 0.31 | 79.99 | 7.9092 | 0.31 | 279.83 | | | | |
| 32 | 7.9312 | 0.29 | 129.20 | 7.9185 | 0.29 | 230.05 | 78 | 7.9215 | 0.32 | 78.38 | 7.9079 | N/A | 281.44 | | | | |
| 34 | 7.9304 | 0.30 | 124.82 | 7.9195 | 0.30 | 234.61 | 80 | 7.8998 | N/A | 76.74 | 7.9087 | N/A | 283.09 | | | | |
| 36 | 7.9308 | 0.30 | 121.03 | 7.9208 | 0.31 | 238.40 | 82 | 7.8909 | N/A | 75.09 | 7.9080 | N/A | 284.73 | | | | |
| 38 | 7.9356 | 0.31 | 117.64 | 7.9190 | 0.31 | 241.90 | 84 | 7.9199 | N/A | 73.42 | 7.9036 | N/A | 286.38 | | | | |
| 40 | 7.9320 | 0.31 | 114.45 | 7.9172 | 0.30 | 244.99 | 86 | N/A | N/A | N/A | N/A | N/A | N/A | | | | |
| 42 | 7.9337 | 0.29 | 111.81 | 7.9191 | 0.30 | 247.80 | 88 | N/A | N/A | N/A | N/A | N/A | N/A | | | | |
| 44 | 7.9312 | 0.30 | 109.15 | 7.9156 | 0.29 | 250.44 | 90 | N/A | N/A | N/A | N/A | N/A | N/A | | | | |

N/A - Not Available

Figure 3. Type-B Standard Uncertainty vs Zenith Angle

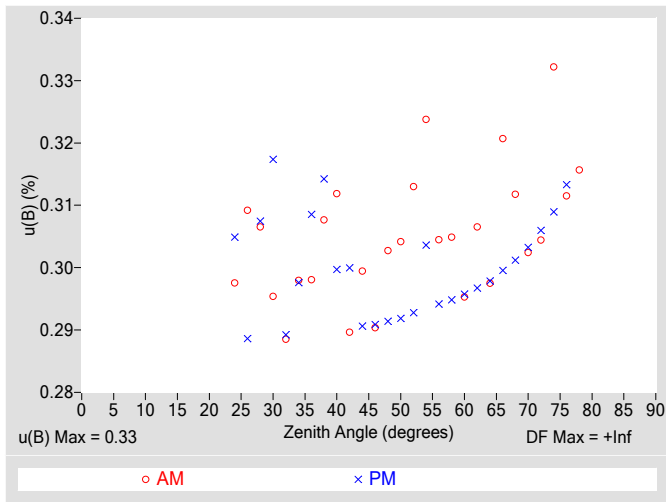


Figure 4. Residuals from Spline Interpolation

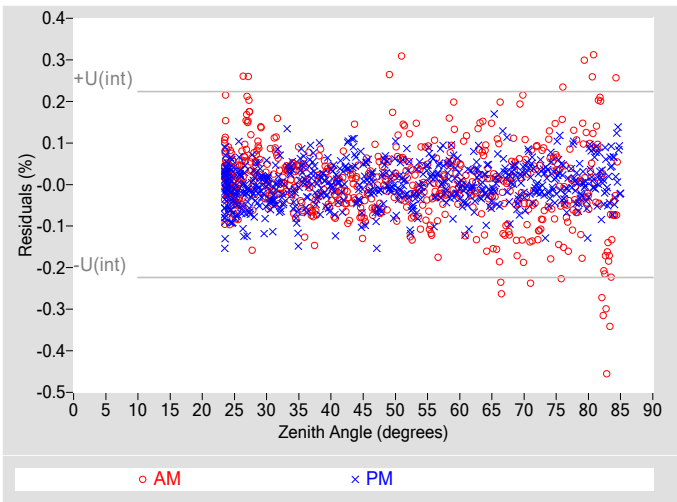


Table 3. Uncertainty using Spline Interpolation ‡

| | |
|---|------------|
| Type-B Standard Uncertainty, $u(B)$ (%) | ± 0.33 |
| Type-A Interpolating Function, $u(int)$ (%) | ± 0.11 |
| Combined Standard Uncertainty, $u(c)$ (%) | ± 0.35 |
| Effective degrees of freedom, $DF(c)$ | 112168 |
| Coverage factor, k | 1.96 |
| Expanded Uncertainty, U_{95} (%) | ± 0.69 |
| AM Valid zenith angle range | 24° to 78° |
| PM Valid zenith angle range | 24° to 76° |

‡ An illustration for how to reduce the uncertainty in calculating the irradiance using a function rather than $R@45^\circ$. Not accredited.

Table 4. Calibration Label Values

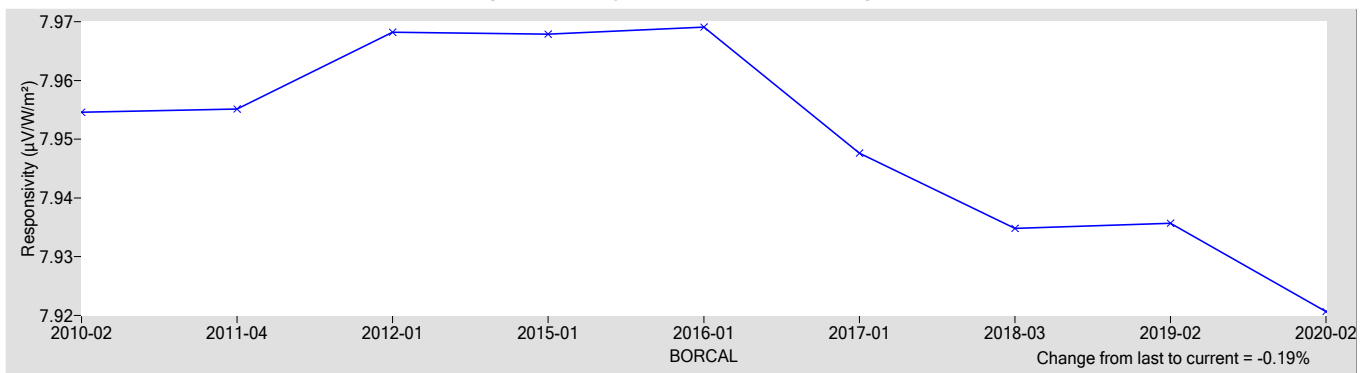
| | |
|----------------------------------|-------------------------------|
| $R @ 45^\circ$ ($\mu V/W/m^2$) | R_{net} ($\mu V/W/m^2$) † |
| 7.9207 | 0 |

† R_{net} determination date: N/A

Table 5. Uncertainty using $R @ 45^\circ$

| | |
|---|----------------|
| Type-B Expanded Uncertainty, $U(B)$ (%) | ± 0.63 |
| Offset Uncertainty, $U(off)$ (%) | +0.20 / -0.12 |
| Expanded Uncertainty, U (%) | +0.83 / -0.75 |
| Effective degrees of freedom, DF | +Inf |
| Coverage factor, k | 1.96 |
| Valid zenith angle range | 30.0° to 60.0° |

Figure 5. History of instrument at Zenith Angle = 45°



References:

- [1] Reda, I.; Hickey, J.; Long, C.; Myers, D.; Stoffel, T.; Wilcox, S.; Michalsky, J. J.; Dutton, E. G.; Nelson, D. (2005). "Using a Blackbody to Calculate Net Longwave Responsivity of Shortwave Solar Pyranometers to Correct for Their Thermal Offset Error During Outdoor Calibration Using the Component Sum Method." *Journal of Atmospheric and Oceanic Technology*, 2005; pp. 1531-1540; NREL Report No. JA-560-36646. doi:10.1175/JTECH1782.1
- [2] Reda, I.; Myers, D.; Stoffel, T. (2008). "Uncertainty Estimate for the Outdoor Calibration of Solar Pyranometers: A Metrologist Perspective." *Measure*. (NCSLI Journal of Measurement Science). Vol. 3(4), December 2008; pp. 58-66; NREL Report No. JA-581-4137
- [3] Reda, I.; Andreas, A. (2004). "Solar Position Algorithm for Solar Radiation Applications." *Solar Energy*. Vol. 76(5), 2004; pp. 577-589; NREL Report No. JA-560-35518. doi:10.1016/j.solener.2003.12.003
- [4] Stoffel, T.; Reda, I. (2009). "NREL Pyrheliometer Comparisons: 22 September - 3 October 2008 (NPC-2008)." 54 pp.; NREL Report No. TP-550-45016.
- [5] Reda, I.; Stoffel, T.; Myers, D. (2003). "Method to Calibrate a Solar Pyranometer for Measuring Reference Diffuse Irradiance." *Solar Energy*. Vol. 74, 2003; pp. 103-112; NREL Report No. JA-560-35025. doi:10.1016/S0038-092X(03)00124-5
- [6] Reda, I. (1996). Calibration of a Solar Absolute Cavity Radiometer with Traceability to the World Radiometric Reference. 79 pp.; NREL Report No. TP-463-20619.
- [7] Reda, I.; Gröbner, J.; Stoffel, T.; Myers, D.; Forgan, B. (2008). Improvements in the Blackbody Calibration of Pyrgometers. ARM 2008 Science Team Meeting (Poster).



National Renewable Energy Laboratory

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Calibration Certificate



| | | | |
|--------------------------|--------------------------|----------------------------------|--------------|
| Test Instrument: | Pyranometer (Ventilated) | Manufacturer: | Kipp & Zonen |
| Model: | CMP22 | Serial Number: | 080017 |
| Calibration Date: | 5/5/2020 | Due Date: | 5/5/2021 |
| Customer: | NREL-SRRL-BMS | Environmental Conditions: | see page 4 |
| Test Dates: | 5/4-5 | | |

This certifies that the above product was calibrated in compliance with ISO/IEC 17025:2017. Measurement uncertainties at the time of calibration are consistent with the Guide to the Expression of Uncertainty in Measurement (GUM) using Reda et al., 2008. All nominal values are traceable to the International System (SI) Units of Measurement.

No statement of compliance with specifications is made or implied on this certificate. However, the estimated uncertainties are the uncertainties of the calibration process; users must add other uncertainties that are relevant to their measuring system, environmental and sky conditions, outdoor set-up, and site location.

The Type-B Standard Uncertainty of using the responsivity at each even zenith angle is reported, and the Expanded Uncertainty of the calibration is reported using two methods:

1. The Expanded Uncertainty of using the responsivity at zenith angle = 45°, within the zenith angle range from 30.0° to 60.0°
2. The Expanded Uncertainty of using Spline Interpolating Functions for the responsivity versus zenith angle.

This certificate applies only to the item identified above and shall not be reproduced other than in full, without specific written approval from the calibration facility. Certificate without signature is not valid.

Table 1. Traceability

| Measurement Type | Instrument | Calibration Date | Calibration Due Date |
|-----------------------|--|------------------|----------------------|
| Beam Irradiance † | Eppley Absolute Cavity Radiometer Model HF, S/N 29219 | 09/27/2019 | 09/27/2020 |
| Diffuse Irradiance † | Hukseflux Pyranometer Model SR25, S/N 2541 | 04/17/2020 | 04/17/2021 |
| Diffuse Irradiance † | Hukseflux Pyranometer Model SR25, S/N 2542 | 04/17/2020 | 04/17/2021 |
| Data Acquisition | NREL Data Acquisition System Model RAP-DAQ, S/N 2005-998 | 02/14/2019 | 02/14/2021 |
| Data Acquisition | NREL Data Acquisition System Model RAP-DAQ, S/N 2005-999 | 02/14/2019 | 02/14/2021 |
| Infrared Irradiance ‡ | Kipp & Zonen Pyrgeometer Model CGR4, S/N 140021 | 04/02/2019 | 04/02/2023 |

† Through the World Radiometric Reference (WRR)

‡ Through the World Infrared Standard Group (WISG)

Number of pages of certificate: 4

Calibration Procedure: BORCAL-P00-Calibration and QA Procedure; available upon request.

Setup: Radiometers are calibrated outdoors, using the sun as the source. Pyranometers and pyrgeometers are installed for horizontal measurements, with their signal connectors oriented north, if their design permits.

The shading disk for the reference diffuse subtends a solid angle of 5°. Pyrheliometers are installed on solar trackers.

Calibrated by: Afshin Andreas, Ibrahim Reda, Peter Gotseff, and RCC

Ibrahim Reda, Technical Manager

Date

For questions or comments, please contact the technical manager at:

ibrahim.reda@nrel.gov; 303-384-6385; 15013 Denver West Parkway, Golden, CO 80401, USA

Calibration Results

080017 Kipp & Zonen CMP22

The responsivity (R , $\mu\text{V}/\text{W}/\text{m}^2$) of the test instrument during calibration is calculated using this Measurement Equation:

$$R = (V - R_{net} * W_{net}) / I \tag{1}$$

where,

- V = radiometer output voltage (microvolts),
 - R_{net} = radiometer net infrared responsivity ($\mu\text{V}/\text{W}/\text{m}^2$), see Table 4,
 - W_{net} = effective net infrared measured by pyrgeometer (W/m^2),
 - = $W_{in} - W_{out} = W_{in} - \sigma * T_c^4$
 - where, W_{in} = incoming infrared (W/m^2), $\sigma = 5.6704\text{e-}8 \text{ W}\cdot\text{m}^{-2}\cdot\text{K}^{-4}$,
 - T_c = case temperature of pyrgeometer (K).
- I = reference irradiance (W/m^2), beam (B) or global (G)
 - where, $G = B * \text{COS}(Z) + D$,
 - Z = zenith angle (degrees),
 - D = reference diffuse irradiance (W/m^2).

Figure 1. Responsivity vs Zenith Angle

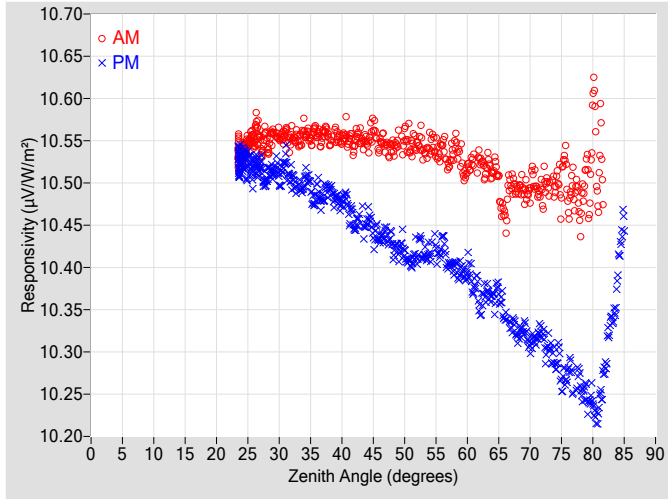


Figure 2. Responsivity vs Local Standard Time

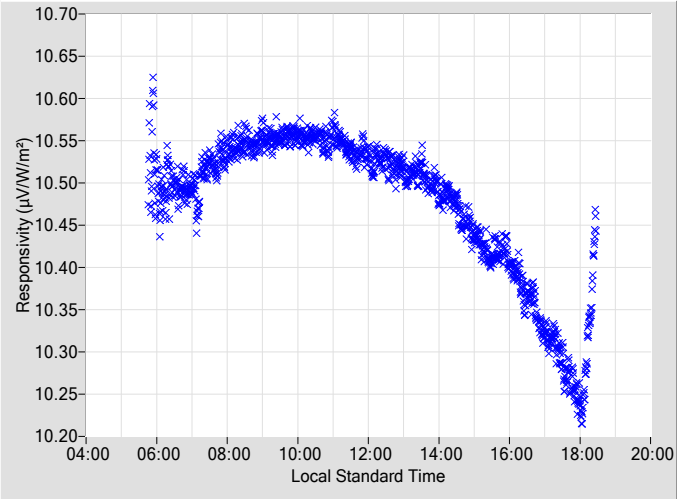


Table 2. Instrument Responsivity (R) and Calibration Type-B Standard Uncertainty, u(B)

| Zenith Angle (deg.) | R ($\mu\text{V}/\text{W}/\text{m}^2$) | u(B) \pm (%) | Azimuth Angle | R ($\mu\text{V}/\text{W}/\text{m}^2$) | u(B) \pm (%) | Azimuth Angle | Zenith Angle (deg.) | R ($\mu\text{V}/\text{W}/\text{m}^2$) | u(B) \pm (%) | Azimuth Angle | R ($\mu\text{V}/\text{W}/\text{m}^2$) | u(B) \pm (%) | Azimuth Angle |
|---------------------|---|----------------|---------------|---|----------------|---------------|---------------------|---|----------------|---------------|---|----------------|---------------|
| 0 | N/A | N/A | N/A | N/A | N/A | N/A | 46 | 10.544 | 0.31 | 106.78 | 10.434 | 0.31 | 252.84 |
| 2 | N/A | N/A | N/A | N/A | N/A | N/A | 48 | 10.541 | 0.33 | 104.51 | 10.427 | 0.31 | 255.09 |
| 4 | N/A | N/A | N/A | N/A | N/A | N/A | 50 | 10.555 | 0.32 | 102.43 | 10.416 | 0.33 | 257.25 |
| 6 | N/A | N/A | N/A | N/A | N/A | N/A | 52 | 10.544 | 0.32 | 100.39 | 10.419 | 0.32 | 259.31 |
| 8 | N/A | N/A | N/A | N/A | N/A | N/A | 54 | 10.547 | 0.35 | 98.42 | 10.417 | 0.32 | 261.24 |
| 10 | N/A | N/A | N/A | N/A | N/A | N/A | 56 | 10.545 | 0.36 | 96.60 | 10.434 | 0.33 | 263.12 |
| 12 | N/A | N/A | N/A | N/A | N/A | N/A | 58 | 10.543 | 0.35 | 94.81 | 10.401 | 0.34 | 264.93 |
| 14 | N/A | N/A | N/A | N/A | N/A | N/A | 60 | 10.516 | 0.34 | 93.07 | 10.400 | 0.37 | 266.68 |
| 16 | N/A | N/A | N/A | N/A | N/A | N/A | 62 | 10.529 | 0.35 | 91.36 | 10.354 | 0.36 | 268.41 |
| 18 | N/A | N/A | N/A | N/A | N/A | N/A | 64 | 10.510 | 0.37 | 89.69 | 10.366 | 0.37 | 270.06 |
| 20 | N/A | N/A | N/A | N/A | N/A | N/A | 66 | 10.459 | 0.38 | 88.05 | 10.340 | 0.38 | 271.73 |
| 22 | N/A | N/A | N/A | N/A | N/A | N/A | 68 | 10.493 | 0.43 | 86.39 | 10.317 | 0.40 | 273.37 |
| 24 | 10.534 | 0.31 | 166.80 | 10.529 | 0.31 | 192.80 | 70 | 10.494 | 0.42 | 84.79 | 10.306 | 0.43 | 275.00 |
| 26 | 10.554 | 0.33 | 150.95 | 10.519 | 0.31 | 209.24 | 72 | 10.492 | 0.45 | 83.20 | 10.321 | 0.46 | 276.61 |
| 28 | 10.549 | 0.33 | 140.77 | 10.505 | 0.31 | 217.98 | 74 | 10.496 | 0.49 | 81.62 | 10.287 | 0.50 | 278.21 |
| 30 | 10.555 | 0.32 | 134.34 | 10.504 | 0.30 | 224.76 | 76 | 10.483 | 0.55 | 80.00 | 10.274 | 0.56 | 279.80 |
| 32 | 10.554 | 0.33 | 129.28 | 10.505 | 0.32 | 229.99 | 78 | 10.464 | 0.62 | 78.40 | 10.263 | N/A | 281.41 |
| 34 | 10.560 | 0.33 | 124.77 | 10.502 | 0.33 | 234.46 | 80 | 10.583 | N/A | 76.76 | 10.241 | N/A | 283.06 |
| 36 | 10.560 | 0.31 | 121.03 | 10.492 | 0.31 | 238.43 | 82 | N/A | N/A | N/A | 10.282 | N/A | 284.71 |
| 38 | 10.550 | 0.32 | 117.59 | 10.492 | 0.31 | 241.85 | 84 | N/A | N/A | N/A | 10.399 | N/A | 286.40 |
| 40 | 10.552 | 0.31 | 114.53 | 10.477 | 0.34 | 245.02 | 86 | N/A | N/A | N/A | N/A | N/A | N/A |
| 42 | 10.546 | 0.32 | 111.70 | 10.447 | 0.32 | 247.83 | 88 | N/A | N/A | N/A | N/A | N/A | N/A |
| 44 | 10.546 | 0.32 | 109.17 | 10.456 | 0.31 | 250.47 | 90 | N/A | N/A | N/A | N/A | N/A | N/A |

N/A - Not Available

Figure 3. Type-B Standard Uncertainty vs Zenith Angle

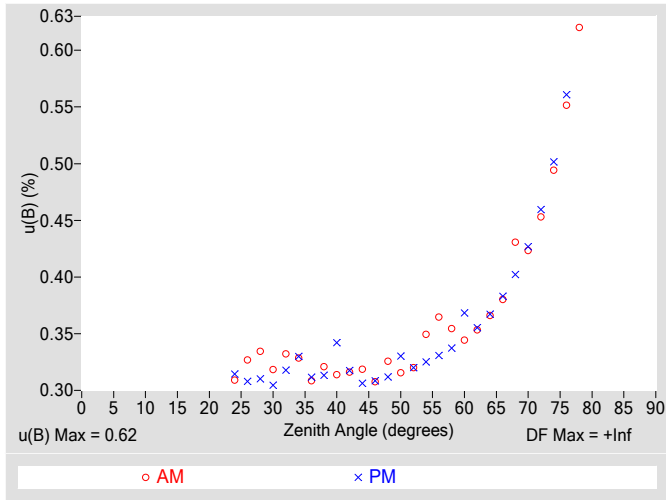


Figure 4. Residuals from Spline Interpolation

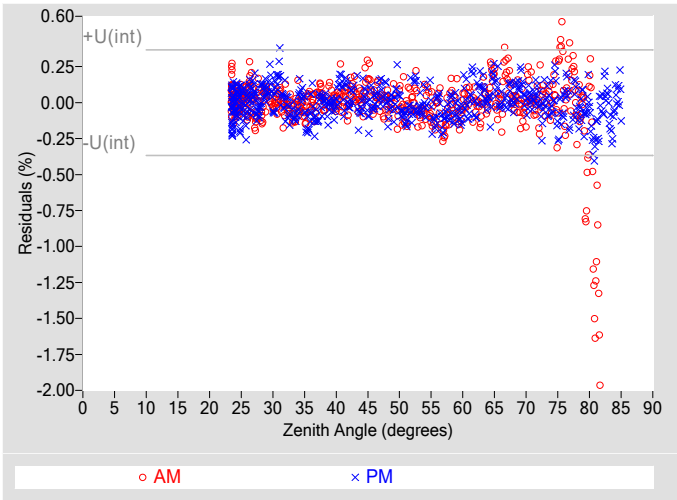


Table 3. Uncertainty using Spline Interpolation ‡

| | |
|---|------------|
| Type-B Standard Uncertainty, $u(B)$ (%) | ± 0.62 |
| Type-A Interpolating Function, $u(int)$ (%) | ± 0.18 |
| Combined Standard Uncertainty, $u(c)$ (%) | ± 0.65 |
| Effective degrees of freedom, $DF(c)$ | 177905 |
| Coverage factor, k | 1.96 |
| Expanded Uncertainty, U_{95} (%) | ± 1.3 |
| AM Valid zenith angle range | 24° to 78° |
| PM Valid zenith angle range | 24° to 76° |

‡ An illustration for how to reduce the uncertainty in calculating the irradiance using a function rather than $R@45^\circ$. Not accredited.

Table 4. Calibration Label Values

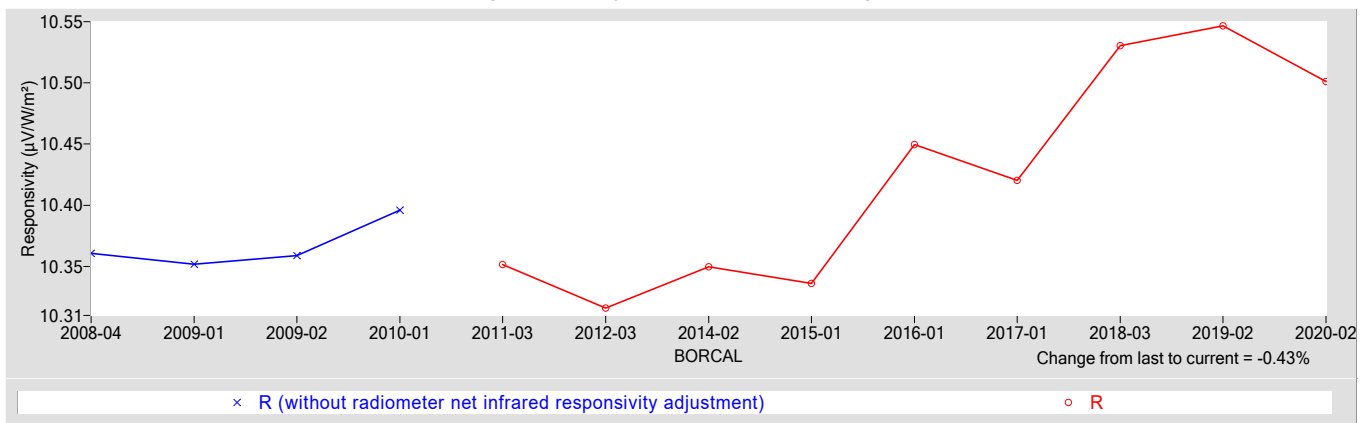
| | |
|----------------------------------|-------------------------------|
| $R @ 45^\circ$ ($\mu V/W/m^2$) | R_{net} ($\mu V/W/m^2$) † |
| 10.501 | 0.087000 |

† R_{net} determination date: Estimated

Table 5. Uncertainty using $R @ 45^\circ$

| | |
|---|----------------|
| Type-B Expanded Uncertainty, $U(B)$ (%) | ± 0.72 |
| Offset Uncertainty, $U(off)$ (%) | +0.56 / -0.96 |
| Expanded Uncertainty, U (%) | +1.3 / -1.7 |
| Effective degrees of freedom, DF | +Inf |
| Coverage factor, k | 1.96 |
| Valid zenith angle range | 30.0° to 60.0° |

Figure 5. History of instrument at Zenith Angle = 45°



References:

- [1] Reda, I.; Hickey, J.; Long, C.; Myers, D.; Stoffel, T.; Wilcox, S.; Michalsky, J. J.; Dutton, E. G.; Nelson, D. (2005). "Using a Blackbody to Calculate Net Longwave Responsivity of Shortwave Solar Pyranometers to Correct for Their Thermal Offset Error During Outdoor Calibration Using the Component Sum Method." *Journal of Atmospheric and Oceanic Technology*, 2005; pp. 1531-1540; NREL Report No. JA-560-36646. doi:10.1175/JTECH1782.1
- [2] Reda, I.; Myers, D.; Stoffel, T. (2008). "Uncertainty Estimate for the Outdoor Calibration of Solar Pyranometers: A Metrologist Perspective." *Measure*. (NCSLI Journal of Measurement Science). Vol. 3(4), December 2008; pp. 58-66; NREL Report No. JA-581-4137
- [3] Reda, I.; Andreas, A. (2004). "Solar Position Algorithm for Solar Radiation Applications." *Solar Energy*. Vol. 76(5), 2004; pp. 577-589; NREL Report No. JA-560-35518. doi:10.1016/j.solener.2003.12.003
- [4] Stoffel, T.; Reda, I. (2009). "NREL Pyrheliometer Comparisons: 22 September - 3 October 2008 (NPC-2008)." 54 pp.; NREL Report No. TP-550-45016.
- [5] Reda, I.; Stoffel, T.; Myers, D. (2003). "Method to Calibrate a Solar Pyranometer for Measuring Reference Diffuse Irradiance." *Solar Energy*. Vol. 74, 2003; pp. 103-112; NREL Report No. JA-560-35025. doi:10.1016/S0038-092X(03)00124-5
- [6] Reda, I. (1996). Calibration of a Solar Absolute Cavity Radiometer with Traceability to the World Radiometric Reference. 79 pp.; NREL Report No. TP-463-20619.
- [7] Reda, I.; Gröbner, J.; Stoffel, T.; Myers, D.; Forgan, B. (2008). Improvements in the Blackbody Calibration of Pyrgometers. ARM 2008 Science Team Meeting (Poster).



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Calibration Certificate



| | | | |
|--------------------------|---------------|----------------------------------|--------------|
| Test Instrument: | Pyranometer | Manufacturer: | Kipp & Zonen |
| Model: | CMP22 | Serial Number: | 100174 |
| Calibration Date: | 5/5/2020 | Due Date: | 5/5/2021 |
| Customer: | NREL-SRRL-BMS | Environmental Conditions: | see page 4 |
| Test Dates: | 5/4-5 | | |

This certifies that the above product was calibrated in compliance with ISO/IEC 17025:2017. Measurement uncertainties at the time of calibration are consistent with the Guide to the Expression of Uncertainty in Measurement (GUM) using Reda et al., 2008. All nominal values are traceable to the International System (SI) Units of Measurement.

No statement of compliance with specifications is made or implied on this certificate. However, the estimated uncertainties are the uncertainties of the calibration process; users must add other uncertainties that are relevant to their measuring system, environmental and sky conditions, outdoor set-up, and site location.

The Type-B Standard Uncertainty of using the responsivity at each even zenith angle is reported, and the Expanded Uncertainty of the calibration is reported using two methods:

1. The Expanded Uncertainty of using the responsivity at zenith angle = 45°, within the zenith angle range from 30.0° to 60.0°
2. The Expanded Uncertainty of using Spline Interpolating Functions for the responsivity versus zenith angle.

This certificate applies only to the item identified above and shall not be reproduced other than in full, without specific written approval from the calibration facility. Certificate without signature is not valid.

Table 1. Traceability

| Measurement Type | Instrument | Calibration Date | Calibration Due Date |
|-----------------------|--|------------------|----------------------|
| Beam Irradiance † | Eppley Absolute Cavity Radiometer Model HF, S/N 29219 | 09/27/2019 | 09/27/2020 |
| Diffuse Irradiance † | Hukseflux Pyranometer Model SR25, S/N 2541 | 04/17/2020 | 04/17/2021 |
| Diffuse Irradiance † | Hukseflux Pyranometer Model SR25, S/N 2542 | 04/17/2020 | 04/17/2021 |
| Data Acquisition | NREL Data Acquisition System Model RAP-DAQ, S/N 2005-998 | 02/14/2019 | 02/14/2021 |
| Data Acquisition | NREL Data Acquisition System Model RAP-DAQ, S/N 2005-999 | 02/14/2019 | 02/14/2021 |
| Infrared Irradiance ‡ | Kipp & Zonen Pyrgeometer Model CG4, S/N FT002 | 04/16/2018 | 04/16/2022 |

† Through the World Radiometric Reference (WRR)

‡ Through the World Infrared Standard Group (WISG)

Number of pages of certificate: 4

Calibration Procedure: BORCAL-P00-Calibration and QA Procedure; available upon request.

Setup: Radiometers are calibrated outdoors, using the sun as the source. Pyranometers and pyrgeometers are installed for horizontal measurements, with their signal connectors oriented north, if their design permits.

The shading disk for the reference diffuse subtends a solid angle of 5°. Pyrheliometers are installed on solar trackers.

Calibrated by: Afshin Andreas, Ibrahim Reda, Peter Gotseff, and RCC

Ibrahim Reda, Technical Manager

Date

For questions or comments, please contact the technical manager at:

ibrahim.reda@nrel.gov; 303-384-6385; 15013 Denver West Parkway, Golden, CO 80401, USA

Calibration Results

100174 Kipp & Zonen CMP22

The responsivity (R , $\mu\text{V}/\text{W}/\text{m}^2$) of the test instrument during calibration is calculated using this Measurement Equation:

$$R = (V - R_{net} * W_{net}) / I \tag{1}$$

where,

- V = radiometer output voltage (microvolts),
- R_{net} = radiometer net infrared responsivity ($\mu\text{V}/\text{W}/\text{m}^2$), see Table 4,
- W_{net} = effective net infrared measured by pyrgeometer (W/m^2),
- = $W_{in} - W_{out} = W_{in} - \sigma * T_c^4$
- where, W_{in} = incoming infrared (W/m^2), $\sigma = 5.6704\text{e-}8 \text{ W}\cdot\text{m}^{-2}\cdot\text{K}^{-4}$,
- T_c = case temperature of pyrgeometer (K).
- I = reference irradiance (W/m^2), beam (B) or global (G)
- where, $G = B * \text{COS}(Z) + D$,
- Z = zenith angle (degrees),
- D = reference diffuse irradiance (W/m^2).

Figure 1. Responsivity vs Zenith Angle

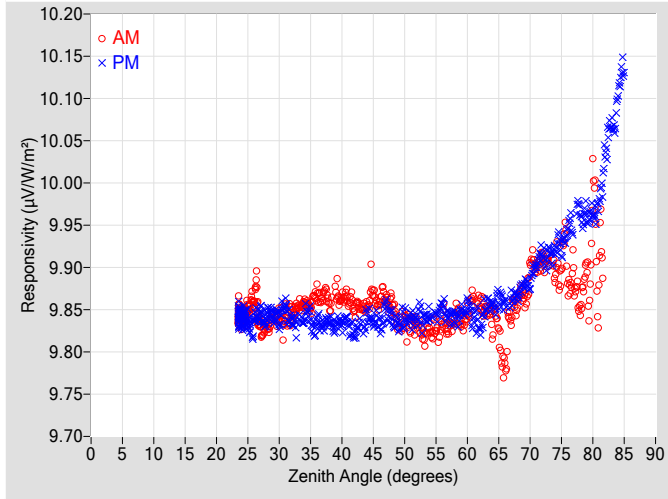


Figure 2. Responsivity vs Local Standard Time

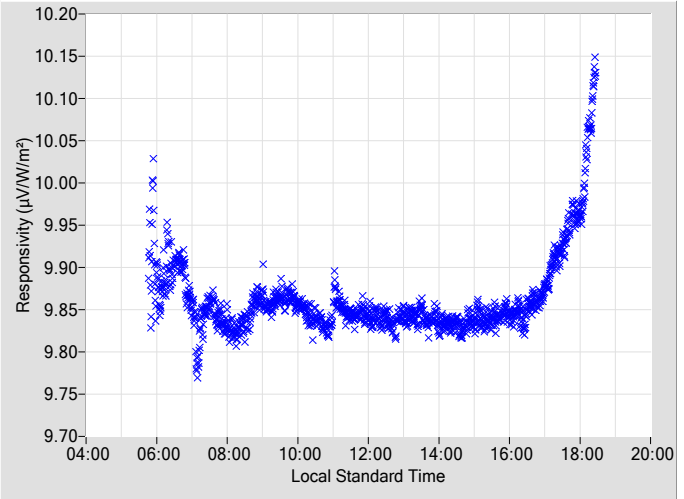


Table 2. Instrument Responsivity (R) and Calibration Type-B Standard Uncertainty, u(B)

| Zenith Angle (deg.) | R ($\mu\text{V}/\text{W}/\text{m}^2$) | u(B) \pm (%) | Azimuth Angle | R ($\mu\text{V}/\text{W}/\text{m}^2$) | u(B) \pm (%) | Azimuth Angle | Zenith Angle (deg.) | R ($\mu\text{V}/\text{W}/\text{m}^2$) | u(B) \pm (%) | Azimuth Angle | R ($\mu\text{V}/\text{W}/\text{m}^2$) | u(B) \pm (%) | Azimuth Angle |
|---------------------|---|----------------|---------------|---|----------------|---------------|---------------------|---|----------------|---------------|---|----------------|---------------|
| 0 | N/A | N/A | N/A | N/A | N/A | N/A | 46 | 9.8572 | 0.32 | 106.77 | 9.8314 | 0.31 | 252.83 |
| 2 | N/A | N/A | N/A | N/A | N/A | N/A | 48 | 9.8592 | 0.33 | 104.56 | 9.8398 | 0.31 | 255.08 |
| 4 | N/A | N/A | N/A | N/A | N/A | N/A | 50 | 9.8364 | 0.36 | 102.42 | 9.8368 | 0.32 | 257.24 |
| 6 | N/A | N/A | N/A | N/A | N/A | N/A | 52 | 9.8328 | 0.34 | 100.41 | 9.8399 | 0.32 | 259.30 |
| 8 | N/A | N/A | N/A | N/A | N/A | N/A | 54 | 9.8256 | 0.36 | 98.46 | 9.8429 | 0.36 | 261.23 |
| 10 | N/A | N/A | N/A | N/A | N/A | N/A | 56 | 9.8413 | 0.37 | 96.59 | 9.8566 | 0.35 | 263.11 |
| 12 | N/A | N/A | N/A | N/A | N/A | N/A | 58 | 9.8417 | 0.34 | 94.80 | 9.8415 | 0.34 | 264.92 |
| 14 | N/A | N/A | N/A | N/A | N/A | N/A | 60 | 9.8437 | 0.34 | 93.06 | 9.8556 | 0.35 | 266.68 |
| 16 | N/A | N/A | N/A | N/A | N/A | N/A | 62 | 9.8575 | 0.35 | 91.36 | 9.8273 | 0.36 | 268.40 |
| 18 | N/A | N/A | N/A | N/A | N/A | N/A | 64 | 9.8338 | 0.39 | 89.68 | 9.8565 | 0.37 | 270.10 |
| 20 | N/A | N/A | N/A | N/A | N/A | N/A | 66 | 9.7813 | 0.41 | 88.04 | 9.8563 | 0.38 | 271.68 |
| 22 | N/A | N/A | N/A | N/A | N/A | N/A | 68 | 9.8542 | 0.40 | 86.43 | 9.8661 | 0.40 | 273.37 |
| 24 | 9.8435 | 0.30 | 166.91 | 9.8403 | 0.32 | 193.10 | 70 | 9.8965 | 0.42 | 84.78 | 9.8801 | 0.43 | 274.99 |
| 26 | 9.8626 | 0.30 | 150.93 | 9.8339 | 0.32 | 209.14 | 72 | 9.9094 | 0.45 | 83.19 | 9.9157 | 0.46 | 276.60 |
| 28 | 9.8310 | 0.35 | 140.83 | 9.8430 | 0.32 | 218.09 | 74 | 9.8939 | 0.54 | 81.61 | 9.9210 | 0.50 | 278.21 |
| 30 | 9.8425 | 0.32 | 134.32 | 9.8385 | 0.31 | 224.63 | 76 | 9.8930 | 0.55 | 80.00 | 9.9456 | 0.56 | 279.80 |
| 32 | 9.8429 | 0.31 | 129.23 | 9.8361 | 0.33 | 230.08 | 78 | 9.8506 | 0.62 | 78.39 | 9.9643 | N/A | 281.41 |
| 34 | 9.8570 | 0.30 | 124.85 | 9.8404 | 0.32 | 234.51 | 80 | 9.9707 | N/A | 76.79 | 9.9644 | N/A | 283.05 |
| 36 | 9.8673 | 0.31 | 121.02 | 9.8353 | 0.33 | 238.42 | 82 | N/A | N/A | N/A | 10.033 | N/A | 284.70 |
| 38 | 9.8558 | 0.32 | 117.58 | 9.8371 | 0.34 | 241.91 | 84 | N/A | N/A | N/A | 10.103 | N/A | 286.35 |
| 40 | 9.8640 | 0.31 | 114.59 | 9.8317 | 0.33 | 244.94 | 86 | N/A | N/A | N/A | N/A | N/A | N/A |
| 42 | 9.8492 | 0.32 | 111.76 | 9.8192 | 0.32 | 247.75 | 88 | N/A | N/A | N/A | N/A | N/A | N/A |
| 44 | 9.8539 | 0.31 | 109.22 | 9.8395 | 0.32 | 250.35 | 90 | N/A | N/A | N/A | N/A | N/A | N/A |

N/A - Not Available

Figure 3. Type-B Standard Uncertainty vs Zenith Angle

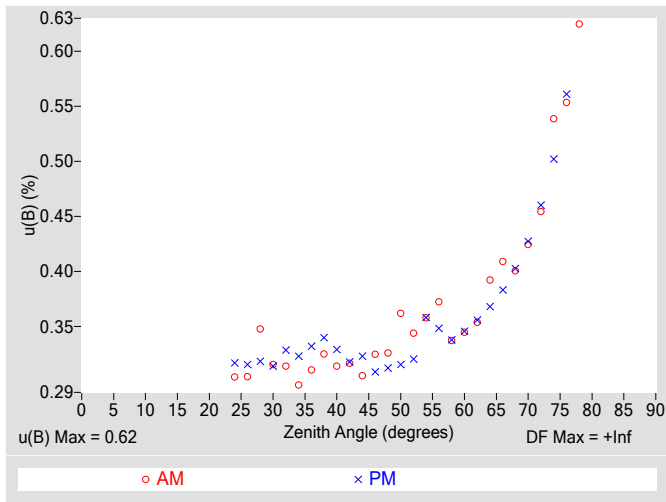


Figure 4. Residuals from Spline Interpolation

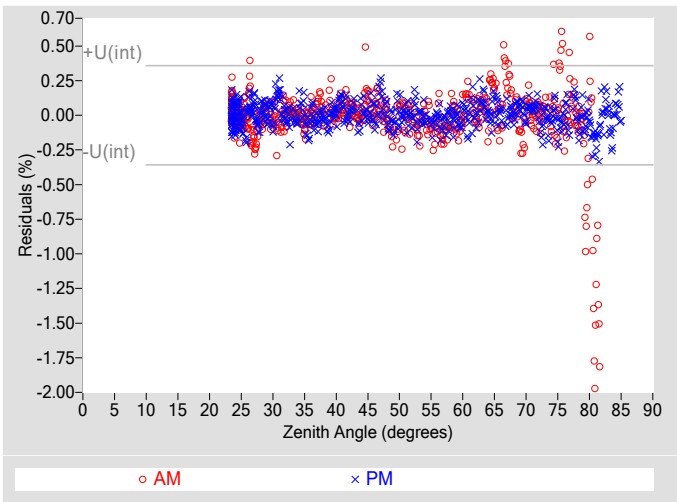


Table 3. Uncertainty using Spline Interpolation ‡

| | |
|---|------------|
| Type-B Standard Uncertainty, $u(B)$ (%) | ± 0.62 |
| Type-A Interpolating Function, $u(int)$ (%) | ± 0.18 |
| Combined Standard Uncertainty, $u(c)$ (%) | ± 0.65 |
| Effective degrees of freedom, $DF(c)$ | 197300 |
| Coverage factor, k | 1.96 |
| Expanded Uncertainty, $U95$ (%) | ± 1.3 |
| AM Valid zenith angle range | 24° to 78° |
| PM Valid zenith angle range | 24° to 76° |

‡ An illustration for how to reduce the uncertainty in calculating the irradiance using a function rather than $R@45^\circ$. Not accredited.

Table 4. Calibration Label Values

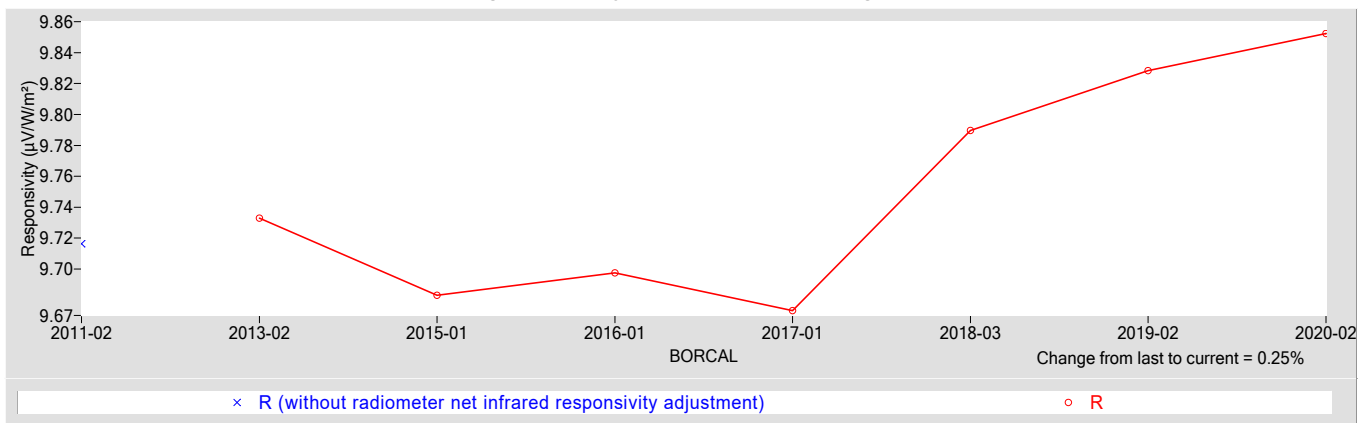
| | |
|----------------------------------|-------------------------------|
| $R @ 45^\circ$ ($\mu V/W/m^2$) | R_{net} ($\mu V/W/m^2$) † |
| 9.8524 | 0.087000 |

† R_{net} determination date: Estimated

Table 5. Uncertainty using $R @ 45^\circ$

| | |
|---|----------------|
| Type-B Expanded Uncertainty, $U(B)$ (%) | ± 0.73 |
| Offset Uncertainty, $U(off)$ (%) | +0.15 / -0.34 |
| Expanded Uncertainty, U (%) | +0.88 / -1.1 |
| Effective degrees of freedom, DF | +Inf |
| Coverage factor, k | 1.96 |
| Valid zenith angle range | 30.0° to 60.0° |

Figure 5. History of instrument at Zenith Angle = 45°



References:

- [1] Reda, I.; Hickey, J.; Long, C.; Myers, D.; Stoffel, T.; Wilcox, S.; Michalsky, J. J.; Dutton, E. G.; Nelson, D. (2005). "Using a Blackbody to Calculate Net Longwave Responsivity of Shortwave Solar Pyranometers to Correct for Their Thermal Offset Error During Outdoor Calibration Using the Component Sum Method." *Journal of Atmospheric and Oceanic Technology*, 2005; pp. 1531-1540; NREL Report No. JA-560-36646. doi:10.1175/JTECH1782.1
- [2] Reda, I.; Myers, D.; Stoffel, T. (2008). "Uncertainty Estimate for the Outdoor Calibration of Solar Pyranometers: A Metrologist Perspective." *Measure*. (NCSLI *Journal of Measurement Science*). Vol. 3(4), December 2008; pp. 58-66; NREL Report No. JA-581-4137
- [3] Reda, I.; Andreas, A. (2004). "Solar Position Algorithm for Solar Radiation Applications." *Solar Energy*. Vol. 76(5), 2004; pp. 577-589; NREL Report No. JA-560-35518. doi:10.1016/j.solener.2003.12.003
- [4] Stoffel, T.; Reda, I. (2009). "NREL Pyrheliometer Comparisons: 22 September - 3 October 2008 (NPC-2008)." 54 pp.; NREL Report No. TP-550-45016.
- [5] Reda, I.; Stoffel, T.; Myers, D. (2003). "Method to Calibrate a Solar Pyranometer for Measuring Reference Diffuse Irradiance." *Solar Energy*. Vol. 74, 2003; pp. 103-112; NREL Report No. JA-560-35025. doi:10.1016/S0038-092X(03)00124-5
- [6] Reda, I. (1996). *Calibration of a Solar Absolute Cavity Radiometer with Traceability to the World Radiometric Reference*. 79 pp.; NREL Report No. TP-463-20619.
- [7] Reda, I.; Gröbner, J.; Stoffel, T.; Myers, D.; Forgan, B. (2008). *Improvements in the Blackbody Calibration of Pyrgometers*. ARM 2008 Science Team Meeting (Poster).



National Renewable Energy Laboratory

Solar Radiation Research Laboratory

Metrology Laboratory

Calibration Certificate



| | | | |
|--------------------------|------------------------|----------------------------------|------------|
| Test Instrument: | Thermopile Pyranometer | Manufacturer: | Apogee |
| Model: | SP-510 | Serial Number: | 1171 |
| Calibration Date: | 5/5/2020 | Due Date: | 5/5/2021 |
| Customer: | NREL-SRRL-BMS | Environmental Conditions: | see page 4 |
| Test Dates: | 5/4-5 | | |

This certifies that the above product was calibrated in compliance with ISO/IEC 17025:2017. Measurement uncertainties at the time of calibration are consistent with the Guide to the Expression of Uncertainty in Measurement (GUM) using Reda et al., 2008. All nominal values are traceable to the International System (SI) Units of Measurement.

No statement of compliance with specifications is made or implied on this certificate. However, the estimated uncertainties are the uncertainties of the calibration process; users must add other uncertainties that are relevant to their measuring system, environmental and sky conditions, outdoor set-up, and site location.

The Type-B Standard Uncertainty of using the responsivity at each even zenith angle is reported, and the Expanded Uncertainty of the calibration is reported using two methods:

1. The Expanded Uncertainty of using the responsivity at zenith angle = 45°, within the zenith angle range from 30.0° to 60.0°
2. The Expanded Uncertainty of using Spline Interpolating Functions for the responsivity versus zenith angle.

This certificate applies only to the item identified above and shall not be reproduced other than in full, without specific written approval from the calibration facility. Certificate without signature is not valid.

Table 1. Traceability

| Measurement Type | Instrument | Calibration Date | Calibration Due Date |
|-----------------------|--|------------------|----------------------|
| Beam Irradiance † | Eppley Absolute Cavity Radiometer Model HF, S/N 29219 | 09/27/2019 | 09/27/2020 |
| Diffuse Irradiance † | Hukseflux Pyranometer Model SR25, S/N 2541 | 04/17/2020 | 04/17/2021 |
| Diffuse Irradiance † | Hukseflux Pyranometer Model SR25, S/N 2542 | 04/17/2020 | 04/17/2021 |
| Data Acquisition | NREL Data Acquisition System Model RAP-DAQ, S/N 2005-998 | 02/14/2019 | 02/14/2021 |
| Data Acquisition | NREL Data Acquisition System Model RAP-DAQ, S/N 2005-999 | 02/14/2019 | 02/14/2021 |
| Infrared Irradiance ‡ | Kipp & Zonen Pyrgeometer Model CG4, S/N FT002 | 04/16/2018 | 04/16/2022 |

† Through the World Radiometric Reference (WRR)

‡ Through the World Infrared Standard Group (WISG)

Number of pages of certificate: 4

Calibration Procedure: BORCAL-P00-Calibration and QA Procedure; available upon request.

Setup: Radiometers are calibrated outdoors, using the sun as the source. Pyranometers and pyrgeometers are installed for horizontal measurements, with their signal connectors oriented north, if their design permits.

The shading disk for the reference diffuse subtends a solid angle of 5°. Pyrheliometers are installed on solar trackers.

Calibrated by: Afshin Andreas, Ibrahim Reda, Peter Gotseff, and RCC

Ibrahim Reda, Technical Manager

Date

For questions or comments, please contact the technical manager at:

ibrahim.reda@nrel.gov; 303-384-6385; 15013 Denver West Parkway, Golden, CO 80401, USA

Calibration Results

1171 Apogee SP-510

The responsivity (R , $\mu\text{V}/\text{W}/\text{m}^2$) of the test instrument during calibration is calculated using this Measurement Equation:

$$R = (V - R_{net} * W_{net}) / I \tag{1}$$

where,

- V = radiometer output voltage (microvolts),
 - R_{net} = radiometer net infrared responsivity ($\mu\text{V}/\text{W}/\text{m}^2$), see Table 4,
 - W_{net} = effective net infrared measured by pyrgeometer (W/m^2),
 - = $W_{in} - W_{out} = W_{in} - \sigma * T_c^4$
 - where, W_{in} = incoming infrared (W/m^2), $\sigma = 5.6704\text{e-}8 \text{ W}\cdot\text{m}^{-2}\cdot\text{K}^{-4}$,
 - T_c = case temperature of radiometer (K).
- I = reference irradiance (W/m^2), beam (B) or global (G)
 - where, $G = B * \text{COS}(Z) + D$,
 - Z = zenith angle (degrees),
 - D = reference diffuse irradiance (W/m^2).

Figure 1. Responsivity vs Zenith Angle

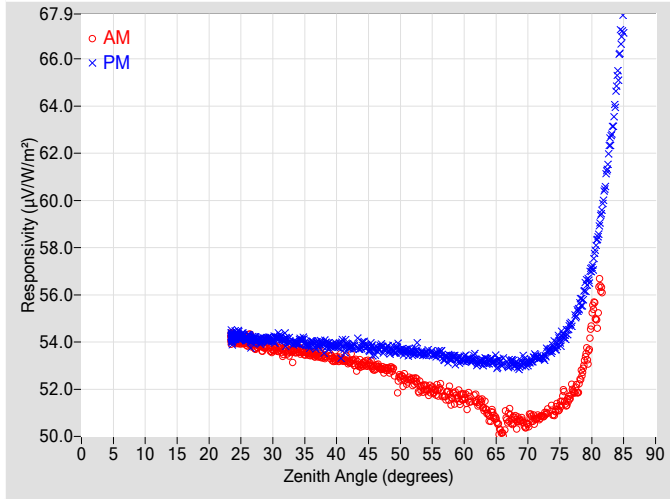


Figure 2. Responsivity vs Local Standard Time

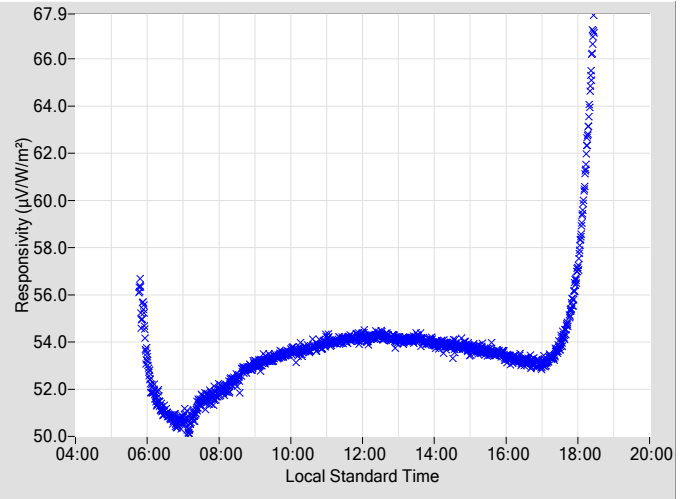


Table 2. Instrument Responsivity (R) and Calibration Type-B Standard Uncertainty, $u(B)$

| Zenith Angle (deg.) | R ($\mu\text{V}/\text{W}/\text{m}^2$) | AM $u(B)$ \pm (%) | Azimuth Angle | R ($\mu\text{V}/\text{W}/\text{m}^2$) | PM $u(B)$ \pm (%) | Azimuth Angle | Zenith Angle (deg.) | R ($\mu\text{V}/\text{W}/\text{m}^2$) | AM $u(B)$ \pm (%) | Azimuth Angle | R ($\mu\text{V}/\text{W}/\text{m}^2$) | PM $u(B)$ \pm (%) | Azimuth Angle |
|---------------------|---|---------------------|---------------|---|---------------------|---------------|---------------------|---|---------------------|---------------|---|---------------------|---------------|
| 0 | N/A | N/A | N/A | N/A | N/A | N/A | 46 | 52.913 | 0.32 | 106.80 | 53.670 | 0.34 | 252.85 |
| 2 | N/A | N/A | N/A | N/A | N/A | N/A | 48 | 52.811 | 0.36 | 104.52 | 53.724 | 0.36 | 255.11 |
| 4 | N/A | N/A | N/A | N/A | N/A | N/A | 50 | 52.536 | 0.34 | 102.44 | 53.646 | 0.33 | 257.26 |
| 6 | N/A | N/A | N/A | N/A | N/A | N/A | 52 | 52.339 | 0.37 | 100.40 | 53.572 | 0.35 | 259.32 |
| 8 | N/A | N/A | N/A | N/A | N/A | N/A | 54 | 52.019 | 0.40 | 98.43 | 53.501 | 0.36 | 261.20 |
| 10 | N/A | N/A | N/A | N/A | N/A | N/A | 56 | 52.024 | 0.38 | 96.61 | 53.516 | 0.35 | 263.13 |
| 12 | N/A | N/A | N/A | N/A | N/A | N/A | 58 | 51.727 | 0.39 | 94.82 | 53.371 | 0.36 | 264.94 |
| 14 | N/A | N/A | N/A | N/A | N/A | N/A | 60 | 51.654 | 0.42 | 93.07 | 53.295 | 0.37 | 266.70 |
| 16 | N/A | N/A | N/A | N/A | N/A | N/A | 62 | 51.520 | 0.41 | 91.33 | 53.141 | 0.39 | 268.42 |
| 18 | N/A | N/A | N/A | N/A | N/A | N/A | 64 | 50.821 | 0.43 | 89.65 | 53.204 | 0.40 | 270.07 |
| 20 | N/A | N/A | N/A | N/A | N/A | N/A | 66 | 50.116 | 0.43 | 88.06 | 53.104 | 0.42 | 271.69 |
| 22 | N/A | N/A | N/A | N/A | N/A | N/A | 68 | 50.654 | 0.46 | 86.40 | 53.053 | 0.45 | 273.38 |
| 24 | 54.129 | 0.32 | 166.82 | 54.240 | 0.33 | 192.94 | 70 | 50.594 | 0.48 | 84.80 | 53.112 | 0.48 | 275.01 |
| 26 | 53.986 | 0.33 | 150.84 | 54.179 | 0.32 | 209.17 | 72 | 50.810 | 0.52 | 83.21 | 53.332 | 0.52 | 276.58 |
| 28 | 53.860 | 0.34 | 140.76 | 54.040 | 0.31 | 218.11 | 74 | 50.975 | 0.57 | 81.59 | 53.798 | 0.61 | 278.22 |
| 30 | 53.667 | 0.33 | 134.45 | 54.072 | 0.33 | 224.79 | 76 | 51.406 | 0.63 | 80.01 | 54.348 | 0.65 | 279.81 |
| 32 | 53.703 | 0.32 | 129.26 | 54.098 | 0.32 | 230.01 | 78 | 52.100 | 0.72 | 78.41 | 55.524 | N/A | 281.43 |
| 34 | 53.668 | 0.33 | 124.79 | 53.994 | 0.33 | 234.48 | 80 | 54.926 | N/A | 76.77 | 57.096 | N/A | 283.02 |
| 36 | 53.513 | 0.32 | 120.97 | 53.939 | 0.31 | 238.45 | 82 | N/A | N/A | N/A | 60.417 | N/A | 284.67 |
| 38 | 53.370 | 0.32 | 117.61 | 53.946 | 0.31 | 241.85 | 84 | N/A | N/A | N/A | 65.262 | N/A | 286.41 |
| 40 | 53.270 | 0.33 | 114.54 | 53.834 | 0.33 | 244.96 | 86 | N/A | N/A | N/A | N/A | N/A | N/A |
| 42 | 53.194 | 0.33 | 111.71 | 53.780 | 0.32 | 247.84 | 88 | N/A | N/A | N/A | N/A | N/A | N/A |
| 44 | 53.020 | 0.32 | 109.19 | 53.873 | 0.34 | 250.39 | 90 | N/A | N/A | N/A | N/A | N/A | N/A |

N/A - Not Available

Figure 3. Type-B Standard Uncertainty vs Zenith Angle

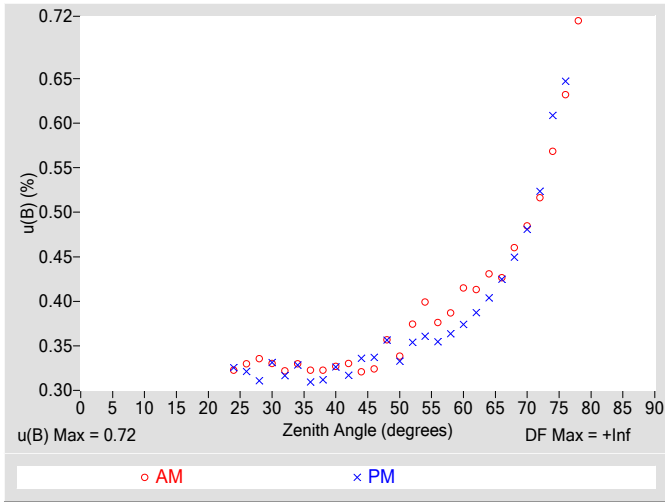


Figure 4. Residuals from Spline Interpolation

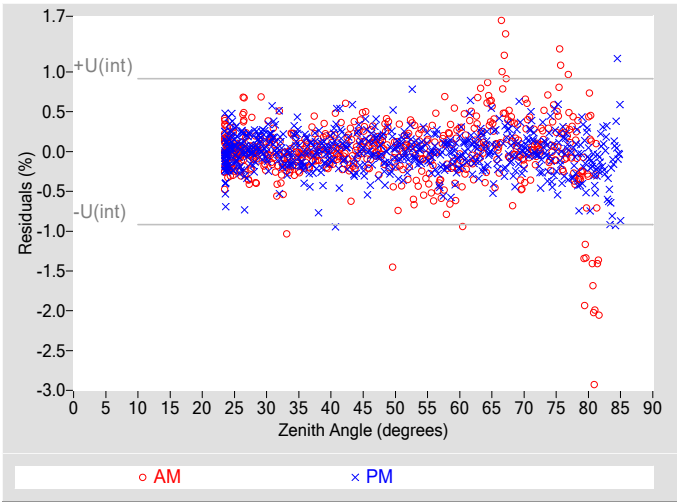


Table 3. Uncertainty using Spline Interpolation ‡

| | |
|---|------------|
| Type-B Standard Uncertainty, $u(B)$ (%) | ± 0.72 |
| Type-A Interpolating Function, $u(int)$ (%) | ± 0.46 |
| Combined Standard Uncertainty, $u(c)$ (%) | ± 0.85 |
| Effective degrees of freedom, $DF(c)$ | 13593 |
| Coverage factor, k | 1.96 |
| Expanded Uncertainty, U_{95} (%) | ± 1.7 |
| AM Valid zenith angle range | 24° to 78° |
| PM Valid zenith angle range | 24° to 76° |

‡ An illustration for how to reduce the uncertainty in calculating the irradiance using a function rather than $R@45^\circ$. Not accredited.

Table 4. Calibration Label Values

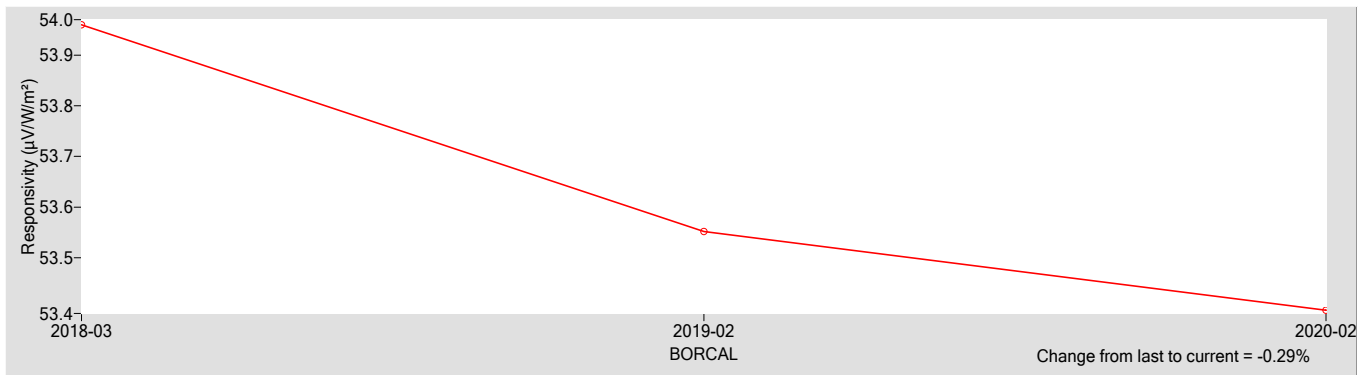
| | |
|----------------------------------|-------------------------------|
| $R @ 45^\circ$ ($\mu V/W/m^2$) | R_{net} ($\mu V/W/m^2$) † |
| 53.397 | 2.5000 |

† R_{net} determination date: Estimated

Table 5. Uncertainty using $R @ 45^\circ$

| | |
|---|----------------|
| Type-B Expanded Uncertainty, $U(B)$ (%) | ± 0.81 |
| Offset Uncertainty, $U(off)$ (%) | +1.3 / -3.3 |
| Expanded Uncertainty, U (%) | +2.1 / -4.1 |
| Effective degrees of freedom, DF | +Inf |
| Coverage factor, k | 1.96 |
| Valid zenith angle range | 30.0° to 60.0° |

Figure 5. History of instrument at Zenith Angle = 45°



References:

[1] Reda, I.; Hickey, J.; Long, C.; Myers, D.; Stoffel, T.; Wilcox, S.; Michalsky, J. J.; Dutton, E. G.; Nelson, D. (2005). "Using a Blackbody to Calculate Net Longwave Responsivity of Shortwave Solar Pyranometers to Correct for Their Thermal Offset Error During Outdoor Calibration Using the Component Sum Method." *Journal of Atmospheric and Oceanic Technology*, 2005; pp. 1531-1540; NREL Report No. JA-560-36646. doi:10.1175/JTECH1782.1

[2] Reda, I.; Myers, D.; Stoffel, T. (2008). "Uncertainty Estimate for the Outdoor Calibration of Solar Pyranometers: A Metrologist Perspective." *Measure*. (NCSLI Journal of Measurement Science). Vol. 3(4), December 2008; pp. 58-66; NREL Report No. JA-581-4137

[3] Reda, I.; Andreas, A. (2004). "Solar Position Algorithm for Solar Radiation Applications." *Solar Energy*. Vol. 76(5), 2004; pp. 577-589; NREL Report No. JA-560-35518. doi:10.1016/j.solener.2003.12.003

[4] Stoffel, T.; Reda, I. (2009). "NREL Pyrheliometer Comparisons: 22 September - 3 October 2008 (NPC-2008)." 54 pp.; NREL Report No. TP-550-45016.

[5] Reda, I.; Stoffel, T.; Myers, D. (2003). "Method to Calibrate a Solar Pyranometer for Measuring Reference Diffuse Irradiance." *Solar Energy*. Vol. 74, 2003; pp. 103-112; NREL Report No. JA-560-35025. doi:10.1016/S0038-092X(03)00124-5

[6] Reda, I. (1996). Calibration of a Solar Absolute Cavity Radiometer with Traceability to the World Radiometric Reference. 79 pp.; NREL Report No. TP-463-20619.

[7] Reda, I.; Gröbner, J.; Stoffel, T.; Myers, D.; Forgan, B. (2008). Improvements in the Blackbody Calibration of Pyrgometers. ARM 2008 Science Team Meeting (Poster).



National Renewable Energy Laboratory

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Metrology Laboratory

Calibration Certificate



| | | | |
|--------------------------|---------------|----------------------------------|--------------|
| Test Instrument: | Pyranometer | Manufacturer: | Kipp & Zonen |
| Model: | CMP22 | Serial Number: | 140043 |
| Calibration Date: | 5/5/2020 | Due Date: | 5/5/2021 |
| Customer: | NREL-SRRL-BMS | Environmental Conditions: | see page 4 |
| Test Dates: | 5/4-5 | | |

This certifies that the above product was calibrated in compliance with ISO/IEC 17025:2017. Measurement uncertainties at the time of calibration are consistent with the Guide to the Expression of Uncertainty in Measurement (GUM) using Reda et al., 2008. All nominal values are traceable to the International System (SI) Units of Measurement.

No statement of compliance with specifications is made or implied on this certificate. However, the estimated uncertainties are the uncertainties of the calibration process; users must add other uncertainties that are relevant to their measuring system, environmental and sky conditions, outdoor set-up, and site location.

The Type-B Standard Uncertainty of using the responsivity at each even zenith angle is reported, and the Expanded Uncertainty of the calibration is reported using two methods:

1. The Expanded Uncertainty of using the responsivity at zenith angle = 45°, within the zenith angle range from 30.0° to 60.0°
2. The Expanded Uncertainty of using Spline Interpolating Functions for the responsivity versus zenith angle.

This certificate applies only to the item identified above and shall not be reproduced other than in full, without specific written approval from the calibration facility. Certificate without signature is not valid.

Table 1. Traceability

| Measurement Type | Instrument | Calibration Date | Calibration Due Date |
|-----------------------|--|------------------|----------------------|
| Beam Irradiance † | Eppley Absolute Cavity Radiometer Model HF, S/N 29219 | 09/27/2019 | 09/27/2020 |
| Diffuse Irradiance † | Hukseflux Pyranometer Model SR25, S/N 2541 | 04/17/2020 | 04/17/2021 |
| Diffuse Irradiance † | Hukseflux Pyranometer Model SR25, S/N 2542 | 04/17/2020 | 04/17/2021 |
| Data Acquisition | NREL Data Acquisition System Model RAP-DAQ, S/N 2005-998 | 02/14/2019 | 02/14/2021 |
| Data Acquisition | NREL Data Acquisition System Model RAP-DAQ, S/N 2005-999 | 02/14/2019 | 02/14/2021 |
| Infrared Irradiance ‡ | Kipp & Zonen Pyrgeometer Model CG4, S/N FT002 | 04/16/2018 | 04/16/2022 |

† Through the World Radiometric Reference (WRR)

‡ Through the World Infrared Standard Group (WISG)

Number of pages of certificate: 4

Calibration Procedure: BORCAL-P00-Calibration and QA Procedure; available upon request.

Setup: Radiometers are calibrated outdoors, using the sun as the source. Pyranometers and pyrgeometers are installed for horizontal measurements, with their signal connectors oriented north, if their design permits.

The shading disk for the reference diffuse subtends a solid angle of 5°. Pyrheliometers are installed on solar trackers.

Calibrated by: Afshin Andreas, Ibrahim Reda, Peter Gotseff, and RCC

Ibrahim Reda, Technical Manager

Date

For questions or comments, please contact the technical manager at:

ibrahim.reda@nrel.gov; 303-384-6385; 15013 Denver West Parkway, Golden, CO 80401, USA

Calibration Results

140043 Kipp & Zonen CMP22

The responsivity (R , $\mu\text{V}/\text{W}/\text{m}^2$) of the test instrument during calibration is calculated using this Measurement Equation:

$$R = (V - R_{net} * W_{net}) / I \tag{1}$$

where,

- V = radiometer output voltage (microvolts),
 - R_{net} = radiometer net infrared responsivity ($\mu\text{V}/\text{W}/\text{m}^2$), see Table 4,
 - W_{net} = effective net infrared measured by pyrgeometer (W/m^2),
 - = $W_{in} - W_{out} = W_{in} - \sigma * T_c^4$
 - where, W_{in} = incoming infrared (W/m^2), $\sigma = 5.6704\text{e-}8 \text{ W}\cdot\text{m}^{-2}\cdot\text{K}^{-4}$,
 - T_c = case temperature of pyrgeometer (K).
- I = reference irradiance (W/m^2), beam (B) or global (G)
 - where, $G = B * \text{COS}(Z) + D$,
 - Z = zenith angle (degrees),
 - D = reference diffuse irradiance (W/m^2).

Figure 1. Responsivity vs Zenith Angle

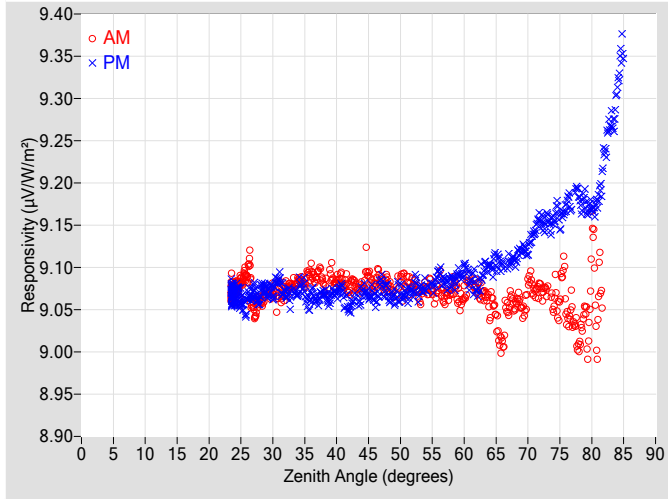


Figure 2. Responsivity vs Local Standard Time

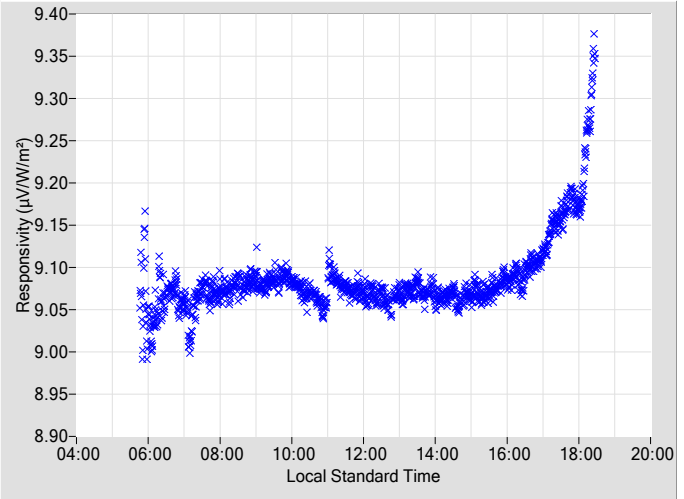


Table 2. Instrument Responsivity (R) and Calibration Type-B Standard Uncertainty, u(B)

| Zenith Angle (deg.) | R ($\mu\text{V}/\text{W}/\text{m}^2$) | u(B) \pm (%) | Azimuth Angle | R ($\mu\text{V}/\text{W}/\text{m}^2$) | u(B) \pm (%) | Azimuth Angle | Zenith Angle (deg.) | R ($\mu\text{V}/\text{W}/\text{m}^2$) | u(B) \pm (%) | Azimuth Angle | R ($\mu\text{V}/\text{W}/\text{m}^2$) | u(B) \pm (%) | Azimuth Angle |
|---------------------|---|----------------|---------------|---|----------------|---------------|---------------------|---|----------------|---------------|---|----------------|---------------|
| 0 | N/A | N/A | N/A | N/A | N/A | N/A | 46 | 9.0791 | 0.32 | 106.77 | 9.0621 | 0.31 | 252.83 |
| 2 | N/A | N/A | N/A | N/A | N/A | N/A | 48 | 9.0827 | 0.33 | 104.56 | 9.0711 | 0.31 | 255.08 |
| 4 | N/A | N/A | N/A | N/A | N/A | N/A | 50 | 9.0842 | 0.36 | 102.42 | 9.0665 | 0.32 | 257.24 |
| 6 | N/A | N/A | N/A | N/A | N/A | N/A | 52 | 9.0804 | 0.34 | 100.41 | 9.0724 | 0.32 | 259.30 |
| 8 | N/A | N/A | N/A | N/A | N/A | N/A | 54 | 9.0756 | 0.36 | 98.46 | 9.0771 | 0.36 | 261.23 |
| 10 | N/A | N/A | N/A | N/A | N/A | N/A | 56 | 9.0805 | 0.37 | 96.59 | 9.0949 | 0.35 | 263.11 |
| 12 | N/A | N/A | N/A | N/A | N/A | N/A | 58 | 9.0737 | 0.34 | 94.80 | 9.0839 | 0.34 | 264.92 |
| 14 | N/A | N/A | N/A | N/A | N/A | N/A | 60 | 9.0659 | 0.35 | 93.06 | 9.0984 | 0.35 | 266.68 |
| 16 | N/A | N/A | N/A | N/A | N/A | N/A | 62 | 9.0763 | 0.35 | 91.36 | 9.0720 | 0.36 | 268.40 |
| 18 | N/A | N/A | N/A | N/A | N/A | N/A | 64 | 9.0541 | 0.39 | 89.68 | 9.1020 | 0.37 | 270.10 |
| 20 | N/A | N/A | N/A | N/A | N/A | N/A | 66 | 9.0080 | 0.41 | 88.04 | 9.1017 | 0.38 | 271.68 |
| 22 | N/A | N/A | N/A | N/A | N/A | N/A | 68 | 9.0533 | 0.40 | 86.43 | 9.1080 | 0.40 | 273.37 |
| 24 | 9.0738 | 0.30 | 166.91 | 9.0677 | 0.32 | 193.10 | 70 | 9.0760 | 0.43 | 84.78 | 9.1201 | 0.43 | 274.99 |
| 26 | 9.0922 | 0.30 | 150.93 | 9.0589 | 0.32 | 209.14 | 72 | 9.0748 | 0.46 | 83.19 | 9.1565 | 0.46 | 276.60 |
| 28 | 9.0617 | 0.35 | 140.83 | 9.0692 | 0.32 | 218.09 | 74 | 9.0570 | 0.54 | 81.61 | 9.1562 | 0.50 | 278.21 |
| 30 | 9.0727 | 0.32 | 134.32 | 9.0711 | 0.31 | 224.63 | 76 | 9.0547 | 0.56 | 80.00 | 9.1742 | 0.56 | 279.80 |
| 32 | 9.0721 | 0.31 | 129.23 | 9.0684 | 0.33 | 230.08 | 78 | 9.0066 | 0.63 | 78.39 | 9.1843 | N/A | 281.41 |
| 34 | 9.0839 | 0.30 | 124.85 | 9.0725 | 0.32 | 234.51 | 80 | 9.1134 | N/A | 76.79 | 9.1717 | N/A | 283.05 |
| 36 | 9.0930 | 0.31 | 121.02 | 9.0662 | 0.33 | 238.42 | 82 | N/A | N/A | N/A | 9.2334 | N/A | 284.70 |
| 38 | 9.0778 | 0.33 | 117.58 | 9.0697 | 0.34 | 241.91 | 84 | N/A | N/A | N/A | 9.3090 | N/A | 286.35 |
| 40 | 9.0848 | 0.31 | 114.59 | 9.0693 | 0.33 | 244.94 | 86 | N/A | N/A | N/A | N/A | N/A | N/A |
| 42 | 9.0728 | 0.32 | 111.76 | 9.0501 | 0.32 | 247.75 | 88 | N/A | N/A | N/A | N/A | N/A | N/A |
| 44 | 9.0770 | 0.31 | 109.22 | 9.0686 | 0.32 | 250.35 | 90 | N/A | N/A | N/A | N/A | N/A | N/A |

N/A - Not Available

Figure 3. Type-B Standard Uncertainty vs Zenith Angle

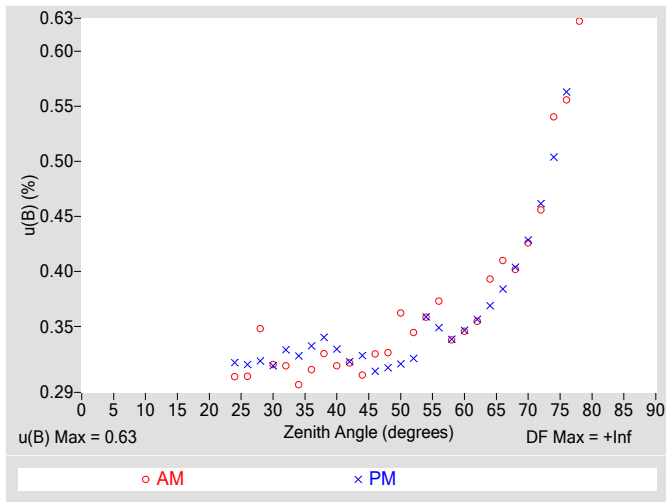


Figure 4. Residuals from Spline Interpolation

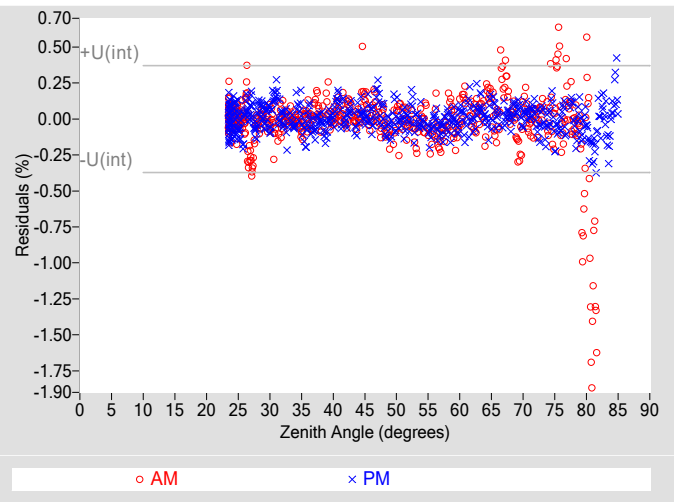


Table 3. Uncertainty using Spline Interpolation ‡

| | |
|---|------------|
| Type-B Standard Uncertainty, $u(B)$ (%) | ± 0.63 |
| Type-A Interpolating Function, $u(int)$ (%) | ± 0.19 |
| Combined Standard Uncertainty, $u(c)$ (%) | ± 0.65 |
| Effective degrees of freedom, $DF(c)$ | 173358 |
| Coverage factor, k | 1.96 |
| Expanded Uncertainty, $U95$ (%) | ± 1.3 |
| AM Valid zenith angle range | 24° to 78° |
| PM Valid zenith angle range | 24° to 76° |

‡ An illustration for how to reduce the uncertainty in calculating the irradiance using a function rather than $R@45^\circ$. Not accredited.

Table 4. Calibration Label Values

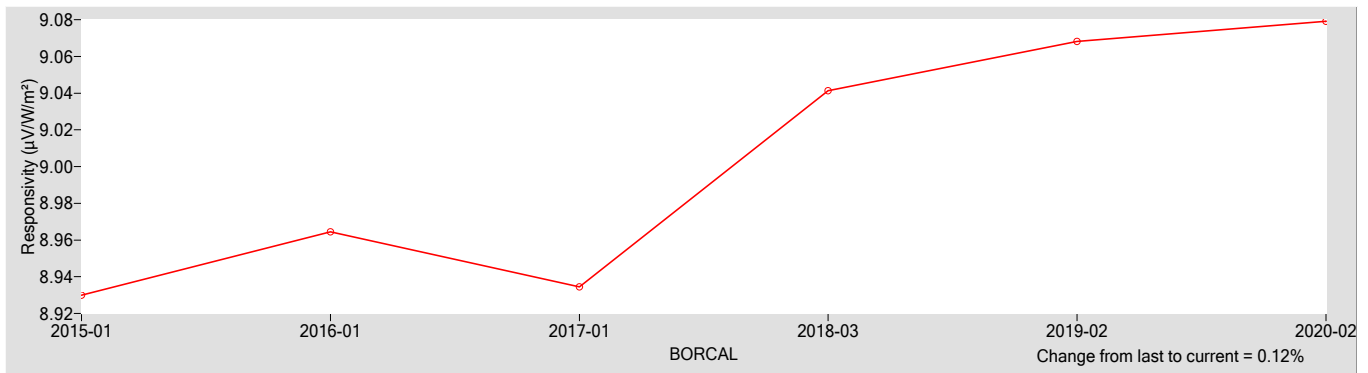
| | |
|----------------------------------|-------------------------------|
| $R @ 45^\circ$ ($\mu V/W/m^2$) | R_{net} ($\mu V/W/m^2$) † |
| 9.0791 | 0.087000 |

† R_{net} determination date: Estimated

Table 5. Uncertainty using $R @ 45^\circ$

| | |
|---|----------------|
| Type-B Expanded Uncertainty, $U(B)$ (%) | ± 0.73 |
| Offset Uncertainty, $U(off)$ (%) | +0.21 / -0.32 |
| Expanded Uncertainty, U (%) | +0.94 / -1.1 |
| Effective degrees of freedom, DF | +Inf |
| Coverage factor, k | 1.96 |
| Valid zenith angle range | 30.0° to 60.0° |

Figure 5. History of instrument at Zenith Angle = 45°



References:

[1] Reda, I.; Hickey, J.; Long, C.; Myers, D.; Stoffel, T.; Wilcox, S.; Michalsky, J. J.; Dutton, E. G.; Nelson, D. (2005). "Using a Blackbody to Calculate Net Longwave Responsivity of Shortwave Solar Pyranometers to Correct for Their Thermal Offset Error During Outdoor Calibration Using the Component Sum Method." *Journal of Atmospheric and Oceanic Technology*, 2005; pp. 1531-1540; NREL Report No. JA-560-36646. doi:10.1175/JTECH1782.1

[2] Reda, I.; Myers, D.; Stoffel, T. (2008). "Uncertainty Estimate for the Outdoor Calibration of Solar Pyranometers: A Metrologist Perspective." *Measure*. (NCSLI Journal of Measurement Science). Vol. 3(4), December 2008; pp. 58-66; NREL Report No. JA-581-4137

[3] Reda, I.; Andreas, A. (2004). "Solar Position Algorithm for Solar Radiation Applications." *Solar Energy*. Vol. 76(5), 2004; pp. 577-589; NREL Report No. JA-560-35518. doi:10.1016/j.solener.2003.12.003

[4] Stoffel, T.; Reda, I. (2009). "NREL Pyrheliometer Comparisons: 22 September - 3 October 2008 (NPC-2008)." 54 pp.; NREL Report No. TP-550-45016.

[5] Reda, I.; Stoffel, T.; Myers, D. (2003). "Method to Calibrate a Solar Pyranometer for Measuring Reference Diffuse Irradiance." *Solar Energy*. Vol. 74, 2003; pp. 103-112; NREL Report No. JA-560-35025. doi:10.1016/S0038-092X(03)00124-5

[6] Reda, I. (1996). Calibration of a Solar Absolute Cavity Radiometer with Traceability to the World Radiometric Reference. 79 pp.; NREL Report No. TP-463-20619.

[7] Reda, I.; Gröbner, J.; Stoffel, T.; Myers, D.; Forgan, B. (2008). Improvements in the Blackbody Calibration of Pyrgometers. ARM 2008 Science Team Meeting (Poster).

Calibration Results

140108 Kipp & Zonen CHP1

The responsivity (R , $\mu\text{V}/\text{W}/\text{m}^2$) of the test instrument during calibration is calculated using this Measurement Equation:

$$R = (V - R_{net} * W_{net}) / I \tag{1}$$

where,

- V = radiometer output voltage (microvolts),
- R_{net} = radiometer net infrared responsivity ($\mu\text{V}/\text{W}/\text{m}^2$), see Table 4,
- W_{net} = effective net infrared measured by pyrgeometer (W/m^2),
- = $W_{in} - W_{out} = W_{in} - \sigma * T_c^4$
- where, W_{in} = incoming infrared (W/m^2), $\sigma = 5.6704\text{e-}8 \text{ W}\cdot\text{m}^{-2}\cdot\text{K}^{-4}$,
- T_c = case temperature of pyrgeometer (K).
- I = reference irradiance (W/m^2), beam (B) or global (G)
- where, $G = B * \text{COS}(Z) + D$,
- Z = zenith angle (degrees),
- D = reference diffuse irradiance (W/m^2).

Figure 1. Responsivity vs Zenith Angle

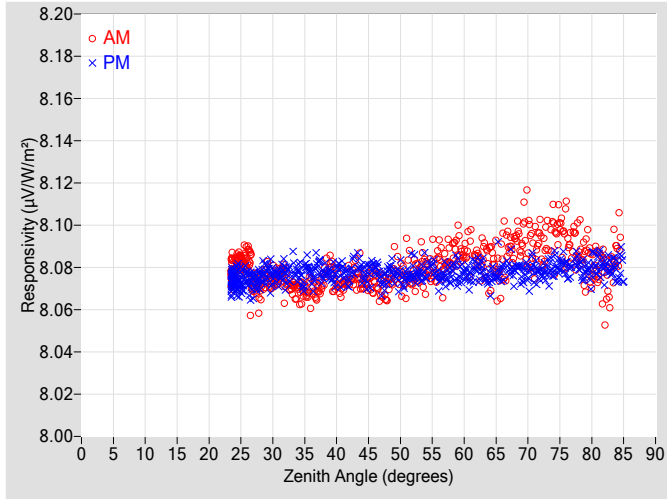


Figure 2. Responsivity vs Local Standard Time

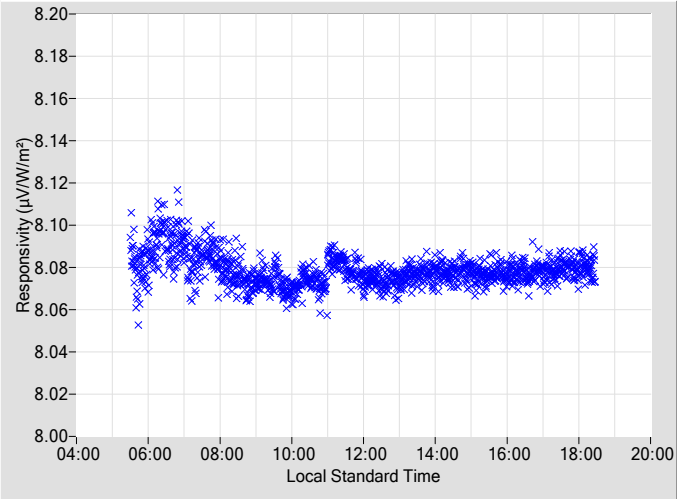


Table 2. Instrument Responsivity (R) and Calibration Type-B Standard Uncertainty, u(B)

| Zenith Angle (deg.) | R ($\mu\text{V}/\text{W}/\text{m}^2$) | AM u(B) \pm (%) | Azimuth Angle | R ($\mu\text{V}/\text{W}/\text{m}^2$) | PM u(B) \pm (%) | Azimuth Angle | Zenith Angle (deg.) | R ($\mu\text{V}/\text{W}/\text{m}^2$) | AM u(B) \pm (%) | Azimuth Angle | R ($\mu\text{V}/\text{W}/\text{m}^2$) | PM u(B) \pm (%) | Azimuth Angle |
|---------------------|---|-------------------|---------------|---|-------------------|---------------|---------------------|---|-------------------|---------------|---|-------------------|---------------|
| 0 | N/A | N/A | N/A | N/A | N/A | N/A | 46 | 8.0730 | 0.29 | 106.76 | 8.0794 | 0.29 | 252.81 |
| 2 | N/A | N/A | N/A | N/A | N/A | N/A | 48 | 8.0692 | 0.30 | 104.54 | 8.0767 | 0.29 | 255.07 |
| 4 | N/A | N/A | N/A | N/A | N/A | N/A | 50 | 8.0745 | 0.30 | 102.41 | 8.0758 | 0.29 | 257.23 |
| 6 | N/A | N/A | N/A | N/A | N/A | N/A | 52 | 8.0753 | 0.31 | 100.37 | 8.0800 | 0.29 | 259.29 |
| 8 | N/A | N/A | N/A | N/A | N/A | N/A | 54 | 8.0783 | 0.32 | 98.50 | 8.0791 | 0.30 | 261.27 |
| 10 | N/A | N/A | N/A | N/A | N/A | N/A | 56 | 8.0857 | 0.30 | 96.58 | 8.0743 | 0.29 | 263.10 |
| 12 | N/A | N/A | N/A | N/A | N/A | N/A | 58 | 8.0833 | 0.30 | 94.79 | 8.0764 | 0.29 | 264.91 |
| 14 | N/A | N/A | N/A | N/A | N/A | N/A | 60 | 8.0863 | 0.30 | 93.05 | 8.0775 | 0.30 | 266.71 |
| 16 | N/A | N/A | N/A | N/A | N/A | N/A | 62 | 8.0855 | 0.31 | 91.35 | 8.0797 | 0.30 | 268.39 |
| 18 | N/A | N/A | N/A | N/A | N/A | N/A | 64 | 8.0812 | 0.30 | 89.68 | 8.0765 | 0.30 | 270.07 |
| 20 | N/A | N/A | N/A | N/A | N/A | N/A | 66 | 8.0854 | 0.32 | 88.03 | 8.0777 | 0.30 | 271.72 |
| 22 | N/A | N/A | N/A | N/A | N/A | N/A | 68 | 8.0923 | 0.31 | 86.42 | 8.0779 | 0.30 | 273.36 |
| 24 | 8.0778 | 0.30 | 167.15 | 8.0749 | 0.30 | 192.94 | 70 | 8.0950 | 0.30 | 84.82 | 8.0765 | 0.30 | 274.98 |
| 26 | 8.0841 | 0.31 | 151.04 | 8.0752 | 0.29 | 209.08 | 72 | 8.0916 | 0.30 | 83.18 | 8.0776 | 0.31 | 276.59 |
| 28 | 8.0690 | 0.31 | 140.90 | 8.0759 | 0.31 | 218.19 | 74 | 8.0956 | 0.33 | 81.60 | 8.0805 | 0.31 | 278.20 |
| 30 | 8.0746 | 0.30 | 134.49 | 8.0756 | 0.32 | 224.72 | 76 | 8.0944 | 0.31 | 79.99 | 8.0790 | 0.31 | 279.83 |
| 32 | 8.0730 | 0.29 | 129.20 | 8.0775 | 0.29 | 230.05 | 78 | 8.0915 | 0.32 | 78.38 | 8.0809 | N/A | 281.44 |
| 34 | 8.0697 | 0.30 | 124.82 | 8.0783 | 0.30 | 234.61 | 80 | 8.0786 | N/A | 76.74 | 8.0794 | N/A | 283.09 |
| 36 | 8.0724 | 0.30 | 121.00 | 8.0763 | 0.31 | 238.40 | 82 | 8.0753 | N/A | 75.09 | 8.0795 | N/A | 284.73 |
| 38 | 8.0755 | 0.31 | 117.64 | 8.0773 | 0.31 | 241.90 | 84 | 8.0898 | N/A | 73.42 | 8.0767 | N/A | 286.38 |
| 40 | 8.0738 | 0.31 | 114.45 | 8.0772 | 0.30 | 244.99 | 86 | N/A | N/A | N/A | N/A | N/A | N/A |
| 42 | 8.0743 | 0.29 | 111.81 | 8.0743 | 0.30 | 247.80 | 88 | N/A | N/A | N/A | N/A | N/A | N/A |
| 44 | 8.0718 | 0.30 | 109.15 | 8.0768 | 0.29 | 250.44 | 90 | N/A | N/A | N/A | N/A | N/A | N/A |

N/A - Not Available

Figure 3. Type-B Standard Uncertainty vs Zenith Angle

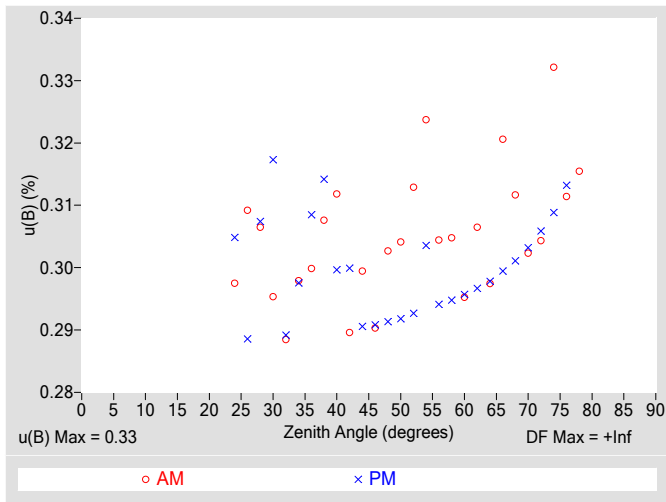


Figure 4. Residuals from Spline Interpolation

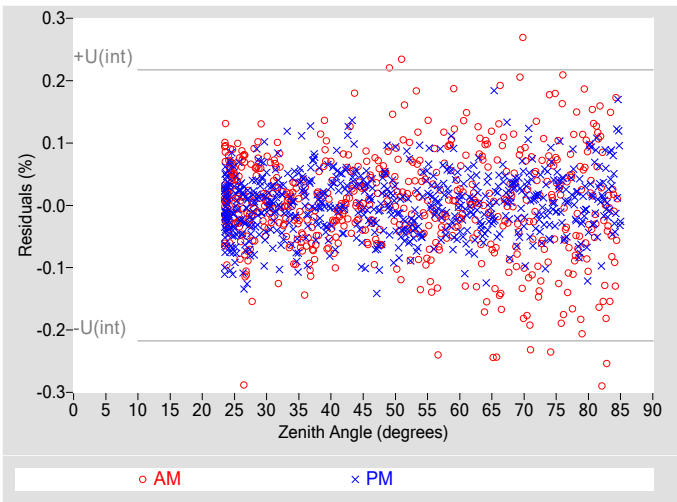


Table 3. Uncertainty using Spline Interpolation ‡

| | |
|---|------------|
| Type-B Standard Uncertainty, $u(B)$ (%) | ± 0.33 |
| Type-A Interpolating Function, $u(int)$ (%) | ± 0.11 |
| Combined Standard Uncertainty, $u(c)$ (%) | ± 0.35 |
| Effective degrees of freedom, $DF(c)$ | 123510 |
| Coverage factor, k | 1.96 |
| Expanded Uncertainty, U_{95} (%) | ± 0.68 |
| AM Valid zenith angle range | 24° to 78° |
| PM Valid zenith angle range | 24° to 76° |

‡ An illustration for how to reduce the uncertainty in calculating the irradiance using a function rather than $R@45^\circ$. Not accredited.

Table 4. Calibration Label Values

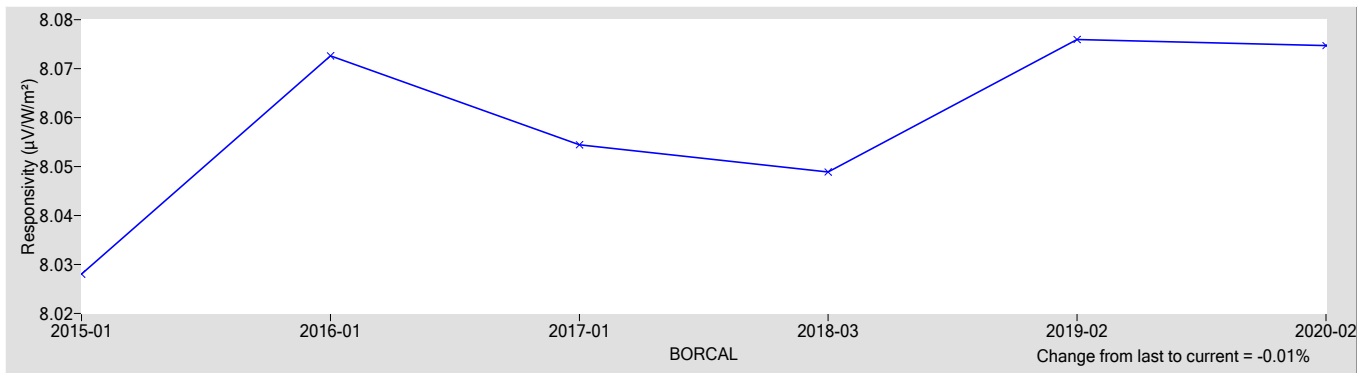
| | |
|----------------------------------|-------------------------------|
| $R @ 45^\circ$ ($\mu V/W/m^2$) | R_{net} ($\mu V/W/m^2$) † |
| 8.0747 | 0 |

† R_{net} determination date: N/A

Table 5. Uncertainty using $R @ 45^\circ$

| | |
|---|----------------|
| Type-B Expanded Uncertainty, $U(B)$ (%) | ± 0.63 |
| Offset Uncertainty, $U(off)$ (%) | +0.14 / -0.068 |
| Expanded Uncertainty, U (%) | +0.78 / -0.70 |
| Effective degrees of freedom, DF | +Inf |
| Coverage factor, k | 1.96 |
| Valid zenith angle range | 30.0° to 60.0° |

Figure 5. History of instrument at Zenith Angle = 45°



References:

- [1] Reda, I.; Hickey, J.; Long, C.; Myers, D.; Stoffel, T.; Wilcox, S.; Michalsky, J. J.; Dutton, E. G.; Nelson, D. (2005). "Using a Blackbody to Calculate Net Longwave Responsivity of Shortwave Solar Pyranometers to Correct for Their Thermal Offset Error During Outdoor Calibration Using the Component Sum Method." *Journal of Atmospheric and Oceanic Technology*, 2005; pp. 1531-1540; NREL Report No. JA-560-36646. doi:10.1175/JTECH1782.1
- [2] Reda, I.; Myers, D.; Stoffel, T. (2008). "Uncertainty Estimate for the Outdoor Calibration of Solar Pyranometers: A Metrologist Perspective." *Measure*. (NCSLI Journal of Measurement Science). Vol. 3(4), December 2008; pp. 58-66; NREL Report No. JA-581-4137
- [3] Reda, I.; Andreas, A. (2004). "Solar Position Algorithm for Solar Radiation Applications." *Solar Energy*. Vol. 76(5), 2004; pp. 577-589; NREL Report No. JA-560-35518. doi:10.1016/j.solener.2003.12.003
- [4] Stoffel, T.; Reda, I. (2009). "NREL Pyrheliometer Comparisons: 22 September - 3 October 2008 (NPC-2008)." 54 pp.; NREL Report No. TP-550-45016.
- [5] Reda, I.; Stoffel, T.; Myers, D. (2003). "Method to Calibrate a Solar Pyranometer for Measuring Reference Diffuse Irradiance." *Solar Energy*. Vol. 74, 2003; pp. 103-112; NREL Report No. JA-560-35025. doi:10.1016/S0038-092X(03)00124-5
- [6] Reda, I. (1996). Calibration of a Solar Absolute Cavity Radiometer with Traceability to the World Radiometric Reference. 79 pp.; NREL Report No. TP-463-20619.
- [7] Reda, I.; Gröbner, J.; Stoffel, T.; Myers, D.; Forgan, B. (2008). Improvements in the Blackbody Calibration of Pyrgometers. ARM 2008 Science Team Meeting (Poster).



National Renewable Energy Laboratory

Solar Radiation Research Laboratory

Metrology Laboratory

Calibration Certificate



| | | | |
|--------------------------|---------------|----------------------------------|--------------|
| Test Instrument: | Pyranometer | Manufacturer: | Kipp & Zonen |
| Model: | CMP11 | Serial Number: | 140712 |
| Calibration Date: | 5/5/2020 | Due Date: | 5/5/2021 |
| Customer: | NREL-SRRL-BMS | Environmental Conditions: | see page 4 |
| Test Dates: | 5/4-5 | | |

This certifies that the above product was calibrated in compliance with ISO/IEC 17025:2017. Measurement uncertainties at the time of calibration are consistent with the Guide to the Expression of Uncertainty in Measurement (GUM) using Reda et al., 2008. All nominal values are traceable to the International System (SI) Units of Measurement.

No statement of compliance with specifications is made or implied on this certificate. However, the estimated uncertainties are the uncertainties of the calibration process; users must add other uncertainties that are relevant to their measuring system, environmental and sky conditions, outdoor set-up, and site location.

The Type-B Standard Uncertainty of using the responsivity at each even zenith angle is reported, and the Expanded Uncertainty of the calibration is reported using two methods:

1. The Expanded Uncertainty of using the responsivity at zenith angle = 45°, within the zenith angle range from 30.0° to 60.0°
2. The Expanded Uncertainty of using Spline Interpolating Functions for the responsivity versus zenith angle.

This certificate applies only to the item identified above and shall not be reproduced other than in full, without specific written approval from the calibration facility. Certificate without signature is not valid.

Table 1. Traceability

| Measurement Type | Instrument | Calibration Date | Calibration Due Date |
|-----------------------|--|------------------|----------------------|
| Beam Irradiance † | Eppley Absolute Cavity Radiometer Model HF, S/N 29219 | 09/27/2019 | 09/27/2020 |
| Diffuse Irradiance † | Hukseflux Pyranometer Model SR25, S/N 2541 | 04/17/2020 | 04/17/2021 |
| Diffuse Irradiance † | Hukseflux Pyranometer Model SR25, S/N 2542 | 04/17/2020 | 04/17/2021 |
| Data Acquisition | NREL Data Acquisition System Model RAP-DAQ, S/N 2005-998 | 02/14/2019 | 02/14/2021 |
| Data Acquisition | NREL Data Acquisition System Model RAP-DAQ, S/N 2005-999 | 02/14/2019 | 02/14/2021 |
| Infrared Irradiance ‡ | Kipp & Zonen Pyrgeometer Model CG4, S/N FT002 | 04/16/2018 | 04/16/2022 |

† Through the World Radiometric Reference (WRR)

‡ Through the World Infrared Standard Group (WISG)

Number of pages of certificate: 4

Calibration Procedure: BORCAL-P00-Calibration and QA Procedure; available upon request.

Setup: Radiometers are calibrated outdoors, using the sun as the source. Pyranometers and pyrgeometers are installed for horizontal measurements, with their signal connectors oriented north, if their design permits.

The shading disk for the reference diffuse subtends a solid angle of 5°. Pyrheliometers are installed on solar trackers.

Calibrated by: Afshin Andreas, Ibrahim Reda, Peter Gotseff, and RCC

Ibrahim Reda, Technical Manager

Date

For questions or comments, please contact the technical manager at:

ibrahim.reda@nrel.gov; 303-384-6385; 15013 Denver West Parkway, Golden, CO 80401, USA

Calibration Results

140712 Kipp & Zonen CMP11

The responsivity (R , $\mu\text{V}/\text{W}/\text{m}^2$) of the test instrument during calibration is calculated using this Measurement Equation:

$$R = (V - R_{net} * W_{net}) / I \tag{1}$$

where,

- V = radiometer output voltage (microvolts),
 - R_{net} = radiometer net infrared responsivity ($\mu\text{V}/\text{W}/\text{m}^2$), see Table 4,
 - W_{net} = effective net infrared measured by pyrgeometer (W/m^2),
 - = $W_{in} - W_{out} = W_{in} - \sigma * T_c^4$
 - where, W_{in} = incoming infrared (W/m^2), $\sigma = 5.6704\text{e-}8 \text{ W}\cdot\text{m}^{-2}\cdot\text{K}^{-4}$,
 - T_c = case temperature of pyrgeometer (K).
- I = reference irradiance (W/m^2), beam (B) or global (G)
 - where, $G = B * \text{COS}(Z) + D$,
 - Z = zenith angle (degrees),
 - D = reference diffuse irradiance (W/m^2).

Figure 1. Responsivity vs Zenith Angle

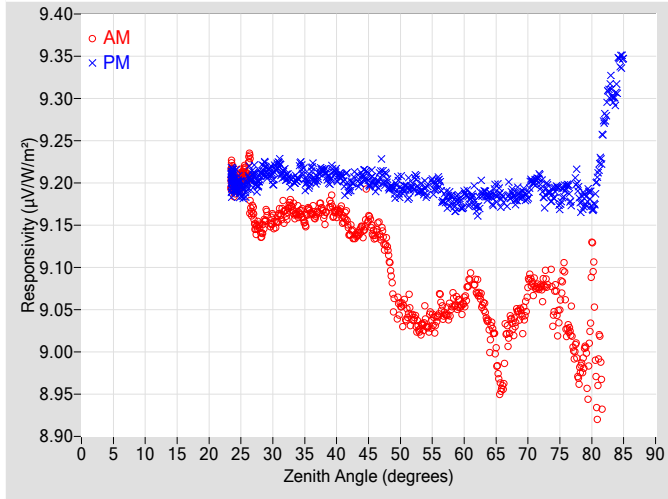


Figure 2. Responsivity vs Local Standard Time

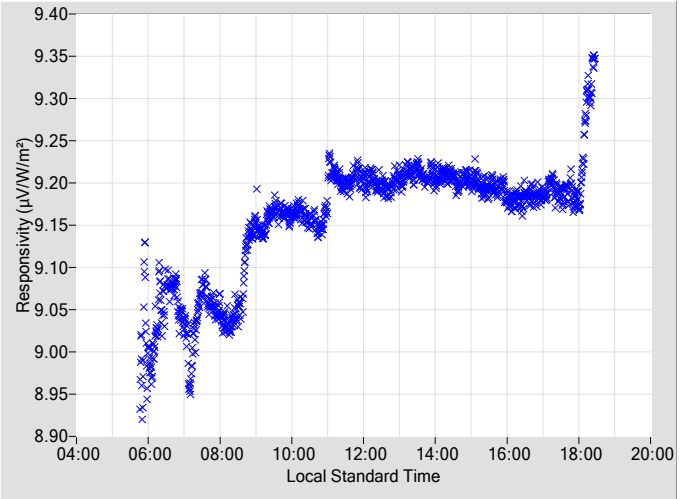


Table 2. Instrument Responsivity (R) and Calibration Type-B Standard Uncertainty, u(B)

| Zenith Angle (deg.) | R ($\mu\text{V}/\text{W}/\text{m}^2$) | AM u(B) \pm (%) | Azimuth Angle | R ($\mu\text{V}/\text{W}/\text{m}^2$) | PM u(B) \pm (%) | Azimuth Angle | Zenith Angle (deg.) | R ($\mu\text{V}/\text{W}/\text{m}^2$) | AM u(B) \pm (%) | Azimuth Angle | R ($\mu\text{V}/\text{W}/\text{m}^2$) | PM u(B) \pm (%) | Azimuth Angle |
|---------------------|---|-------------------|---------------|---|-------------------|---------------|---------------------|---|-------------------|---------------|---|-------------------|---------------|
| 0 | N/A | N/A | N/A | N/A | N/A | N/A | 46 | 9.1384 | 0.31 | 106.83 | 9.1979 | 0.31 | 252.82 |
| 2 | N/A | N/A | N/A | N/A | N/A | N/A | 48 | 9.1213 | 0.33 | 104.55 | 9.1992 | 0.32 | 255.14 |
| 4 | N/A | N/A | N/A | N/A | N/A | N/A | 50 | 9.0540 | 0.34 | 102.41 | 9.1931 | 0.32 | 257.24 |
| 6 | N/A | N/A | N/A | N/A | N/A | N/A | 52 | 9.0400 | 0.35 | 100.32 | 9.1971 | 0.34 | 259.30 |
| 8 | N/A | N/A | N/A | N/A | N/A | N/A | 54 | 9.0360 | 0.36 | 98.46 | 9.1925 | 0.33 | 261.23 |
| 10 | N/A | N/A | N/A | N/A | N/A | N/A | 56 | 9.0533 | 0.38 | 96.58 | 9.2006 | 0.34 | 263.10 |
| 12 | N/A | N/A | N/A | N/A | N/A | N/A | 58 | 9.0541 | 0.34 | 94.77 | 9.1806 | 0.34 | 264.92 |
| 14 | N/A | N/A | N/A | N/A | N/A | N/A | 60 | 9.0598 | 0.35 | 93.05 | 9.1818 | 0.37 | 266.67 |
| 16 | N/A | N/A | N/A | N/A | N/A | N/A | 62 | 9.0754 | 0.38 | 91.35 | 9.1689 | 0.36 | 268.40 |
| 18 | N/A | N/A | N/A | N/A | N/A | N/A | 64 | 9.0217 | 0.40 | 89.68 | 9.1851 | 0.38 | 270.10 |
| 20 | N/A | N/A | N/A | N/A | N/A | N/A | 66 | 8.9577 | 0.42 | 88.04 | 9.1796 | 0.39 | 271.68 |
| 22 | N/A | N/A | N/A | N/A | N/A | N/A | 68 | 9.0351 | 0.44 | 86.42 | 9.1804 | 0.41 | 273.36 |
| 24 | 9.2007 | 0.31 | 167.06 | 9.2020 | 0.32 | 193.07 | 70 | 9.0754 | 0.44 | 84.78 | 9.1864 | 0.44 | 274.99 |
| 26 | 9.2133 | 0.31 | 150.99 | 9.1996 | 0.30 | 209.07 | 72 | 9.0733 | 0.47 | 83.19 | 9.2009 | 0.47 | 276.60 |
| 28 | 9.1429 | 0.32 | 140.64 | 9.2077 | 0.32 | 218.08 | 74 | 9.0542 | 0.51 | 81.61 | 9.1880 | 0.52 | 278.20 |
| 30 | 9.1552 | 0.32 | 134.50 | 9.2082 | 0.33 | 224.62 | 76 | 9.0436 | 0.61 | 79.99 | 9.1954 | 0.58 | 279.79 |
| 32 | 9.1621 | 0.32 | 129.23 | 9.2075 | 0.32 | 230.07 | 78 | 8.9718 | 0.65 | 78.39 | 9.1850 | N/A | 281.40 |
| 34 | 9.1648 | 0.30 | 124.84 | 9.2104 | 0.31 | 234.50 | 80 | 9.0835 | N/A | 76.79 | 9.1749 | N/A | 283.05 |
| 36 | 9.1643 | 0.30 | 121.03 | 9.2117 | 0.30 | 238.41 | 82 | N/A | N/A | N/A | 9.2728 | N/A | 284.69 |
| 38 | 9.1619 | 0.31 | 117.58 | 9.2151 | 0.32 | 241.95 | 84 | N/A | N/A | N/A | 9.3253 | N/A | 286.39 |
| 40 | 9.1658 | 0.33 | 114.58 | 9.2095 | 0.31 | 244.93 | 86 | N/A | N/A | N/A | N/A | N/A | N/A |
| 42 | 9.1439 | 0.35 | 111.75 | 9.1938 | 0.32 | 247.74 | 88 | N/A | N/A | N/A | N/A | N/A | N/A |
| 44 | 9.1441 | 0.31 | 109.22 | 9.2085 | 0.34 | 250.39 | 90 | N/A | N/A | N/A | N/A | N/A | N/A |

N/A - Not Available

Figure 3. Type-B Standard Uncertainty vs Zenith Angle

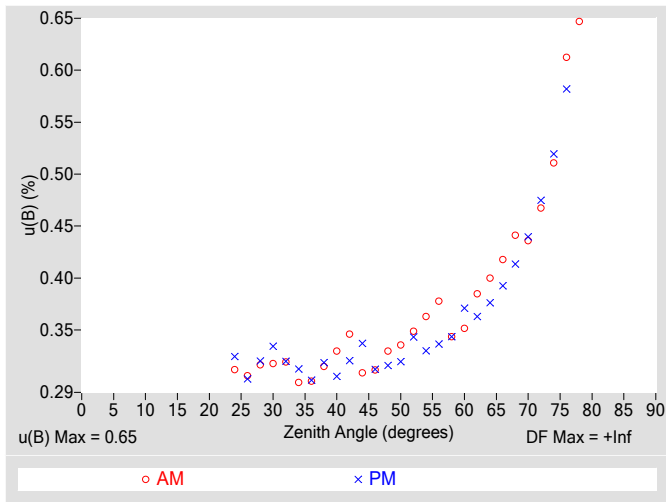


Figure 4. Residuals from Spline Interpolation

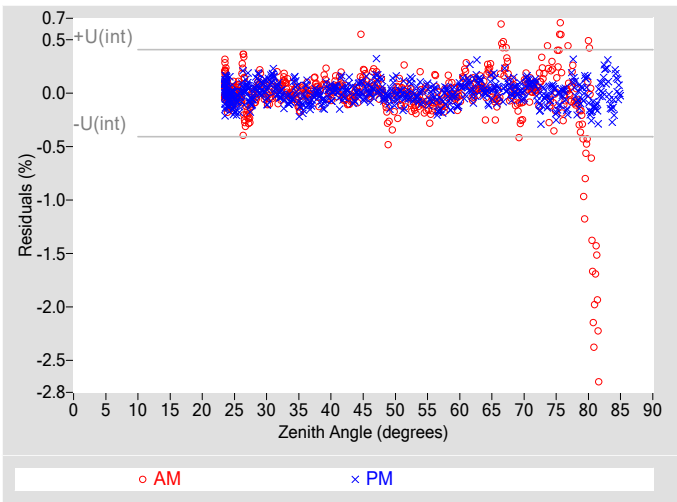


Table 3. Uncertainty using Spline Interpolation ‡

| | |
|---|------------|
| Type-B Standard Uncertainty, $u(B)$ (%) | ± 0.65 |
| Type-A Interpolating Function, $u(int)$ (%) | ± 0.20 |
| Combined Standard Uncertainty, $u(c)$ (%) | ± 0.68 |
| Effective degrees of freedom, $DF(c)$ | 139338 |
| Coverage factor, k | 1.96 |
| Expanded Uncertainty, $U95$ (%) | ± 1.3 |
| AM Valid zenith angle range | 24° to 78° |
| PM Valid zenith angle range | 24° to 76° |

‡ An illustration for how to reduce the uncertainty in calculating the irradiance using a function rather than $R@45^\circ$. Not accredited.

Table 4. Calibration Label Values

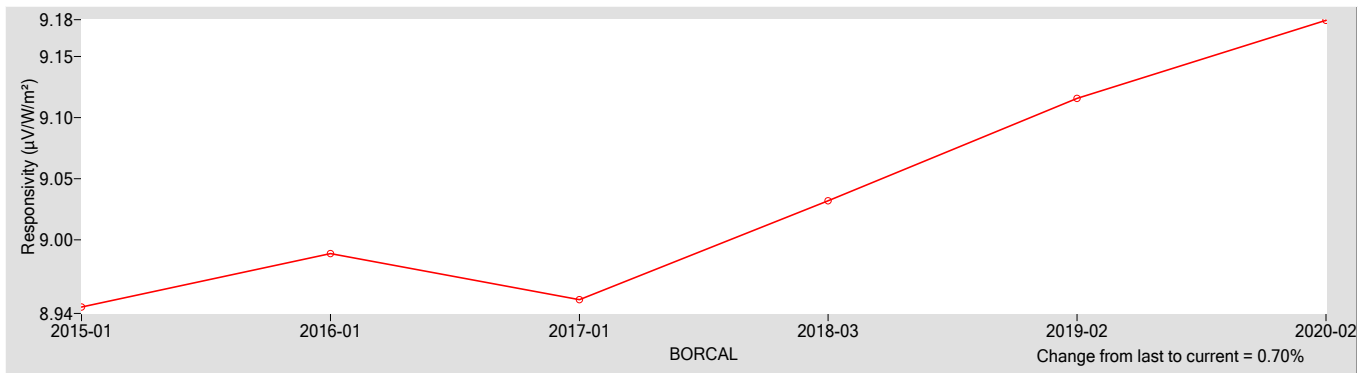
| | |
|----------------------------------|-------------------------------|
| $R @ 45^\circ$ ($\mu V/W/m^2$) | R_{net} ($\mu V/W/m^2$) † |
| 9.1796 | 0.20500 |

† R_{net} determination date: Estimated

Table 5. Uncertainty using $R @ 45^\circ$

| | |
|---|----------------|
| Type-B Expanded Uncertainty, $U(B)$ (%) | ± 0.74 |
| Offset Uncertainty, $U(off)$ (%) | +0.39 / -1.6 |
| Expanded Uncertainty, U (%) | +1.1 / -2.3 |
| Effective degrees of freedom, DF | +Inf |
| Coverage factor, k | 1.96 |
| Valid zenith angle range | 30.0° to 60.0° |

Figure 5. History of instrument at Zenith Angle = 45°



References:

[1] Reda, I.; Hickey, J.; Long, C.; Myers, D.; Stoffel, T.; Wilcox, S.; Michalsky, J. J.; Dutton, E. G.; Nelson, D. (2005). "Using a Blackbody to Calculate Net Longwave Responsivity of Shortwave Solar Pyranometers to Correct for Their Thermal Offset Error During Outdoor Calibration Using the Component Sum Method." *Journal of Atmospheric and Oceanic Technology*, 2005; pp. 1531-1540; NREL Report No. JA-560-36646. doi:10.1175/JTECH1782.1

[2] Reda, I.; Myers, D.; Stoffel, T. (2008). "Uncertainty Estimate for the Outdoor Calibration of Solar Pyranometers: A Metrologist Perspective." *Measure*. (NCSLI Journal of Measurement Science). Vol. 3(4), December 2008; pp. 58-66; NREL Report No. JA-581-4137

[3] Reda, I.; Andreas, A. (2004). "Solar Position Algorithm for Solar Radiation Applications." *Solar Energy*. Vol. 76(5), 2004; pp. 577-589; NREL Report No. JA-560-35518. doi:10.1016/j.solener.2003.12.003

[4] Stoffel, T.; Reda, I. (2009). "NREL Pyrheliometer Comparisons: 22 September - 3 October 2008 (NPC-2008)." 54 pp.; NREL Report No. TP-550-45016.

[5] Reda, I.; Stoffel, T.; Myers, D. (2003). "Method to Calibrate a Solar Pyranometer for Measuring Reference Diffuse Irradiance." *Solar Energy*. Vol. 74, 2003; pp. 103-112; NREL Report No. JA-560-35025. doi:10.1016/S0038-092X(03)00124-5

[6] Reda, I. (1996). Calibration of a Solar Absolute Cavity Radiometer with Traceability to the World Radiometric Reference. 79 pp.; NREL Report No. TP-463-20619.

[7] Reda, I.; Gröbner, J.; Stoffel, T.; Myers, D.; Forgan, B. (2008). Improvements in the Blackbody Calibration of Pyrgometers. ARM 2008 Science Team Meeting (Poster).



National Renewable Energy Laboratory

Solar Radiation Research Laboratory

Metrology Laboratory

Calibration Certificate



| | | | |
|--------------------------|---------------|----------------------------------|--------------|
| Test Instrument: | Pyranometer | Manufacturer: | Kipp & Zonen |
| Model: | CMP11 | Serial Number: | 140713 |
| Calibration Date: | 5/5/2020 | Due Date: | 5/5/2021 |
| Customer: | NREL-SRRL-BMS | Environmental Conditions: | see page 4 |
| Test Dates: | 5/4-5 | | |

This certifies that the above product was calibrated in compliance with ISO/IEC 17025:2017. Measurement uncertainties at the time of calibration are consistent with the Guide to the Expression of Uncertainty in Measurement (GUM) using Reda et al., 2008. All nominal values are traceable to the International System (SI) Units of Measurement.

No statement of compliance with specifications is made or implied on this certificate. However, the estimated uncertainties are the uncertainties of the calibration process; users must add other uncertainties that are relevant to their measuring system, environmental and sky conditions, outdoor set-up, and site location.

The Type-B Standard Uncertainty of using the responsivity at each even zenith angle is reported, and the Expanded Uncertainty of the calibration is reported using two methods:

1. The Expanded Uncertainty of using the responsivity at zenith angle = 45°, within the zenith angle range from 30.0° to 60.0°
2. The Expanded Uncertainty of using Spline Interpolating Functions for the responsivity versus zenith angle.

This certificate applies only to the item identified above and shall not be reproduced other than in full, without specific written approval from the calibration facility. Certificate without signature is not valid.

Table 1. Traceability

| Measurement Type | Instrument | Calibration Date | Calibration Due Date |
|-----------------------|--|------------------|----------------------|
| Beam Irradiance † | Eppley Absolute Cavity Radiometer Model HF, S/N 29219 | 09/27/2019 | 09/27/2020 |
| Diffuse Irradiance † | Hukseflux Pyranometer Model SR25, S/N 2541 | 04/17/2020 | 04/17/2021 |
| Diffuse Irradiance † | Hukseflux Pyranometer Model SR25, S/N 2542 | 04/17/2020 | 04/17/2021 |
| Data Acquisition | NREL Data Acquisition System Model RAP-DAQ, S/N 2005-998 | 02/14/2019 | 02/14/2021 |
| Data Acquisition | NREL Data Acquisition System Model RAP-DAQ, S/N 2005-999 | 02/14/2019 | 02/14/2021 |
| Infrared Irradiance ‡ | Kipp & Zonen Pyrgeometer Model CG4, S/N FT002 | 04/16/2018 | 04/16/2022 |

† Through the World Radiometric Reference (WRR)

‡ Through the World Infrared Standard Group (WISG)

Number of pages of certificate: 4

Calibration Procedure: BORCAL-P00-Calibration and QA Procedure; available upon request.

Setup: Radiometers are calibrated outdoors, using the sun as the source. Pyranometers and pyrgeometers are installed for horizontal measurements, with their signal connectors oriented north, if their design permits.

The shading disk for the reference diffuse subtends a solid angle of 5°. Pyrheliometers are installed on solar trackers.

Calibrated by: Afshin Andreas, Ibrahim Reda, Peter Gotseff, and RCC

Ibrahim Reda, Technical Manager

Date

For questions or comments, please contact the technical manager at:

ibrahim.reda@nrel.gov; 303-384-6385; 15013 Denver West Parkway, Golden, CO 80401, USA

Calibration Results

140713 Kipp & Zonen CMP11

The responsivity (R , $\mu\text{V}/\text{W}/\text{m}^2$) of the test instrument during calibration is calculated using this Measurement Equation:

$$R = (V - R_{net} * W_{net}) / I \tag{1}$$

where,

- V = radiometer output voltage (microvolts),
 - R_{net} = radiometer net infrared responsivity ($\mu\text{V}/\text{W}/\text{m}^2$), see Table 4,
 - W_{net} = effective net infrared measured by pyrgeometer (W/m^2),
 - = $W_{in} - W_{out} = W_{in} - \sigma * T_c^4$
 - where, W_{in} = incoming infrared (W/m^2), $\sigma = 5.6704\text{e-}8 \text{ W}\cdot\text{m}^{-2}\cdot\text{K}^{-4}$,
 - T_c = case temperature of pyrgeometer (K).
- I = reference irradiance (W/m^2), beam (B) or global (G)
 - where, $G = B * \text{COS}(Z) + D$,
 - Z = zenith angle (degrees),
 - D = reference diffuse irradiance (W/m^2).

Figure 1. Responsivity vs Zenith Angle

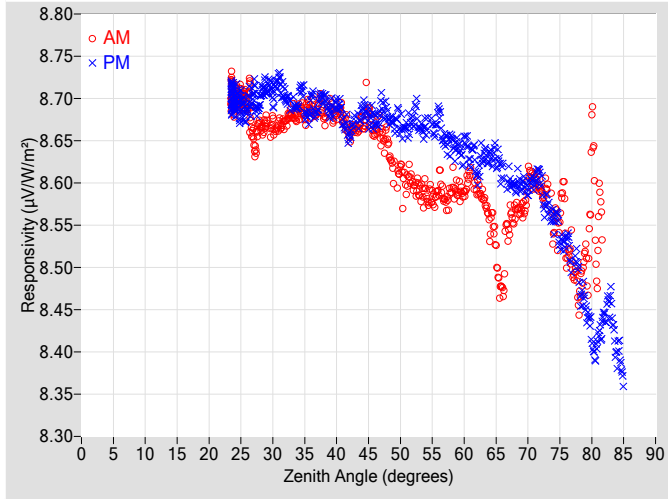


Figure 2. Responsivity vs Local Standard Time

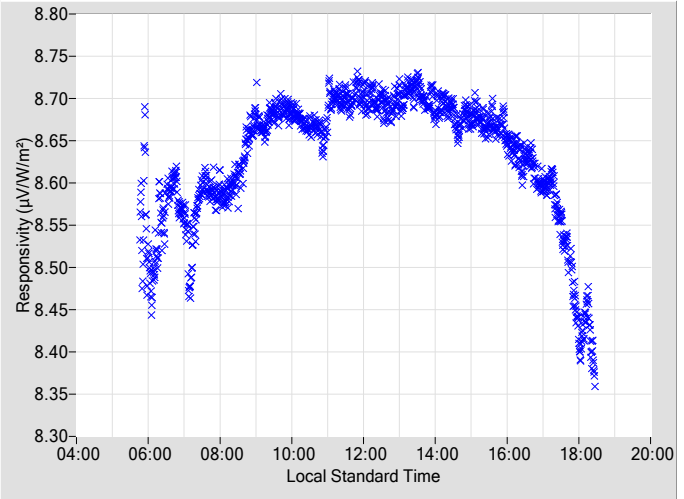


Table 2. Instrument Responsivity (R) and Calibration Type-B Standard Uncertainty, u(B)

| Zenith | | | AM | | | PM | | | Zenith | | | AM | | | PM | | |
|--------|---------------------------------------|-----------|---------|---------------------------------------|-----------|---------|--------|---------------------------------------|-----------|---------|---------------------------------------|-----------|---------|---------------------------------------|-----------|---------|--|
| Angle | R | u(B) | Azimuth | R | u(B) | Azimuth | Angle | R | u(B) | Azimuth | R | u(B) | Azimuth | R | u(B) | Azimuth | |
| (deg.) | ($\mu\text{V}/\text{W}/\text{m}^2$) | \pm (%) | Angle | ($\mu\text{V}/\text{W}/\text{m}^2$) | \pm (%) | Angle | (deg.) | ($\mu\text{V}/\text{W}/\text{m}^2$) | \pm (%) | Angle | ($\mu\text{V}/\text{W}/\text{m}^2$) | \pm (%) | Angle | ($\mu\text{V}/\text{W}/\text{m}^2$) | \pm (%) | Angle | |
| 0 | N/A | N/A | N/A | N/A | N/A | N/A | 46 | 8.6605 | 0.31 | 106.83 | 8.6746 | 0.31 | 252.82 | | | | |
| 2 | N/A | N/A | N/A | N/A | N/A | N/A | 48 | 8.6506 | 0.33 | 104.55 | 8.6788 | 0.32 | 255.14 | | | | |
| 4 | N/A | N/A | N/A | N/A | N/A | N/A | 50 | 8.6162 | 0.34 | 102.41 | 8.6662 | 0.32 | 257.24 | | | | |
| 6 | N/A | N/A | N/A | N/A | N/A | N/A | 52 | 8.5967 | 0.35 | 100.32 | 8.6741 | 0.34 | 259.30 | | | | |
| 8 | N/A | N/A | N/A | N/A | N/A | N/A | 54 | 8.5894 | 0.36 | 98.46 | 8.6679 | 0.33 | 261.23 | | | | |
| 10 | N/A | N/A | N/A | N/A | N/A | N/A | 56 | 8.5992 | 0.38 | 96.58 | 8.6818 | 0.34 | 263.10 | | | | |
| 12 | N/A | N/A | N/A | N/A | N/A | N/A | 58 | 8.5975 | 0.34 | 94.77 | 8.6486 | 0.34 | 264.92 | | | | |
| 14 | N/A | N/A | N/A | N/A | N/A | N/A | 60 | 8.5876 | 0.35 | 93.05 | 8.6410 | 0.37 | 266.67 | | | | |
| 16 | N/A | N/A | N/A | N/A | N/A | N/A | 62 | 8.5953 | 0.39 | 91.35 | 8.6085 | 0.36 | 268.40 | | | | |
| 18 | N/A | N/A | N/A | N/A | N/A | N/A | 64 | 8.5497 | 0.40 | 89.68 | 8.6316 | 0.38 | 270.10 | | | | |
| 20 | N/A | N/A | N/A | N/A | N/A | N/A | 66 | 8.4740 | 0.42 | 88.04 | 8.6106 | 0.39 | 271.68 | | | | |
| 22 | N/A | N/A | N/A | N/A | N/A | N/A | 68 | 8.5656 | 0.44 | 86.42 | 8.5950 | 0.42 | 273.36 | | | | |
| 24 | 8.6975 | 0.31 | 167.06 | 8.6983 | 0.32 | 193.07 | 70 | 8.6010 | 0.44 | 84.78 | 8.5919 | 0.44 | 274.99 | | | | |
| 26 | 8.6974 | 0.31 | 150.99 | 8.6897 | 0.30 | 209.07 | 72 | 8.5907 | 0.47 | 83.19 | 8.6028 | 0.48 | 276.60 | | | | |
| 28 | 8.6680 | 0.32 | 140.64 | 8.6989 | 0.32 | 218.08 | 74 | 8.5471 | 0.51 | 81.61 | 8.5572 | 0.52 | 278.20 | | | | |
| 30 | 8.6683 | 0.32 | 134.50 | 8.7032 | 0.33 | 224.62 | 76 | 8.5275 | 0.62 | 79.99 | 8.5337 | 0.59 | 279.79 | | | | |
| 32 | 8.6713 | 0.32 | 129.23 | 8.7001 | 0.32 | 230.07 | 78 | 8.4601 | 0.65 | 78.39 | 8.4843 | N/A | 281.40 | | | | |
| 34 | 8.6835 | 0.30 | 124.84 | 8.6970 | 0.31 | 234.50 | 80 | 8.6290 | N/A | 76.79 | 8.4167 | N/A | 283.05 | | | | |
| 36 | 8.6849 | 0.30 | 121.03 | 8.6971 | 0.30 | 238.41 | 82 | N/A | N/A | N/A | 8.4416 | N/A | 284.69 | | | | |
| 38 | 8.6779 | 0.32 | 117.58 | 8.7026 | 0.32 | 241.95 | 84 | N/A | N/A | N/A | 8.3989 | N/A | 286.39 | | | | |
| 40 | 8.6823 | 0.33 | 114.58 | 8.6932 | 0.31 | 244.93 | 86 | N/A | N/A | N/A | N/A | N/A | N/A | | | | |
| 42 | 8.6575 | 0.35 | 111.75 | 8.6543 | 0.32 | 247.74 | 88 | N/A | N/A | N/A | N/A | N/A | N/A | | | | |
| 44 | 8.6727 | 0.31 | 109.22 | 8.6864 | 0.34 | 250.39 | 90 | N/A | N/A | N/A | N/A | N/A | N/A | | | | |

N/A - Not Available

Figure 3. Type-B Standard Uncertainty vs Zenith Angle

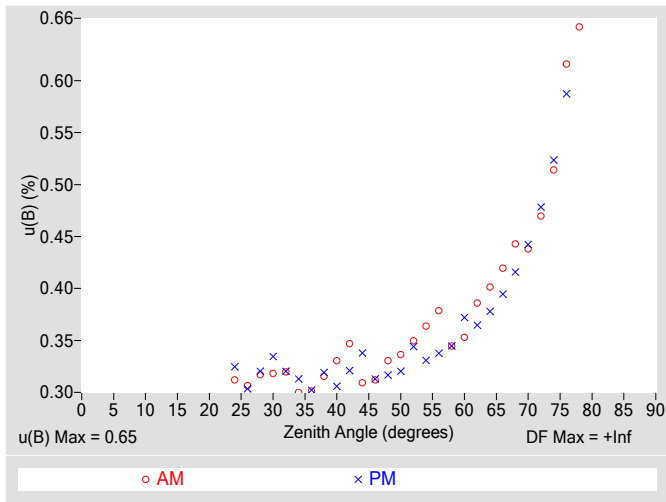


Figure 4. Residuals from Spline Interpolation

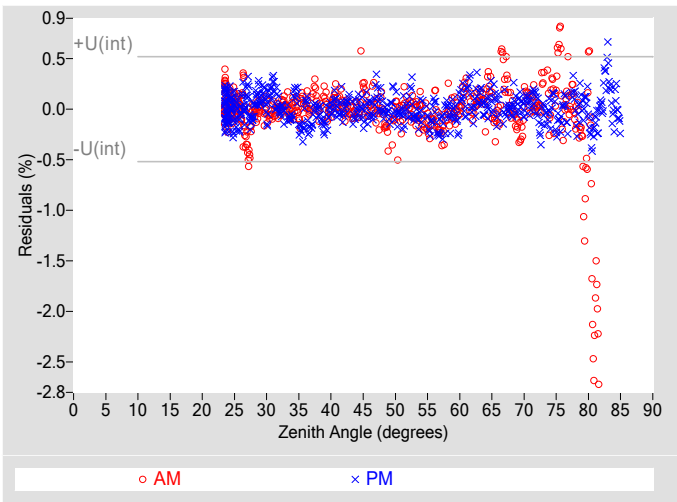


Table 3. Uncertainty using Spline Interpolation ‡

| | |
|---|------------|
| Type-B Standard Uncertainty, $u(B)$ (%) | ± 0.65 |
| Type-A Interpolating Function, $u(int)$ (%) | ± 0.26 |
| Combined Standard Uncertainty, $u(c)$ (%) | ± 0.70 |
| Effective degrees of freedom, $DF(c)$ | 60569 |
| Coverage factor, k | 1.96 |
| Expanded Uncertainty, $U95$ (%) | ± 1.4 |
| AM Valid zenith angle range | 24° to 78° |
| PM Valid zenith angle range | 24° to 76° |

‡ An illustration for how to reduce the uncertainty in calculating the irradiance using a function rather than $R@45^\circ$. Not accredited.

Table 4. Calibration Label Values

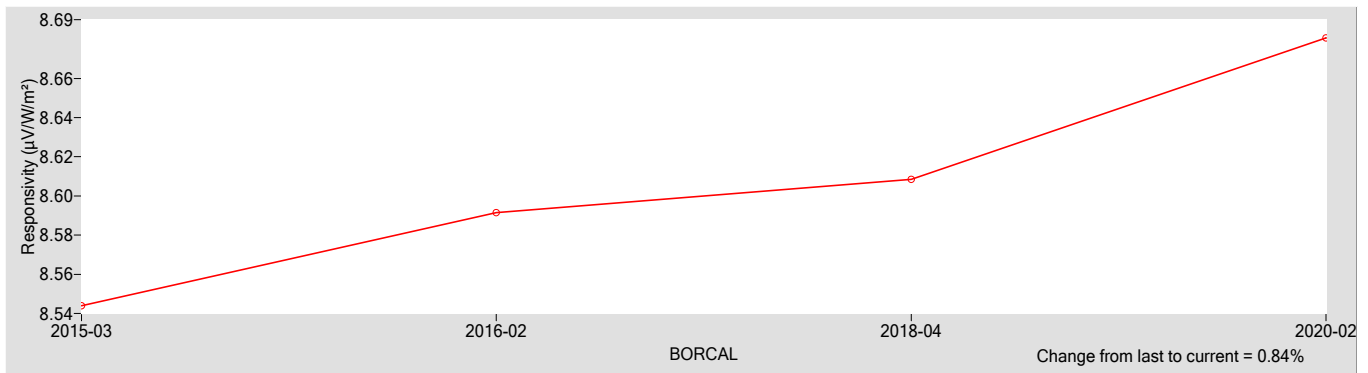
| | |
|----------------------------------|-------------------------------|
| $R @ 45^\circ$ ($\mu V/W/m^2$) | R_{net} ($\mu V/W/m^2$) † |
| 8.6806 | 0.20500 |

† R_{net} determination date: Estimated

Table 5. Uncertainty using $R @ 45^\circ$

| | |
|---|----------------|
| Type-B Expanded Uncertainty, $U(B)$ (%) | ± 0.74 |
| Offset Uncertainty, $U(off)$ (%) | +0.26 / -1.1 |
| Expanded Uncertainty, U (%) | +1.0 / -1.8 |
| Effective degrees of freedom, DF | +Inf |
| Coverage factor, k | 1.96 |
| Valid zenith angle range | 30.0° to 60.0° |

Figure 5. History of instrument at Zenith Angle = 45°



References:

- [1] Reda, I.; Hickey, J.; Long, C.; Myers, D.; Stoffel, T.; Wilcox, S.; Michalsky, J. J.; Dutton, E. G.; Nelson, D. (2005). "Using a Blackbody to Calculate Net Longwave Responsivity of Shortwave Solar Pyranometers to Correct for Their Thermal Offset Error During Outdoor Calibration Using the Component Sum Method." *Journal of Atmospheric and Oceanic Technology*, 2005; pp. 1531-1540; NREL Report No. JA-560-36646. doi:10.1175/JTECH1782.1
- [2] Reda, I.; Myers, D.; Stoffel, T. (2008). "Uncertainty Estimate for the Outdoor Calibration of Solar Pyranometers: A Metrologist Perspective." *Measure*. (NCSLI Journal of Measurement Science). Vol. 3(4), December 2008; pp. 58-66; NREL Report No. JA-581-4137
- [3] Reda, I.; Andreas, A. (2004). "Solar Position Algorithm for Solar Radiation Applications." *Solar Energy*. Vol. 76(5), 2004; pp. 577-589; NREL Report No. JA-560-35518. doi:10.1016/j.solener.2003.12.003
- [4] Stoffel, T.; Reda, I. (2009). "NREL Pyrheliometer Comparisons: 22 September - 3 October 2008 (NPC-2008)." 54 pp.; NREL Report No. TP-550-45016.
- [5] Reda, I.; Stoffel, T.; Myers, D. (2003). "Method to Calibrate a Solar Pyranometer for Measuring Reference Diffuse Irradiance." *Solar Energy*. Vol. 74, 2003; pp. 103-112; NREL Report No. JA-560-35025. doi:10.1016/S0038-092X(03)00124-5
- [6] Reda, I. (1996). Calibration of a Solar Absolute Cavity Radiometer with Traceability to the World Radiometric Reference. 79 pp.; NREL Report No. TP-463-20619.
- [7] Reda, I.; Gröbner, J.; Stoffel, T.; Myers, D.; Forgan, B. (2008). Improvements in the Blackbody Calibration of Pyrgometers. ARM 2008 Science Team Meeting (Poster).

National Renewable Energy Laboratory

Solar Radiation Research Laboratory

Metrology Laboratory

Calibration Certificate



Test Instrument: Silicon Pyranometer **Manufacturer:** Kipp & Zonen
Model: SP-LITE2 **Serial Number:** 151027
Calibration Date: 5/5/2020 **Due Date:** 5/5/2021
Customer: NREL-SRRL-BMS **Environmental Conditions:** see page 4
Test Dates: 5/4-5

This certifies that the above product was calibrated in compliance with ISO/IEC 17025:2017. Measurement uncertainties at the time of calibration are consistent with the Guide to the Expression of Uncertainty in Measurement (GUM) using Reda et al., 2008. All nominal values are traceable to the International System (SI) Units of Measurement.

No statement of compliance with specifications is made or implied on this certificate. However, the estimated uncertainties are the uncertainties of the calibration process; users must add other uncertainties that are relevant to their measuring system, environmental and sky conditions, outdoor set-up, and site location.

The Type-B Standard Uncertainty of using the responsivity at each even zenith angle is reported, and the Expanded Uncertainty of the calibration is reported using two methods:

1. The Expanded Uncertainty of using the responsivity at zenith angle = 45°, within the zenith angle range from 30.0° to 60.0°
2. The Expanded Uncertainty of using Spline Interpolating Functions for the responsivity versus zenith angle.

This certificate applies only to the item identified above and shall not be reproduced other than in full, without specific written approval from the calibration facility. Certificate without signature is not valid.

Table 1. Traceability

| Measurement Type | Instrument | Calibration Date | Calibration Due Date |
|----------------------|--|------------------|----------------------|
| Beam Irradiance † | Eppley Absolute Cavity Radiometer Model HF, S/N 29219 | 09/27/2019 | 09/27/2020 |
| Diffuse Irradiance † | Hukseflux Pyranometer Model SR25, S/N 2541 | 04/17/2020 | 04/17/2021 |
| Diffuse Irradiance † | Hukseflux Pyranometer Model SR25, S/N 2542 | 04/17/2020 | 04/17/2021 |
| Data Acquisition | NREL Data Acquisition System Model RAP-DAQ, S/N 2005-998 | 02/14/2019 | 02/14/2021 |
| Data Acquisition | NREL Data Acquisition System Model RAP-DAQ, S/N 2005-999 | 02/14/2019 | 02/14/2021 |

† Through the World Radiometric Reference (WRR)

Number of pages of certificate: 4

Calibration Procedure: BORCAL-P00-Calibration and QA Procedure; available upon request.

Setup: Radiometers are calibrated outdoors, using the sun as the source. Pyranometers and pyrgeometers are installed for horizontal measurements, with their signal connectors oriented north, if their design permits.
The shading disk for the reference diffuse subtends a solid angle of 5°. Pyrheliometers are installed on solar trackers.

Calibrated by: Afshin Andreas, Ibrahim Reda, Peter Gotseff, and RCC

Ibrahim Reda, Technical Manager

Date

For questions or comments, please contact the technical manager at:

ibrahim.reda@nrel.gov; 303-384-6385; 15013 Denver West Parkway, Golden, CO 80401, USA

Calibration Results

151027 Kipp & Zonen SP-LITE2

The responsivity (R , $\mu\text{V}/\text{W}/\text{m}^2$) of the test instrument during calibration is calculated using this Measurement Equation:

$$R = (V - R_{net} * W_{net}) / I \tag{1}$$

where,

- V = radiometer output voltage (microvolts),
 - R_{net} = radiometer net infrared responsivity ($\mu\text{V}/\text{W}/\text{m}^2$), see Table 4,
 - W_{net} = effective net infrared measured by pyrgeometer (W/m^2),
 - = $W_{in} - W_{out} = W_{in} - \sigma * T_c^4$
 - where, W_{in} = incoming infrared (W/m^2), $\sigma = 5.6704\text{e-}8 \text{ W}\cdot\text{m}^{-2}\cdot\text{K}^{-4}$,
 - T_c = case temperature of pyrgeometer (K).
- I = reference irradiance (W/m^2), beam (B) or global (G)
 - where, $G = B * \text{COS}(Z) + D$,
 - Z = zenith angle (degrees),
 - D = reference diffuse irradiance (W/m^2).

Figure 1. Responsivity vs Zenith Angle

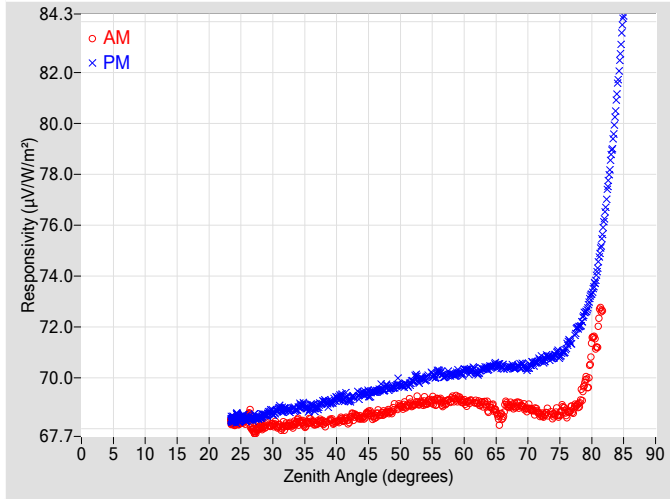


Figure 2. Responsivity vs Local Standard Time

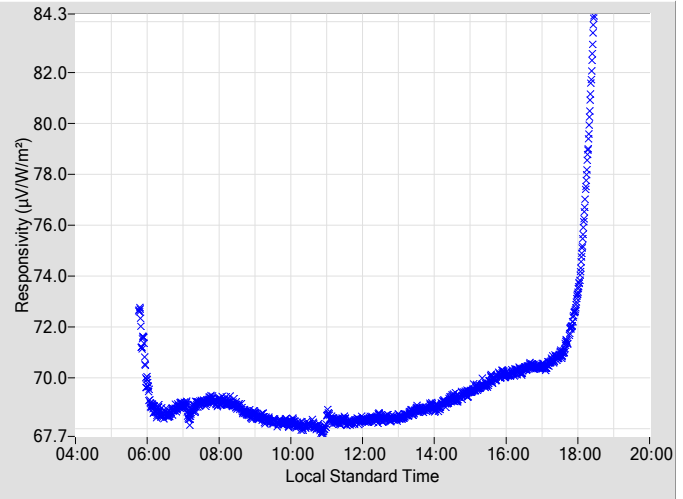


Table 2. Instrument Responsivity (R) and Calibration Type-B Standard Uncertainty, $u(B)$

| Zenith Angle (deg.) | R ($\mu\text{V}/\text{W}/\text{m}^2$) | AM $u(B)$ \pm (%) | Azimuth Angle | R ($\mu\text{V}/\text{W}/\text{m}^2$) | PM $u(B)$ \pm (%) | Azimuth Angle | Zenith Angle (deg.) | R ($\mu\text{V}/\text{W}/\text{m}^2$) | AM $u(B)$ \pm (%) | Azimuth Angle | R ($\mu\text{V}/\text{W}/\text{m}^2$) | PM $u(B)$ \pm (%) | Azimuth Angle |
|---------------------|---|---------------------|---------------|---|---------------------|---------------|---------------------|---|---------------------|---------------|---|---------------------|---------------|
| 0 | N/A | N/A | N/A | N/A | N/A | N/A | 46 | 68.489 | 0.31 | 106.77 | 69.468 | 0.32 | 252.82 |
| 2 | N/A | N/A | N/A | N/A | N/A | N/A | 48 | 68.673 | 0.31 | 104.55 | 69.632 | 0.32 | 255.08 |
| 4 | N/A | N/A | N/A | N/A | N/A | N/A | 50 | 68.911 | 0.33 | 102.41 | 69.711 | 0.33 | 257.23 |
| 6 | N/A | N/A | N/A | N/A | N/A | N/A | 52 | 68.917 | 0.35 | 100.38 | 69.911 | 0.32 | 259.29 |
| 8 | N/A | N/A | N/A | N/A | N/A | N/A | 54 | 68.967 | 0.32 | 98.40 | 69.970 | 0.32 | 261.22 |
| 10 | N/A | N/A | N/A | N/A | N/A | N/A | 56 | 69.158 | 0.36 | 96.58 | 70.254 | 0.33 | 263.10 |
| 12 | N/A | N/A | N/A | N/A | N/A | N/A | 58 | 69.159 | 0.38 | 94.75 | 70.143 | 0.33 | 264.91 |
| 14 | N/A | N/A | N/A | N/A | N/A | N/A | 60 | 69.064 | 0.34 | 93.05 | 70.272 | 0.34 | 266.67 |
| 16 | N/A | N/A | N/A | N/A | N/A | N/A | 62 | 69.040 | 0.35 | 91.35 | 70.182 | 0.35 | 268.39 |
| 18 | N/A | N/A | N/A | N/A | N/A | N/A | 64 | 68.799 | 0.36 | 89.68 | 70.423 | 0.36 | 270.09 |
| 20 | N/A | N/A | N/A | N/A | N/A | N/A | 66 | 68.519 | 0.40 | 88.03 | 70.429 | 0.38 | 271.72 |
| 22 | N/A | N/A | N/A | N/A | N/A | N/A | 68 | 68.899 | 0.39 | 86.42 | 70.381 | 0.40 | 273.36 |
| 24 | 68.261 | 0.31 | 167.32 | 68.399 | 0.31 | 193.01 | 70 | 68.809 | 0.42 | 84.82 | 70.398 | 0.42 | 274.99 |
| 26 | 68.421 | 0.32 | 151.05 | 68.378 | 0.31 | 209.06 | 72 | 68.551 | 0.45 | 83.18 | 70.735 | 0.45 | 276.60 |
| 28 | 68.082 | 0.33 | 140.91 | 68.458 | 0.31 | 218.07 | 74 | 68.520 | 0.49 | 81.61 | 70.834 | 0.49 | 278.20 |
| 30 | 68.150 | 0.31 | 134.42 | 68.628 | 0.29 | 224.61 | 76 | 68.588 | 0.54 | 79.99 | 71.226 | 0.55 | 279.83 |
| 32 | 68.103 | 0.30 | 129.21 | 68.773 | 0.32 | 230.02 | 78 | 68.965 | 0.61 | 78.39 | 72.009 | N/A | 281.44 |
| 34 | 68.293 | 0.31 | 124.83 | 68.853 | 0.32 | 234.61 | 80 | 71.249 | N/A | 76.74 | 73.377 | N/A | 283.09 |
| 36 | 68.311 | 0.31 | 121.06 | 68.887 | 0.31 | 238.40 | 82 | N/A | N/A | N/A | 76.425 | N/A | 284.73 |
| 38 | 68.209 | 0.31 | 117.65 | 69.082 | 0.31 | 241.82 | 84 | N/A | N/A | N/A | 81.323 | N/A | 286.39 |
| 40 | 68.292 | 0.32 | 114.46 | 69.207 | 0.33 | 244.99 | 86 | N/A | N/A | N/A | N/A | N/A | N/A |
| 42 | 68.341 | 0.31 | 111.82 | 69.110 | 0.33 | 247.81 | 88 | N/A | N/A | N/A | N/A | N/A | N/A |
| 44 | 68.421 | 0.30 | 109.15 | 69.384 | 0.36 | 250.45 | 90 | N/A | N/A | N/A | N/A | N/A | N/A |

N/A - Not Available

Figure 3. Type-B Standard Uncertainty vs Zenith Angle

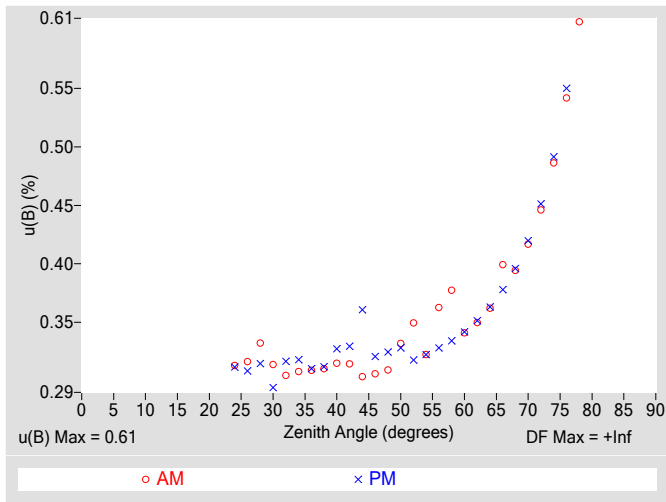


Figure 4. Residuals from Spline Interpolation

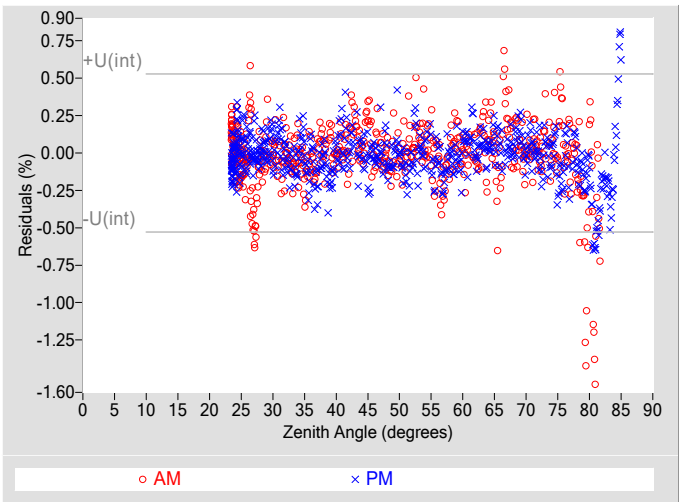


Table 3. Uncertainty using Spline Interpolation ‡

| | |
|---|------------|
| Type-B Standard Uncertainty, $u(B)$ (%) | ± 0.61 |
| Type-A Interpolating Function, $u(int)$ (%) | ± 0.26 |
| Combined Standard Uncertainty, $u(c)$ (%) | ± 0.66 |
| Effective degrees of freedom, $DF(c)$ | 45325 |
| Coverage factor, k | 1.96 |
| Expanded Uncertainty, $U95$ (%) | ± 1.3 |
| AM Valid zenith angle range | 24° to 78° |
| PM Valid zenith angle range | 24° to 76° |

‡ An illustration for how to reduce the uncertainty in calculating the irradiance using a function rather than $R@45^\circ$. Not accredited.

Table 4. Calibration Label Values

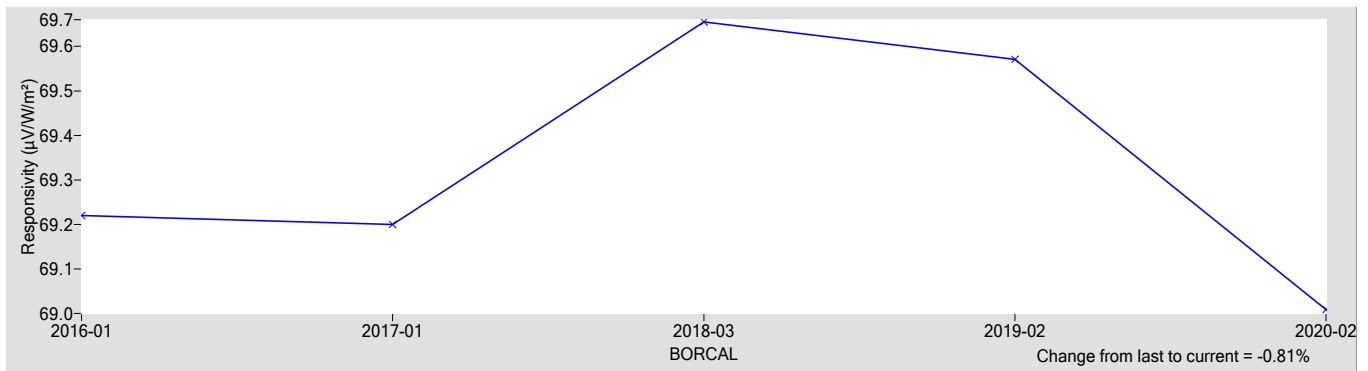
| | |
|----------------------------------|-------------------------------|
| $R @ 45^\circ$ ($\mu V/W/m^2$) | R_{net} ($\mu V/W/m^2$) † |
| 69.009 | 0 |

† R_{net} determination date: N/A

Table 5. Uncertainty using $R @ 45^\circ$

| | |
|---|----------------|
| Type-B Expanded Uncertainty, $U(B)$ (%) | ± 0.74 |
| Offset Uncertainty, $U(off)$ (%) | +1.8 / -1.3 |
| Expanded Uncertainty, U (%) | +2.6 / -2.1 |
| Effective degrees of freedom, DF | +Inf |
| Coverage factor, k | 1.96 |
| Valid zenith angle range | 30.0° to 60.0° |

Figure 5. History of instrument at Zenith Angle = 45°



References:

[1] Reda, I.; Hickey, J.; Long, C.; Myers, D.; Stoffel, T.; Wilcox, S.; Michalsky, J. J.; Dutton, E. G.; Nelson, D. (2005). "Using a Blackbody to Calculate Net Longwave Responsivity of Shortwave Solar Pyranometers to Correct for Their Thermal Offset Error During Outdoor Calibration Using the Component Sum Method." *Journal of Atmospheric and Oceanic Technology*, 2005; pp. 1531-1540; NREL Report No. JA-560-36646. doi:10.1175/JTECH1782.1

[2] Reda, I.; Myers, D.; Stoffel, T. (2008). "Uncertainty Estimate for the Outdoor Calibration of Solar Pyranometers: A Metrologist Perspective." *Measure*. (NCSLI Journal of Measurement Science). Vol. 3(4), December 2008; pp. 58-66; NREL Report No. JA-581-4137

[3] Reda, I.; Andreas, A. (2004). "Solar Position Algorithm for Solar Radiation Applications." *Solar Energy*. Vol. 76(5), 2004; pp. 577-589; NREL Report No. JA-560-35518. doi:10.1016/j.solener.2003.12.003

[4] Stoffel, T.; Reda, I. (2009). "NREL Pyrheliometer Comparisons: 22 September - 3 October 2008 (NPC-2008)." 54 pp.; NREL Report No. TP-550-45016.

[5] Reda, I.; Stoffel, T.; Myers, D. (2003). "Method to Calibrate a Solar Pyranometer for Measuring Reference Diffuse Irradiance." *Solar Energy*. Vol. 74, 2003; pp. 103-112; NREL Report No. JA-560-35025. doi:10.1016/S0038-092X(03)00124-5

[6] Reda, I. (1996). Calibration of a Solar Absolute Cavity Radiometer with Traceability to the World Radiometric Reference. 79 pp.; NREL Report No. TP-463-20619.

[7] Reda, I.; Gröbner, J.; Stoffel, T.; Myers, D.; Forgan, B. (2008). Improvements in the Blackbody Calibration of Pyrgometers. ARM 2008 Science Team Meeting (Poster).



National Renewable Energy Laboratory

Solar Radiation Research Laboratory

Metrology Laboratory

Calibration Certificate



| | | | |
|--------------------------|---------------|----------------------------------|--------------|
| Test Instrument: | Pyranometer | Manufacturer: | Kipp & Zonen |
| Model: | CMP22 | Serial Number: | 160430 |
| Calibration Date: | 5/5/2020 | Due Date: | 5/5/2021 |
| Customer: | NREL-SRRL-BMS | Environmental Conditions: | see page 4 |
| Test Dates: | 5/4-5 | | |

This certifies that the above product was calibrated in compliance with ISO/IEC 17025:2017. Measurement uncertainties at the time of calibration are consistent with the Guide to the Expression of Uncertainty in Measurement (GUM) using Reda et al., 2008. All nominal values are traceable to the International System (SI) Units of Measurement.

No statement of compliance with specifications is made or implied on this certificate. However, the estimated uncertainties are the uncertainties of the calibration process; users must add other uncertainties that are relevant to their measuring system, environmental and sky conditions, outdoor set-up, and site location.

The Type-B Standard Uncertainty of using the responsivity at each even zenith angle is reported, and the Expanded Uncertainty of the calibration is reported using two methods:

1. The Expanded Uncertainty of using the responsivity at zenith angle = 45°, within the zenith angle range from 30.0° to 60.0°
2. The Expanded Uncertainty of using Spline Interpolating Functions for the responsivity versus zenith angle.

This certificate applies only to the item identified above and shall not be reproduced other than in full, without specific written approval from the calibration facility. Certificate without signature is not valid.

Table 1. Traceability

| Measurement Type | Instrument | Calibration Date | Calibration Due Date |
|-----------------------|--|------------------|----------------------|
| Beam Irradiance † | Eppley Absolute Cavity Radiometer Model HF, S/N 29219 | 09/27/2019 | 09/27/2020 |
| Diffuse Irradiance † | Hukseflux Pyranometer Model SR25, S/N 2541 | 04/17/2020 | 04/17/2021 |
| Diffuse Irradiance † | Hukseflux Pyranometer Model SR25, S/N 2542 | 04/17/2020 | 04/17/2021 |
| Data Acquisition | NREL Data Acquisition System Model RAP-DAQ, S/N 2005-998 | 02/14/2019 | 02/14/2021 |
| Data Acquisition | NREL Data Acquisition System Model RAP-DAQ, S/N 2005-999 | 02/14/2019 | 02/14/2021 |
| Infrared Irradiance ‡ | Kipp & Zonen Pyrgeometer Model CG4, S/N FT002 | 04/16/2018 | 04/16/2022 |

† Through the World Radiometric Reference (WRR)

‡ Through the World Infrared Standard Group (WISG)

Number of pages of certificate: 4

Calibration Procedure: BORCAL-P00-Calibration and QA Procedure; available upon request.

Setup: Radiometers are calibrated outdoors, using the sun as the source. Pyranometers and pyrgeometers are installed for horizontal measurements, with their signal connectors oriented north, if their design permits.

The shading disk for the reference diffuse subtends a solid angle of 5°. Pyrheliometers are installed on solar trackers.

Calibrated by: Afshin Andreas, Ibrahim Reda, Peter Gotseff, and RCC

Ibrahim Reda, Technical Manager

Date

For questions or comments, please contact the technical manager at:

ibrahim.reda@nrel.gov; 303-384-6385; 15013 Denver West Parkway, Golden, CO 80401, USA

Calibration Results

160430 Kipp & Zonen CMP22

The responsivity (R , $\mu\text{V}/\text{W}/\text{m}^2$) of the test instrument during calibration is calculated using this Measurement Equation:

$$R = (V - R_{net} * W_{net}) / I \tag{1}$$

where,

- V = radiometer output voltage (microvolts),
 - R_{net} = radiometer net infrared responsivity ($\mu\text{V}/\text{W}/\text{m}^2$), see Table 4,
 - W_{net} = effective net infrared measured by pyrgeometer (W/m^2),
 - = $W_{in} - W_{out} = W_{in} - \sigma * T_c^4$
 - where, W_{in} = incoming infrared (W/m^2), $\sigma = 5.6704\text{e-}8 \text{ W}\cdot\text{m}^{-2}\cdot\text{K}^{-4}$,
 - T_c = case temperature of pyrgeometer (K).
- I = reference irradiance (W/m^2), beam (B) or global (G)
 - where, $G = B * \text{COS}(Z) + D$,
 - Z = zenith angle (degrees),
 - D = reference diffuse irradiance (W/m^2).

Figure 1. Responsivity vs Zenith Angle

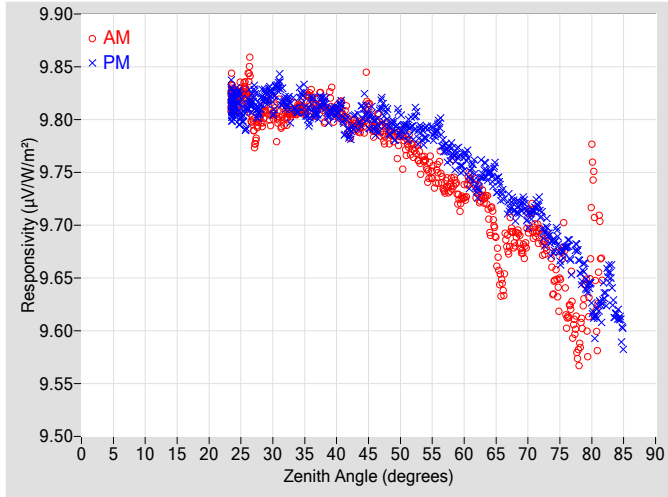


Figure 2. Responsivity vs Local Standard Time

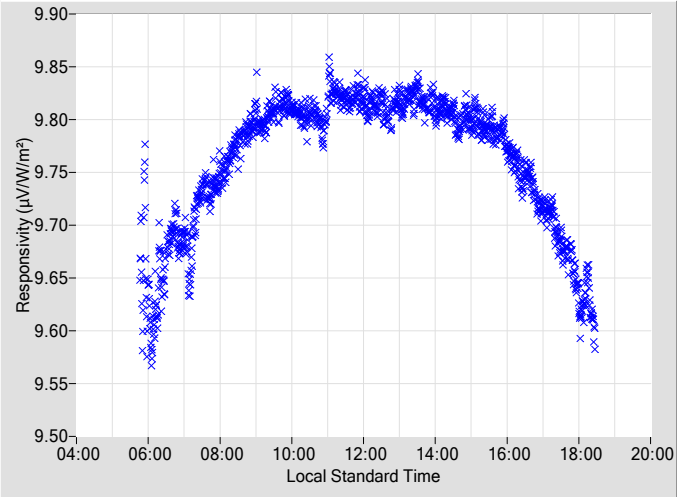


Table 2. Instrument Responsivity (R) and Calibration Type-B Standard Uncertainty, u(B)

| Zenith | | | AM | | | PM | | | Zenith | | | AM | | | PM | | |
|--------|---------------------------------------|-------|---------|---------------------------------------|-------|---------|--------|---------------------------------------|--------|---------|---------------------------------------|-------|---------|---------------------------------------|-------|---------|--|
| Angle | R | u(B) | Azimuth | R | u(B) | Azimuth | Angle | R | u(B) | Azimuth | R | u(B) | Azimuth | R | u(B) | Azimuth | |
| (deg.) | ($\mu\text{V}/\text{W}/\text{m}^2$) | ± (%) | Angle | ($\mu\text{V}/\text{W}/\text{m}^2$) | ± (%) | Angle | (deg.) | ($\mu\text{V}/\text{W}/\text{m}^2$) | ± (%) | Angle | ($\mu\text{V}/\text{W}/\text{m}^2$) | ± (%) | Angle | ($\mu\text{V}/\text{W}/\text{m}^2$) | ± (%) | Angle | |
| 0 | N/A | N/A | N/A | N/A | N/A | N/A | 46 | 9.7905 | 0.32 | 106.77 | 9.7931 | 0.31 | 252.83 | | | | |
| 2 | N/A | N/A | N/A | N/A | N/A | N/A | 48 | 9.7900 | 0.33 | 104.56 | 9.7994 | 0.31 | 255.08 | | | | |
| 4 | N/A | N/A | N/A | N/A | N/A | N/A | 50 | 9.7841 | 0.36 | 102.42 | 9.7911 | 0.32 | 257.24 | | | | |
| 6 | N/A | N/A | N/A | N/A | N/A | N/A | 52 | 9.7707 | 0.34 | 100.41 | 9.7924 | 0.32 | 259.30 | | | | |
| 8 | N/A | N/A | N/A | N/A | N/A | N/A | 54 | 9.7560 | 0.36 | 98.46 | 9.7874 | 0.36 | 261.23 | | | | |
| 10 | N/A | N/A | N/A | N/A | N/A | N/A | 56 | 9.7555 | 0.37 | 96.59 | 9.7957 | 0.35 | 263.11 | | | | |
| 12 | N/A | N/A | N/A | N/A | N/A | N/A | 58 | 9.7369 | 0.34 | 94.85 | 9.7691 | 0.34 | 264.92 | | | | |
| 14 | N/A | N/A | N/A | N/A | N/A | N/A | 60 | 9.7280 | 0.34 | 93.06 | 9.7625 | 0.35 | 266.68 | | | | |
| 16 | N/A | N/A | N/A | N/A | N/A | N/A | 62 | 9.7327 | 0.35 | 91.36 | 9.7328 | 0.36 | 268.40 | | | | |
| 18 | N/A | N/A | N/A | N/A | N/A | N/A | 64 | 9.7041 | 0.39 | 89.68 | 9.7493 | 0.37 | 270.10 | | | | |
| 20 | N/A | N/A | N/A | N/A | N/A | N/A | 66 | 9.6396 | 0.41 | 88.04 | 9.7283 | 0.38 | 271.68 | | | | |
| 22 | N/A | N/A | N/A | N/A | N/A | N/A | 68 | 9.6849 | 0.40 | 86.43 | 9.7132 | 0.40 | 273.37 | | | | |
| 24 | 9.8191 | 0.30 | 166.91 | 9.8157 | 0.32 | 193.10 | 70 | 9.6984 | 0.42 | 84.78 | 9.7061 | 0.43 | 274.99 | | | | |
| 26 | 9.8282 | 0.30 | 150.93 | 9.8076 | 0.32 | 209.14 | 72 | 9.6895 | 0.45 | 83.19 | 9.7109 | 0.46 | 276.60 | | | | |
| 28 | 9.8013 | 0.35 | 140.83 | 9.8149 | 0.32 | 218.09 | 74 | 9.6449 | 0.54 | 81.61 | 9.6811 | 0.50 | 278.21 | | | | |
| 30 | 9.8085 | 0.32 | 134.32 | 9.8174 | 0.31 | 224.63 | 76 | 9.6268 | 0.55 | 80.00 | 9.6805 | 0.56 | 279.80 | | | | |
| 32 | 9.8037 | 0.31 | 129.23 | 9.8158 | 0.33 | 230.08 | 78 | 9.5790 | 0.63 | 78.39 | 9.6657 | N/A | 281.41 | | | | |
| 34 | 9.8103 | 0.30 | 124.85 | 9.8131 | 0.32 | 234.51 | 80 | 9.7189 | N/A | 76.79 | 9.6272 | N/A | 283.05 | | | | |
| 36 | 9.8183 | 0.31 | 121.02 | 9.8120 | 0.33 | 238.42 | 82 | N/A | N/A | N/A | 9.6336 | N/A | 284.70 | | | | |
| 38 | 9.8056 | 0.32 | 117.58 | 9.8174 | 0.34 | 241.91 | 84 | N/A | N/A | N/A | 9.6153 | N/A | 286.35 | | | | |
| 40 | 9.8083 | 0.31 | 114.59 | 9.8063 | 0.33 | 244.94 | 86 | N/A | N/A | N/A | N/A | N/A | N/A | | | | |
| 42 | 9.7903 | 0.32 | 111.76 | 9.7860 | 0.32 | 247.75 | 88 | N/A | N/A | N/A | N/A | N/A | N/A | | | | |
| 44 | 9.7947 | 0.31 | 109.22 | 9.8061 | 0.32 | 250.35 | 90 | N/A | N/A | N/A | N/A | N/A | N/A | | | | |

N/A - Not Available

Figure 3. Type-B Standard Uncertainty vs Zenith Angle

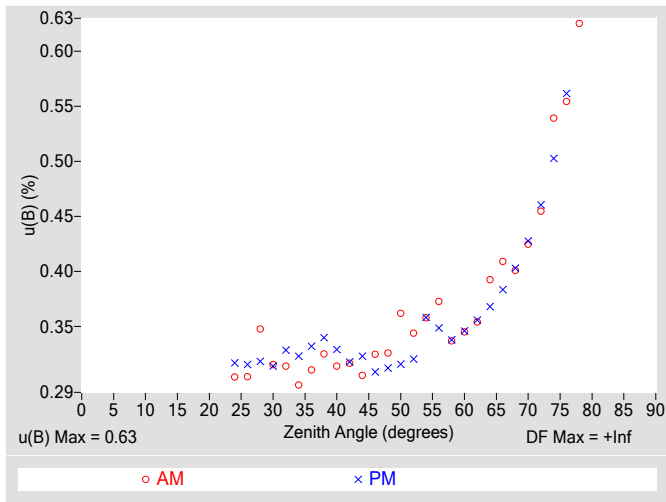


Figure 4. Residuals from Spline Interpolation

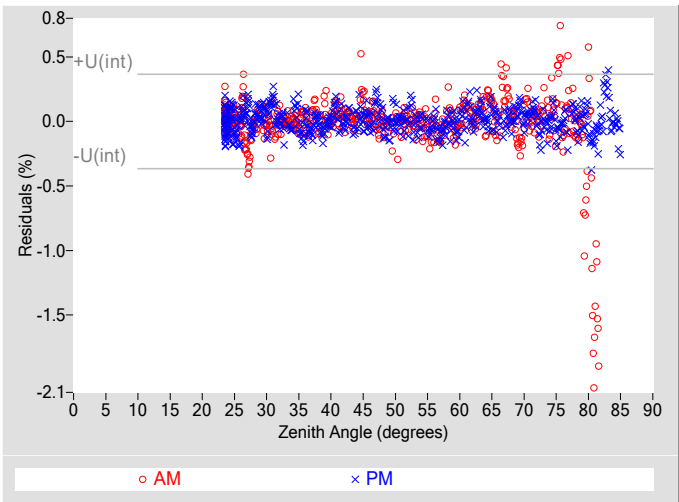


Table 3. Uncertainty using Spline Interpolation ‡

| | |
|---|------------|
| Type-B Standard Uncertainty, $u(B)$ (%) | ± 0.63 |
| Type-A Interpolating Function, $u(int)$ (%) | ± 0.18 |
| Combined Standard Uncertainty, $u(c)$ (%) | ± 0.65 |
| Effective degrees of freedom, $DF(c)$ | 183648 |
| Coverage factor, k | 1.96 |
| Expanded Uncertainty, $U95$ (%) | ± 1.3 |
| AM Valid zenith angle range | 24° to 78° |
| PM Valid zenith angle range | 24° to 76° |

‡ An illustration for how to reduce the uncertainty in calculating the irradiance using a function rather than $R@45^\circ$. Not accredited.

Table 4. Calibration Label Values

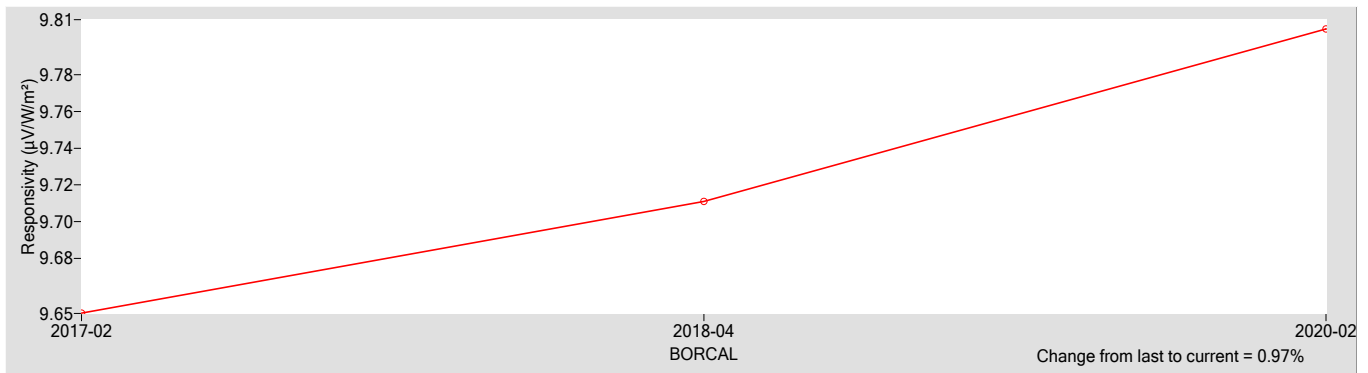
| | |
|----------------------------------|-------------------------------|
| $R @ 45^\circ$ ($\mu V/W/m^2$) | R_{net} ($\mu V/W/m^2$) † |
| 9.8050 | 0.087000 |

† R_{net} determination date: Estimated

Table 5. Uncertainty using $R @ 45^\circ$

| | |
|---|----------------|
| Type-B Expanded Uncertainty, $U(B)$ (%) | ± 0.73 |
| Offset Uncertainty, $U(off)$ (%) | +0.14 / -0.79 |
| Expanded Uncertainty, U (%) | +0.87 / -1.5 |
| Effective degrees of freedom, DF | +Inf |
| Coverage factor, k | 1.96 |
| Valid zenith angle range | 30.0° to 60.0° |

Figure 5. History of instrument at Zenith Angle = 45°



References:

- [1] Reda, I.; Hickey, J.; Long, C.; Myers, D.; Stoffel, T.; Wilcox, S.; Michalsky, J. J.; Dutton, E. G.; Nelson, D. (2005). "Using a Blackbody to Calculate Net Longwave Responsivity of Shortwave Solar Pyranometers to Correct for Their Thermal Offset Error During Outdoor Calibration Using the Component Sum Method." *Journal of Atmospheric and Oceanic Technology*, 2005; pp. 1531-1540; NREL Report No. JA-560-36646. doi:10.1175/JTECH1782.1
- [2] Reda, I.; Myers, D.; Stoffel, T. (2008). "Uncertainty Estimate for the Outdoor Calibration of Solar Pyranometers: A Metrologist Perspective." *Measure*. (NCSLI Journal of Measurement Science). Vol. 3(4), December 2008; pp. 58-66; NREL Report No. JA-581-4137
- [3] Reda, I.; Andreas, A. (2004). "Solar Position Algorithm for Solar Radiation Applications." *Solar Energy*. Vol. 76(5), 2004; pp. 577-589; NREL Report No. JA-560-35518. doi:10.1016/j.solener.2003.12.003
- [4] Stoffel, T.; Reda, I. (2009). "NREL Pyrheliometer Comparisons: 22 September - 3 October 2008 (NPC-2008)." 54 pp.; NREL Report No. TP-550-45016.
- [5] Reda, I.; Stoffel, T.; Myers, D. (2003). "Method to Calibrate a Solar Pyranometer for Measuring Reference Diffuse Irradiance." *Solar Energy*. Vol. 74, 2003; pp. 103-112; NREL Report No. JA-560-35025. doi:10.1016/S0038-092X(03)00124-5
- [6] Reda, I. (1996). Calibration of a Solar Absolute Cavity Radiometer with Traceability to the World Radiometric Reference. 79 pp.; NREL Report No. TP-463-20619.
- [7] Reda, I.; Gröbner, J.; Stoffel, T.; Myers, D.; Forgan, B. (2008). Improvements in the Blackbody Calibration of Pyrgometers. ARM 2008 Science Team Meeting (Poster).



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Calibration Certificate



| | | | |
|--------------------------|---------------------|----------------------------------|--------------|
| Test Instrument: | Silicon Pyranometer | Manufacturer: | Kipp & Zonen |
| Model: | SP-LITE2 | Serial Number: | 194362 |
| Calibration Date: | 5/5/2020 | Due Date: | 5/5/2021 |
| Customer: | NREL-SRRL-BMS | Environmental Conditions: | see page 4 |
| Test Dates: | 5/4-5 | | |

This certifies that the above product was calibrated in compliance with ISO/IEC 17025:2017. Measurement uncertainties at the time of calibration are consistent with the Guide to the Expression of Uncertainty in Measurement (GUM) using Reda et al., 2008. All nominal values are traceable to the International System (SI) Units of Measurement.

No statement of compliance with specifications is made or implied on this certificate. However, the estimated uncertainties are the uncertainties of the calibration process; users must add other uncertainties that are relevant to their measuring system, environmental and sky conditions, outdoor set-up, and site location.

The Type-B Standard Uncertainty of using the responsivity at each even zenith angle is reported, and the Expanded Uncertainty of the calibration is reported using two methods:

1. The Expanded Uncertainty of using the responsivity at zenith angle = 45°, within the zenith angle range from 30.0° to 60.0°
2. The Expanded Uncertainty of using Spline Interpolating Functions for the responsivity versus zenith angle.

This certificate applies only to the item identified above and shall not be reproduced other than in full, without specific written approval from the calibration facility. Certificate without signature is not valid.

Table 1. Traceability

| Measurement Type | Instrument | Calibration Date | Calibration Due Date |
|----------------------|--|------------------|----------------------|
| Beam Irradiance † | Eppley Absolute Cavity Radiometer Model HF, S/N 29219 | 09/27/2019 | 09/27/2020 |
| Diffuse Irradiance † | Hukseflux Pyranometer Model SR25, S/N 2541 | 04/17/2020 | 04/17/2021 |
| Diffuse Irradiance † | Hukseflux Pyranometer Model SR25, S/N 2542 | 04/17/2020 | 04/17/2021 |
| Data Acquisition | NREL Data Acquisition System Model RAP-DAQ, S/N 2005-998 | 02/14/2019 | 02/14/2021 |
| Data Acquisition | NREL Data Acquisition System Model RAP-DAQ, S/N 2005-999 | 02/14/2019 | 02/14/2021 |

† Through the World Radiometric Reference (WRR)

Number of pages of certificate: 4

Calibration Procedure: BORCAL-P00-Calibration and QA Procedure; available upon request.

Setup: Radiometers are calibrated outdoors, using the sun as the source. Pyranometers and pyrgeometers are installed for horizontal measurements, with their signal connectors oriented north, if their design permits.

The shading disk for the reference diffuse subtends a solid angle of 5°. Pyrheliometers are installed on solar trackers.

Calibrated by: Afshin Andreas, Ibrahim Reda, Peter Gotseff, and RCC

Ibrahim Reda, Technical Manager

Date

For questions or comments, please contact the technical manager at:

ibrahim.reda@nrel.gov; 303-384-6385; 15013 Denver West Parkway, Golden, CO 80401, USA

Calibration Results

194362 Kipp & Zonen SP-LITE2

The responsivity (R , $\mu\text{V}/\text{W}/\text{m}^2$) of the test instrument during calibration is calculated using this Measurement Equation:

$$R = (V - R_{net} * W_{net}) / I \tag{1}$$

where,

- V = radiometer output voltage (microvolts),
 - R_{net} = radiometer net infrared responsivity ($\mu\text{V}/\text{W}/\text{m}^2$), see Table 4,
 - W_{net} = effective net infrared measured by pyrgeometer (W/m^2),
 - = $W_{in} - W_{out} = W_{in} - \sigma * T_c^4$
 - where, W_{in} = incoming infrared (W/m^2), $\sigma = 5.6704\text{e-}8 \text{ W}\cdot\text{m}^{-2}\cdot\text{K}^{-4}$,
 - T_c = case temperature of pyrgeometer (K).
- I = reference irradiance (W/m^2), beam (B) or global (G)
 - where, $G = B * \text{COS}(Z) + D$,
 - Z = zenith angle (degrees),
 - D = reference diffuse irradiance (W/m^2).

Figure 1. Responsivity vs Zenith Angle

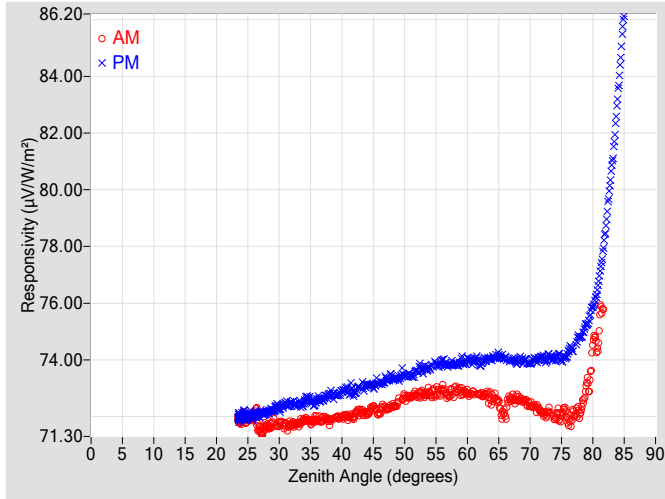


Figure 2. Responsivity vs Local Standard Time

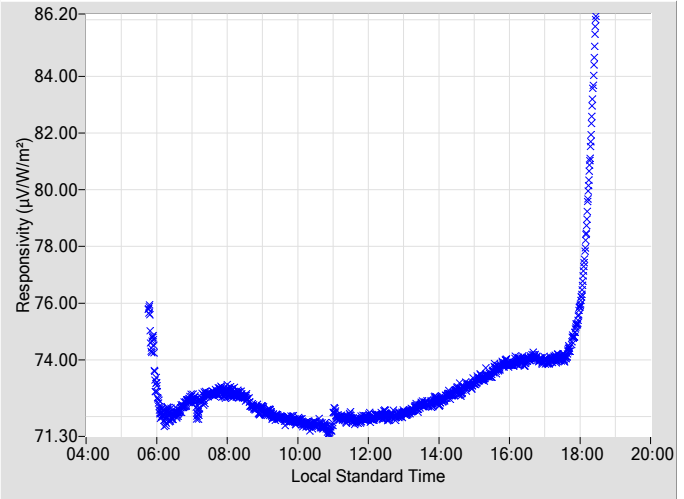


Table 2. Instrument Responsivity (R) and Calibration Type-B Standard Uncertainty, $u(B)$

| Zenith Angle (deg.) | R ($\mu\text{V}/\text{W}/\text{m}^2$) | AM $u(B)$ \pm (%) | Azimuth Angle | R ($\mu\text{V}/\text{W}/\text{m}^2$) | PM $u(B)$ \pm (%) | Azimuth Angle | Zenith Angle (deg.) | R ($\mu\text{V}/\text{W}/\text{m}^2$) | AM $u(B)$ \pm (%) | Azimuth Angle | R ($\mu\text{V}/\text{W}/\text{m}^2$) | PM $u(B)$ \pm (%) | Azimuth Angle |
|---------------------|---|---------------------|---------------|---|---------------------|---------------|---------------------|---|---------------------|---------------|---|---------------------|---------------|
| 0 | N/A | N/A | N/A | N/A | N/A | N/A | 46 | 72.165 | 0.31 | 106.77 | 73.182 | 0.32 | 252.82 |
| 2 | N/A | N/A | N/A | N/A | N/A | N/A | 48 | 72.364 | 0.31 | 104.55 | 73.400 | 0.32 | 255.08 |
| 4 | N/A | N/A | N/A | N/A | N/A | N/A | 50 | 72.678 | 0.33 | 102.41 | 73.455 | 0.33 | 257.23 |
| 6 | N/A | N/A | N/A | N/A | N/A | N/A | 52 | 72.745 | 0.35 | 100.38 | 73.628 | 0.32 | 259.29 |
| 8 | N/A | N/A | N/A | N/A | N/A | N/A | 54 | 72.849 | 0.34 | 98.45 | 73.733 | 0.32 | 261.22 |
| 10 | N/A | N/A | N/A | N/A | N/A | N/A | 56 | 72.969 | 0.36 | 96.58 | 73.973 | 0.33 | 263.10 |
| 12 | N/A | N/A | N/A | N/A | N/A | N/A | 58 | 72.902 | 0.38 | 94.75 | 73.852 | 0.33 | 264.91 |
| 14 | N/A | N/A | N/A | N/A | N/A | N/A | 60 | 72.820 | 0.34 | 93.05 | 73.995 | 0.34 | 266.67 |
| 16 | N/A | N/A | N/A | N/A | N/A | N/A | 62 | 72.792 | 0.35 | 91.35 | 73.859 | 0.35 | 268.39 |
| 18 | N/A | N/A | N/A | N/A | N/A | N/A | 64 | 72.595 | 0.36 | 89.68 | 74.067 | 0.36 | 270.09 |
| 20 | N/A | N/A | N/A | N/A | N/A | N/A | 66 | 72.118 | 0.40 | 88.03 | 74.047 | 0.38 | 271.72 |
| 22 | N/A | N/A | N/A | N/A | N/A | N/A | 68 | 72.653 | 0.39 | 86.42 | 73.904 | 0.40 | 273.36 |
| 24 | 71.872 | 0.31 | 167.32 | 72.025 | 0.31 | 193.01 | 70 | 72.441 | 0.42 | 84.82 | 73.887 | 0.42 | 274.99 |
| 26 | 72.022 | 0.32 | 151.05 | 72.006 | 0.31 | 209.06 | 72 | 72.114 | 0.45 | 83.18 | 74.091 | 0.45 | 276.60 |
| 28 | 71.674 | 0.33 | 140.91 | 72.142 | 0.31 | 218.07 | 74 | 71.968 | 0.49 | 81.61 | 74.062 | 0.49 | 278.20 |
| 30 | 71.720 | 0.31 | 134.42 | 72.274 | 0.29 | 224.61 | 76 | 71.868 | 0.54 | 79.99 | 74.245 | 0.55 | 279.83 |
| 32 | 71.723 | 0.30 | 129.21 | 72.477 | 0.32 | 230.02 | 78 | 72.156 | 0.61 | 78.39 | 74.804 | N/A | 281.44 |
| 34 | 71.895 | 0.31 | 124.83 | 72.540 | 0.32 | 234.61 | 80 | 74.459 | N/A | 76.74 | 75.930 | N/A | 283.09 |
| 36 | 71.908 | 0.31 | 121.06 | 72.588 | 0.31 | 238.40 | 82 | N/A | N/A | N/A | 78.677 | N/A | 284.73 |
| 38 | 71.844 | 0.31 | 117.65 | 72.793 | 0.31 | 241.82 | 84 | N/A | N/A | N/A | 83.342 | N/A | 286.39 |
| 40 | 71.987 | 0.31 | 114.46 | 72.884 | 0.33 | 244.99 | 86 | N/A | N/A | N/A | N/A | N/A | N/A |
| 42 | 72.013 | 0.31 | 111.82 | 72.820 | 0.33 | 247.81 | 88 | N/A | N/A | N/A | N/A | N/A | N/A |
| 44 | 72.095 | 0.30 | 109.15 | 73.113 | 0.36 | 250.45 | 90 | N/A | N/A | N/A | N/A | N/A | N/A |

N/A - Not Available

Figure 3. Type-B Standard Uncertainty vs Zenith Angle

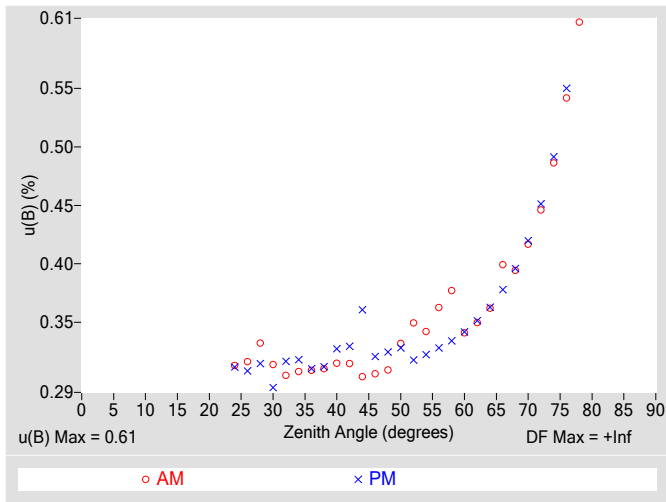


Figure 4. Residuals from Spline Interpolation

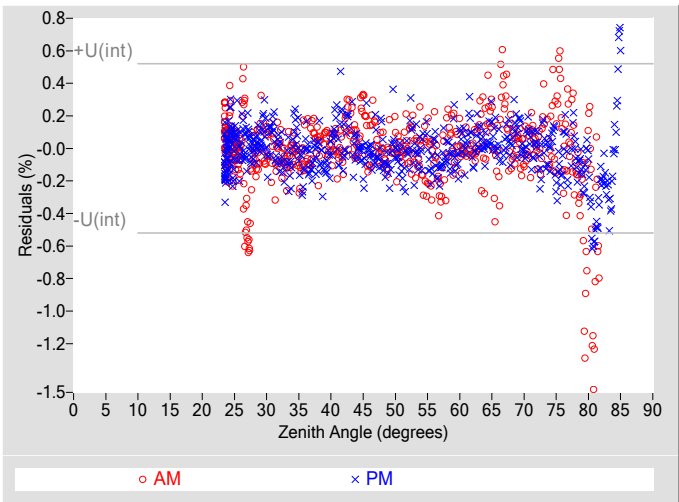


Table 3. Uncertainty using Spline Interpolation ‡

| | |
|---|------------|
| Type-B Standard Uncertainty, $u(B)$ (%) | ± 0.61 |
| Type-A Interpolating Function, $u(int)$ (%) | ± 0.26 |
| Combined Standard Uncertainty, $u(c)$ (%) | ± 0.66 |
| Effective degrees of freedom, $DF(c)$ | 47457 |
| Coverage factor, k | 1.96 |
| Expanded Uncertainty, U_{95} (%) | ± 1.3 |
| AM Valid zenith angle range | 24° to 78° |
| PM Valid zenith angle range | 24° to 76° |

‡ An illustration for how to reduce the uncertainty in calculating the irradiance using a function rather than $R@45^\circ$. Not accredited.

Table 4. Calibration Label Values

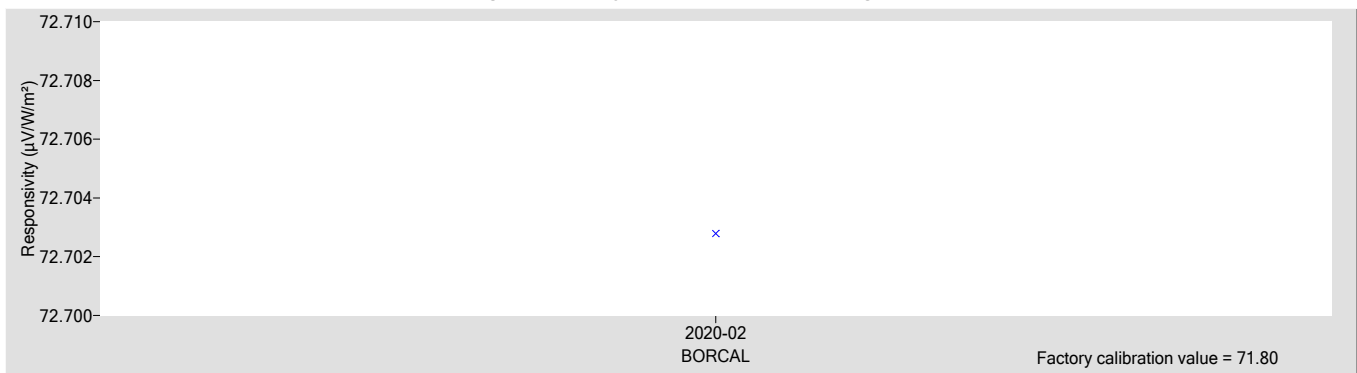
| | |
|----------------------------------|-------------------------------|
| $R @ 45^\circ$ ($\mu V/W/m^2$) | R_{net} ($\mu V/W/m^2$) † |
| 72.703 | 0 |

† R_{net} determination date: N/A

Table 5. Uncertainty using $R @ 45^\circ$

| | |
|---|----------------|
| Type-B Expanded Uncertainty, $U(B)$ (%) | ± 0.74 |
| Offset Uncertainty, $U(off)$ (%) | +1.8 / -1.4 |
| Expanded Uncertainty, U (%) | +2.5 / -2.1 |
| Effective degrees of freedom, DF | +Inf |
| Coverage factor, k | 1.96 |
| Valid zenith angle range | 30.0° to 60.0° |

Figure 5. History of instrument at Zenith Angle = 45°



References:

[1] Reda, I.; Hickey, J.; Long, C.; Myers, D.; Stoffel, T.; Wilcox, S.; Michalsky, J. J.; Dutton, E. G.; Nelson, D. (2005). "Using a Blackbody to Calculate Net Longwave Responsivity of Shortwave Solar Pyranometers to Correct for Their Thermal Offset Error During Outdoor Calibration Using the Component Sum Method." *Journal of Atmospheric and Oceanic Technology*, 2005; pp. 1531-1540; NREL Report No. JA-560-36646. doi:10.1175/JTECH1782.1

[2] Reda, I.; Myers, D.; Stoffel, T. (2008). "Uncertainty Estimate for the Outdoor Calibration of Solar Pyranometers: A Metrologist Perspective." *Measure*. (NCSLI Journal of Measurement Science). Vol. 3(4), December 2008; pp. 58-66; NREL Report No. JA-581-4137

[3] Reda, I.; Andreas, A. (2004). "Solar Position Algorithm for Solar Radiation Applications." *Solar Energy*. Vol. 76(5), 2004; pp. 577-589; NREL Report No. JA-560-35518. doi:10.1016/j.solener.2003.12.003

[4] Stoffel, T.; Reda, I. (2009). "NREL Pyrheliometer Comparisons: 22 September - 3 October 2008 (NPC-2008)." 54 pp.; NREL Report No. TP-550-45016.

[5] Reda, I.; Stoffel, T.; Myers, D. (2003). "Method to Calibrate a Solar Pyranometer for Measuring Reference Diffuse Irradiance." *Solar Energy*. Vol. 74, 2003; pp. 103-112; NREL Report No. JA-560-35025. doi:10.1016/S0038-092X(03)00124-5

[6] Reda, I. (1996). *Calibration of a Solar Absolute Cavity Radiometer with Traceability to the World Radiometric Reference*. 79 pp.; NREL Report No. TP-463-20619.

[7] Reda, I.; Gröbner, J.; Stoffel, T.; Myers, D.; Forgan, B. (2008). *Improvements in the Blackbody Calibration of Pyrgometers*. ARM 2008 Science Team Meeting (Poster).

National Renewable Energy Laboratory

Solar Radiation Research Laboratory

Metrology Laboratory

Calibration Certificate



Test Instrument: Black and White Pyranometer **Manufacturer:** Eppley
Model: 8-48 **Serial Number:** 21096
Calibration Date: 5/5/2020 **Due Date:** 5/5/2021
Customer: NREL-SRRL-BMS **Environmental Conditions:** see page 4
Test Dates: 5/4-5

This certifies that the above product was calibrated in compliance with ISO/IEC 17025:2017. Measurement uncertainties at the time of calibration are consistent with the Guide to the Expression of Uncertainty in Measurement (GUM) using Reda et al., 2008. All nominal values are traceable to the International System (SI) Units of Measurement.

No statement of compliance with specifications is made or implied on this certificate. However, the estimated uncertainties are the uncertainties of the calibration process; users must add other uncertainties that are relevant to their measuring system, environmental and sky conditions, outdoor set-up, and site location.

The Type-B Standard Uncertainty of using the responsivity at each even zenith angle is reported, and the Expanded Uncertainty of the calibration is reported using two methods:

1. The Expanded Uncertainty of using the responsivity at zenith angle = 45°, within the zenith angle range from 30.0° to 60.0°
2. The Expanded Uncertainty of using Spline Interpolating Functions for the responsivity versus zenith angle.

This certificate applies only to the item identified above and shall not be reproduced other than in full, without specific written approval from the calibration facility. Certificate without signature is not valid.

Table 1. Traceability

| Measurement Type | Instrument | Calibration Date | Calibration Due Date |
|----------------------|--|------------------|----------------------|
| Beam Irradiance † | Eppley Absolute Cavity Radiometer Model HF, S/N 29219 | 09/27/2019 | 09/27/2020 |
| Diffuse Irradiance † | Hukseflux Pyranometer Model SR25, S/N 2541 | 04/17/2020 | 04/17/2021 |
| Diffuse Irradiance † | Hukseflux Pyranometer Model SR25, S/N 2542 | 04/17/2020 | 04/17/2021 |
| Data Acquisition | NREL Data Acquisition System Model RAP-DAQ, S/N 2005-998 | 02/14/2019 | 02/14/2021 |
| Data Acquisition | NREL Data Acquisition System Model RAP-DAQ, S/N 2005-999 | 02/14/2019 | 02/14/2021 |

† Through the World Radiometric Reference (WRR)

Number of pages of certificate: 4

Calibration Procedure: BORCAL-P00-Calibration and QA Procedure; available upon request.

Setup: Radiometers are calibrated outdoors, using the sun as the source. Pyranometers and pyrgeometers are installed for horizontal measurements, with their signal connectors oriented north, if their design permits.
The shading disk for the reference diffuse subtends a solid angle of 5°. Pyrheliometers are installed on solar trackers.

Calibrated by: Afshin Andreas, Ibrahim Reda, Peter Gotseff, and RCC

Ibrahim Reda, Technical Manager

Date

For questions or comments, please contact the technical manager at:
ibrahim.reda@nrel.gov; 303-384-6385; 15013 Denver West Parkway, Golden, CO 80401, USA

Calibration Results

21096 Eppley 8-48

The responsivity (R , $\mu\text{V}/\text{W}/\text{m}^2$) of the test instrument during calibration is calculated using this Measurement Equation:

$$R = (V - R_{net} * W_{net}) / I \tag{1}$$

where,

- V = radiometer output voltage (microvolts),
 - R_{net} = radiometer net infrared responsivity ($\mu\text{V}/\text{W}/\text{m}^2$), see Table 4,
 - W_{net} = effective net infrared measured by pyrgeometer (W/m^2),
 - = $W_{in} - W_{out} = W_{in} - \sigma * T_c^4$
 - where, W_{in} = incoming infrared (W/m^2), $\sigma = 5.6704\text{e-}8 \text{ W}\cdot\text{m}^{-2}\cdot\text{K}^{-4}$,
 - T_c = case temperature of pyrgeometer (K).
- I = reference irradiance (W/m^2), beam (B) or global (G)
 - where, $G = B * \text{COS}(Z) + D$,
 - Z = zenith angle (degrees),
 - D = reference diffuse irradiance (W/m^2).

Figure 1. Responsivity vs Zenith Angle

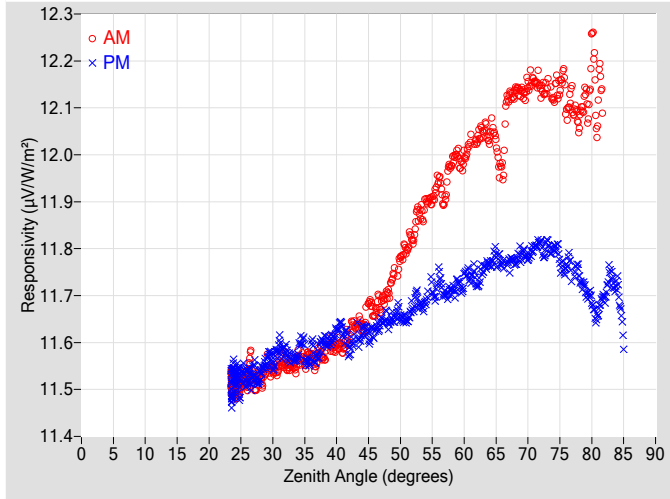


Figure 2. Responsivity vs Local Standard Time

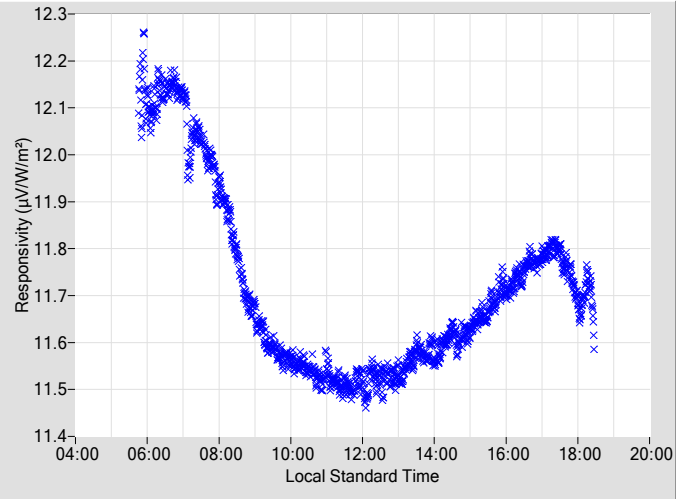


Table 2. Instrument Responsivity (R) and Calibration Type-B Standard Uncertainty, u(B)

| Zenith | | | AM | | | PM | | | Zenith | | | AM | | | PM | | |
|--------|---------------------------------------|-----------|---------|---------------------------------------|-----------|---------|--------|---------------------------------------|-----------|---------|---------------------------------------|-----------|---------|---------------------------------------|-----------|---------|--|
| Angle | R | u(B) | Azimuth | R | u(B) | Azimuth | Angle | R | u(B) | Azimuth | R | u(B) | Azimuth | R | u(B) | Azimuth | |
| (deg.) | ($\mu\text{V}/\text{W}/\text{m}^2$) | \pm (%) | Angle | ($\mu\text{V}/\text{W}/\text{m}^2$) | \pm (%) | Angle | (deg.) | ($\mu\text{V}/\text{W}/\text{m}^2$) | \pm (%) | Angle | ($\mu\text{V}/\text{W}/\text{m}^2$) | \pm (%) | Angle | ($\mu\text{V}/\text{W}/\text{m}^2$) | \pm (%) | Angle | |
| 0 | N/A | N/A | N/A | N/A | N/A | N/A | 46 | 11.663 | 0.31 | 106.75 | 11.623 | 0.31 | 252.80 | | | | |
| 2 | N/A | N/A | N/A | N/A | N/A | N/A | 48 | 11.705 | 0.33 | 104.53 | 11.649 | 0.33 | 255.06 | | | | |
| 4 | N/A | N/A | N/A | N/A | N/A | N/A | 50 | 11.776 | 0.33 | 102.45 | 11.656 | 0.33 | 257.21 | | | | |
| 6 | N/A | N/A | N/A | N/A | N/A | N/A | 52 | 11.819 | 0.36 | 100.42 | 11.678 | 0.35 | 259.28 | | | | |
| 8 | N/A | N/A | N/A | N/A | N/A | N/A | 54 | 11.898 | 0.32 | 98.48 | 11.692 | 0.32 | 261.26 | | | | |
| 10 | N/A | N/A | N/A | N/A | N/A | N/A | 56 | 11.948 | 0.35 | 96.62 | 11.738 | 0.35 | 263.14 | | | | |
| 12 | N/A | N/A | N/A | N/A | N/A | N/A | 58 | 11.980 | 0.34 | 94.78 | 11.712 | 0.34 | 264.90 | | | | |
| 14 | N/A | N/A | N/A | N/A | N/A | N/A | 60 | 11.990 | 0.36 | 93.04 | 11.735 | 0.36 | 266.71 | | | | |
| 16 | N/A | N/A | N/A | N/A | N/A | N/A | 62 | 12.034 | 0.35 | 91.34 | 11.725 | 0.35 | 268.38 | | | | |
| 18 | N/A | N/A | N/A | N/A | N/A | N/A | 64 | 12.042 | 0.36 | 89.67 | 11.767 | 0.37 | 270.08 | | | | |
| 20 | N/A | N/A | N/A | N/A | N/A | N/A | 66 | 11.974 | 0.40 | 88.02 | 11.767 | 0.38 | 271.71 | | | | |
| 22 | N/A | N/A | N/A | N/A | N/A | N/A | 68 | 12.134 | 0.40 | 86.41 | 11.772 | 0.40 | 273.39 | | | | |
| 24 | 11.506 | 0.30 | 167.09 | 11.531 | 0.31 | 192.86 | 70 | 12.147 | 0.42 | 84.81 | 11.781 | 0.42 | 274.97 | | | | |
| 26 | 11.517 | 0.30 | 151.01 | 11.528 | 0.32 | 209.19 | 72 | 12.140 | 0.45 | 83.22 | 11.812 | 0.46 | 276.59 | | | | |
| 28 | 11.528 | 0.30 | 140.77 | 11.529 | 0.30 | 218.16 | 74 | 12.123 | 0.53 | 81.60 | 11.800 | 0.50 | 278.19 | | | | |
| 30 | 11.544 | 0.32 | 134.47 | 11.554 | 0.31 | 224.70 | 76 | 12.112 | 0.55 | 80.02 | 11.762 | 0.56 | 279.82 | | | | |
| 32 | 11.556 | 0.33 | 129.19 | 11.584 | 0.32 | 230.03 | 78 | 12.071 | 0.76 | 78.38 | 11.744 | N/A | 281.43 | | | | |
| 34 | 11.568 | 0.33 | 124.80 | 11.581 | 0.32 | 234.59 | 80 | 12.218 | N/A | 76.73 | 11.687 | N/A | 283.08 | | | | |
| 36 | 11.574 | 0.32 | 120.95 | 11.587 | 0.31 | 238.50 | 82 | N/A | N/A | N/A | 11.698 | N/A | 284.72 | | | | |
| 38 | 11.565 | 0.32 | 117.63 | 11.602 | 0.31 | 241.88 | 84 | N/A | N/A | N/A | 11.721 | N/A | 286.38 | | | | |
| 40 | 11.594 | 0.31 | 114.48 | 11.626 | 0.32 | 244.93 | 86 | N/A | N/A | N/A | N/A | N/A | N/A | | | | |
| 42 | 11.603 | 0.32 | 111.80 | 11.581 | 0.30 | 247.79 | 88 | N/A | N/A | N/A | N/A | N/A | N/A | | | | |
| 44 | 11.631 | 0.30 | 109.14 | 11.623 | 0.31 | 250.43 | 90 | N/A | N/A | N/A | N/A | N/A | N/A | | | | |

N/A - Not Available

Figure 3. Type-B Standard Uncertainty vs Zenith Angle

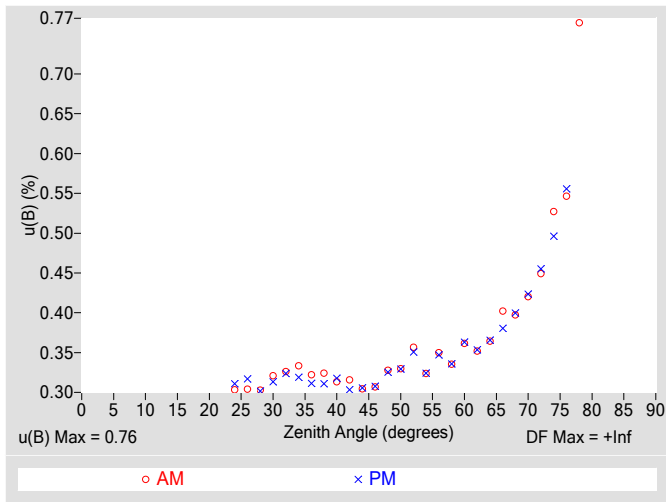


Figure 4. Residuals from Spline Interpolation

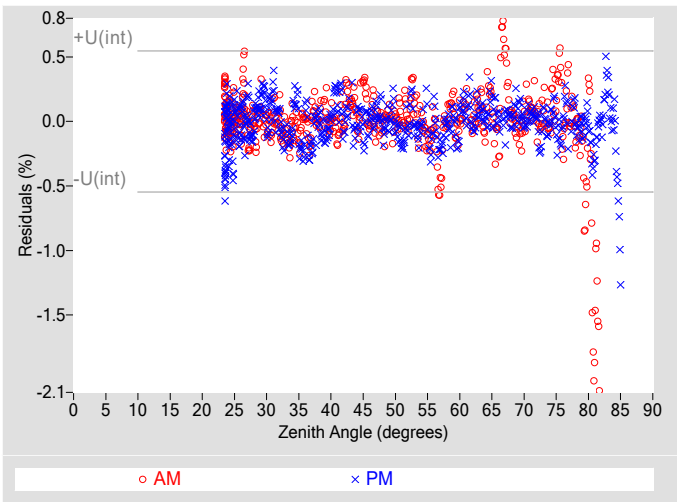


Table 3. Uncertainty using Spline Interpolation ‡

| | |
|---|------------|
| Type-B Standard Uncertainty, u(B) (%) | ±0.76 |
| Type-A Interpolating Function, u(int) (%) | ±0.27 |
| Combined Standard Uncertainty, u(c) (%) | ±0.81 |
| Effective degrees of freedom, DF(c) | 89560 |
| Coverage factor, k | 1.96 |
| Expanded Uncertainty, U95 (%) | ±1.6 |
| AM Valid zenith angle range | 24° to 78° |
| PM Valid zenith angle range | 24° to 76° |

‡ An illustration for how to reduce the uncertainty in calculating the irradiance using a function rather than R@45°. Not accredited.

Table 4. Calibration Label Values

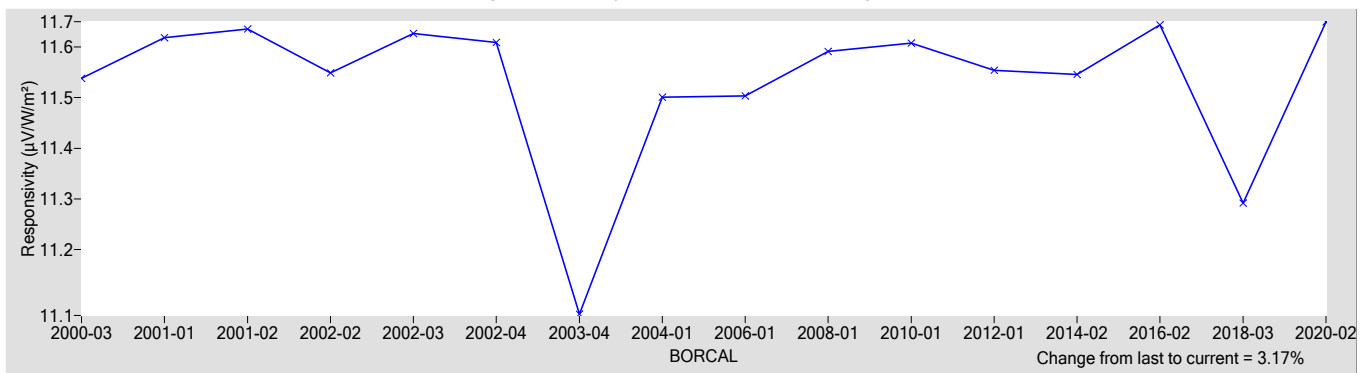
| | |
|-------------------|------------------|
| R @ 45° (μV/W/m²) | Rnet (μV/W/m²) † |
| 11.649 | 0 |

† Rnet determination date: N/A

Table 5. Uncertainty using R @ 45°

| | |
|---------------------------------------|----------------|
| Type-B Expanded Uncertainty, U(B) (%) | ±0.71 |
| Offset Uncertainty, U(off) (%) | +2.9 / -0.90 |
| Expanded Uncertainty, U (%) | +3.6 / -1.6 |
| Effective degrees of freedom, DF | +Inf |
| Coverage factor, k | 1.96 |
| Valid zenith angle range | 30.0° to 60.0° |

Figure 5. History of instrument at Zenith Angle = 45°



References:

[1] Reda, I.; Hickey, J.; Long, C.; Myers, D.; Stoffel, T.; Wilcox, S.; Michalsky, J. J.; Dutton, E. G.; Nelson, D. (2005). "Using a Blackbody to Calculate Net Longwave Responsivity of Shortwave Solar Pyranometers to Correct for Their Thermal Offset Error During Outdoor Calibration Using the Component Sum Method." *Journal of Atmospheric and Oceanic Technology*, 2005; pp. 1531-1540; NREL Report No. JA-560-36646. doi:10.1175/JTECH1782.1

[2] Reda, I.; Myers, D.; Stoffel, T. (2008). "Uncertainty Estimate for the Outdoor Calibration of Solar Pyranometers: A Metrologist Perspective." *Measure*. (NCSLI Journal of Measurement Science). Vol. 3(4), December 2008; pp. 58-66; NREL Report No. JA-581-4137

[3] Reda, I.; Andreas, A. (2004). "Solar Position Algorithm for Solar Radiation Applications." *Solar Energy*. Vol. 76(5), 2004; pp. 577-589; NREL Report No. JA-560-35518. doi:10.1016/j.solener.2003.12.003

[4] Stoffel, T.; Reda, I. (2009). "NREL Pyrheliometer Comparisons: 22 September - 3 October 2008 (NPC-2008)." 54 pp.; NREL Report No. TP-550-45016.

[5] Reda, I.; Stoffel, T.; Myers, D. (2003). "Method to Calibrate a Solar Pyranometer for Measuring Reference Diffuse Irradiance." *Solar Energy*. Vol. 74, 2003; pp. 103-112; NREL Report No. JA-560-35025. doi:10.1016/S0038-092X(03)00124-5

[6] Reda, I. (1996). *Calibration of a Solar Absolute Cavity Radiometer with Traceability to the World Radiometric Reference*. 79 pp.; NREL Report No. TP-463-20619.

[7] Reda, I.; Gröbner, J.; Stoffel, T.; Myers, D.; Forgan, B. (2008). *Improvements in the Blackbody Calibration of Pyrgometers*. ARM 2008 Science Team Meeting (Poster).



National Renewable Energy Laboratory

Solar Radiation Research Laboratory

Metrology Laboratory

Calibration Certificate



| | | | |
|--------------------------|---------------|----------------------------------|------------|
| Test Instrument: | Pyranometer | Manufacturer: | Hukseflux |
| Model: | SR25 | Serial Number: | 2530 |
| Calibration Date: | 5/5/2020 | Due Date: | 5/5/2021 |
| Customer: | NREL-SRRL-BMS | Environmental Conditions: | see page 4 |
| Test Dates: | 5/4-5 | | |

This certifies that the above product was calibrated in compliance with ISO/IEC 17025:2017. Measurement uncertainties at the time of calibration are consistent with the Guide to the Expression of Uncertainty in Measurement (GUM) using Reda et al., 2008. All nominal values are traceable to the International System (SI) Units of Measurement.

No statement of compliance with specifications is made or implied on this certificate. However, the estimated uncertainties are the uncertainties of the calibration process; users must add other uncertainties that are relevant to their measuring system, environmental and sky conditions, outdoor set-up, and site location.

The Type-B Standard Uncertainty of using the responsivity at each even zenith angle is reported, and the Expanded Uncertainty of the calibration is reported using two methods:

1. The Expanded Uncertainty of using the responsivity at zenith angle = 45°, within the zenith angle range from 30.0° to 60.0°
2. The Expanded Uncertainty of using Spline Interpolating Functions for the responsivity versus zenith angle.

This certificate applies only to the item identified above and shall not be reproduced other than in full, without specific written approval from the calibration facility. Certificate without signature is not valid.

Table 1. Traceability

| Measurement Type | Instrument | Calibration Date | Calibration Due Date |
|-----------------------|--|------------------|----------------------|
| Beam Irradiance † | Eppley Absolute Cavity Radiometer Model HF, S/N 29219 | 09/27/2019 | 09/27/2020 |
| Diffuse Irradiance † | Hukseflux Pyranometer Model SR25, S/N 2541 | 04/17/2020 | 04/17/2021 |
| Diffuse Irradiance † | Hukseflux Pyranometer Model SR25, S/N 2542 | 04/17/2020 | 04/17/2021 |
| Data Acquisition | NREL Data Acquisition System Model RAP-DAQ, S/N 2005-998 | 02/14/2019 | 02/14/2021 |
| Data Acquisition | NREL Data Acquisition System Model RAP-DAQ, S/N 2005-999 | 02/14/2019 | 02/14/2021 |
| Infrared Irradiance ‡ | Kipp & Zonen Pyrgeometer Model CG4, S/N FT002 | 04/16/2018 | 04/16/2022 |

† Through the World Radiometric Reference (WRR)

‡ Through the World Infrared Standard Group (WISG)

Number of pages of certificate: 4

Calibration Procedure: BORCAL-P00-Calibration and QA Procedure; available upon request.

Setup: Radiometers are calibrated outdoors, using the sun as the source. Pyranometers and pyrgeometers are installed for horizontal measurements, with their signal connectors oriented north, if their design permits.

The shading disk for the reference diffuse subtends a solid angle of 5°. Pyrheliometers are installed on solar trackers.

Calibrated by: Afshin Andreas, Ibrahim Reda, Peter Gotseff, and RCC

Ibrahim Reda, Technical Manager

Date

For questions or comments, please contact the technical manager at:

ibrahim.reda@nrel.gov; 303-384-6385; 15013 Denver West Parkway, Golden, CO 80401, USA

Calibration Results

2530 Hukseflux SR25

The responsivity (R , $\mu\text{V}/\text{W}/\text{m}^2$) of the test instrument during calibration is calculated using this Measurement Equation:

$$R = (V - R_{net} * W_{net}) / I \quad [1]$$

where,

- V = radiometer output voltage (microvolts),
 - R_{net} = radiometer net infrared responsivity ($\mu\text{V}/\text{W}/\text{m}^2$), see Table 4,
 - W_{net} = effective net infrared measured by pyrgeometer (W/m^2),
 - = $W_{in} - W_{out} = W_{in} - \sigma * T_c^4$
 - where, W_{in} = incoming infrared (W/m^2), $\sigma = 5.6704\text{e-}8 \text{ W}\cdot\text{m}^{-2}\cdot\text{K}^{-4}$,
 - T_c = case temperature of pyrgeometer (K).
- I = reference irradiance (W/m^2), beam (B) or global (G)
 where, $G = B * \text{COS}(Z) + D$,
 Z = zenith angle (degrees),
 D = reference diffuse irradiance (W/m^2).

Figure 1. Responsivity vs Zenith Angle

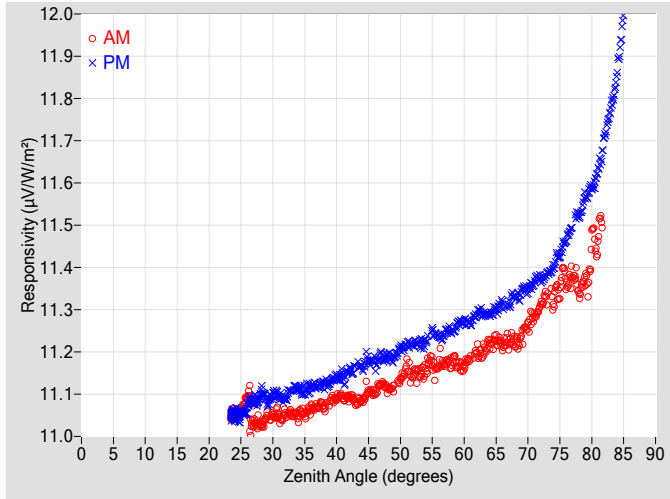


Figure 2. Responsivity vs Local Standard Time

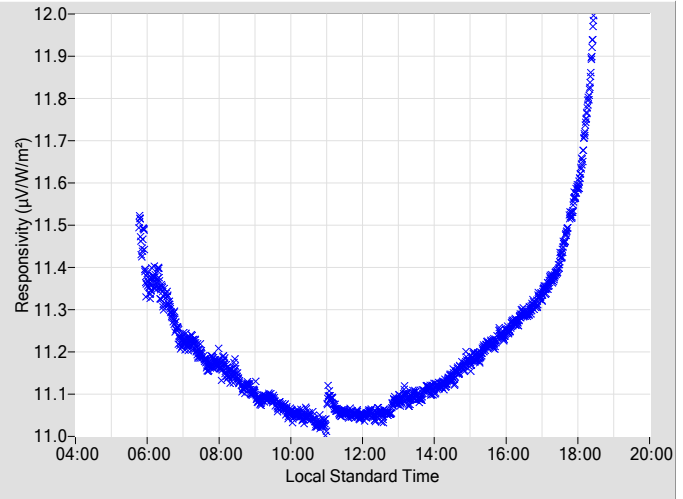


Table 2. Instrument Responsivity (R) and Calibration Type-B Standard Uncertainty, $u(B)$

| Zenith Angle (deg.) | R ($\mu\text{V}/\text{W}/\text{m}^2$) | AM $u(B)$ \pm (%) | Azimuth Angle | R ($\mu\text{V}/\text{W}/\text{m}^2$) | PM $u(B)$ \pm (%) | Azimuth Angle | Zenith Angle (deg.) | R ($\mu\text{V}/\text{W}/\text{m}^2$) | AM $u(B)$ \pm (%) | Azimuth Angle | R ($\mu\text{V}/\text{W}/\text{m}^2$) | PM $u(B)$ \pm (%) | Azimuth Angle |
|---------------------|---|---------------------|---------------|---|---------------------|---------------|---------------------|---|---------------------|---------------|---|---------------------|---------------|
| 0 | N/A | N/A | N/A | N/A | N/A | N/A | 46 | 11.103 | 0.31 | 106.83 | 11.173 | 0.31 | 252.88 |
| 2 | N/A | N/A | N/A | N/A | N/A | N/A | 48 | 11.113 | 0.34 | 104.55 | 11.192 | 0.31 | 255.13 |
| 4 | N/A | N/A | N/A | N/A | N/A | N/A | 50 | 11.135 | 0.38 | 102.41 | 11.209 | 0.31 | 257.29 |
| 6 | N/A | N/A | N/A | N/A | N/A | N/A | 52 | 11.147 | 0.37 | 100.32 | 11.218 | 0.34 | 259.29 |
| 8 | N/A | N/A | N/A | N/A | N/A | N/A | 54 | 11.160 | 0.34 | 98.45 | 11.226 | 0.32 | 261.22 |
| 10 | N/A | N/A | N/A | N/A | N/A | N/A | 56 | 11.174 | 0.36 | 96.63 | 11.237 | 0.33 | 263.10 |
| 12 | N/A | N/A | N/A | N/A | N/A | N/A | 58 | 11.172 | 0.40 | 94.79 | 11.248 | 0.34 | 264.91 |
| 14 | N/A | N/A | N/A | N/A | N/A | N/A | 60 | 11.167 | 0.34 | 93.05 | 11.270 | 0.34 | 266.67 |
| 16 | N/A | N/A | N/A | N/A | N/A | N/A | 62 | 11.201 | 0.35 | 91.35 | 11.289 | 0.35 | 268.39 |
| 18 | N/A | N/A | N/A | N/A | N/A | N/A | 64 | 11.223 | 0.39 | 89.68 | 11.290 | 0.37 | 270.09 |
| 20 | N/A | N/A | N/A | N/A | N/A | N/A | 66 | 11.216 | 0.38 | 88.03 | 11.313 | 0.38 | 271.67 |
| 22 | N/A | N/A | N/A | N/A | N/A | N/A | 68 | 11.224 | 0.40 | 86.42 | 11.329 | 0.40 | 273.36 |
| 24 | 11.055 | 0.31 | 167.01 | 11.052 | 0.30 | 193.28 | 70 | 11.262 | 0.42 | 84.78 | 11.345 | 0.42 | 274.99 |
| 26 | 11.092 | 0.32 | 151.16 | 11.066 | 0.31 | 208.97 | 72 | 11.311 | 0.45 | 83.18 | 11.373 | 0.46 | 276.60 |
| 28 | 11.029 | 0.33 | 140.65 | 11.098 | 0.32 | 218.07 | 74 | 11.318 | 0.49 | 81.61 | 11.401 | 0.54 | 278.20 |
| 30 | 11.049 | 0.32 | 134.38 | 11.099 | 0.32 | 224.61 | 76 | 11.365 | 0.55 | 79.99 | 11.466 | 0.56 | 279.79 |
| 32 | 11.052 | 0.31 | 129.22 | 11.089 | 0.32 | 230.06 | 78 | 11.338 | 0.62 | 78.39 | 11.524 | N/A | 281.40 |
| 34 | 11.050 | 0.32 | 124.83 | 11.113 | 0.30 | 234.52 | 80 | 11.450 | N/A | 76.79 | 11.591 | N/A | 283.05 |
| 36 | 11.066 | 0.32 | 121.00 | 11.117 | 0.31 | 238.40 | 82 | N/A | N/A | N/A | 11.707 | N/A | 284.69 |
| 38 | 11.069 | 0.30 | 117.57 | 11.124 | 0.31 | 241.90 | 84 | N/A | N/A | N/A | 11.868 | N/A | 286.38 |
| 40 | 11.090 | 0.33 | 114.58 | 11.141 | 0.33 | 244.93 | 86 | N/A | N/A | N/A | N/A | N/A | N/A |
| 42 | 11.092 | 0.32 | 111.74 | 11.156 | 0.30 | 247.81 | 88 | N/A | N/A | N/A | N/A | N/A | N/A |
| 44 | 11.085 | 0.30 | 109.21 | 11.164 | 0.32 | 250.38 | 90 | N/A | N/A | N/A | N/A | N/A | N/A |

N/A - Not Available

Figure 3. Type-B Standard Uncertainty vs Zenith Angle

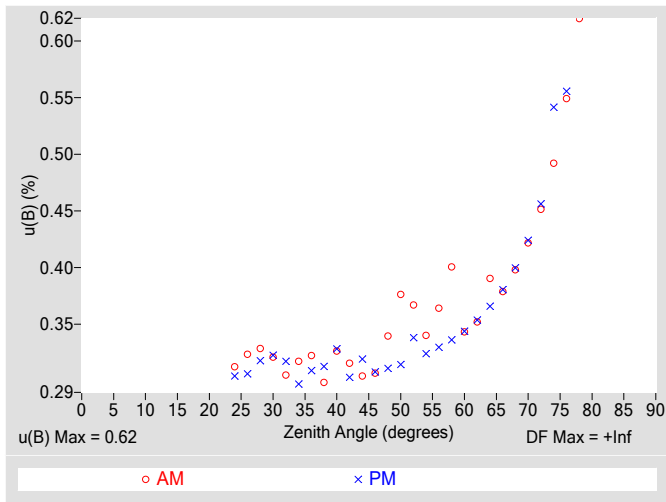


Figure 4. Residuals from Spline Interpolation

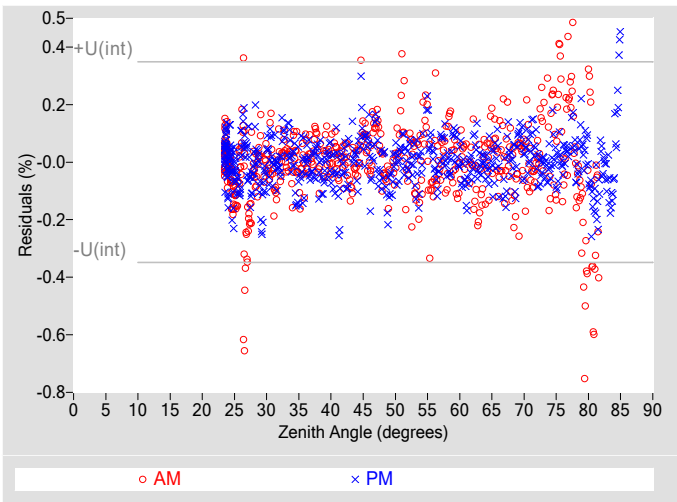


Table 3. Uncertainty using Spline Interpolation ‡

| | |
|---|------------|
| Type-B Standard Uncertainty, $u(B)$ (%) | ± 0.62 |
| Type-A Interpolating Function, $u(int)$ (%) | ± 0.17 |
| Combined Standard Uncertainty, $u(c)$ (%) | ± 0.64 |
| Effective degrees of freedom, $DF(c)$ | 211310 |
| Coverage factor, k | 1.96 |
| Expanded Uncertainty, U_{95} (%) | ± 1.3 |
| AM Valid zenith angle range | 24° to 78° |
| PM Valid zenith angle range | 24° to 76° |

‡ An illustration for how to reduce the uncertainty in calculating the irradiance using a function rather than $R@45^\circ$. Not accredited.

Table 4. Calibration Label Values

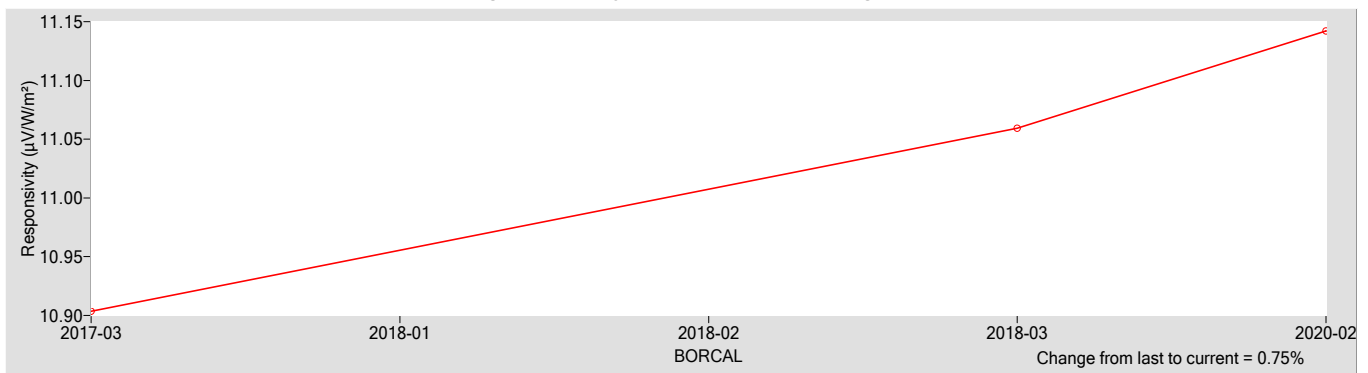
| | |
|----------------------------------|-------------------------------|
| $R @ 45^\circ$ ($\mu V/W/m^2$) | R_{net} ($\mu V/W/m^2$) † |
| 11.142 | 0.043000 |

† R_{net} determination date: Estimated

Table 5. Uncertainty using $R @ 45^\circ$

| | |
|---|----------------|
| Type-B Expanded Uncertainty, $U(B)$ (%) | ± 0.79 |
| Offset Uncertainty, $U(off)$ (%) | +1.1 / -0.84 |
| Expanded Uncertainty, U (%) | +1.9 / -1.6 |
| Effective degrees of freedom, DF | +Inf |
| Coverage factor, k | 1.96 |
| Valid zenith angle range | 30.0° to 60.0° |

Figure 5. History of instrument at Zenith Angle = 45°



References:

[1] Reda, I.; Hickey, J.; Long, C.; Myers, D.; Stoffel, T.; Wilcox, S.; Michalsky, J. J.; Dutton, E. G.; Nelson, D. (2005). "Using a Blackbody to Calculate Net Longwave Responsivity of Shortwave Solar Pyranometers to Correct for Their Thermal Offset Error During Outdoor Calibration Using the Component Sum Method." *Journal of Atmospheric and Oceanic Technology*, 2005; pp. 1531-1540; NREL Report No. JA-560-36646. doi:10.1175/JTECH1782.1

[2] Reda, I.; Myers, D.; Stoffel, T. (2008). "Uncertainty Estimate for the Outdoor Calibration of Solar Pyranometers: A Metrologist Perspective." *Measure*. (NCSLI Journal of Measurement Science). Vol. 3(4), December 2008; pp. 58-66; NREL Report No. JA-581-4137

[3] Reda, I.; Andreas, A. (2004). "Solar Position Algorithm for Solar Radiation Applications." *Solar Energy*. Vol. 76(5), 2004; pp. 577-589; NREL Report No. JA-560-35518. doi:10.1016/j.solener.2003.12.003

[4] Stoffel, T.; Reda, I. (2009). "NREL Pyrheliometer Comparisons: 22 September - 3 October 2008 (NPC-2008)." 54 pp.; NREL Report No. TP-550-45016.

[5] Reda, I.; Stoffel, T.; Myers, D. (2003). "Method to Calibrate a Solar Pyranometer for Measuring Reference Diffuse Irradiance." *Solar Energy*. Vol. 74, 2003; pp. 103-112; NREL Report No. JA-560-35025. doi:10.1016/S0038-092X(03)00124-5

[6] Reda, I. (1996). Calibration of a Solar Absolute Cavity Radiometer with Traceability to the World Radiometric Reference. 79 pp.; NREL Report No. TP-463-20619.

[7] Reda, I.; Gröbner, J.; Stoffel, T.; Myers, D.; Forgan, B. (2008). Improvements in the Blackbody Calibration of Pyrgometers. ARM 2008 Science Team Meeting (Poster).



National Renewable Energy Laboratory

Solar Radiation Research Laboratory

Metrology Laboratory

Calibration Certificate



| | | | |
|--------------------------|---------------|----------------------------------|------------|
| Test Instrument: | Pyranometer | Manufacturer: | Hukseflux |
| Model: | SR25 | Serial Number: | 2543 |
| Calibration Date: | 5/5/2020 | Due Date: | 5/5/2021 |
| Customer: | NREL-SRRL-BMS | Environmental Conditions: | see page 4 |
| Test Dates: | 5/4-5 | | |

This certifies that the above product was calibrated in compliance with ISO/IEC 17025:2017. Measurement uncertainties at the time of calibration are consistent with the Guide to the Expression of Uncertainty in Measurement (GUM) using Reda et al., 2008. All nominal values are traceable to the International System (SI) Units of Measurement.

No statement of compliance with specifications is made or implied on this certificate. However, the estimated uncertainties are the uncertainties of the calibration process; users must add other uncertainties that are relevant to their measuring system, environmental and sky conditions, outdoor set-up, and site location.

The Type-B Standard Uncertainty of using the responsivity at each even zenith angle is reported, and the Expanded Uncertainty of the calibration is reported using two methods:

1. The Expanded Uncertainty of using the responsivity at zenith angle = 45°, within the zenith angle range from 30.0° to 60.0°
2. The Expanded Uncertainty of using Spline Interpolating Functions for the responsivity versus zenith angle.

This certificate applies only to the item identified above and shall not be reproduced other than in full, without specific written approval from the calibration facility. Certificate without signature is not valid.

Table 1. Traceability

| Measurement Type | Instrument | Calibration Date | Calibration Due Date |
|-----------------------|--|------------------|----------------------|
| Beam Irradiance † | Eppley Absolute Cavity Radiometer Model HF, S/N 29219 | 09/27/2019 | 09/27/2020 |
| Diffuse Irradiance † | Hukseflux Pyranometer Model SR25, S/N 2541 | 04/17/2020 | 04/17/2021 |
| Diffuse Irradiance † | Hukseflux Pyranometer Model SR25, S/N 2542 | 04/17/2020 | 04/17/2021 |
| Data Acquisition | NREL Data Acquisition System Model RAP-DAQ, S/N 2005-998 | 02/14/2019 | 02/14/2021 |
| Data Acquisition | NREL Data Acquisition System Model RAP-DAQ, S/N 2005-999 | 02/14/2019 | 02/14/2021 |
| Infrared Irradiance ‡ | Kipp & Zonen Pyrgeometer Model CG4, S/N FT002 | 04/16/2018 | 04/16/2022 |

† Through the World Radiometric Reference (WRR)

‡ Through the World Infrared Standard Group (WISG)

Number of pages of certificate: 4

Calibration Procedure: BORCAL-P00-Calibration and QA Procedure; available upon request.

Setup: Radiometers are calibrated outdoors, using the sun as the source. Pyranometers and pyrgeometers are installed for horizontal measurements, with their signal connectors oriented north, if their design permits.

The shading disk for the reference diffuse subtends a solid angle of 5°. Pyrheliometers are installed on solar trackers.

Calibrated by: Afshin Andreas, Ibrahim Reda, Peter Gotseff, and RCC

Ibrahim Reda, Technical Manager

Date

For questions or comments, please contact the technical manager at:

ibrahim.reda@nrel.gov; 303-384-6385; 15013 Denver West Parkway, Golden, CO 80401, USA

Calibration Results

2543 Hukseflux SR25

The responsivity (R , $\mu\text{V}/\text{W}/\text{m}^2$) of the test instrument during calibration is calculated using this Measurement Equation:

$$R = (V - R_{net} * W_{net}) / I \quad [1]$$

where,

- V = radiometer output voltage (microvolts),
 - R_{net} = radiometer net infrared responsivity ($\mu\text{V}/\text{W}/\text{m}^2$), see Table 4,
 - W_{net} = effective net infrared measured by pyrgeometer (W/m^2),
 - = $W_{in} - W_{out} = W_{in} - \sigma * T_c^4$
 - where, W_{in} = incoming infrared (W/m^2), $\sigma = 5.6704\text{e-}8 \text{ W}\cdot\text{m}^{-2}\cdot\text{K}^{-4}$,
 - T_c = case temperature of pyrgeometer (K).
- I = reference irradiance (W/m^2), beam (B) or global (G)
 where, $G = B * \text{COS}(Z) + D$,
 Z = zenith angle (degrees),
 D = reference diffuse irradiance (W/m^2).

Figure 1. Responsivity vs Zenith Angle

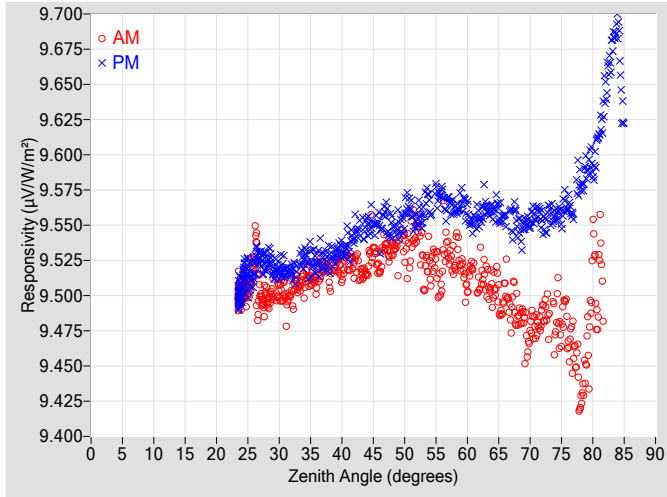


Figure 2. Responsivity vs Local Standard Time

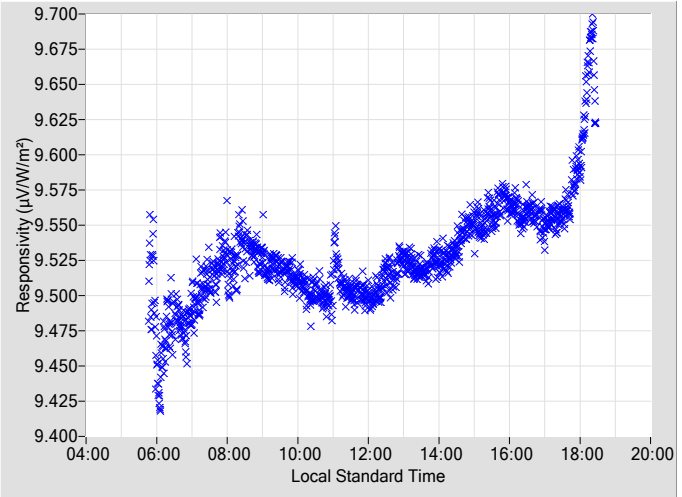


Table 2. Instrument Responsivity (R) and Calibration Type-B Standard Uncertainty, u(B)

| Zenith Angle (deg.) | R ($\mu\text{V}/\text{W}/\text{m}^2$) | AM u(B) \pm (%) | Azimuth Angle | R ($\mu\text{V}/\text{W}/\text{m}^2$) | PM u(B) \pm (%) | Azimuth Angle | Zenith Angle (deg.) | R ($\mu\text{V}/\text{W}/\text{m}^2$) | AM u(B) \pm (%) | Azimuth Angle | R ($\mu\text{V}/\text{W}/\text{m}^2$) | PM u(B) \pm (%) | Azimuth Angle |
|---------------------|---|-------------------|---------------|---|-------------------|---------------|---------------------|---|-------------------|---------------|---|-------------------|---------------|
| 0 | N/A | N/A | N/A | N/A | N/A | N/A | 46 | 9.5200 | 0.31 | 106.83 | 9.5474 | 0.31 | 252.88 |
| 2 | N/A | N/A | N/A | N/A | N/A | N/A | 48 | 9.5336 | 0.34 | 104.55 | 9.5509 | 0.31 | 255.13 |
| 4 | N/A | N/A | N/A | N/A | N/A | N/A | 50 | 9.5355 | 0.38 | 102.41 | 9.5566 | 0.32 | 257.29 |
| 6 | N/A | N/A | N/A | N/A | N/A | N/A | 52 | 9.5458 | 0.37 | 100.32 | 9.5558 | 0.34 | 259.29 |
| 8 | N/A | N/A | N/A | N/A | N/A | N/A | 54 | 9.5216 | 0.34 | 98.45 | 9.5643 | 0.32 | 261.22 |
| 10 | N/A | N/A | N/A | N/A | N/A | N/A | 56 | 9.5123 | 0.35 | 96.68 | 9.5723 | 0.33 | 263.10 |
| 12 | N/A | N/A | N/A | N/A | N/A | N/A | 58 | 9.5232 | 0.40 | 94.79 | 9.5600 | 0.34 | 264.91 |
| 14 | N/A | N/A | N/A | N/A | N/A | N/A | 60 | 9.5075 | 0.34 | 93.05 | 9.5589 | 0.34 | 266.67 |
| 16 | N/A | N/A | N/A | N/A | N/A | N/A | 62 | 9.5129 | 0.35 | 91.35 | 9.5542 | 0.35 | 268.39 |
| 18 | N/A | N/A | N/A | N/A | N/A | N/A | 64 | 9.5066 | 0.39 | 89.68 | 9.5605 | 0.37 | 270.09 |
| 20 | N/A | N/A | N/A | N/A | N/A | N/A | 66 | 9.5075 | 0.38 | 88.03 | 9.5547 | 0.38 | 271.67 |
| 22 | N/A | N/A | N/A | N/A | N/A | N/A | 68 | 9.4863 | 0.40 | 86.42 | 9.5505 | 0.40 | 273.36 |
| 24 | 9.5021 | 0.31 | 167.01 | 9.5050 | 0.30 | 193.28 | 70 | 9.4755 | 0.42 | 84.78 | 9.5515 | 0.43 | 274.99 |
| 26 | 9.5268 | 0.32 | 151.16 | 9.5171 | 0.31 | 208.97 | 72 | 9.4864 | 0.45 | 83.18 | 9.5513 | 0.46 | 276.60 |
| 28 | 9.4986 | 0.33 | 140.65 | 9.5244 | 0.32 | 218.07 | 74 | 9.4759 | 0.49 | 81.61 | 9.5560 | 0.54 | 278.20 |
| 30 | 9.5032 | 0.32 | 134.38 | 9.5193 | 0.32 | 224.61 | 76 | 9.4715 | 0.55 | 79.99 | 9.5638 | 0.56 | 279.79 |
| 32 | 9.5002 | 0.31 | 129.22 | 9.5169 | 0.32 | 230.06 | 78 | 9.4220 | 0.62 | 78.39 | 9.5782 | N/A | 281.40 |
| 34 | 9.5119 | 0.32 | 124.83 | 9.5273 | 0.30 | 234.52 | 80 | 9.5222 | N/A | 76.79 | 9.5910 | N/A | 283.05 |
| 36 | 9.5143 | 0.32 | 121.00 | 9.5239 | 0.31 | 238.40 | 82 | N/A | N/A | N/A | 9.6425 | N/A | 284.69 |
| 38 | 9.5119 | 0.30 | 117.57 | 9.5265 | 0.31 | 241.90 | 84 | N/A | N/A | N/A | 9.6916 | N/A | 286.38 |
| 40 | 9.5165 | 0.33 | 114.58 | 9.5317 | 0.33 | 244.93 | 86 | N/A | N/A | N/A | N/A | N/A | N/A |
| 42 | 9.5223 | 0.32 | 111.74 | 9.5438 | 0.30 | 247.81 | 88 | N/A | N/A | N/A | N/A | N/A | N/A |
| 44 | 9.5159 | 0.30 | 109.21 | 9.5510 | 0.32 | 250.38 | 90 | N/A | N/A | N/A | N/A | N/A | N/A |

N/A - Not Available

Figure 3. Type-B Standard Uncertainty vs Zenith Angle

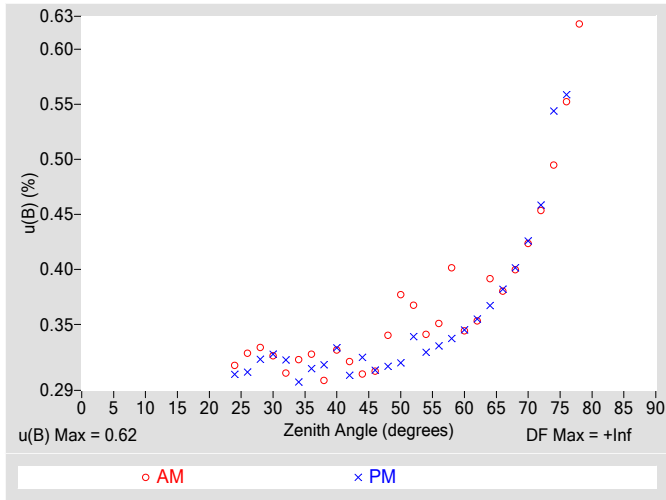


Figure 4. Residuals from Spline Interpolation

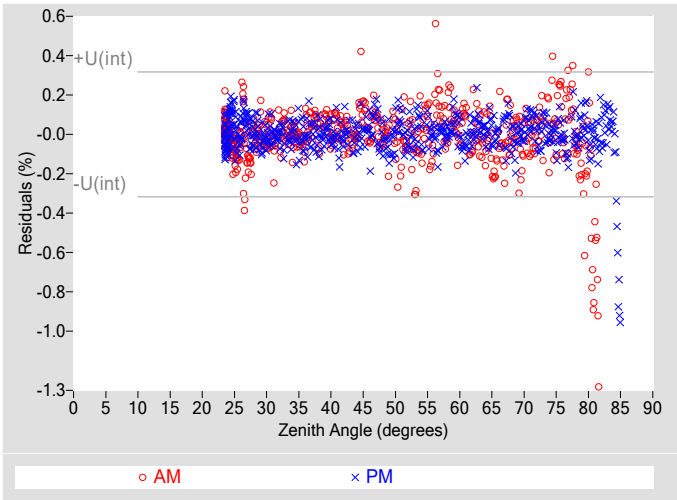


Table 3. Uncertainty using Spline Interpolation ‡

| | |
|---|------------|
| Type-B Standard Uncertainty, $u(B)$ (%) | ± 0.62 |
| Type-A Interpolating Function, $u(int)$ (%) | ± 0.16 |
| Combined Standard Uncertainty, $u(c)$ (%) | ± 0.64 |
| Effective degrees of freedom, $DF(c)$ | 308525 |
| Coverage factor, k | 1.96 |
| Expanded Uncertainty, U_{95} (%) | ± 1.3 |
| AM Valid zenith angle range | 24° to 78° |
| PM Valid zenith angle range | 24° to 76° |

‡ An illustration for how to reduce the uncertainty in calculating the irradiance using a function rather than $R@45^\circ$. Not accredited.

Table 4. Calibration Label Values

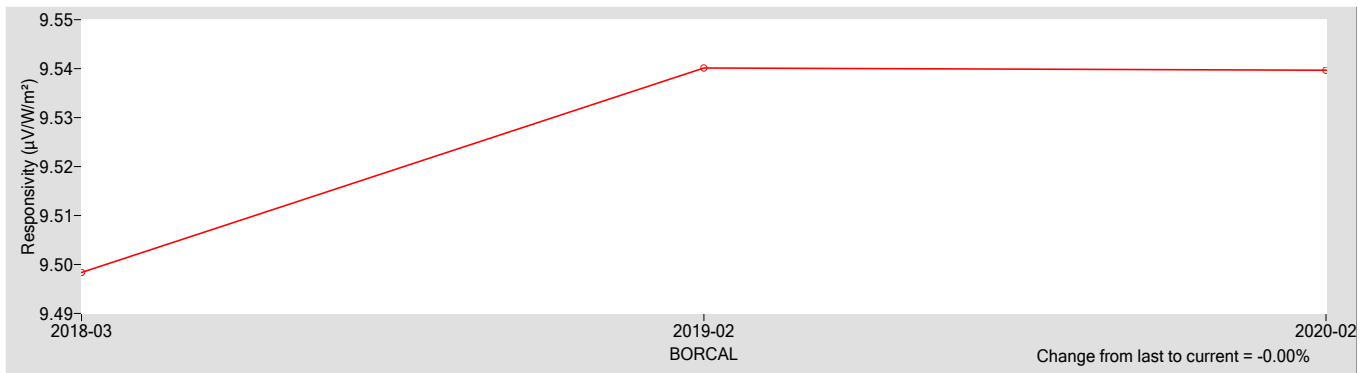
| | |
|----------------------------------|-------------------------------|
| $R @ 45^\circ$ ($\mu V/W/m^2$) | R_{net} ($\mu V/W/m^2$) † |
| 9.5397 | 0.043000 |

† R_{net} determination date: Estimated

Table 5. Uncertainty using $R @ 45^\circ$

| | |
|---|----------------|
| Type-B Expanded Uncertainty, $U(B)$ (%) | ± 0.79 |
| Offset Uncertainty, $U(off)$ (%) | +0.34 / -0.41 |
| Expanded Uncertainty, U (%) | +1.1 / -1.2 |
| Effective degrees of freedom, DF | +Inf |
| Coverage factor, k | 1.96 |
| Valid zenith angle range | 30.0° to 60.0° |

Figure 5. History of instrument at Zenith Angle = 45°



References:

[1] Reda, I.; Hickey, J.; Long, C.; Myers, D.; Stoffel, T.; Wilcox, S.; Michalsky, J. J.; Dutton, E. G.; Nelson, D. (2005). "Using a Blackbody to Calculate Net Longwave Responsivity of Shortwave Solar Pyranometers to Correct for Their Thermal Offset Error During Outdoor Calibration Using the Component Sum Method." *Journal of Atmospheric and Oceanic Technology*, 2005; pp. 1531-1540; NREL Report No. JA-560-36646. doi:10.1175/JTECH1782.1

[2] Reda, I.; Myers, D.; Stoffel, T. (2008). "Uncertainty Estimate for the Outdoor Calibration of Solar Pyranometers: A Metrologist Perspective." *Measure*. (NCSLI Journal of Measurement Science). Vol. 3(4), December 2008; pp. 58-66; NREL Report No. JA-581-4137

[3] Reda, I.; Andreas, A. (2004). "Solar Position Algorithm for Solar Radiation Applications." *Solar Energy*. Vol. 76(5), 2004; pp. 577-589; NREL Report No. JA-560-35518. doi:10.1016/j.solener.2003.12.003

[4] Stoffel, T.; Reda, I. (2009). "NREL Pyrheliometer Comparisons: 22 September - 3 October 2008 (NPC-2008)." 54 pp.; NREL Report No. TP-550-45016.

[5] Reda, I.; Stoffel, T.; Myers, D. (2003). "Method to Calibrate a Solar Pyranometer for Measuring Reference Diffuse Irradiance." *Solar Energy*. Vol. 74, 2003; pp. 103-112; NREL Report No. JA-560-35025. doi:10.1016/S0038-092X(03)00124-5

[6] Reda, I. (1996). Calibration of a Solar Absolute Cavity Radiometer with Traceability to the World Radiometric Reference. 79 pp.; NREL Report No. TP-463-20619.

[7] Reda, I.; Gröbner, J.; Stoffel, T.; Myers, D.; Forgan, B. (2008). Improvements in the Blackbody Calibration of Pyrgometers. ARM 2008 Science Team Meeting (Poster).



National Renewable Energy Laboratory

Solar Radiation Research Laboratory

Metrology Laboratory

Calibration Certificate



| | | | |
|--------------------------|---|----------------------------------|------------|
| Test Instrument: | Precision Spectral Pyranometer (Ventilated) | Manufacturer: | Eppley |
| Model: | PSP | Serial Number: | 28402F3 |
| Calibration Date: | 5/5/2020 | Due Date: | 5/5/2021 |
| Customer: | NREL-SRRL-BMS | Environmental Conditions: | see page 4 |
| Test Dates: | 5/4-5 | | |

This certifies that the above product was calibrated in compliance with ISO/IEC 17025:2017. Measurement uncertainties at the time of calibration are consistent with the Guide to the Expression of Uncertainty in Measurement (GUM) using Reda et al., 2008. All nominal values are traceable to the International System (SI) Units of Measurement.

No statement of compliance with specifications is made or implied on this certificate. However, the estimated uncertainties are the uncertainties of the calibration process; users must add other uncertainties that are relevant to their measuring system, environmental and sky conditions, outdoor set-up, and site location.

The Type-B Standard Uncertainty of using the responsivity at each even zenith angle is reported, and the Expanded Uncertainty of the calibration is reported using two methods:

1. The Expanded Uncertainty of using the responsivity at zenith angle = 45°, within the zenith angle range from 30.0° to 60.0°
2. The Expanded Uncertainty of using Spline Interpolating Functions for the responsivity versus zenith angle.

This certificate applies only to the item identified above and shall not be reproduced other than in full, without specific written approval from the calibration facility. Certificate without signature is not valid.

Table 1. Traceability

| Measurement Type | Instrument | Calibration Date | Calibration Due Date |
|-----------------------|--|------------------|----------------------|
| Beam Irradiance † | Eppley Absolute Cavity Radiometer Model HF, S/N 29219 | 09/27/2019 | 09/27/2020 |
| Diffuse Irradiance † | Hukseflux Pyranometer Model SR25, S/N 2541 | 04/17/2020 | 04/17/2021 |
| Diffuse Irradiance † | Hukseflux Pyranometer Model SR25, S/N 2542 | 04/17/2020 | 04/17/2021 |
| Data Acquisition | NREL Data Acquisition System Model RAP-DAQ, S/N 2005-998 | 02/14/2019 | 02/14/2021 |
| Data Acquisition | NREL Data Acquisition System Model RAP-DAQ, S/N 2005-999 | 02/14/2019 | 02/14/2021 |
| Infrared Irradiance ‡ | Eppley Downwelling Pyrgeometer (Ventilated) Model PIR-V, S/N 31203F3 | 04/02/2019 | 04/02/2023 |

† Through the World Radiometric Reference (WRR)

‡ Through the World Infrared Standard Group (WISG)

Number of pages of certificate: 4

Calibration Procedure: BORCAL-P00-Calibration and QA Procedure; available upon request.

Setup: Radiometers are calibrated outdoors, using the sun as the source. Pyranometers and pyrgeometers are installed for horizontal measurements, with their signal connectors oriented north, if their design permits.

The shading disk for the reference diffuse subtends a solid angle of 5°. Pyrheliometers are installed on solar trackers.

Calibrated by: Afshin Andreas, Ibrahim Reda, Peter Gotseff, and RCC

Ibrahim Reda, Technical Manager

Date

For questions or comments, please contact the technical manager at:
ibrahim.reda@nrel.gov; 303-384-6385; 15013 Denver West Parkway, Golden, CO 80401, USA

Calibration Results

28402F3 Eppley PSP

The responsivity (R , $\mu\text{V}/\text{W}/\text{m}^2$) of the test instrument during calibration is calculated using this Measurement Equation:

$$R = (V - R_{net} * W_{net}) / I \tag{1}$$

where,

- V = radiometer output voltage (microvolts),
 - R_{net} = radiometer net infrared responsivity ($\mu\text{V}/\text{W}/\text{m}^2$), see Table 4,
 - W_{net} = effective net infrared measured by pyrgeometer (W/m^2),
 - = $W_{in} - W_{out} = W_{in} - \sigma * T_c^4$
 - where, W_{in} = incoming infrared (W/m^2), $\sigma = 5.6704\text{e-}8 \text{ W}\cdot\text{m}^{-2}\cdot\text{K}^{-4}$,
 - T_c = case temperature of pyrgeometer (K).
- I = reference irradiance (W/m^2), beam (B) or global (G)
 - where, $G = B * \text{COS}(Z) + D$,
 - Z = zenith angle (degrees),
 - D = reference diffuse irradiance (W/m^2).

Figure 1. Responsivity vs Zenith Angle

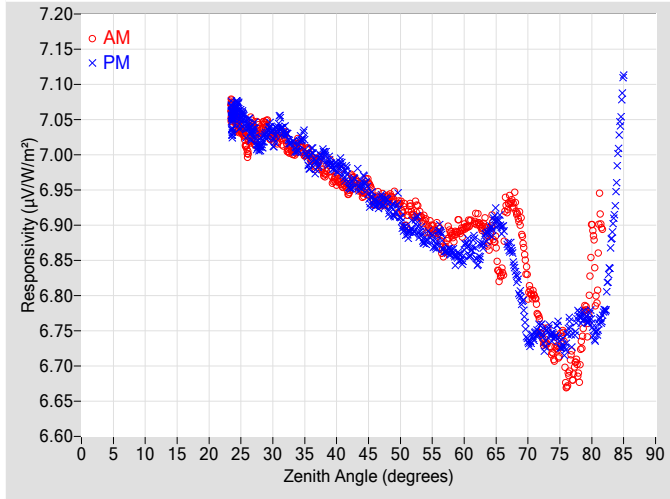


Figure 2. Responsivity vs Local Standard Time

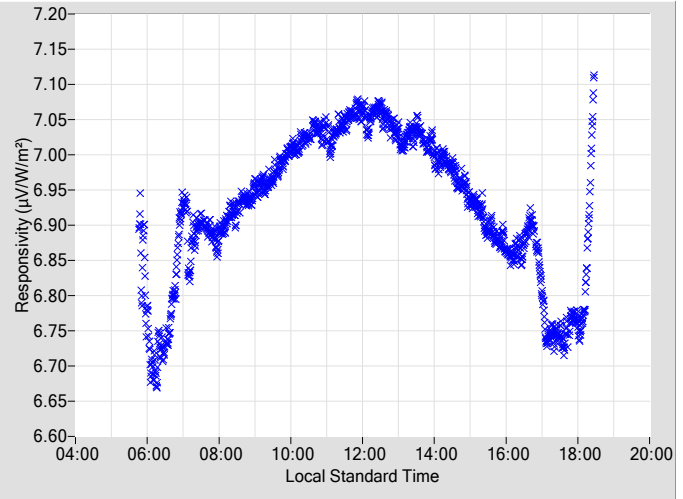


Table 2. Instrument Responsivity (R) and Calibration Type-B Standard Uncertainty, $u(B)$

| Zenith Angle (deg.) | R ($\mu\text{V}/\text{W}/\text{m}^2$) | AM $u(B)$ \pm (%) | Azimuth Angle | R ($\mu\text{V}/\text{W}/\text{m}^2$) | PM $u(B)$ \pm (%) | Azimuth Angle | Zenith Angle (deg.) | R ($\mu\text{V}/\text{W}/\text{m}^2$) | AM $u(B)$ \pm (%) | Azimuth Angle | R ($\mu\text{V}/\text{W}/\text{m}^2$) | PM $u(B)$ \pm (%) | Azimuth Angle |
|---------------------|---|---------------------|---------------|---|---------------------|---------------|---------------------|---|---------------------|---------------|---|---------------------|---------------|
| 0 | N/A | N/A | N/A | N/A | N/A | N/A | 46 | 6.9340 | 0.33 | 106.79 | 6.9316 | 0.34 | 252.84 |
| 2 | N/A | N/A | N/A | N/A | N/A | N/A | 48 | 6.9377 | 0.34 | 104.51 | 6.9297 | 0.33 | 255.10 |
| 4 | N/A | N/A | N/A | N/A | N/A | N/A | 50 | 6.9302 | 0.37 | 102.43 | 6.9093 | 0.34 | 257.25 |
| 6 | N/A | N/A | N/A | N/A | N/A | N/A | 52 | 6.9146 | 0.36 | 100.40 | 6.8967 | 0.36 | 259.31 |
| 8 | N/A | N/A | N/A | N/A | N/A | N/A | 54 | 6.9013 | 0.35 | 98.42 | 6.8780 | 0.35 | 261.24 |
| 10 | N/A | N/A | N/A | N/A | N/A | N/A | 56 | 6.8924 | 0.36 | 96.60 | 6.8905 | 0.36 | 263.12 |
| 12 | N/A | N/A | N/A | N/A | N/A | N/A | 58 | 6.8880 | 0.38 | 94.82 | 6.8624 | 0.37 | 264.93 |
| 14 | N/A | N/A | N/A | N/A | N/A | N/A | 60 | 6.8945 | 0.38 | 93.07 | 6.8635 | 0.40 | 266.69 |
| 16 | N/A | N/A | N/A | N/A | N/A | N/A | 62 | 6.9077 | 0.42 | 91.37 | 6.8526 | 0.41 | 268.41 |
| 18 | N/A | N/A | N/A | N/A | N/A | N/A | 64 | 6.8794 | 0.42 | 89.69 | 6.8932 | 0.41 | 270.07 |
| 20 | N/A | N/A | N/A | N/A | N/A | N/A | 66 | 6.8390 | 0.42 | 88.05 | 6.8948 | 0.44 | 271.74 |
| 22 | N/A | N/A | N/A | N/A | N/A | N/A | 68 | 6.9280 | 0.45 | 86.39 | 6.8331 | 0.46 | 273.38 |
| 24 | 7.0529 | 0.31 | 166.91 | 7.0609 | 0.32 | 193.13 | 70 | 6.8169 | 0.48 | 84.79 | 6.7351 | 0.50 | 275.00 |
| 26 | 7.0111 | 0.33 | 150.96 | 7.0407 | 0.34 | 209.09 | 72 | 6.7523 | 0.52 | 83.20 | 6.7529 | 0.54 | 276.57 |
| 28 | 7.0345 | 0.35 | 140.78 | 7.0122 | 0.31 | 217.99 | 74 | 6.7162 | 0.57 | 81.62 | 6.7415 | 0.60 | 278.21 |
| 30 | 7.0246 | 0.34 | 134.32 | 7.0235 | 0.33 | 224.77 | 76 | 6.6771 | 0.69 | 80.01 | 6.7344 | 0.68 | 279.81 |
| 32 | 7.0212 | 0.32 | 129.15 | 7.0312 | 0.34 | 230.00 | 78 | 6.6966 | 0.73 | 78.40 | 6.7731 | N/A | 281.42 |
| 34 | 7.0152 | 0.32 | 124.77 | 7.0092 | 0.32 | 234.38 | 80 | 6.8767 | N/A | 76.76 | 6.7611 | N/A | 283.06 |
| 36 | 6.9947 | 0.33 | 121.04 | 6.9981 | 0.31 | 238.43 | 82 | N/A | N/A | N/A | 6.7788 | N/A | 284.71 |
| 38 | 6.9745 | 0.32 | 117.60 | 7.0014 | 0.31 | 241.85 | 84 | N/A | N/A | N/A | 6.9887 | N/A | 286.40 |
| 40 | 6.9634 | 0.33 | 114.53 | 6.9814 | 0.33 | 245.10 | 86 | N/A | N/A | N/A | N/A | N/A | N/A |
| 42 | 6.9526 | 0.35 | 111.70 | 6.9552 | 0.35 | 247.83 | 88 | N/A | N/A | N/A | N/A | N/A | N/A |
| 44 | 6.9454 | 0.35 | 109.18 | 6.9600 | 0.32 | 250.41 | 90 | N/A | N/A | N/A | N/A | N/A | N/A |

N/A - Not Available

Figure 3. Type-B Standard Uncertainty vs Zenith Angle

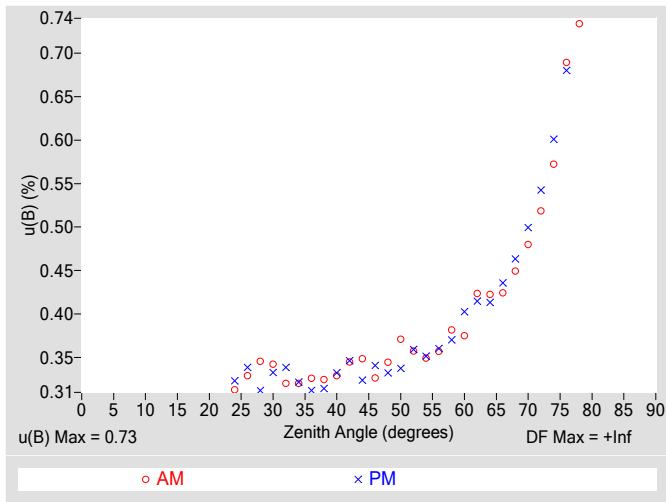


Figure 4. Residuals from Spline Interpolation

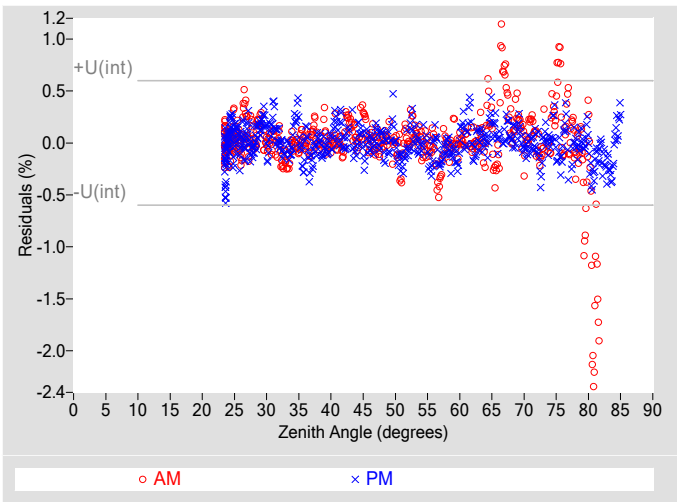


Table 3. Uncertainty using Spline Interpolation ‡

| | |
|---|------------|
| Type-B Standard Uncertainty, $u(B)$ (%) | ± 0.73 |
| Type-A Interpolating Function, $u(int)$ (%) | ± 0.30 |
| Combined Standard Uncertainty, $u(c)$ (%) | ± 0.79 |
| Effective degrees of freedom, $DF(c)$ | 56097 |
| Coverage factor, k | 1.96 |
| Expanded Uncertainty, $U95$ (%) | ± 1.6 |
| AM Valid zenith angle range | 24° to 78° |
| PM Valid zenith angle range | 24° to 76° |

‡ An illustration for how to reduce the uncertainty in calculating the irradiance using a function rather than $R@45^\circ$. Not accredited.

Table 4. Calibration Label Values

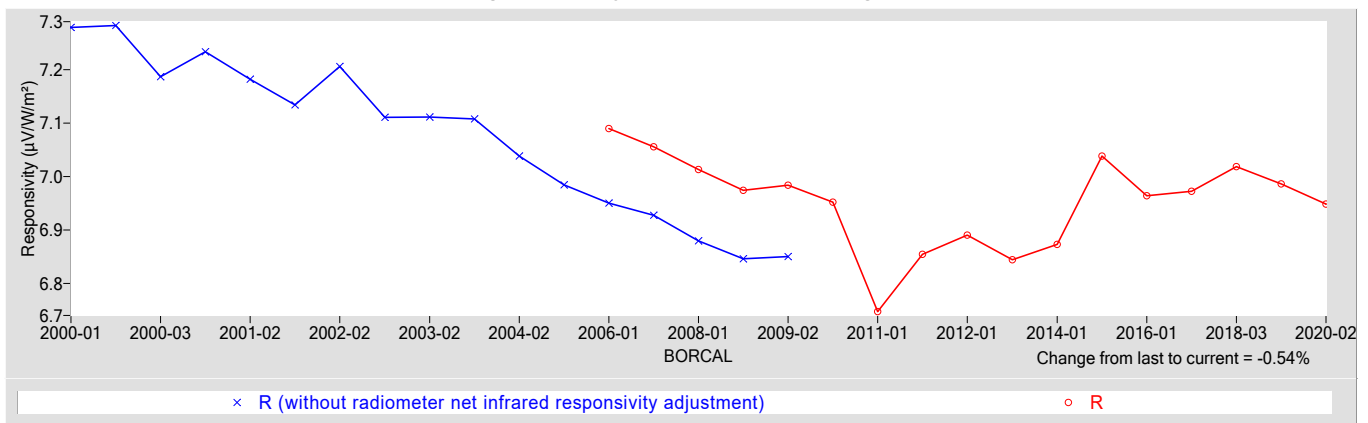
| | |
|----------------------------------|-------------------------------|
| $R @ 45^\circ$ ($\mu V/W/m^2$) | R_{net} ($\mu V/W/m^2$) † |
| 6.9486 | 0.64000 |

† R_{net} determination date: 02/28/2006

Table 5. Uncertainty using $R @ 45^\circ$

| | |
|---|----------------|
| Type-B Expanded Uncertainty, $U(B)$ (%) | ± 0.79 |
| Offset Uncertainty, $U(off)$ (%) | +1.2 / -1.2 |
| Expanded Uncertainty, U (%) | +2.0 / -2.0 |
| Effective degrees of freedom, DF | +Inf |
| Coverage factor, k | 1.96 |
| Valid zenith angle range | 30.0° to 60.0° |

Figure 5. History of instrument at Zenith Angle = 45°



References:

- [1] Reda, I.; Hickey, J.; Long, C.; Myers, D.; Stoffel, T.; Wilcox, S.; Michalsky, J. J.; Dutton, E. G.; Nelson, D. (2005). "Using a Blackbody to Calculate Net Longwave Responsivity of Shortwave Solar Pyranometers to Correct for Their Thermal Offset Error During Outdoor Calibration Using the Component Sum Method." *Journal of Atmospheric and Oceanic Technology*, 2005; pp. 1531-1540; NREL Report No. JA-560-36646. doi:10.1175/JTECH1782.1
- [2] Reda, I.; Myers, D.; Stoffel, T. (2008). "Uncertainty Estimate for the Outdoor Calibration of Solar Pyranometers: A Metrologist Perspective." *Measure*. (NCSLI Journal of Measurement Science). Vol. 3(4), December 2008; pp. 58-66; NREL Report No. JA-581-4137
- [3] Reda, I.; Andreas, A. (2004). "Solar Position Algorithm for Solar Radiation Applications." *Solar Energy*. Vol. 76(5), 2004; pp. 577-589; NREL Report No. JA-560-35518. doi:10.1016/j.solener.2003.12.003
- [4] Stoffel, T.; Reda, I. (2009). "NREL Pyrheliometer Comparisons: 22 September - 3 October 2008 (NPC-2008)." 54 pp.; NREL Report No. TP-550-45016.
- [5] Reda, I.; Stoffel, T.; Myers, D. (2003). "Method to Calibrate a Solar Pyranometer for Measuring Reference Diffuse Irradiance." *Solar Energy*. Vol. 74, 2003; pp. 103-112; NREL Report No. JA-560-35025. doi:10.1016/S0038-092X(03)00124-5
- [6] Reda, I. (1996). Calibration of a Solar Absolute Cavity Radiometer with Traceability to the World Radiometric Reference. 79 pp.; NREL Report No. TP-463-20619.
- [7] Reda, I.; Gröbner, J.; Stoffel, T.; Myers, D.; Forgan, B. (2008). Improvements in the Blackbody Calibration of Pyrgometers. ARM 2008 Science Team Meeting (Poster).

National Renewable Energy Laboratory

Solar Radiation Research Laboratory

Metrology Laboratory

Calibration Certificate



Test Instrument: Normal Incidence Pyrheliometer **Manufacturer:** Eppley
Model: NIP **Serial Number:** 31137E6
Calibration Date: 5/5/2020 **Due Date:** 5/5/2021
Customer: NREL-SRRL-BMS **Environmental Conditions:** see page 4
Test Dates: 5/4-5

This certifies that the above product was calibrated in compliance with ISO/IEC 17025:2017. Measurement uncertainties at the time of calibration are consistent with the Guide to the Expression of Uncertainty in Measurement (GUM) using Reda et al., 2008. All nominal values are traceable to the International System (SI) Units of Measurement.

No statement of compliance with specifications is made or implied on this certificate. However, the estimated uncertainties are the uncertainties of the calibration process; users must add other uncertainties that are relevant to their measuring system, environmental and sky conditions, outdoor set-up, and site location.

The Type-B Standard Uncertainty of using the responsivity at each even zenith angle is reported, and the Expanded Uncertainty of the calibration is reported using two methods:

1. The Expanded Uncertainty of using the responsivity at zenith angle = 45°, within the zenith angle range from 30.0° to 60.0°
2. The Expanded Uncertainty of using Spline Interpolating Functions for the responsivity versus zenith angle.

This certificate applies only to the item identified above and shall not be reproduced other than in full, without specific written approval from the calibration facility. Certificate without signature is not valid.

Table 1. Traceability

| Measurement Type | Instrument | Calibration Date | Calibration Due Date |
|----------------------|--|------------------|----------------------|
| Beam Irradiance † | Eppley Absolute Cavity Radiometer Model HF, S/N 29219 | 09/27/2019 | 09/27/2020 |
| Diffuse Irradiance † | Hukseflux Pyranometer Model SR25, S/N 2541 | 04/17/2020 | 04/17/2021 |
| Diffuse Irradiance † | Hukseflux Pyranometer Model SR25, S/N 2542 | 04/17/2020 | 04/17/2021 |
| Data Acquisition | NREL Data Acquisition System Model RAP-DAQ, S/N 2005-998 | 02/14/2019 | 02/14/2021 |
| Data Acquisition | NREL Data Acquisition System Model RAP-DAQ, S/N 2005-999 | 02/14/2019 | 02/14/2021 |

† Through the World Radiometric Reference (WRR)

Number of pages of certificate: 4

Calibration Procedure: BORCAL-P00-Calibration and QA Procedure; available upon request.

Setup: Radiometers are calibrated outdoors, using the sun as the source. Pyranometers and pyrgeometers are installed for horizontal measurements, with their signal connectors oriented north, if their design permits.

The shading disk for the reference diffuse subtends a solid angle of 5°. Pyrheliometers are installed on solar trackers.

Calibrated by: Afshin Andreas, Ibrahim Reda, Peter Gotseff, and RCC

Ibrahim Reda, Technical Manager

Date

For questions or comments, please contact the technical manager at:

ibrahim.reda@nrel.gov; 303-384-6385; 15013 Denver West Parkway, Golden, CO 80401, USA

Calibration Results

31137E6 Eppley NIP

The responsivity (R , $\mu\text{V}/\text{W}/\text{m}^2$) of the test instrument during calibration is calculated using this Measurement Equation:

$$R = (V - R_{net} * W_{net}) / I \tag{1}$$

where,

- V = radiometer output voltage (microvolts),
 - R_{net} = radiometer net infrared responsivity ($\mu\text{V}/\text{W}/\text{m}^2$), see Table 4,
 - W_{net} = effective net infrared measured by pyrgeometer (W/m^2),
 - $= W_{in} - W_{out} = W_{in} - \sigma * T_c^4$
 - where, W_{in} = incoming infrared (W/m^2), $\sigma = 5.6704\text{e-}8 \text{ W}\cdot\text{m}^{-2}\cdot\text{K}^{-4}$,
 - T_c = case temperature of pyrgeometer (K).
- I = reference irradiance (W/m^2), beam (B) or global (G)
 - where, $G = B * \text{COS}(Z) + D$,
 - Z = zenith angle (degrees),
 - D = reference diffuse irradiance (W/m^2).

Figure 1. Responsivity vs Zenith Angle

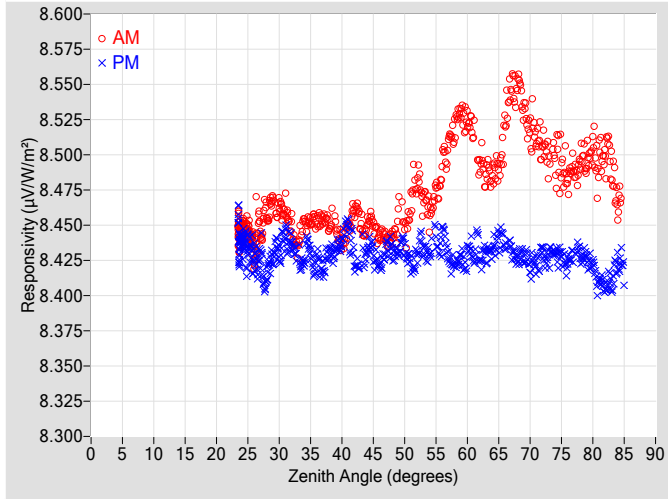


Figure 2. Responsivity vs Local Standard Time

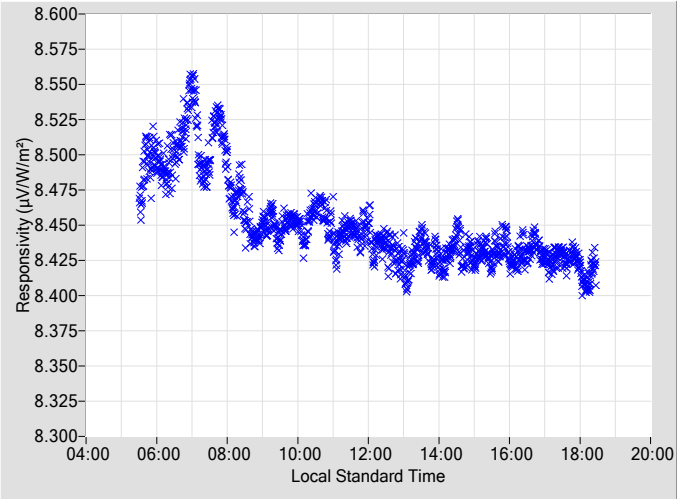


Table 2. Instrument Responsivity (R) and Calibration Type-B Standard Uncertainty, u(B)

| Zenith Angle (deg.) | R ($\mu\text{V}/\text{W}/\text{m}^2$) | u(B) \pm (%) | Azimuth Angle | R ($\mu\text{V}/\text{W}/\text{m}^2$) | u(B) \pm (%) | Azimuth Angle | Zenith Angle (deg.) | R ($\mu\text{V}/\text{W}/\text{m}^2$) | u(B) \pm (%) | Azimuth Angle | R ($\mu\text{V}/\text{W}/\text{m}^2$) | u(B) \pm (%) | Azimuth Angle |
|---------------------|---|----------------|---------------|---|----------------|---------------|---------------------|---|----------------|---------------|---|----------------|---------------|
| 0 | N/A | N/A | N/A | N/A | N/A | N/A | 46 | 8.4418 | 0.30 | 106.75 | 8.4209 | 0.29 | 252.81 |
| 2 | N/A | N/A | N/A | N/A | N/A | N/A | 48 | 8.4430 | 0.30 | 104.54 | 8.4341 | 0.29 | 255.06 |
| 4 | N/A | N/A | N/A | N/A | N/A | N/A | 50 | 8.4473 | 0.33 | 102.42 | 8.4342 | 0.31 | 257.22 |
| 6 | N/A | N/A | N/A | N/A | N/A | N/A | 52 | 8.4799 | 0.32 | 100.42 | 8.4294 | 0.30 | 259.28 |
| 8 | N/A | N/A | N/A | N/A | N/A | N/A | 54 | 8.4594 | 0.30 | 98.49 | 8.4320 | 0.29 | 261.26 |
| 10 | N/A | N/A | N/A | N/A | N/A | N/A | 56 | 8.4924 | 0.29 | 96.62 | 8.4434 | 0.30 | 263.14 |
| 12 | N/A | N/A | N/A | N/A | N/A | N/A | 58 | 8.5182 | 0.33 | 94.78 | 8.4228 | 0.29 | 264.90 |
| 14 | N/A | N/A | N/A | N/A | N/A | N/A | 60 | 8.5227 | 0.30 | 93.04 | 8.4290 | 0.31 | 266.71 |
| 16 | N/A | N/A | N/A | N/A | N/A | N/A | 62 | 8.4947 | 0.30 | 91.34 | 8.4269 | 0.30 | 268.38 |
| 18 | N/A | N/A | N/A | N/A | N/A | N/A | 64 | 8.4850 | 0.31 | 89.67 | 8.4338 | 0.30 | 270.08 |
| 20 | N/A | N/A | N/A | N/A | N/A | N/A | 66 | 8.5214 | 0.31 | 88.03 | 8.4350 | 0.30 | 271.71 |
| 22 | N/A | N/A | N/A | N/A | N/A | N/A | 68 | 8.5484 | 0.30 | 86.42 | 8.4260 | 0.30 | 273.39 |
| 24 | 8.4469 | 0.30 | 166.99 | 8.4383 | 0.30 | 193.03 | 70 | 8.5152 | 0.30 | 84.81 | 8.4199 | 0.30 | 274.98 |
| 26 | 8.4330 | 0.31 | 151.02 | 8.4265 | 0.31 | 209.20 | 72 | 8.5035 | 0.30 | 83.22 | 8.4317 | 0.31 | 276.59 |
| 28 | 8.4571 | 0.30 | 140.63 | 8.4142 | 0.31 | 218.17 | 74 | 8.4969 | 0.32 | 81.60 | 8.4305 | 0.31 | 278.19 |
| 30 | 8.4635 | 0.29 | 134.43 | 8.4289 | 0.30 | 224.70 | 76 | 8.4818 | 0.33 | 79.98 | 8.4226 | 0.31 | 279.82 |
| 32 | 8.4470 | 0.30 | 129.23 | 8.4368 | 0.30 | 230.04 | 78 | 8.4964 | 0.32 | 78.38 | 8.4285 | N/A | 281.43 |
| 34 | 8.4532 | 0.30 | 124.79 | 8.4259 | 0.30 | 234.54 | 80 | 8.5041 | N/A | 76.74 | 8.4216 | N/A | 283.08 |
| 36 | 8.4518 | 0.31 | 120.85 | 8.4258 | 0.31 | 238.50 | 82 | 8.4983 | N/A | 75.12 | 8.4053 | N/A | 284.72 |
| 38 | 8.4482 | 0.31 | 117.64 | 8.4308 | 0.29 | 241.89 | 84 | 8.4672 | N/A | 73.41 | 8.4202 | N/A | 286.38 |
| 40 | 8.4373 | 0.30 | 114.49 | 8.4384 | 0.31 | 244.98 | 86 | N/A | N/A | N/A | N/A | N/A | N/A |
| 42 | 8.4605 | 0.29 | 111.80 | 8.4239 | 0.29 | 247.79 | 88 | N/A | N/A | N/A | N/A | N/A | N/A |
| 44 | 8.4498 | 0.30 | 109.14 | 8.4315 | 0.31 | 250.43 | 90 | N/A | N/A | N/A | N/A | N/A | N/A |

N/A - Not Available

Figure 3. Type-B Standard Uncertainty vs Zenith Angle

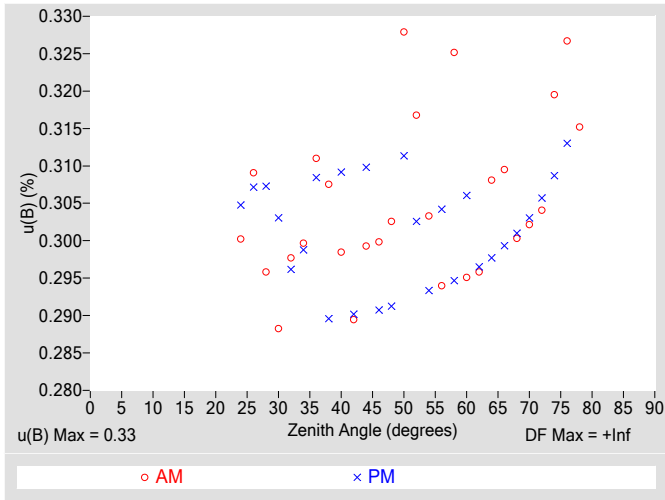


Figure 4. Residuals from Spline Interpolation

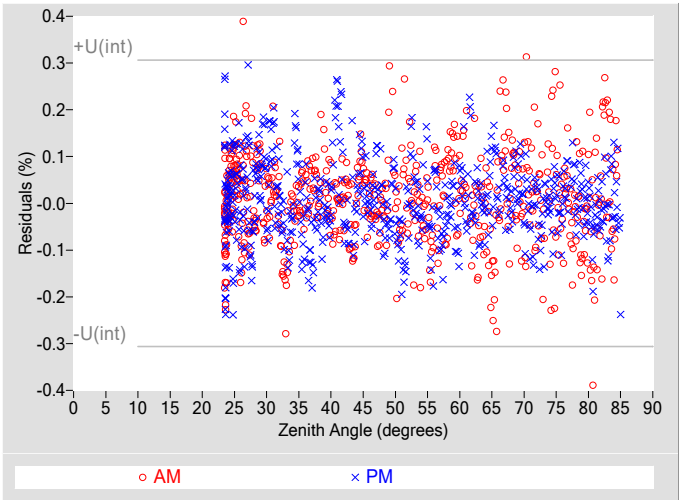


Table 3. Uncertainty using Spline Interpolation ‡

| | |
|---|------------|
| Type-B Standard Uncertainty, $u(B)$ (%) | ± 0.33 |
| Type-A Interpolating Function, $u(int)$ (%) | ± 0.15 |
| Combined Standard Uncertainty, $u(c)$ (%) | ± 0.36 |
| Effective degrees of freedom, $DF(c)$ | 35774 |
| Coverage factor, k | 1.96 |
| Expanded Uncertainty, U_{95} (%) | ± 0.71 |
| AM Valid zenith angle range | 24° to 78° |
| PM Valid zenith angle range | 24° to 76° |

‡ An illustration for how to reduce the uncertainty in calculating the irradiance using a function rather than $R@45^\circ$. Not accredited.

Table 4. Calibration Label Values

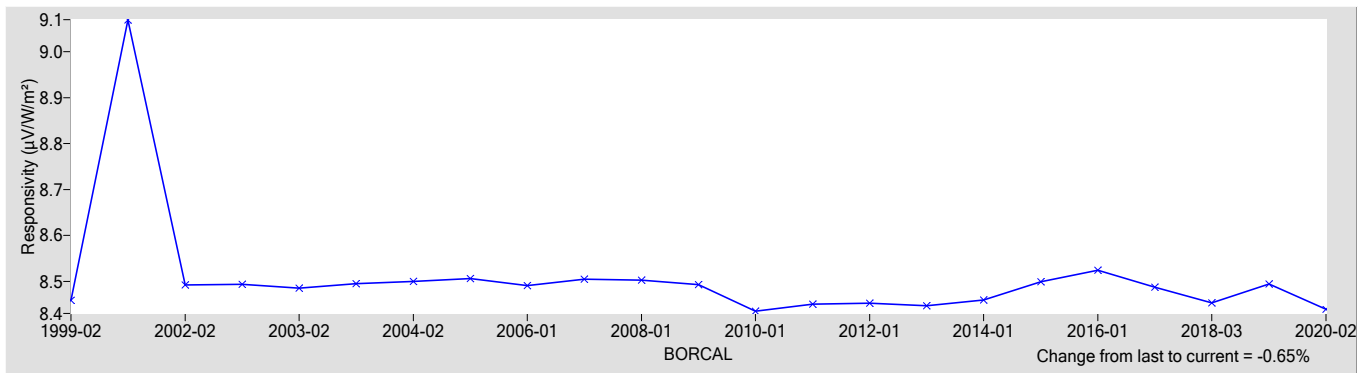
| | |
|----------------------------------|-------------------------------|
| $R @ 45^\circ$ ($\mu V/W/m^2$) | R_{net} ($\mu V/W/m^2$) † |
| 8.4394 | 0 |

† R_{net} determination date: N/A

Table 5. Uncertainty using $R @ 45^\circ$

| | |
|---|----------------|
| Type-B Expanded Uncertainty, $U(B)$ (%) | ± 0.64 |
| Offset Uncertainty, $U(off)$ (%) | +0.99 / -0.22 |
| Expanded Uncertainty, U (%) | +1.6 / -0.86 |
| Effective degrees of freedom, DF | +Inf |
| Coverage factor, k | 1.96 |
| Valid zenith angle range | 30.0° to 60.0° |

Figure 5. History of instrument at Zenith Angle = 45°



References:

- [1] Reda, I.; Hickey, J.; Long, C.; Myers, D.; Stoffel, T.; Wilcox, S.; Michalsky, J. J.; Dutton, E. G.; Nelson, D. (2005). "Using a Blackbody to Calculate Net Longwave Responsivity of Shortwave Solar Pyranometers to Correct for Their Thermal Offset Error During Outdoor Calibration Using the Component Sum Method." *Journal of Atmospheric and Oceanic Technology*, 2005; pp. 1531-1540; NREL Report No. JA-560-36646. doi:10.1175/JTECH1782.1
- [2] Reda, I.; Myers, D.; Stoffel, T. (2008). "Uncertainty Estimate for the Outdoor Calibration of Solar Pyranometers: A Metrologist Perspective." *Measure*. (NCSLI Journal of Measurement Science). Vol. 3(4), December 2008; pp. 58-66; NREL Report No. JA-581-4137
- [3] Reda, I.; Andreas, A. (2004). "Solar Position Algorithm for Solar Radiation Applications." *Solar Energy*. Vol. 76(5), 2004; pp. 577-589; NREL Report No. JA-560-35518. doi:10.1016/j.solener.2003.12.003
- [4] Stoffel, T.; Reda, I. (2009). "NREL Pyrheliometer Comparisons: 22 September - 3 October 2008 (NPC-2008)." 54 pp.; NREL Report No. TP-550-45016.
- [5] Reda, I.; Stoffel, T.; Myers, D. (2003). "Method to Calibrate a Solar Pyranometer for Measuring Reference Diffuse Irradiance." *Solar Energy*. Vol. 74, 2003; pp. 103-112; NREL Report No. JA-560-35025. doi:10.1016/S0038-092X(03)00124-5
- [6] Reda, I. (1996). Calibration of a Solar Absolute Cavity Radiometer with Traceability to the World Radiometric Reference. 79 pp.; NREL Report No. TP-463-20619.
- [7] Reda, I.; Gröbner, J.; Stoffel, T.; Myers, D.; Forgan, B. (2008). Improvements in the Blackbody Calibration of Pyrgometers. ARM 2008 Science Team Meeting (Poster).

National Renewable Energy Laboratory

Solar Radiation Research Laboratory

Metrology Laboratory

Calibration Certificate



Test Instrument: Black and White Pyranometer **Manufacturer:** Eppley
Model: 8-48 **Serial Number:** 34722
Calibration Date: 5/5/2020 **Due Date:** 5/5/2021
Customer: NREL-SRRL-BMS **Environmental Conditions:** see page 4
Test Dates: 5/4-5

This certifies that the above product was calibrated in compliance with ISO/IEC 17025:2017. Measurement uncertainties at the time of calibration are consistent with the Guide to the Expression of Uncertainty in Measurement (GUM) using Reda et al., 2008. All nominal values are traceable to the International System (SI) Units of Measurement.

No statement of compliance with specifications is made or implied on this certificate. However, the estimated uncertainties are the uncertainties of the calibration process; users must add other uncertainties that are relevant to their measuring system, environmental and sky conditions, outdoor set-up, and site location.

The Type-B Standard Uncertainty of using the responsivity at each even zenith angle is reported, and the Expanded Uncertainty of the calibration is reported using two methods:

1. The Expanded Uncertainty of using the responsivity at zenith angle = 45°, within the zenith angle range from 30.0° to 60.0°
2. The Expanded Uncertainty of using Spline Interpolating Functions for the responsivity versus zenith angle.

This certificate applies only to the item identified above and shall not be reproduced other than in full, without specific written approval from the calibration facility. Certificate without signature is not valid.

Table 1. Traceability

| Measurement Type | Instrument | Calibration Date | Calibration Due Date |
|----------------------|--|------------------|----------------------|
| Beam Irradiance † | Eppley Absolute Cavity Radiometer Model HF, S/N 29219 | 09/27/2019 | 09/27/2020 |
| Diffuse Irradiance † | Hukseflux Pyranometer Model SR25, S/N 2541 | 04/17/2020 | 04/17/2021 |
| Diffuse Irradiance † | Hukseflux Pyranometer Model SR25, S/N 2542 | 04/17/2020 | 04/17/2021 |
| Data Acquisition | NREL Data Acquisition System Model RAP-DAQ, S/N 2005-998 | 02/14/2019 | 02/14/2021 |
| Data Acquisition | NREL Data Acquisition System Model RAP-DAQ, S/N 2005-999 | 02/14/2019 | 02/14/2021 |

† Through the World Radiometric Reference (WRR)

Number of pages of certificate: 4

Calibration Procedure: BORCAL-P00-Calibration and QA Procedure; available upon request.

Setup: Radiometers are calibrated outdoors, using the sun as the source. Pyranometers and pyrgeometers are installed for horizontal measurements, with their signal connectors oriented north, if their design permits.

The shading disk for the reference diffuse subtends a solid angle of 5°. Pyrheliometers are installed on solar trackers.

Calibrated by: Afshin Andreas, Ibrahim Reda, Peter Gotseff, and RCC

Ibrahim Reda, Technical Manager

Date

For questions or comments, please contact the technical manager at:

ibrahim.reda@nrel.gov; 303-384-6385; 15013 Denver West Parkway, Golden, CO 80401, USA

Calibration Results

34722 Eppley 8-48

The responsivity (R , $\mu\text{V}/\text{W}/\text{m}^2$) of the test instrument during calibration is calculated using this Measurement Equation:

$$R = (V - R_{net} * W_{net}) / I \quad [1]$$

where,

- V = radiometer output voltage (microvolts),
- R_{net} = radiometer net infrared responsivity ($\mu\text{V}/\text{W}/\text{m}^2$), see Table 4,
- W_{net} = effective net infrared measured by pyrgeometer (W/m^2),
- = $W_{in} - W_{out} = W_{in} - \sigma * T_c^4$
- where, W_{in} = incoming infrared (W/m^2), $\sigma = 5.6704\text{e-}8 \text{ W}\cdot\text{m}^{-2}\cdot\text{K}^{-4}$,
- T_c = case temperature of pyrgeometer (K).
- I = reference irradiance (W/m^2), beam (B) or global (G)
- where, $G = B * \text{COS}(Z) + D$,
- Z = zenith angle (degrees),
- D = reference diffuse irradiance (W/m^2).

Figure 1. Responsivity vs Zenith Angle

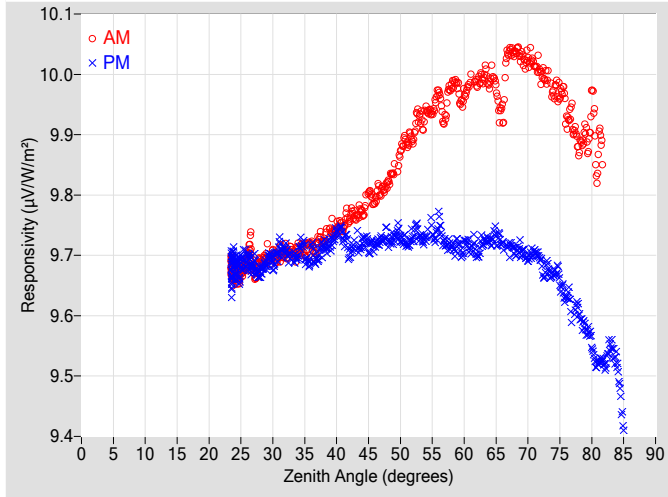


Figure 2. Responsivity vs Local Standard Time

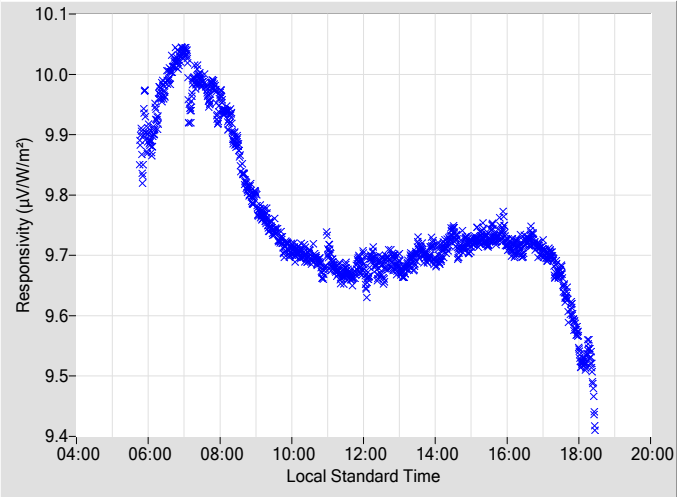


Table 2. Instrument Responsivity (R) and Calibration Type-B Standard Uncertainty, u(B)

| Zenith Angle (deg.) | R ($\mu\text{V}/\text{W}/\text{m}^2$) | u(B) \pm (%) | Azimuth Angle | R ($\mu\text{V}/\text{W}/\text{m}^2$) | u(B) \pm (%) | Azimuth Angle | Zenith Angle (deg.) | R ($\mu\text{V}/\text{W}/\text{m}^2$) | u(B) \pm (%) | Azimuth Angle | R ($\mu\text{V}/\text{W}/\text{m}^2$) | u(B) \pm (%) | Azimuth Angle |
|---------------------|---|----------------|---------------|---|----------------|---------------|---------------------|---|----------------|---------------|---|----------------|---------------|
| 0 | N/A | N/A | N/A | N/A | N/A | N/A | 46 | 9.7898 | 0.31 | 106.75 | 9.7166 | 0.31 | 252.80 |
| 2 | N/A | N/A | N/A | N/A | N/A | N/A | 48 | 9.8199 | 0.33 | 104.53 | 9.7300 | 0.33 | 255.06 |
| 4 | N/A | N/A | N/A | N/A | N/A | N/A | 50 | 9.8682 | 0.33 | 102.45 | 9.7301 | 0.33 | 257.21 |
| 6 | N/A | N/A | N/A | N/A | N/A | N/A | 52 | 9.8922 | 0.36 | 100.42 | 9.7336 | 0.35 | 259.28 |
| 8 | N/A | N/A | N/A | N/A | N/A | N/A | 54 | 9.9369 | 0.32 | 98.48 | 9.7318 | 0.32 | 261.26 |
| 10 | N/A | N/A | N/A | N/A | N/A | N/A | 56 | 9.9696 | 0.35 | 96.62 | 9.7536 | 0.35 | 263.14 |
| 12 | N/A | N/A | N/A | N/A | N/A | N/A | 58 | 9.9789 | 0.34 | 94.78 | 9.7160 | 0.34 | 264.90 |
| 14 | N/A | N/A | N/A | N/A | N/A | N/A | 60 | 9.9625 | 0.36 | 93.04 | 9.7160 | 0.36 | 266.71 |
| 16 | N/A | N/A | N/A | N/A | N/A | N/A | 62 | 9.9879 | 0.35 | 91.34 | 9.7011 | 0.35 | 268.38 |
| 18 | N/A | N/A | N/A | N/A | N/A | N/A | 64 | 9.9896 | 0.37 | 89.67 | 9.7232 | 0.37 | 270.08 |
| 20 | N/A | N/A | N/A | N/A | N/A | N/A | 66 | 9.9386 | 0.40 | 88.02 | 9.7175 | 0.38 | 271.71 |
| 22 | N/A | N/A | N/A | N/A | N/A | N/A | 68 | 10.036 | 0.40 | 86.41 | 9.7060 | 0.40 | 273.39 |
| 24 | 9.6687 | 0.30 | 167.09 | 9.6878 | 0.31 | 192.86 | 70 | 10.023 | 0.42 | 84.81 | 9.6945 | 0.42 | 274.97 |
| 26 | 9.6909 | 0.30 | 151.01 | 9.6907 | 0.32 | 209.19 | 72 | 9.9998 | 0.45 | 83.22 | 9.6913 | 0.46 | 276.59 |
| 28 | 9.6909 | 0.30 | 140.77 | 9.6708 | 0.30 | 218.16 | 74 | 9.9689 | 0.53 | 81.60 | 9.6706 | 0.50 | 278.19 |
| 30 | 9.7005 | 0.32 | 134.47 | 9.6861 | 0.31 | 224.70 | 76 | 9.9358 | 0.55 | 80.02 | 9.6307 | 0.56 | 279.82 |
| 32 | 9.7047 | 0.33 | 129.19 | 9.7097 | 0.32 | 230.03 | 78 | 9.8793 | 0.77 | 78.38 | 9.6041 | N/A | 281.43 |
| 34 | 9.7114 | 0.33 | 124.80 | 9.7037 | 0.32 | 234.59 | 80 | 9.9480 | N/A | 76.73 | 9.5516 | N/A | 283.08 |
| 36 | 9.7183 | 0.32 | 120.95 | 9.7060 | 0.31 | 238.50 | 82 | N/A | N/A | N/A | 9.5188 | N/A | 284.72 |
| 38 | 9.7234 | 0.32 | 117.63 | 9.7139 | 0.31 | 241.88 | 84 | N/A | N/A | N/A | 9.5176 | N/A | 286.38 |
| 40 | 9.7441 | 0.31 | 114.48 | 9.7387 | 0.32 | 244.93 | 86 | N/A | N/A | N/A | N/A | N/A | N/A |
| 42 | 9.7592 | 0.32 | 111.80 | 9.7021 | 0.30 | 247.79 | 88 | N/A | N/A | N/A | N/A | N/A | N/A |
| 44 | 9.7701 | 0.30 | 109.14 | 9.7214 | 0.31 | 250.43 | 90 | N/A | N/A | N/A | N/A | N/A | N/A |

N/A - Not Available

Figure 3. Type-B Standard Uncertainty vs Zenith Angle

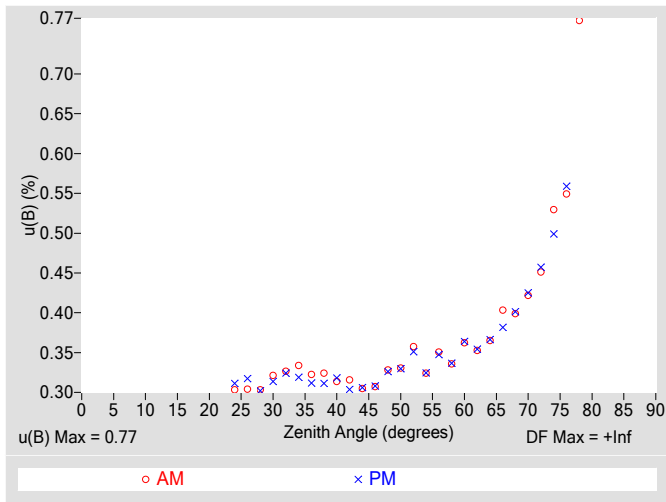


Figure 4. Residuals from Spline Interpolation

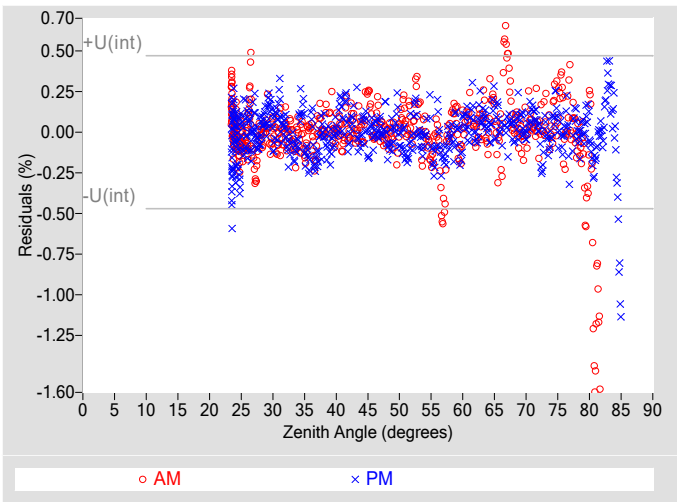


Table 3. Uncertainty using Spline Interpolation ‡

| | |
|---|------------|
| Type-B Standard Uncertainty, $u(B)$ (%) | ± 0.77 |
| Type-A Interpolating Function, $u(int)$ (%) | ± 0.24 |
| Combined Standard Uncertainty, $u(c)$ (%) | ± 0.80 |
| Effective degrees of freedom, $DF(c)$ | 155388 |
| Coverage factor, k | 1.96 |
| Expanded Uncertainty, U_{95} (%) | ± 1.6 |
| AM Valid zenith angle range | 24° to 78° |
| PM Valid zenith angle range | 24° to 76° |

‡ An illustration for how to reduce the uncertainty in calculating the irradiance using a function rather than $R@45^\circ$. Not accredited.

Table 4. Calibration Label Values

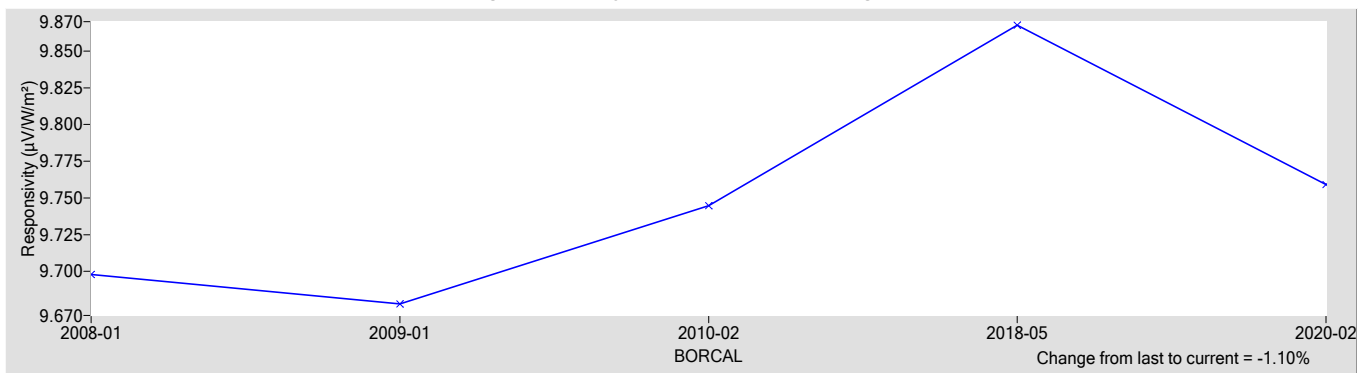
| | |
|----------------------------------|-------------------------------|
| $R @ 45^\circ$ ($\mu V/W/m^2$) | R_{net} ($\mu V/W/m^2$) † |
| 9.7590 | 0 |

† R_{net} determination date: N/A

Table 5. Uncertainty using $R @ 45^\circ$

| | |
|---|----------------|
| Type-B Expanded Uncertainty, $U(B)$ (%) | ± 0.71 |
| Offset Uncertainty, $U(off)$ (%) | +2.3 / -0.75 |
| Expanded Uncertainty, U (%) | +3.0 / -1.5 |
| Effective degrees of freedom, DF | +Inf |
| Coverage factor, k | 1.96 |
| Valid zenith angle range | 30.0° to 60.0° |

Figure 5. History of instrument at Zenith Angle = 45°



References:

- [1] Reda, I.; Hickey, J.; Long, C.; Myers, D.; Stoffel, T.; Wilcox, S.; Michalsky, J. J.; Dutton, E. G.; Nelson, D. (2005). "Using a Blackbody to Calculate Net Longwave Responsivity of Shortwave Solar Pyranometers to Correct for Their Thermal Offset Error During Outdoor Calibration Using the Component Sum Method." *Journal of Atmospheric and Oceanic Technology*, 2005; pp. 1531-1540; NREL Report No. JA-560-36646. doi:10.1175/JTECH1782.1
- [2] Reda, I.; Myers, D.; Stoffel, T. (2008). "Uncertainty Estimate for the Outdoor Calibration of Solar Pyranometers: A Metrologist Perspective." *Measure*. (NCSLI Journal of Measurement Science). Vol. 3(4), December 2008; pp. 58-66; NREL Report No. JA-581-4137
- [3] Reda, I.; Andreas, A. (2004). "Solar Position Algorithm for Solar Radiation Applications." *Solar Energy*. Vol. 76(5), 2004; pp. 577-589; NREL Report No. JA-560-35518. doi:10.1016/j.solener.2003.12.003
- [4] Stoffel, T.; Reda, I. (2009). "NREL Pyrheliometer Comparisons: 22 September - 3 October 2008 (NPC-2008)." 54 pp.; NREL Report No. TP-550-45016.
- [5] Reda, I.; Stoffel, T.; Myers, D. (2003). "Method to Calibrate a Solar Pyranometer for Measuring Reference Diffuse Irradiance." *Solar Energy*. Vol. 74, 2003; pp. 103-112; NREL Report No. JA-560-35025. doi:10.1016/S0038-092X(03)00124-5
- [6] Reda, I. (1996). Calibration of a Solar Absolute Cavity Radiometer with Traceability to the World Radiometric Reference. 79 pp.; NREL Report No. TP-463-20619.
- [7] Reda, I.; Gröbner, J.; Stoffel, T.; Myers, D.; Forgan, B. (2008). Improvements in the Blackbody Calibration of Pyrgometers. ARM 2008 Science Team Meeting (Poster).



National Renewable Energy Laboratory

Solar Radiation Research Laboratory

Metrology Laboratory

Calibration Certificate



| | | | |
|--------------------------|-----------------|----------------------------------|------------|
| Test Instrument: | GPP Pyranometer | Manufacturer: | Eppley |
| Model: | GPP | Serial Number: | 37831F3 |
| Calibration Date: | 5/5/2020 | Due Date: | 5/5/2021 |
| Customer: | NREL-SRRL-BMS | Environmental Conditions: | see page 4 |
| Test Dates: | 5/4-5 | | |

This certifies that the above product was calibrated in compliance with ISO/IEC 17025:2017. Measurement uncertainties at the time of calibration are consistent with the Guide to the Expression of Uncertainty in Measurement (GUM) using Reda et al., 2008. All nominal values are traceable to the International System (SI) Units of Measurement.

No statement of compliance with specifications is made or implied on this certificate. However, the estimated uncertainties are the uncertainties of the calibration process; users must add other uncertainties that are relevant to their measuring system, environmental and sky conditions, outdoor set-up, and site location.

The Type-B Standard Uncertainty of using the responsivity at each even zenith angle is reported, and the Expanded Uncertainty of the calibration is reported using two methods:

1. The Expanded Uncertainty of using the responsivity at zenith angle = 45°, within the zenith angle range from 30.0° to 60.0°
2. The Expanded Uncertainty of using Spline Interpolating Functions for the responsivity versus zenith angle.

This certificate applies only to the item identified above and shall not be reproduced other than in full, without specific written approval from the calibration facility. Certificate without signature is not valid.

Table 1. Traceability

| Measurement Type | Instrument | Calibration Date | Calibration Due Date |
|-----------------------|--|------------------|----------------------|
| Beam Irradiance † | Eppley Absolute Cavity Radiometer Model HF, S/N 29219 | 09/27/2019 | 09/27/2020 |
| Diffuse Irradiance † | Hukseflux Pyranometer Model SR25, S/N 2541 | 04/17/2020 | 04/17/2021 |
| Diffuse Irradiance † | Hukseflux Pyranometer Model SR25, S/N 2542 | 04/17/2020 | 04/17/2021 |
| Data Acquisition | NREL Data Acquisition System Model RAP-DAQ, S/N 2005-998 | 02/14/2019 | 02/14/2021 |
| Data Acquisition | NREL Data Acquisition System Model RAP-DAQ, S/N 2005-999 | 02/14/2019 | 02/14/2021 |
| Infrared Irradiance ‡ | Kipp & Zonen Pyrgeometer Model CG4, S/N FT002 | 04/16/2018 | 04/16/2022 |

† Through the World Radiometric Reference (WRR)

‡ Through the World Infrared Standard Group (WISG)

Number of pages of certificate: 4

Calibration Procedure: BORCAL-P00-Calibration and QA Procedure; available upon request.

Setup: Radiometers are calibrated outdoors, using the sun as the source. Pyranometers and pyrgeometers are installed for horizontal measurements, with their signal connectors oriented north, if their design permits.

The shading disk for the reference diffuse subtends a solid angle of 5°. Pyrheliometers are installed on solar trackers.

Calibrated by: Afshin Andreas, Ibrahim Reda, Peter Gotseff, and RCC

Ibrahim Reda, Technical Manager

Date

For questions or comments, please contact the technical manager at:

ibrahim.reda@nrel.gov; 303-384-6385; 15013 Denver West Parkway, Golden, CO 80401, USA

Calibration Results

37831F3 Eppley GPP

The responsivity (R , $\mu\text{V}/\text{W}/\text{m}^2$) of the test instrument during calibration is calculated using this Measurement Equation:

$$R = (V - R_{net} * W_{net}) / I \tag{1}$$

where,

- V = radiometer output voltage (microvolts),
 - R_{net} = radiometer net infrared responsivity ($\mu\text{V}/\text{W}/\text{m}^2$), see Table 4,
 - W_{net} = effective net infrared measured by pyrgeometer (W/m^2),
 - = $W_{in} - W_{out} = W_{in} - \sigma * T_c^4$
 - where, W_{in} = incoming infrared (W/m^2), $\sigma = 5.6704\text{e-}8 \text{ W}\cdot\text{m}^{-2}\cdot\text{K}^{-4}$,
 - T_c = case temperature of pyrgeometer (K).
- I = reference irradiance (W/m^2), beam (B) or global (G)
 - where, $G = B * \text{COS}(Z) + D$,
 - Z = zenith angle (degrees),
 - D = reference diffuse irradiance (W/m^2).

Figure 1. Responsivity vs Zenith Angle

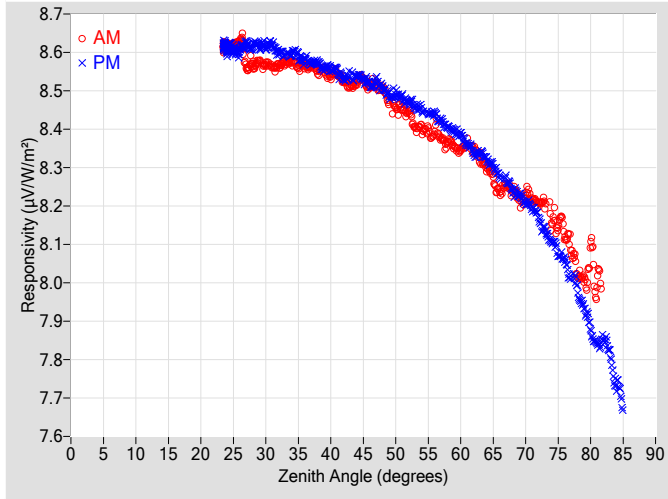


Figure 2. Responsivity vs Local Standard Time

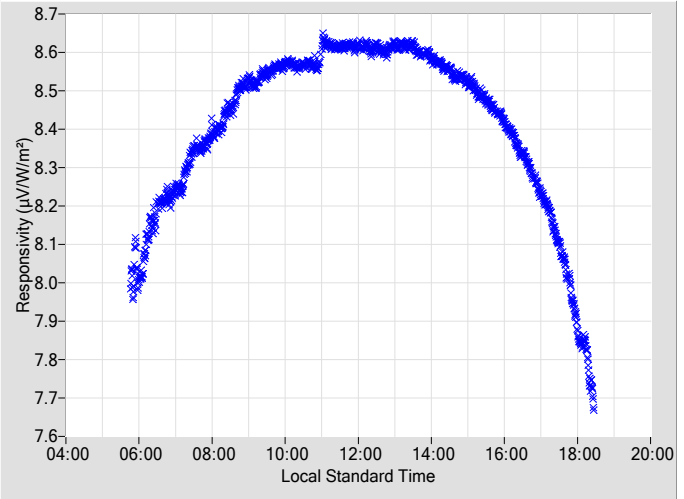


Table 2. Instrument Responsivity (R) and Calibration Type-B Standard Uncertainty, $u(B)$

| Zenith Angle (deg.) | R ($\mu\text{V}/\text{W}/\text{m}^2$) | AM $u(B)$ \pm (%) | AM Azimuth Angle | R ($\mu\text{V}/\text{W}/\text{m}^2$) | PM $u(B)$ \pm (%) | PM Azimuth Angle | Zenith Angle (deg.) | R ($\mu\text{V}/\text{W}/\text{m}^2$) | AM $u(B)$ \pm (%) | AM Azimuth Angle | R ($\mu\text{V}/\text{W}/\text{m}^2$) | PM $u(B)$ \pm (%) | PM Azimuth Angle |
|---------------------|---|---------------------|------------------|---|---------------------|------------------|---------------------|---|---------------------|------------------|---|---------------------|------------------|
| 0 | N/A | N/A | N/A | N/A | N/A | N/A | 46 | 8.5089 | 0.32 | 106.82 | 8.5162 | 0.31 | 252.88 |
| 2 | N/A | N/A | N/A | N/A | N/A | N/A | 48 | 8.5066 | 0.33 | 104.54 | 8.5079 | 0.31 | 255.13 |
| 4 | N/A | N/A | N/A | N/A | N/A | N/A | 50 | 8.4564 | 0.35 | 102.40 | 8.4888 | 0.33 | 257.28 |
| 6 | N/A | N/A | N/A | N/A | N/A | N/A | 52 | 8.4449 | 0.32 | 100.42 | 8.4687 | 0.32 | 259.29 |
| 8 | N/A | N/A | N/A | N/A | N/A | N/A | 54 | 8.4009 | 0.36 | 98.45 | 8.4508 | 0.34 | 261.22 |
| 10 | N/A | N/A | N/A | N/A | N/A | N/A | 56 | 8.3974 | 0.33 | 96.63 | 8.4403 | 0.33 | 263.10 |
| 12 | N/A | N/A | N/A | N/A | N/A | N/A | 58 | 8.3648 | 0.34 | 94.79 | 8.4052 | 0.34 | 264.91 |
| 14 | N/A | N/A | N/A | N/A | N/A | N/A | 60 | 8.3462 | 0.35 | 93.05 | 8.3855 | 0.37 | 266.67 |
| 16 | N/A | N/A | N/A | N/A | N/A | N/A | 62 | 8.3469 | 0.38 | 91.34 | 8.3356 | 0.36 | 268.39 |
| 18 | N/A | N/A | N/A | N/A | N/A | N/A | 64 | 8.2989 | 0.40 | 89.67 | 8.3221 | 0.37 | 270.08 |
| 20 | N/A | N/A | N/A | N/A | N/A | N/A | 66 | 8.2386 | 0.39 | 88.03 | 8.2788 | 0.39 | 271.67 |
| 22 | N/A | N/A | N/A | N/A | N/A | N/A | 68 | 8.2384 | 0.41 | 86.42 | 8.2368 | 0.41 | 273.35 |
| 24 | 8.6167 | 0.32 | 166.95 | 8.6114 | 0.32 | 193.02 | 70 | 8.2313 | 0.47 | 84.82 | 8.2079 | 0.44 | 274.98 |
| 26 | 8.6237 | 0.32 | 151.04 | 8.6051 | 0.34 | 209.01 | 72 | 8.2057 | 0.46 | 83.18 | 8.1691 | 0.47 | 276.59 |
| 28 | 8.5654 | 0.32 | 140.77 | 8.6175 | 0.34 | 218.06 | 74 | 8.1589 | 0.51 | 81.60 | 8.1059 | 0.56 | 278.19 |
| 30 | 8.5694 | 0.31 | 134.49 | 8.6164 | 0.33 | 224.61 | 76 | 8.1238 | 0.61 | 79.98 | 8.0589 | 0.62 | 279.79 |
| 32 | 8.5650 | 0.32 | 129.30 | 8.6008 | 0.30 | 230.05 | 78 | 8.0178 | 0.64 | 78.38 | 7.9797 | N/A | 281.40 |
| 34 | 8.5750 | 0.33 | 124.82 | 8.5958 | 0.30 | 234.42 | 80 | 8.0807 | N/A | 76.78 | 7.8784 | N/A | 283.04 |
| 36 | 8.5653 | 0.32 | 121.00 | 8.5820 | 0.34 | 238.40 | 82 | N/A | N/A | N/A | 7.8525 | N/A | 284.69 |
| 38 | 8.5476 | 0.30 | 117.58 | 8.5732 | 0.30 | 241.89 | 84 | N/A | N/A | N/A | 7.7369 | N/A | 286.43 |
| 40 | 8.5397 | 0.33 | 114.57 | 8.5549 | 0.33 | 244.99 | 86 | N/A | N/A | N/A | N/A | N/A | N/A |
| 42 | 8.5234 | 0.32 | 111.74 | 8.5325 | 0.31 | 247.80 | 88 | N/A | N/A | N/A | N/A | N/A | N/A |
| 44 | 8.5197 | 0.31 | 109.21 | 8.5385 | 0.31 | 250.38 | 90 | N/A | N/A | N/A | N/A | N/A | N/A |

N/A - Not Available

Figure 3. Type-B Standard Uncertainty vs Zenith Angle

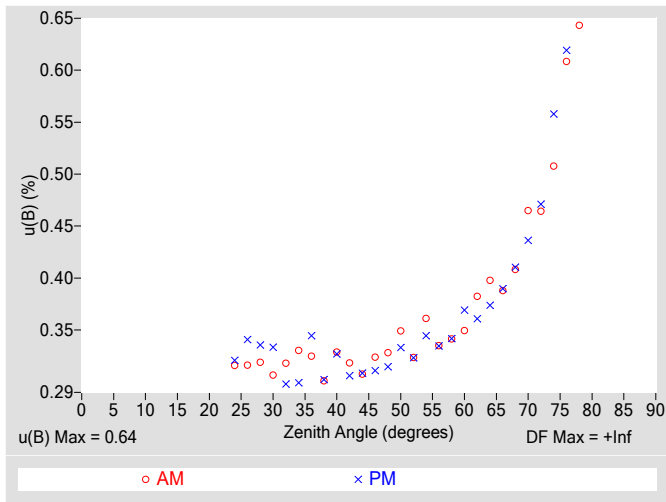


Figure 4. Residuals from Spline Interpolation

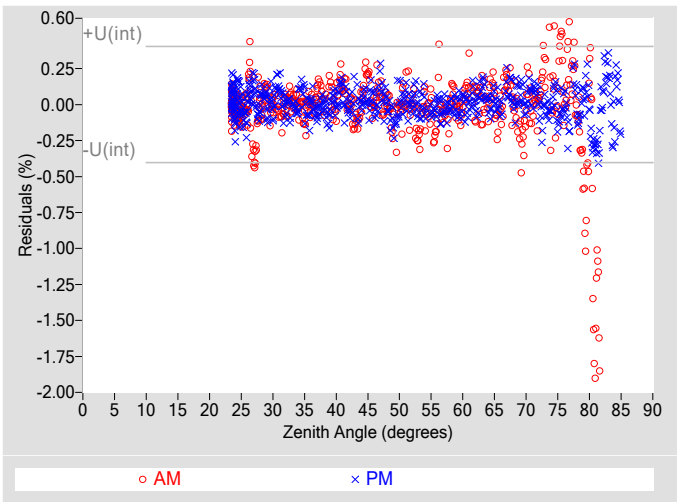


Table 3. Uncertainty using Spline Interpolation ‡

| | |
|---|------------|
| Type-B Standard Uncertainty, $u(B)$ (%) | ± 0.64 |
| Type-A Interpolating Function, $u(int)$ (%) | ± 0.20 |
| Combined Standard Uncertainty, $u(c)$ (%) | ± 0.67 |
| Effective degrees of freedom, $DF(c)$ | 142055 |
| Coverage factor, k | 1.96 |
| Expanded Uncertainty, U_{95} (%) | ± 1.3 |
| AM Valid zenith angle range | 24° to 78° |
| PM Valid zenith angle range | 24° to 76° |

‡ An illustration for how to reduce the uncertainty in calculating the irradiance using a function rather than $R@45^\circ$. Not accredited.

Table 4. Calibration Label Values

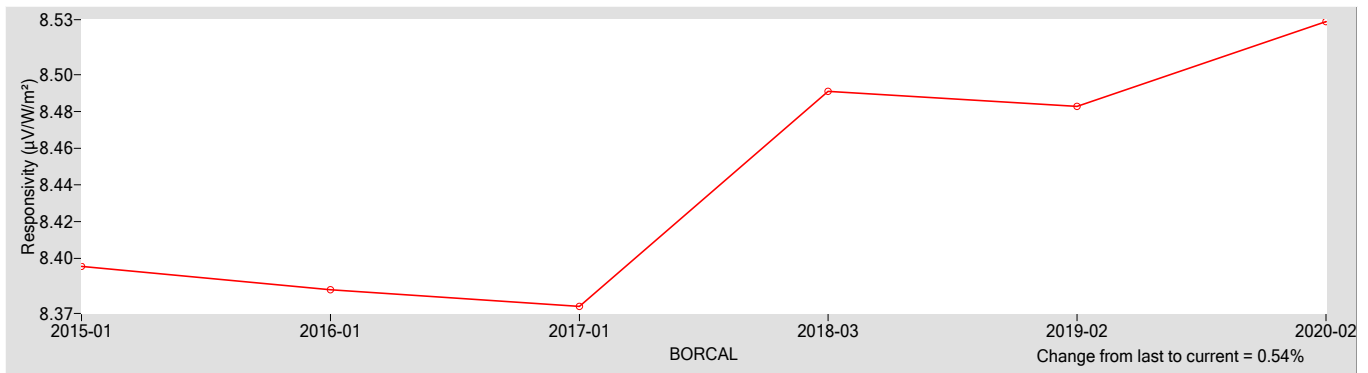
| | |
|----------------------------------|-------------------------------|
| $R @ 45^\circ$ ($\mu V/W/m^2$) | R_{net} ($\mu V/W/m^2$) † |
| 8.5290 | 0.15000 |

† R_{net} determination date: Estimated

Table 5. Uncertainty using $R @ 45^\circ$

| | |
|---|----------------|
| Type-B Expanded Uncertainty, $U(B)$ (%) | ± 0.72 |
| Offset Uncertainty, $U(off)$ (%) | +1.0 / -2.1 |
| Expanded Uncertainty, U (%) | +1.7 / -2.9 |
| Effective degrees of freedom, DF | +Inf |
| Coverage factor, k | 1.96 |
| Valid zenith angle range | 30.0° to 60.0° |

Figure 5. History of instrument at Zenith Angle = 45°



References:

[1] Reda, I.; Hickey, J.; Long, C.; Myers, D.; Stoffel, T.; Wilcox, S.; Michalsky, J. J.; Dutton, E. G.; Nelson, D. (2005). "Using a Blackbody to Calculate Net Longwave Responsivity of Shortwave Solar Pyranometers to Correct for Their Thermal Offset Error During Outdoor Calibration Using the Component Sum Method." *Journal of Atmospheric and Oceanic Technology*, 2005; pp. 1531-1540; NREL Report No. JA-560-36646. doi:10.1175/JTECH1782.1

[2] Reda, I.; Myers, D.; Stoffel, T. (2008). "Uncertainty Estimate for the Outdoor Calibration of Solar Pyranometers: A Metrologist Perspective." *Measure*. (NCSLI Journal of Measurement Science). Vol. 3(4), December 2008; pp. 58-66; NREL Report No. JA-581-4137

[3] Reda, I.; Andreas, A. (2004). "Solar Position Algorithm for Solar Radiation Applications." *Solar Energy*. Vol. 76(5), 2004; pp. 577-589; NREL Report No. JA-560-35518. doi:10.1016/j.solener.2003.12.003

[4] Stoffel, T.; Reda, I. (2009). "NREL Pyrheliometer Comparisons: 22 September - 3 October 2008 (NPC-2008)." 54 pp.; NREL Report No. TP-550-45016.

[5] Reda, I.; Stoffel, T.; Myers, D. (2003). "Method to Calibrate a Solar Pyranometer for Measuring Reference Diffuse Irradiance." *Solar Energy*. Vol. 74, 2003; pp. 103-112; NREL Report No. JA-560-35025. doi:10.1016/S0038-092X(03)00124-5

[6] Reda, I. (1996). *Calibration of a Solar Absolute Cavity Radiometer with Traceability to the World Radiometric Reference*. 79 pp.; NREL Report No. TP-463-20619.

[7] Reda, I.; Gröbner, J.; Stoffel, T.; Myers, D.; Forgan, B. (2008). *Improvements in the Blackbody Calibration of Pyrgometers*. ARM 2008 Science Team Meeting (Poster).



National Renewable Energy Laboratory

Solar Radiation Research Laboratory

Metrology Laboratory

Calibration Certificate



| | | | |
|--------------------------|---|----------------------------------|------------|
| Test Instrument: | Standard Precision Pyranometer (Ventilated) | Manufacturer: | Eppley |
| Model: | SPP | Serial Number: | 37839F3 |
| Calibration Date: | 5/5/2020 | Due Date: | 5/5/2021 |
| Customer: | NREL-SRRL-BMS | Environmental Conditions: | see page 4 |
| Test Dates: | 5/4-5 | | |

This certifies that the above product was calibrated in compliance with ISO/IEC 17025:2017. Measurement uncertainties at the time of calibration are consistent with the Guide to the Expression of Uncertainty in Measurement (GUM) using Reda et al., 2008. All nominal values are traceable to the International System (SI) Units of Measurement.

No statement of compliance with specifications is made or implied on this certificate. However, the estimated uncertainties are the uncertainties of the calibration process; users must add other uncertainties that are relevant to their measuring system, environmental and sky conditions, outdoor set-up, and site location.

The Type-B Standard Uncertainty of using the responsivity at each even zenith angle is reported, and the Expanded Uncertainty of the calibration is reported using two methods:

1. The Expanded Uncertainty of using the responsivity at zenith angle = 45°, within the zenith angle range from 30.0° to 60.0°
2. The Expanded Uncertainty of using Spline Interpolating Functions for the responsivity versus zenith angle.

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Table 1. Traceability

| Measurement Type | Instrument | Calibration Date | Calibration Due Date |
|-----------------------|--|------------------|----------------------|
| Beam Irradiance † | Eppley Absolute Cavity Radiometer Model HF, S/N 29219 | 09/27/2019 | 09/27/2020 |
| Diffuse Irradiance † | Hukseflux Pyranometer Model SR25, S/N 2541 | 04/17/2020 | 04/17/2021 |
| Diffuse Irradiance † | Hukseflux Pyranometer Model SR25, S/N 2542 | 04/17/2020 | 04/17/2021 |
| Data Acquisition | NREL Data Acquisition System Model RAP-DAQ, S/N 2005-998 | 02/14/2019 | 02/14/2021 |
| Data Acquisition | NREL Data Acquisition System Model RAP-DAQ, S/N 2005-999 | 02/14/2019 | 02/14/2021 |
| Infrared Irradiance ‡ | Eppley Downwelling Pyrgeometer (Ventilated) Model PIR-V, S/N 31203F3 | 04/02/2019 | 04/02/2023 |

† Through the World Radiometric Reference (WRR)

‡ Through the World Infrared Standard Group (WISG)

Number of pages of certificate: 4

Calibration Procedure: BORCAL-P00-Calibration and QA Procedure; available upon request.

Setup: Radiometers are calibrated outdoors, using the sun as the source. Pyranometers and pyrgeometers are installed for horizontal measurements, with their signal connectors oriented north, if their design permits.

The shading disk for the reference diffuse subtends a solid angle of 5°. Pyrheliometers are installed on solar trackers.

Calibrated by: Afshin Andreas, Ibrahim Reda, Peter Gotseff, and RCC

Ibrahim Reda, Technical Manager

Date

For questions or comments, please contact the technical manager at:

ibrahim.reda@nrel.gov; 303-384-6385; 15013 Denver West Parkway, Golden, CO 80401, USA

Calibration Results

37839F3 Eppley SPP

The responsivity (R , $\mu\text{V}/\text{W}/\text{m}^2$) of the test instrument during calibration is calculated using this Measurement Equation:

$$R = (V - R_{net} * W_{net}) / I \tag{1}$$

where,

- V = radiometer output voltage (microvolts),
 - R_{net} = radiometer net infrared responsivity ($\mu\text{V}/\text{W}/\text{m}^2$), see Table 4,
 - W_{net} = effective net infrared measured by pyrgeometer (W/m^2),
 - = $W_{in} - W_{out} = W_{in} - \sigma * T_c^4$
 - where, W_{in} = incoming infrared (W/m^2), $\sigma = 5.6704\text{e-}8 \text{ W}\cdot\text{m}^{-2}\cdot\text{K}^{-4}$,
 - T_c = case temperature of pyrgeometer (K).
- I = reference irradiance (W/m^2), beam (B) or global (G)
 - where, $G = B * \text{COS}(Z) + D$,
 - Z = zenith angle (degrees),
 - D = reference diffuse irradiance (W/m^2).

Figure 1. Responsivity vs Zenith Angle

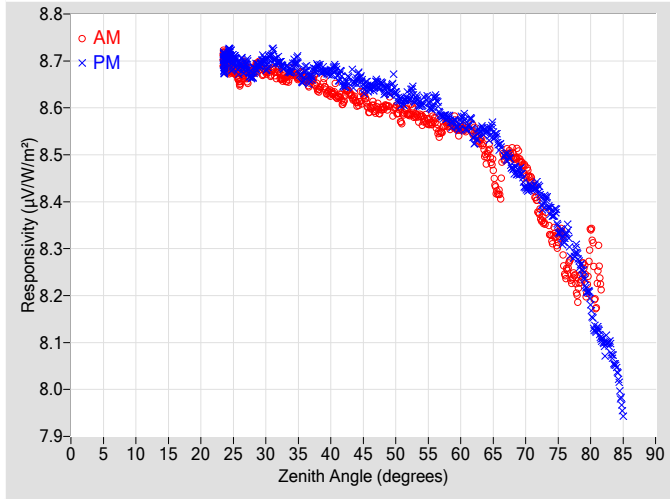


Figure 2. Responsivity vs Local Standard Time

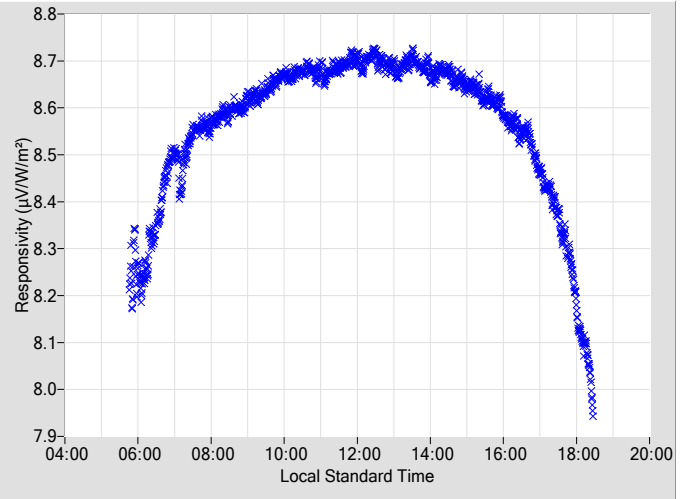


Table 2. Instrument Responsivity (R) and Calibration Type-B Standard Uncertainty, u(B)

| Zenith Angle (deg.) | R ($\mu\text{V}/\text{W}/\text{m}^2$) | u(B) \pm (%) | Azimuth Angle | R ($\mu\text{V}/\text{W}/\text{m}^2$) | u(B) \pm (%) | Azimuth Angle | Zenith Angle (deg.) | R ($\mu\text{V}/\text{W}/\text{m}^2$) | u(B) \pm (%) | Azimuth Angle | R ($\mu\text{V}/\text{W}/\text{m}^2$) | u(B) \pm (%) | Azimuth Angle |
|---------------------|---|----------------|---------------|---|----------------|---------------|---------------------|---|----------------|---------------|---|----------------|---------------|
| 0 | N/A | N/A | N/A | N/A | N/A | N/A | 46 | 8.5968 | 0.32 | 106.79 | 8.6418 | 0.33 | 252.84 |
| 2 | N/A | N/A | N/A | N/A | N/A | N/A | 48 | 8.5988 | 0.34 | 104.51 | 8.6443 | 0.32 | 255.10 |
| 4 | N/A | N/A | N/A | N/A | N/A | N/A | 50 | 8.5986 | 0.36 | 102.43 | 8.6313 | 0.33 | 257.25 |
| 6 | N/A | N/A | N/A | N/A | N/A | N/A | 52 | 8.5857 | 0.35 | 100.40 | 8.6245 | 0.35 | 259.31 |
| 8 | N/A | N/A | N/A | N/A | N/A | N/A | 54 | 8.5774 | 0.34 | 98.42 | 8.6085 | 0.34 | 261.24 |
| 10 | N/A | N/A | N/A | N/A | N/A | N/A | 56 | 8.5729 | 0.34 | 96.60 | 8.6203 | 0.35 | 263.12 |
| 12 | N/A | N/A | N/A | N/A | N/A | N/A | 58 | 8.5656 | 0.37 | 94.82 | 8.5794 | 0.35 | 264.93 |
| 14 | N/A | N/A | N/A | N/A | N/A | N/A | 60 | 8.5531 | 0.36 | 93.07 | 8.5706 | 0.39 | 266.69 |
| 16 | N/A | N/A | N/A | N/A | N/A | N/A | 62 | 8.5509 | 0.41 | 91.37 | 8.5362 | 0.40 | 268.41 |
| 18 | N/A | N/A | N/A | N/A | N/A | N/A | 64 | 8.4972 | 0.41 | 89.69 | 8.5513 | 0.39 | 270.07 |
| 20 | N/A | N/A | N/A | N/A | N/A | N/A | 66 | 8.4213 | 0.40 | 88.05 | 8.5186 | 0.41 | 271.74 |
| 22 | N/A | N/A | N/A | N/A | N/A | N/A | 68 | 8.4993 | 0.43 | 86.39 | 8.4682 | 0.44 | 273.38 |
| 24 | 8.6917 | 0.31 | 166.91 | 8.7083 | 0.32 | 193.13 | 70 | 8.4644 | 0.45 | 84.79 | 8.4282 | 0.47 | 275.00 |
| 26 | 8.6613 | 0.33 | 150.96 | 8.6902 | 0.33 | 209.09 | 72 | 8.3831 | 0.49 | 83.20 | 8.4287 | 0.50 | 276.57 |
| 28 | 8.6790 | 0.34 | 140.78 | 8.6706 | 0.31 | 217.99 | 74 | 8.3239 | 0.54 | 81.62 | 8.3748 | 0.56 | 278.21 |
| 30 | 8.6770 | 0.34 | 134.32 | 8.6911 | 0.33 | 224.77 | 76 | 8.2549 | 0.65 | 80.01 | 8.3226 | 0.63 | 279.81 |
| 32 | 8.6758 | 0.31 | 129.15 | 8.6982 | 0.33 | 230.00 | 78 | 8.2100 | 0.68 | 78.40 | 8.2882 | N/A | 281.42 |
| 34 | 8.6748 | 0.31 | 124.77 | 8.6818 | 0.32 | 234.38 | 80 | 8.3188 | N/A | 76.76 | 8.1808 | N/A | 283.06 |
| 36 | 8.6611 | 0.32 | 121.04 | 8.6763 | 0.31 | 238.43 | 82 | N/A | N/A | N/A | 8.0937 | N/A | 284.71 |
| 38 | 8.6412 | 0.32 | 117.60 | 8.6880 | 0.31 | 241.85 | 84 | N/A | N/A | N/A | 8.0410 | N/A | 286.40 |
| 40 | 8.6316 | 0.32 | 114.53 | 8.6767 | 0.33 | 245.10 | 86 | N/A | N/A | N/A | N/A | N/A | N/A |
| 42 | 8.6180 | 0.34 | 111.70 | 8.6480 | 0.34 | 247.83 | 88 | N/A | N/A | N/A | N/A | N/A | N/A |
| 44 | 8.6102 | 0.34 | 109.18 | 8.6618 | 0.32 | 250.41 | 90 | N/A | N/A | N/A | N/A | N/A | N/A |

N/A - Not Available

Figure 3. Type-B Standard Uncertainty vs Zenith Angle

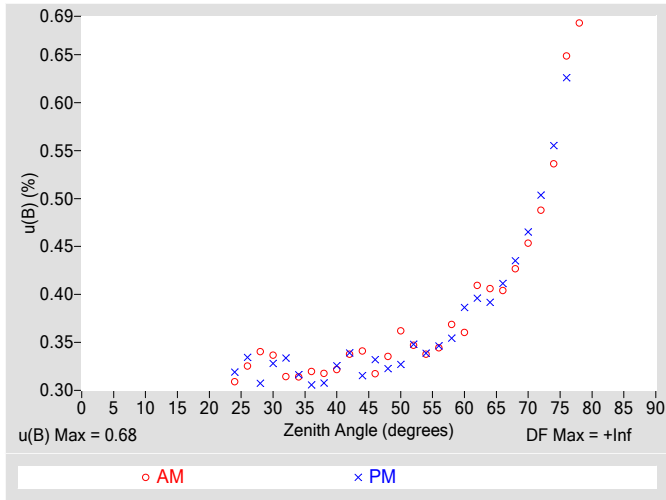


Figure 4. Residuals from Spline Interpolation

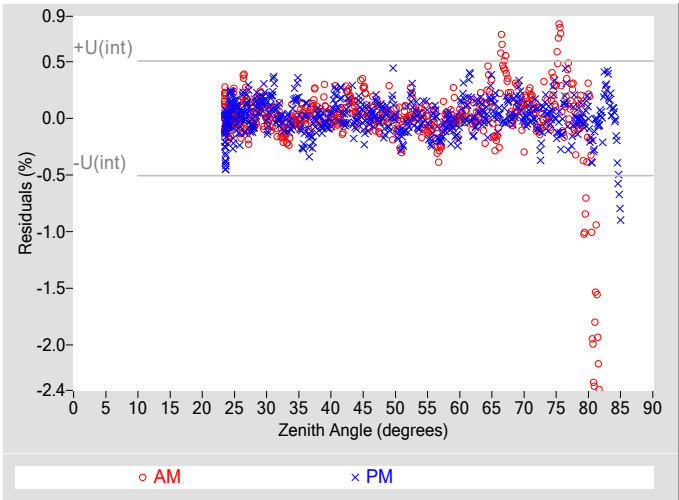


Table 3. Uncertainty using Spline Interpolation ‡

| | |
|---|------------|
| Type-B Standard Uncertainty, $u(B)$ (%) | ± 0.68 |
| Type-A Interpolating Function, $u(int)$ (%) | ± 0.25 |
| Combined Standard Uncertainty, $u(c)$ (%) | ± 0.73 |
| Effective degrees of freedom, $DF(c)$ | 79169 |
| Coverage factor, k | 1.96 |
| Expanded Uncertainty, U_{95} (%) | ± 1.4 |
| AM Valid zenith angle range | 24° to 78° |
| PM Valid zenith angle range | 24° to 76° |

‡ An illustration for how to reduce the uncertainty in calculating the irradiance using a function rather than $R@45^\circ$. Not accredited.

Table 4. Calibration Label Values

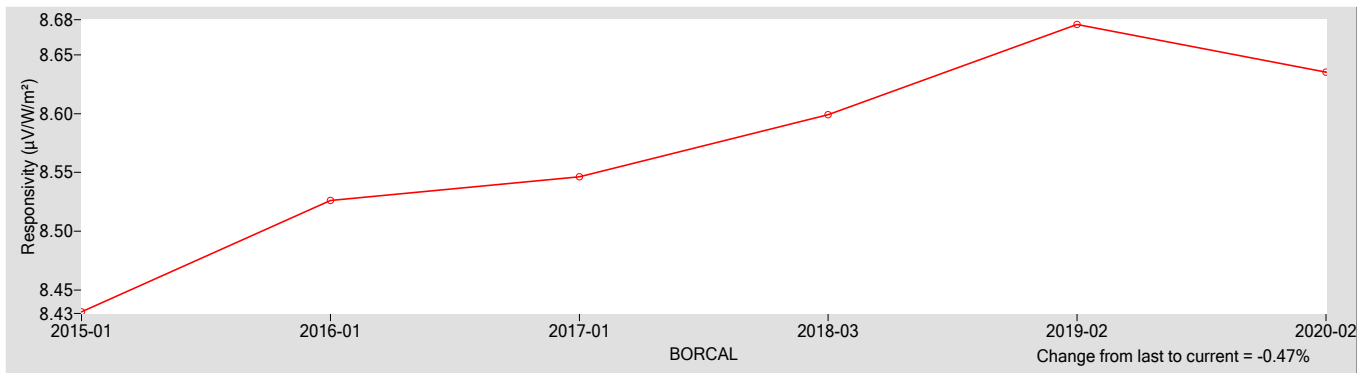
| | |
|----------------------------------|-------------------------------|
| $R @ 45^\circ$ ($\mu V/W/m^2$) | R_{net} ($\mu V/W/m^2$) † |
| 8.6353 | 0.30000 |

† R_{net} determination date: Estimated

Table 5. Uncertainty using $R @ 45^\circ$

| | |
|---|----------------|
| Type-B Expanded Uncertainty, $U(B)$ (%) | ± 0.76 |
| Offset Uncertainty, $U(off)$ (%) | +0.73 / -0.95 |
| Expanded Uncertainty, U (%) | +1.5 / -1.7 |
| Effective degrees of freedom, DF | +Inf |
| Coverage factor, k | 1.96 |
| Valid zenith angle range | 30.0° to 60.0° |

Figure 5. History of instrument at Zenith Angle = 45°



References:

- [1] Reda, I.; Hickey, J.; Long, C.; Myers, D.; Stoffel, T.; Wilcox, S.; Michalsky, J. J.; Dutton, E. G.; Nelson, D. (2005). "Using a Blackbody to Calculate Net Longwave Responsivity of Shortwave Solar Pyranometers to Correct for Their Thermal Offset Error During Outdoor Calibration Using the Component Sum Method." *Journal of Atmospheric and Oceanic Technology*, 2005; pp. 1531-1540; NREL Report No. JA-560-36646. doi:10.1175/JTECH1782.1
- [2] Reda, I.; Myers, D.; Stoffel, T. (2008). "Uncertainty Estimate for the Outdoor Calibration of Solar Pyranometers: A Metrologist Perspective." *Measure*. (NCSLI Journal of Measurement Science). Vol. 3(4), December 2008; pp. 58-66; NREL Report No. JA-581-4137
- [3] Reda, I.; Andreas, A. (2004). "Solar Position Algorithm for Solar Radiation Applications." *Solar Energy*. Vol. 76(5), 2004; pp. 577-589; NREL Report No. JA-560-35518. doi:10.1016/j.solener.2003.12.003
- [4] Stoffel, T.; Reda, I. (2009). "NREL Pyrheliometer Comparisons: 22 September - 3 October 2008 (NPC-2008)." 54 pp.; NREL Report No. TP-550-45016.
- [5] Reda, I.; Stoffel, T.; Myers, D. (2003). "Method to Calibrate a Solar Pyranometer for Measuring Reference Diffuse Irradiance." *Solar Energy*. Vol. 74, 2003; pp. 103-112; NREL Report No. JA-560-35025. doi:10.1016/S0038-092X(03)00124-5
- [6] Reda, I. (1996). Calibration of a Solar Absolute Cavity Radiometer with Traceability to the World Radiometric Reference. 79 pp.; NREL Report No. TP-463-20619.
- [7] Reda, I.; Gröbner, J.; Stoffel, T.; Myers, D.; Forgan, B. (2008). Improvements in the Blackbody Calibration of Pyrgometers. ARM 2008 Science Team Meeting (Poster).



National Renewable Energy Laboratory

Solar Radiation Research Laboratory

Metrology Laboratory

Calibration Certificate



| | | | |
|--------------------------|--------------------------------------|----------------------------------|------------|
| Test Instrument: | Short Normal Incidence Pyrheliometer | Manufacturer: | Eppley |
| Model: | sNIP | Serial Number: | 37882E6 |
| Calibration Date: | 5/5/2020 | Due Date: | 5/5/2021 |
| Customer: | NREL-SRRL-BMS | Environmental Conditions: | see page 4 |
| Test Dates: | 5/4-5 | | |

This certifies that the above product was calibrated in compliance with ISO/IEC 17025:2017. Measurement uncertainties at the time of calibration are consistent with the Guide to the Expression of Uncertainty in Measurement (GUM) using Reda et al., 2008. All nominal values are traceable to the International System (SI) Units of Measurement.

No statement of compliance with specifications is made or implied on this certificate. However, the estimated uncertainties are the uncertainties of the calibration process; users must add other uncertainties that are relevant to their measuring system, environmental and sky conditions, outdoor set-up, and site location.

The Type-B Standard Uncertainty of using the responsivity at each even zenith angle is reported, and the Expanded Uncertainty of the calibration is reported using two methods:

1. The Expanded Uncertainty of using the responsivity at zenith angle = 45°, within the zenith angle range from 30.0° to 60.0°
2. The Expanded Uncertainty of using Spline Interpolating Functions for the responsivity versus zenith angle.

This certificate applies only to the item identified above and shall not be reproduced other than in full, without specific written approval from the calibration facility. Certificate without signature is not valid.

Table 1. Traceability

| Measurement Type | Instrument | Calibration Date | Calibration Due Date |
|----------------------|--|------------------|----------------------|
| Beam Irradiance † | Eppley Absolute Cavity Radiometer Model HF, S/N 29219 | 09/27/2019 | 09/27/2020 |
| Diffuse Irradiance † | Hukseflux Pyranometer Model SR25, S/N 2541 | 04/17/2020 | 04/17/2021 |
| Diffuse Irradiance † | Hukseflux Pyranometer Model SR25, S/N 2542 | 04/17/2020 | 04/17/2021 |
| Data Acquisition | NREL Data Acquisition System Model RAP-DAQ, S/N 2005-998 | 02/14/2019 | 02/14/2021 |
| Data Acquisition | NREL Data Acquisition System Model RAP-DAQ, S/N 2005-999 | 02/14/2019 | 02/14/2021 |

† Through the World Radiometric Reference (WRR)

Number of pages of certificate: 4

Calibration Procedure: BORCAL-P00-Calibration and QA Procedure; available upon request.

Setup: Radiometers are calibrated outdoors, using the sun as the source. Pyranometers and pyrgeometers are installed for horizontal measurements, with their signal connectors oriented north, if their design permits.

The shading disk for the reference diffuse subtends a solid angle of 5°. Pyrheliometers are installed on solar trackers.

Calibrated by: Afshin Andreas, Ibrahim Reda, Peter Gotseff, and RCC

Ibrahim Reda, Technical Manager

Date

For questions or comments, please contact the technical manager at:

ibrahim.reda@nrel.gov; 303-384-6385; 15013 Denver West Parkway, Golden, CO 80401, USA

Calibration Results

37882E6 Eppler sNIP

The responsivity (R , $\mu\text{V}/\text{W}/\text{m}^2$) of the test instrument during calibration is calculated using this Measurement Equation:

$$R = (V - R_{net} * W_{net}) / I \tag{1}$$

where,

- V = radiometer output voltage (microvolts),
 - R_{net} = radiometer net infrared responsivity ($\mu\text{V}/\text{W}/\text{m}^2$), see Table 4,
 - W_{net} = effective net infrared measured by pyrgeometer (W/m^2),
 - = $W_{in} - W_{out} = W_{in} - \sigma * T_c^4$
 - where, W_{in} = incoming infrared (W/m^2), $\sigma = 5.6704 \times 10^{-8} \text{ W} \cdot \text{m}^{-2} \cdot \text{K}^{-4}$,
 - T_c = case temperature of pyrgeometer (K).
- I = reference irradiance (W/m^2), beam (B) or global (G)
 - where, $G = B * \text{COS}(Z) + D$,
 - Z = zenith angle (degrees),
 - D = reference diffuse irradiance (W/m^2).

Figure 1. Responsivity vs Zenith Angle

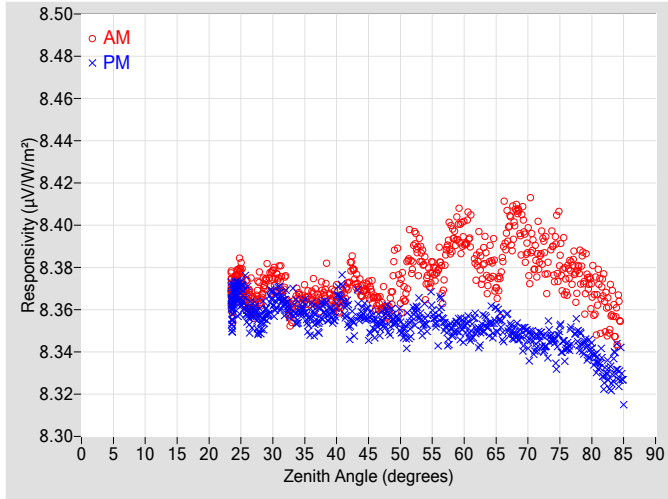


Figure 2. Responsivity vs Local Standard Time

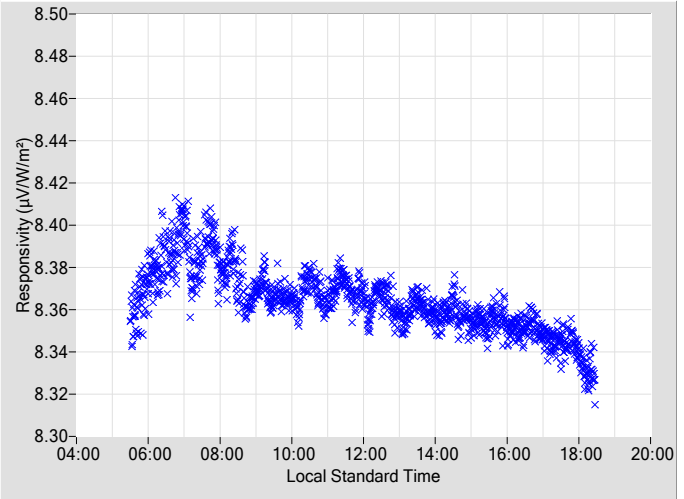


Table 2. Instrument Responsivity (R) and Calibration Type-B Standard Uncertainty, u(B)

| Zenith | | | AM | | | PM | | | Zenith | | | AM | | | PM | | |
|--------|---------------------------------------|-----------|---------|---------------------------------------|-----------|---------|--------|---------------------------------------|-----------|---------|---------------------------------------|-----------|---------|---------------------------------------|-----------|---------|--|
| Angle | R | u(B) | Azimuth | R | u(B) | Azimuth | Angle | R | u(B) | Azimuth | R | u(B) | Azimuth | R | u(B) | Azimuth | |
| (deg.) | ($\mu\text{V}/\text{W}/\text{m}^2$) | \pm (%) | Angle | ($\mu\text{V}/\text{W}/\text{m}^2$) | \pm (%) | Angle | (deg.) | ($\mu\text{V}/\text{W}/\text{m}^2$) | \pm (%) | Angle | ($\mu\text{V}/\text{W}/\text{m}^2$) | \pm (%) | Angle | ($\mu\text{V}/\text{W}/\text{m}^2$) | \pm (%) | Angle | |
| 0 | N/A | N/A | N/A | N/A | N/A | N/A | 46 | 8.3643 | 0.30 | 106.75 | 8.3521 | 0.29 | 252.81 | | | | |
| 2 | N/A | N/A | N/A | N/A | N/A | N/A | 48 | 8.3584 | 0.30 | 104.54 | 8.3577 | 0.29 | 255.06 | | | | |
| 4 | N/A | N/A | N/A | N/A | N/A | N/A | 50 | 8.3690 | 0.33 | 102.42 | 8.3530 | 0.31 | 257.22 | | | | |
| 6 | N/A | N/A | N/A | N/A | N/A | N/A | 52 | 8.3852 | 0.32 | 100.42 | 8.3571 | 0.30 | 259.28 | | | | |
| 8 | N/A | N/A | N/A | N/A | N/A | N/A | 54 | 8.3758 | 0.30 | 98.49 | 8.3553 | 0.29 | 261.26 | | | | |
| 10 | N/A | N/A | N/A | N/A | N/A | N/A | 56 | 8.3815 | 0.29 | 96.62 | 8.3611 | 0.29 | 263.17 | | | | |
| 12 | N/A | N/A | N/A | N/A | N/A | N/A | 58 | 8.3923 | 0.33 | 94.78 | 8.3506 | 0.29 | 264.90 | | | | |
| 14 | N/A | N/A | N/A | N/A | N/A | N/A | 60 | 8.3932 | 0.30 | 93.04 | 8.3507 | 0.31 | 266.71 | | | | |
| 16 | N/A | N/A | N/A | N/A | N/A | N/A | 62 | 8.3837 | 0.30 | 91.34 | 8.3501 | 0.30 | 268.38 | | | | |
| 18 | N/A | N/A | N/A | N/A | N/A | N/A | 64 | 8.3796 | 0.31 | 89.67 | 8.3537 | 0.30 | 270.08 | | | | |
| 20 | N/A | N/A | N/A | N/A | N/A | N/A | 66 | 8.3838 | 0.31 | 88.03 | 8.3493 | 0.30 | 271.71 | | | | |
| 22 | N/A | N/A | N/A | N/A | N/A | N/A | 68 | 8.4031 | 0.30 | 86.42 | 8.3493 | 0.30 | 273.39 | | | | |
| 24 | 8.3700 | 0.30 | 166.85 | 8.3671 | 0.30 | 193.03 | 70 | 8.3853 | 0.30 | 84.81 | 8.3451 | 0.30 | 274.98 | | | | |
| 26 | 8.3670 | 0.31 | 151.02 | 8.3592 | 0.31 | 209.20 | 72 | 8.3854 | 0.30 | 83.22 | 8.3467 | 0.31 | 276.59 | | | | |
| 28 | 8.3672 | 0.30 | 140.63 | 8.3543 | 0.31 | 218.17 | 74 | 8.3869 | 0.32 | 81.60 | 8.3455 | 0.31 | 278.19 | | | | |
| 30 | 8.3755 | 0.29 | 134.43 | 8.3636 | 0.30 | 224.70 | 76 | 8.3741 | 0.33 | 79.98 | 8.3410 | 0.31 | 279.82 | | | | |
| 32 | 8.3701 | 0.30 | 129.23 | 8.3633 | 0.30 | 230.04 | 78 | 8.3796 | 0.32 | 78.38 | 8.3461 | N/A | 281.43 | | | | |
| 34 | 8.3672 | 0.30 | 124.79 | 8.3564 | 0.30 | 234.54 | 80 | 8.3686 | N/A | 76.74 | 8.3399 | N/A | 283.08 | | | | |
| 36 | 8.3657 | 0.31 | 120.85 | 8.3574 | 0.31 | 238.50 | 82 | 8.3650 | N/A | 75.12 | 8.3278 | N/A | 284.72 | | | | |
| 38 | 8.3669 | 0.31 | 117.64 | 8.3600 | 0.29 | 241.89 | 84 | 8.3558 | N/A | 73.41 | 8.3313 | N/A | 286.38 | | | | |
| 40 | 8.3638 | 0.30 | 114.49 | 8.3642 | 0.31 | 244.98 | 86 | N/A | N/A | N/A | N/A | N/A | N/A | | | | |
| 42 | 8.3748 | 0.29 | 111.80 | 8.3535 | 0.29 | 247.79 | 88 | N/A | N/A | N/A | N/A | N/A | N/A | | | | |
| 44 | 8.3680 | 0.30 | 109.14 | 8.3579 | 0.31 | 250.43 | 90 | N/A | N/A | N/A | N/A | N/A | N/A | | | | |

N/A - Not Available

Figure 3. Type-B Standard Uncertainty vs Zenith Angle

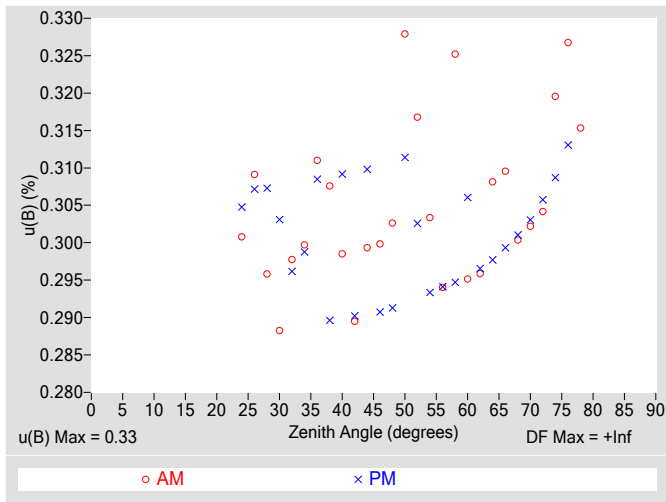


Figure 4. Residuals from Spline Interpolation

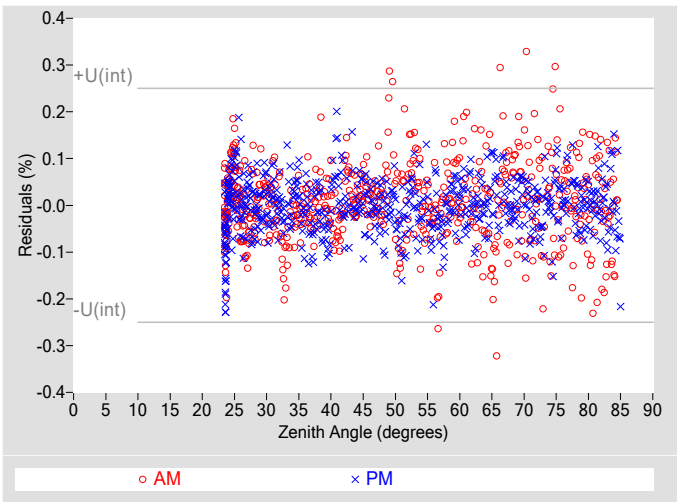


Table 3. Uncertainty using Spline Interpolation ‡

| | |
|---|------------|
| Type-B Standard Uncertainty, $u(B)$ (%) | ± 0.33 |
| Type-A Interpolating Function, $u(int)$ (%) | ± 0.12 |
| Combined Standard Uncertainty, $u(c)$ (%) | ± 0.35 |
| Effective degrees of freedom, $DF(c)$ | 71018 |
| Coverage factor, k | 1.96 |
| Expanded Uncertainty, U_{95} (%) | ± 0.69 |
| AM Valid zenith angle range | 24° to 78° |
| PM Valid zenith angle range | 24° to 76° |

‡ An illustration for how to reduce the uncertainty in calculating the irradiance using a function rather than $R@45^\circ$. Not accredited.

Table 4. Calibration Label Values

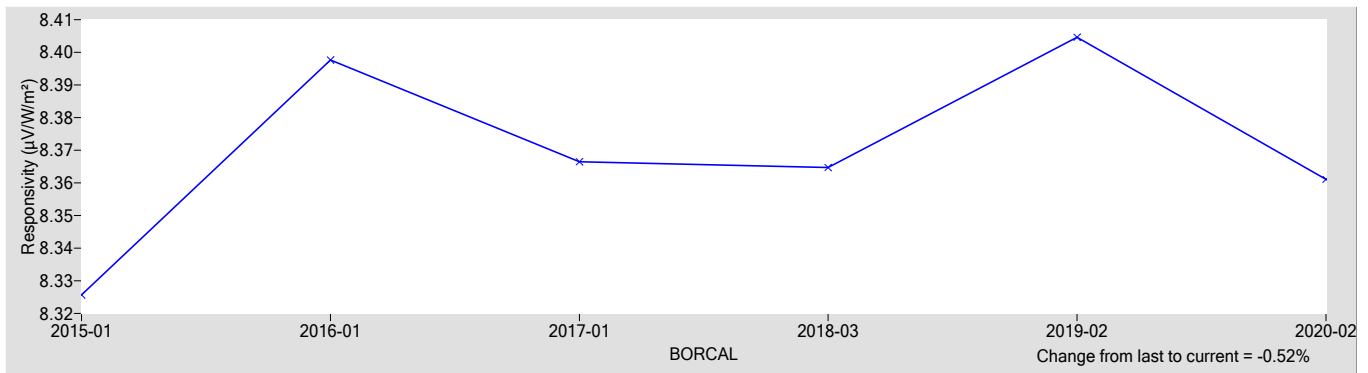
| | |
|----------------------------------|-------------------------------|
| $R @ 45^\circ$ ($\mu V/W/m^2$) | R_{net} ($\mu V/W/m^2$) † |
| 8.3611 | 0 |

† R_{net} determination date: N/A

Table 5. Uncertainty using $R @ 45^\circ$

| | |
|---|----------------|
| Type-B Expanded Uncertainty, $U(B)$ (%) | ± 0.64 |
| Offset Uncertainty, $U(off)$ (%) | +0.38 / -0.12 |
| Expanded Uncertainty, U (%) | +1.0 / -0.77 |
| Effective degrees of freedom, DF | +Inf |
| Coverage factor, k | 1.96 |
| Valid zenith angle range | 30.0° to 60.0° |

Figure 5. History of instrument at Zenith Angle = 45°



References:

[1] Reda, I.; Hickey, J.; Long, C.; Myers, D.; Stoffel, T.; Wilcox, S.; Michalsky, J. J.; Dutton, E. G.; Nelson, D. (2005). "Using a Blackbody to Calculate Net Longwave Responsivity of Shortwave Solar Pyranometers to Correct for Their Thermal Offset Error During Outdoor Calibration Using the Component Sum Method." *Journal of Atmospheric and Oceanic Technology*, 2005; pp. 1531-1540; NREL Report No. JA-560-36646. doi:10.1175/JTECH1782.1

[2] Reda, I.; Myers, D.; Stoffel, T. (2008). "Uncertainty Estimate for the Outdoor Calibration of Solar Pyranometers: A Metrologist Perspective." *Measure*. (NCSLI Journal of Measurement Science). Vol. 3(4), December 2008; pp. 58-66; NREL Report No. JA-581-4137

[3] Reda, I.; Andreas, A. (2004). "Solar Position Algorithm for Solar Radiation Applications." *Solar Energy*. Vol. 76(5), 2004; pp. 577-589; NREL Report No. JA-560-35518. doi:10.1016/j.solener.2003.12.003

[4] Stoffel, T.; Reda, I. (2009). "NREL Pyrheliometer Comparisons: 22 September - 3 October 2008 (NPC-2008)." 54 pp.; NREL Report No. TP-550-45016.

[5] Reda, I.; Stoffel, T.; Myers, D. (2003). "Method to Calibrate a Solar Pyranometer for Measuring Reference Diffuse Irradiance." *Solar Energy*. Vol. 74, 2003; pp. 103-112; NREL Report No. JA-560-35025. doi:10.1016/S0038-092X(03)00124-5

[6] Reda, I. (1996). Calibration of a Solar Absolute Cavity Radiometer with Traceability to the World Radiometric Reference. 79 pp.; NREL Report No. TP-463-20619.

[7] Reda, I.; Gröbner, J.; Stoffel, T.; Myers, D.; Forgan, B. (2008). Improvements in the Blackbody Calibration of Pyrgometers. ARM 2008 Science Team Meeting (Poster).



National Renewable Energy Laboratory

Solar Radiation Research Laboratory

Metrology Laboratory

Calibration Certificate



| | | | |
|--------------------------|---|----------------------------------|------------|
| Test Instrument: | Standard Precision Pyranometer (Ventilated) | Manufacturer: | Eppley |
| Model: | SPP | Serial Number: | 38924F3 |
| Calibration Date: | 5/5/2020 | Due Date: | 5/5/2021 |
| Customer: | NREL-SRRL-BMS | Environmental Conditions: | see page 4 |
| Test Dates: | 5/4-5 | | |

This certifies that the above product was calibrated in compliance with ISO/IEC 17025:2017. Measurement uncertainties at the time of calibration are consistent with the Guide to the Expression of Uncertainty in Measurement (GUM) using Reda et al., 2008. All nominal values are traceable to the International System (SI) Units of Measurement.

No statement of compliance with specifications is made or implied on this certificate. However, the estimated uncertainties are the uncertainties of the calibration process; users must add other uncertainties that are relevant to their measuring system, environmental and sky conditions, outdoor set-up, and site location.

The Type-B Standard Uncertainty of using the responsivity at each even zenith angle is reported, and the Expanded Uncertainty of the calibration is reported using two methods:

1. The Expanded Uncertainty of using the responsivity at zenith angle = 45°, within the zenith angle range from 30.0° to 60.0°
2. The Expanded Uncertainty of using Spline Interpolating Functions for the responsivity versus zenith angle.

This certificate applies only to the item identified above and shall not be reproduced other than in full, without specific written approval from the calibration facility. Certificate without signature is not valid.

Table 1. Traceability

| Measurement Type | Instrument | Calibration Date | Calibration Due Date |
|-----------------------|--|------------------|----------------------|
| Beam Irradiance † | Eppley Absolute Cavity Radiometer Model HF, S/N 29219 | 09/27/2019 | 09/27/2020 |
| Diffuse Irradiance † | Hukseflux Pyranometer Model SR25, S/N 2541 | 04/17/2020 | 04/17/2021 |
| Diffuse Irradiance † | Hukseflux Pyranometer Model SR25, S/N 2542 | 04/17/2020 | 04/17/2021 |
| Data Acquisition | NREL Data Acquisition System Model RAP-DAQ, S/N 2005-998 | 02/14/2019 | 02/14/2021 |
| Data Acquisition | NREL Data Acquisition System Model RAP-DAQ, S/N 2005-999 | 02/14/2019 | 02/14/2021 |
| Infrared Irradiance ‡ | Eppley Downwelling Pyrgeometer (Ventilated) Model PIR-V, S/N 31203F3 | 04/02/2019 | 04/02/2023 |

† Through the World Radiometric Reference (WRR)

‡ Through the World Infrared Standard Group (WISG)

Number of pages of certificate: 4

Calibration Procedure: BORCAL-P00-Calibration and QA Procedure; available upon request.

Setup: Radiometers are calibrated outdoors, using the sun as the source. Pyranometers and pyrgeometers are installed for horizontal measurements, with their signal connectors oriented north, if their design permits.

The shading disk for the reference diffuse subtends a solid angle of 5°. Pyrheliometers are installed on solar trackers.

Calibrated by: Afshin Andreas, Ibrahim Reda, Peter Gotseff, and RCC

Ibrahim Reda, Technical Manager

Date

For questions or comments, please contact the technical manager at:
ibrahim.reda@nrel.gov; 303-384-6385; 15013 Denver West Parkway, Golden, CO 80401, USA

Calibration Results

38924F3 Eppley SPP

The responsivity (R , $\mu\text{V}/\text{W}/\text{m}^2$) of the test instrument during calibration is calculated using this Measurement Equation:

$$R = (V - R_{net} * W_{net}) / I \tag{1}$$

where,

- V = radiometer output voltage (microvolts),
 - R_{net} = radiometer net infrared responsivity ($\mu\text{V}/\text{W}/\text{m}^2$), see Table 4,
 - W_{net} = effective net infrared measured by pyrgeometer (W/m^2),
 - = $W_{in} - W_{out} = W_{in} - \sigma * T_c^4$
 - where, W_{in} = incoming infrared (W/m^2), $\sigma = 5.6704\text{e-}8 \text{ W}\cdot\text{m}^{-2}\cdot\text{K}^{-4}$,
 - T_c = case temperature of pyrgeometer (K).
- I = reference irradiance (W/m^2), beam (B) or global (G)
 - where, $G = B * \text{COS}(Z) + D$,
 - Z = zenith angle (degrees),
 - D = reference diffuse irradiance (W/m^2).

Figure 1. Responsivity vs Zenith Angle

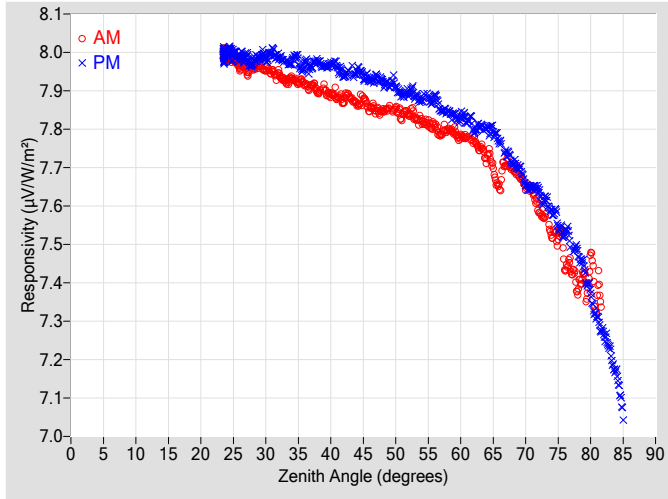


Figure 2. Responsivity vs Local Standard Time

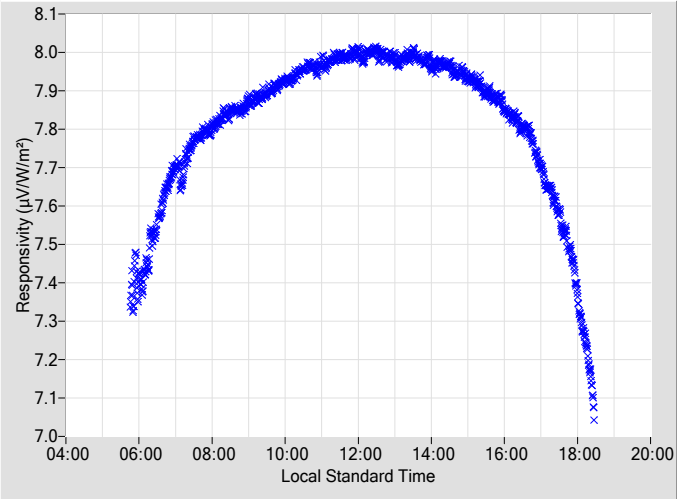


Table 2. Instrument Responsivity (R) and Calibration Type-B Standard Uncertainty, $u(B)$

| Zenith Angle (deg.) | R ($\mu\text{V}/\text{W}/\text{m}^2$) | AM $u(B)$ \pm (%) | Azimuth Angle | R ($\mu\text{V}/\text{W}/\text{m}^2$) | PM $u(B)$ \pm (%) | Azimuth Angle | Zenith Angle (deg.) | R ($\mu\text{V}/\text{W}/\text{m}^2$) | AM $u(B)$ \pm (%) | Azimuth Angle | R ($\mu\text{V}/\text{W}/\text{m}^2$) | PM $u(B)$ \pm (%) | Azimuth Angle |
|---------------------|---|---------------------|---------------|---|---------------------|---------------|---------------------|---|---------------------|---------------|---|---------------------|---------------|
| 0 | N/A | N/A | N/A | N/A | N/A | N/A | 46 | 7.8527 | 0.31 | 106.79 | 7.9286 | 0.33 | 252.84 |
| 2 | N/A | N/A | N/A | N/A | N/A | N/A | 48 | 7.8478 | 0.33 | 104.51 | 7.9229 | 0.32 | 255.10 |
| 4 | N/A | N/A | N/A | N/A | N/A | N/A | 50 | 7.8524 | 0.36 | 102.43 | 7.9089 | 0.32 | 257.25 |
| 6 | N/A | N/A | N/A | N/A | N/A | N/A | 52 | 7.8373 | 0.34 | 100.40 | 7.8957 | 0.34 | 259.31 |
| 8 | N/A | N/A | N/A | N/A | N/A | N/A | 54 | 7.8205 | 0.33 | 98.42 | 7.8770 | 0.33 | 261.24 |
| 10 | N/A | N/A | N/A | N/A | N/A | N/A | 56 | 7.8095 | 0.34 | 96.60 | 7.8858 | 0.34 | 263.12 |
| 12 | N/A | N/A | N/A | N/A | N/A | N/A | 58 | 7.7973 | 0.36 | 94.82 | 7.8451 | 0.35 | 264.93 |
| 14 | N/A | N/A | N/A | N/A | N/A | N/A | 60 | 7.7788 | 0.36 | 93.07 | 7.8338 | 0.38 | 266.69 |
| 16 | N/A | N/A | N/A | N/A | N/A | N/A | 62 | 7.7728 | 0.40 | 91.37 | 7.7988 | 0.39 | 268.41 |
| 18 | N/A | N/A | N/A | N/A | N/A | N/A | 64 | 7.7252 | 0.40 | 89.69 | 7.8026 | 0.38 | 270.07 |
| 20 | N/A | N/A | N/A | N/A | N/A | N/A | 66 | 7.6525 | 0.40 | 88.05 | 7.7661 | 0.40 | 271.74 |
| 22 | N/A | N/A | N/A | N/A | N/A | N/A | 68 | 7.6978 | 0.42 | 86.39 | 7.7086 | 0.42 | 273.38 |
| 24 | 7.9893 | 0.31 | 166.91 | 8.0009 | 0.32 | 193.13 | 70 | 7.6506 | 0.45 | 84.79 | 7.6541 | 0.45 | 275.00 |
| 26 | 7.9656 | 0.32 | 150.96 | 7.9887 | 0.33 | 209.09 | 72 | 7.5936 | 0.48 | 83.20 | 7.6415 | 0.49 | 276.57 |
| 28 | 7.9627 | 0.34 | 140.78 | 7.9718 | 0.31 | 217.99 | 74 | 7.5274 | 0.52 | 81.62 | 7.5824 | 0.54 | 278.21 |
| 30 | 7.9560 | 0.33 | 134.32 | 7.9836 | 0.33 | 224.77 | 76 | 7.4500 | 0.64 | 80.01 | 7.5287 | 0.61 | 279.81 |
| 32 | 7.9437 | 0.31 | 129.15 | 7.9876 | 0.33 | 230.00 | 78 | 7.3862 | 0.67 | 78.40 | 7.4813 | N/A | 281.42 |
| 34 | 7.9320 | 0.31 | 124.77 | 7.9747 | 0.31 | 234.38 | 80 | 7.4544 | N/A | 76.76 | 7.3730 | N/A | 283.06 |
| 36 | 7.9175 | 0.32 | 121.04 | 7.9718 | 0.30 | 238.43 | 82 | N/A | N/A | N/A | 7.2652 | N/A | 284.71 |
| 38 | 7.8974 | 0.32 | 117.60 | 7.9765 | 0.31 | 241.85 | 84 | N/A | N/A | N/A | 7.1576 | N/A | 286.40 |
| 40 | 7.8898 | 0.32 | 114.53 | 7.9691 | 0.32 | 245.10 | 86 | N/A | N/A | N/A | N/A | N/A | N/A |
| 42 | 7.8745 | 0.34 | 111.70 | 7.9384 | 0.34 | 247.83 | 88 | N/A | N/A | N/A | N/A | N/A | N/A |
| 44 | 7.8660 | 0.34 | 109.18 | 7.9501 | 0.31 | 250.41 | 90 | N/A | N/A | N/A | N/A | N/A | N/A |

N/A - Not Available

Figure 3. Type-B Standard Uncertainty vs Zenith Angle

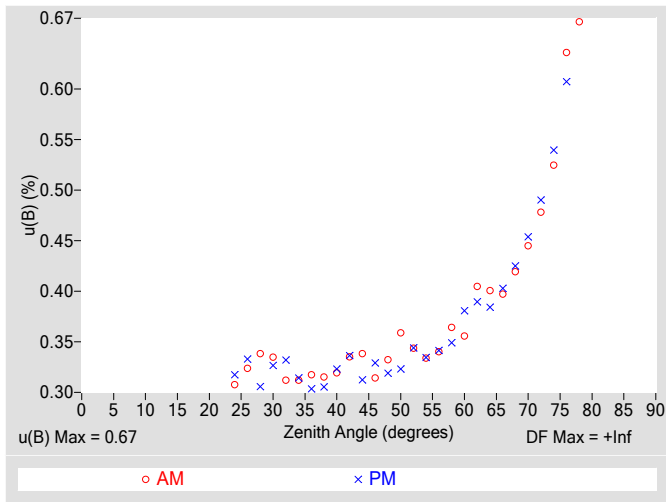


Figure 4. Residuals from Spline Interpolation

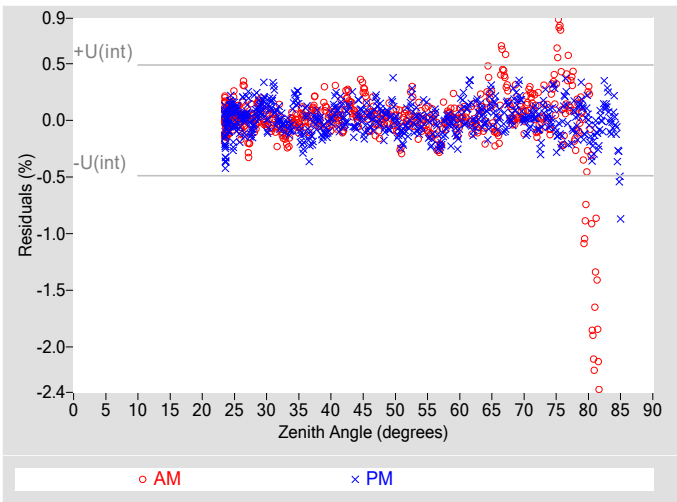


Table 3. Uncertainty using Spline Interpolation ‡

| | |
|---|------------|
| Type-B Standard Uncertainty, $u(B)$ (%) | ± 0.67 |
| Type-A Interpolating Function, $u(int)$ (%) | ± 0.24 |
| Combined Standard Uncertainty, $u(c)$ (%) | ± 0.71 |
| Effective degrees of freedom, $DF(c)$ | 82232 |
| Coverage factor, k | 1.96 |
| Expanded Uncertainty, U_{95} (%) | ± 1.4 |
| AM Valid zenith angle range | 24° to 78° |
| PM Valid zenith angle range | 24° to 76° |

‡ An illustration for how to reduce the uncertainty in calculating the irradiance using a function rather than $R@45^\circ$. Not accredited.

Table 4. Calibration Label Values

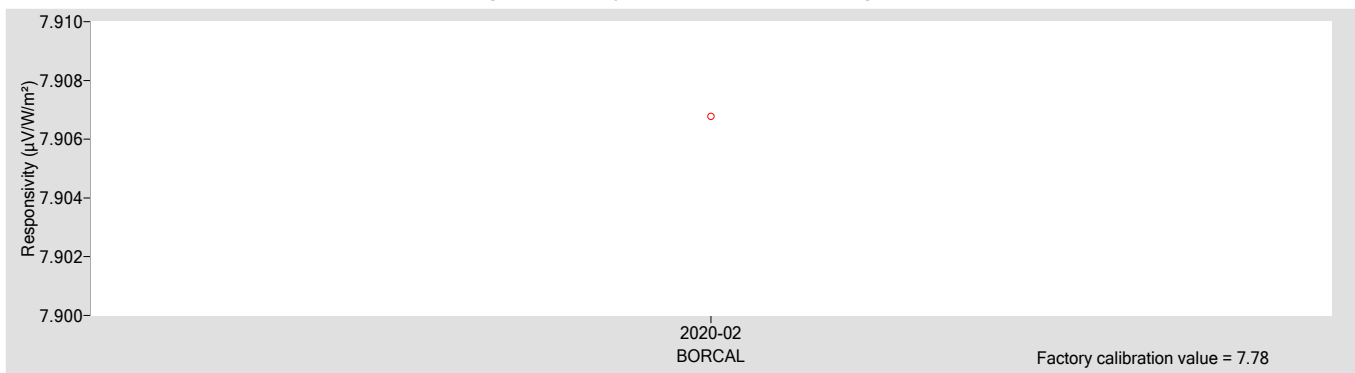
| | |
|----------------------------------|-------------------------------|
| $R @ 45^\circ$ ($\mu V/W/m^2$) | R_{net} ($\mu V/W/m^2$) † |
| 7.9068 | 0.22000 |

† R_{net} determination date: Estimated

Table 5. Uncertainty using $R @ 45^\circ$

| | |
|---|----------------|
| Type-B Expanded Uncertainty, $U(B)$ (%) | ± 0.75 |
| Offset Uncertainty, $U(off)$ (%) | +1.0 / -1.6 |
| Expanded Uncertainty, U (%) | +1.8 / -2.4 |
| Effective degrees of freedom, DF | +Inf |
| Coverage factor, k | 1.96 |
| Valid zenith angle range | 30.0° to 60.0° |

Figure 5. History of instrument at Zenith Angle = 45°



References:

[1] Reda, I.; Hickey, J.; Long, C.; Myers, D.; Stoffel, T.; Wilcox, S.; Michalsky, J. J.; Dutton, E. G.; Nelson, D. (2005). "Using a Blackbody to Calculate Net Longwave Responsivity of Shortwave Solar Pyranometers to Correct for Their Thermal Offset Error During Outdoor Calibration Using the Component Sum Method." *Journal of Atmospheric and Oceanic Technology*, 2005; pp. 1531-1540; NREL Report No. JA-560-36646. doi:10.1175/JTECH1782.1

[2] Reda, I.; Myers, D.; Stoffel, T. (2008). "Uncertainty Estimate for the Outdoor Calibration of Solar Pyranometers: A Metrologist Perspective." *Measure*. (NCSLI *Journal of Measurement Science*). Vol. 3(4), December 2008; pp. 58-66; NREL Report No. JA-581-4137

[3] Reda, I.; Andreas, A. (2004). "Solar Position Algorithm for Solar Radiation Applications." *Solar Energy*. Vol. 76(5), 2004; pp. 577-589; NREL Report No. JA-560-35518. doi:10.1016/j.solener.2003.12.003

[4] Stoffel, T.; Reda, I. (2009). "NREL Pyrheliometer Comparisons: 22 September - 3 October 2008 (NPC-2008)." 54 pp.; NREL Report No. TP-550-45016.

[5] Reda, I.; Stoffel, T.; Myers, D. (2003). "Method to Calibrate a Solar Pyranometer for Measuring Reference Diffuse Irradiance." *Solar Energy*. Vol. 74, 2003; pp. 103-112; NREL Report No. JA-560-35025. doi:10.1016/S0038-092X(03)00124-5

[6] Reda, I. (1996). *Calibration of a Solar Absolute Cavity Radiometer with Traceability to the World Radiometric Reference*. 79 pp.; NREL Report No. TP-463-20619.

[7] Reda, I.; Gröbner, J.; Stoffel, T.; Myers, D.; Forgan, B. (2008). *Improvements in the Blackbody Calibration of Pyrgometers*. ARM 2008 Science Team Meeting (Poster).



National Renewable Energy Laboratory

Solar Radiation Research Laboratory

Metrology Laboratory

Calibration Certificate



| | | | |
|--------------------------|----------------|----------------------------------|------------|
| Test Instrument: | Si pyranometer | Manufacturer: | Apogee |
| Model: | SP-110 | Serial Number: | 40337 |
| Calibration Date: | 5/5/2020 | Due Date: | 5/5/2021 |
| Customer: | NREL-SRRL-BMS | Environmental Conditions: | see page 4 |
| Test Dates: | 5/4-5 | | |

This certifies that the above product was calibrated in compliance with ISO/IEC 17025:2017. Measurement uncertainties at the time of calibration are consistent with the Guide to the Expression of Uncertainty in Measurement (GUM) using Reda et al., 2008. All nominal values are traceable to the International System (SI) Units of Measurement.

No statement of compliance with specifications is made or implied on this certificate. However, the estimated uncertainties are the uncertainties of the calibration process; users must add other uncertainties that are relevant to their measuring system, environmental and sky conditions, outdoor set-up, and site location.

The Type-B Standard Uncertainty of using the responsivity at each even zenith angle is reported, and the Expanded Uncertainty of the calibration is reported using two methods:

1. The Expanded Uncertainty of using the responsivity at zenith angle = 45°, within the zenith angle range from 30.0° to 60.0°
2. The Expanded Uncertainty of using Spline Interpolating Functions for the responsivity versus zenith angle.

This certificate applies only to the item identified above and shall not be reproduced other than in full, without specific written approval from the calibration facility. Certificate without signature is not valid.

Table 1. Traceability

| Measurement Type | Instrument | Calibration Date | Calibration Due Date |
|----------------------|--|------------------|----------------------|
| Beam Irradiance † | Eppley Absolute Cavity Radiometer Model HF, S/N 29219 | 09/27/2019 | 09/27/2020 |
| Diffuse Irradiance † | Hukseflux Pyranometer Model SR25, S/N 2541 | 04/17/2020 | 04/17/2021 |
| Diffuse Irradiance † | Hukseflux Pyranometer Model SR25, S/N 2542 | 04/17/2020 | 04/17/2021 |
| Data Acquisition | NREL Data Acquisition System Model RAP-DAQ, S/N 2005-998 | 02/14/2019 | 02/14/2021 |
| Data Acquisition | NREL Data Acquisition System Model RAP-DAQ, S/N 2005-999 | 02/14/2019 | 02/14/2021 |

† Through the World Radiometric Reference (WRR)

Number of pages of certificate: 4

Calibration Procedure: BORCAL-P00-Calibration and QA Procedure; available upon request.

Setup: Radiometers are calibrated outdoors, using the sun as the source. Pyranometers and pyrgeometers are installed for horizontal measurements, with their signal connectors oriented north, if their design permits.
The shading disk for the reference diffuse subtends a solid angle of 5°. Pyrheliometers are installed on solar trackers.

Calibrated by: Afshin Andreas, Ibrahim Reda, Peter Gotseff, and RCC

Ibrahim Reda, Technical Manager

Date

For questions or comments, please contact the technical manager at:
ibrahim.reda@nrel.gov; 303-384-6385; 15013 Denver West Parkway, Golden, CO 80401, USA

Calibration Results

40337 Apogee SP-110

The responsivity (R , $\mu\text{V}/\text{W}/\text{m}^2$) of the test instrument during calibration is calculated using this Measurement Equation:

$$R = (V - R_{net} * W_{net}) / I \tag{1}$$

where,

- V = radiometer output voltage (microvolts),
 - R_{net} = radiometer net infrared responsivity ($\mu\text{V}/\text{W}/\text{m}^2$), see Table 4,
 - W_{net} = effective net infrared measured by pyrgeometer (W/m^2),
 - = $W_{in} - W_{out} = W_{in} - \sigma * T_c^4$
 - where, W_{in} = incoming infrared (W/m^2), $\sigma = 5.6704\text{e-}8 \text{ W}\cdot\text{m}^{-2}\cdot\text{K}^{-4}$,
 - T_c = case temperature of pyrgeometer (K).
- I = reference irradiance (W/m^2), beam (B) or global (G)
 - where, $G = B * \text{COS}(Z) + D$,
 - Z = zenith angle (degrees),
 - D = reference diffuse irradiance (W/m^2).

Figure 1. Responsivity vs Zenith Angle

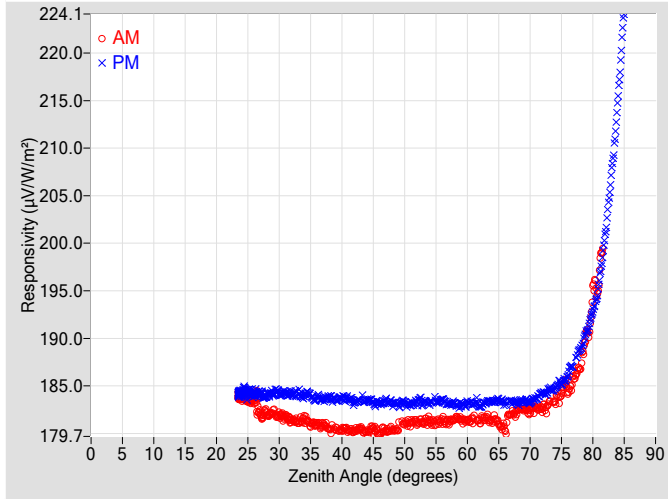


Figure 2. Responsivity vs Local Standard Time

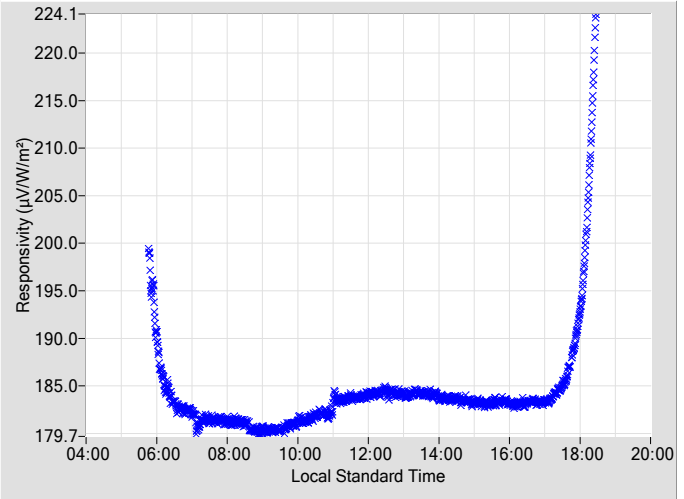


Table 2. Instrument Responsivity (R) and Calibration Type-B Standard Uncertainty, $u(B)$

| Zenith Angle (deg.) | R ($\mu\text{V}/\text{W}/\text{m}^2$) | AM $u(B)$ \pm (%) | Azimuth Angle | R ($\mu\text{V}/\text{W}/\text{m}^2$) | PM $u(B)$ \pm (%) | Azimuth Angle | Zenith Angle (deg.) | R ($\mu\text{V}/\text{W}/\text{m}^2$) | AM $u(B)$ \pm (%) | Azimuth Angle | R ($\mu\text{V}/\text{W}/\text{m}^2$) | PM $u(B)$ \pm (%) | Azimuth Angle |
|---------------------|---|---------------------|---------------|---|---------------------|---------------|---------------------|---|---------------------|---------------|---|---------------------|---------------|
| 0 | N/A | N/A | N/A | N/A | N/A | N/A | 46 | 179.86 | 0.31 | 106.80 | 183.17 | 0.31 | 252.79 |
| 2 | N/A | N/A | N/A | N/A | N/A | N/A | 48 | 180.47 | 0.31 | 104.58 | 183.21 | 0.35 | 255.10 |
| 4 | N/A | N/A | N/A | N/A | N/A | N/A | 50 | 181.08 | 0.34 | 102.44 | 183.24 | 0.31 | 257.26 |
| 6 | N/A | N/A | N/A | N/A | N/A | N/A | 52 | 181.14 | 0.32 | 100.40 | 183.35 | 0.32 | 259.26 |
| 8 | N/A | N/A | N/A | N/A | N/A | N/A | 54 | 181.35 | 0.37 | 98.48 | 183.24 | 0.34 | 261.25 |
| 10 | N/A | N/A | N/A | N/A | N/A | N/A | 56 | 181.39 | 0.37 | 96.61 | 183.54 | 0.35 | 263.12 |
| 12 | N/A | N/A | N/A | N/A | N/A | N/A | 58 | 181.53 | 0.35 | 94.82 | 183.08 | 0.33 | 264.94 |
| 14 | N/A | N/A | N/A | N/A | N/A | N/A | 60 | 181.38 | 0.34 | 93.07 | 183.14 | 0.34 | 266.69 |
| 16 | N/A | N/A | N/A | N/A | N/A | N/A | 62 | 181.36 | 0.35 | 91.32 | 182.82 | 0.35 | 268.42 |
| 18 | N/A | N/A | N/A | N/A | N/A | N/A | 64 | 181.33 | 0.36 | 89.70 | 183.40 | 0.36 | 270.07 |
| 20 | N/A | N/A | N/A | N/A | N/A | N/A | 66 | 180.59 | 0.38 | 88.01 | 183.20 | 0.38 | 271.70 |
| 22 | N/A | N/A | N/A | N/A | N/A | N/A | 68 | 182.41 | 0.39 | 86.40 | 183.20 | 0.40 | 273.38 |
| 24 | 183.78 | 0.32 | 167.05 | 184.30 | 0.31 | 192.79 | 70 | 182.42 | 0.45 | 84.80 | 183.28 | 0.42 | 274.97 |
| 26 | 183.66 | 0.30 | 150.98 | 184.20 | 0.30 | 209.16 | 72 | 182.75 | 0.45 | 83.21 | 184.30 | 0.45 | 276.62 |
| 28 | 182.13 | 0.31 | 140.72 | 184.03 | 0.31 | 218.13 | 74 | 183.52 | 0.49 | 81.58 | 184.81 | 0.49 | 278.18 |
| 30 | 181.89 | 0.33 | 134.44 | 184.26 | 0.32 | 224.67 | 76 | 184.55 | 0.54 | 80.01 | 186.23 | 0.55 | 279.81 |
| 32 | 181.30 | 0.29 | 129.20 | 184.16 | 0.30 | 230.00 | 78 | 187.18 | 0.61 | 78.37 | 188.94 | N/A | 281.42 |
| 34 | 181.51 | 0.30 | 124.88 | 184.02 | 0.30 | 234.57 | 80 | 194.57 | N/A | 76.77 | 192.95 | N/A | 283.07 |
| 36 | 180.99 | 0.31 | 120.96 | 183.78 | 0.31 | 238.47 | 82 | N/A | N/A | N/A | 201.10 | N/A | 284.71 |
| 38 | 180.38 | 0.33 | 117.63 | 183.84 | 0.30 | 241.86 | 84 | N/A | N/A | N/A | 215.09 | N/A | 286.37 |
| 40 | 180.38 | 0.31 | 114.61 | 183.80 | 0.30 | 244.96 | 86 | N/A | N/A | N/A | N/A | N/A | N/A |
| 42 | 180.27 | 0.30 | 111.78 | 183.24 | 0.32 | 247.77 | 88 | N/A | N/A | N/A | N/A | N/A | N/A |
| 44 | 180.15 | 0.32 | 109.18 | 183.48 | 0.30 | 250.42 | 90 | N/A | N/A | N/A | N/A | N/A | N/A |

N/A - Not Available

Figure 3. Type-B Standard Uncertainty vs Zenith Angle

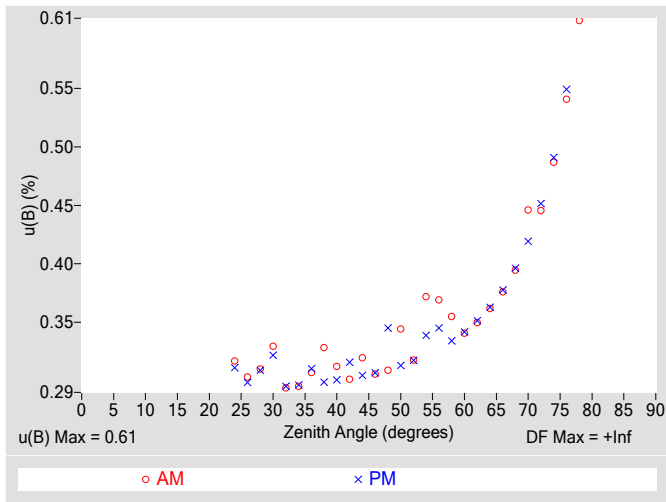


Figure 4. Residuals from Spline Interpolation

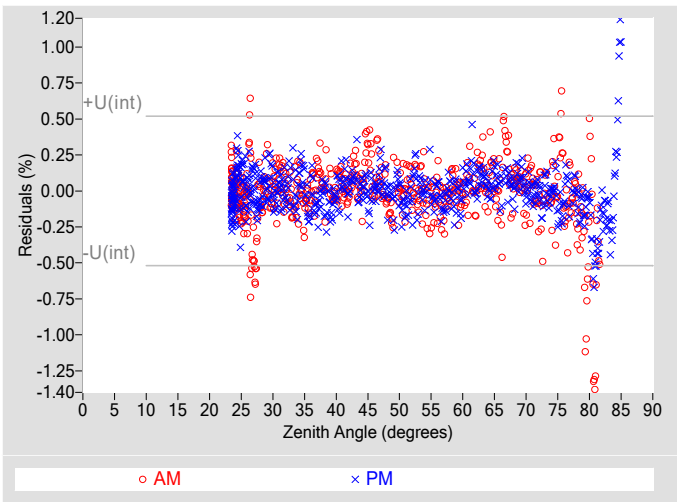


Table 3. Uncertainty using Spline Interpolation ‡

| | |
|---|------------|
| Type-B Standard Uncertainty, $u(B)$ (%) | ± 0.61 |
| Type-A Interpolating Function, $u(int)$ (%) | ± 0.26 |
| Combined Standard Uncertainty, $u(c)$ (%) | ± 0.66 |
| Effective degrees of freedom, $DF(c)$ | 48351 |
| Coverage factor, k | 1.96 |
| Expanded Uncertainty, $U95$ (%) | ± 1.3 |
| AM Valid zenith angle range | 24° to 78° |
| PM Valid zenith angle range | 24° to 76° |

‡ An illustration for how to reduce the uncertainty in calculating the irradiance using a function rather than $R@45^\circ$. Not accredited.

Table 4. Calibration Label Values

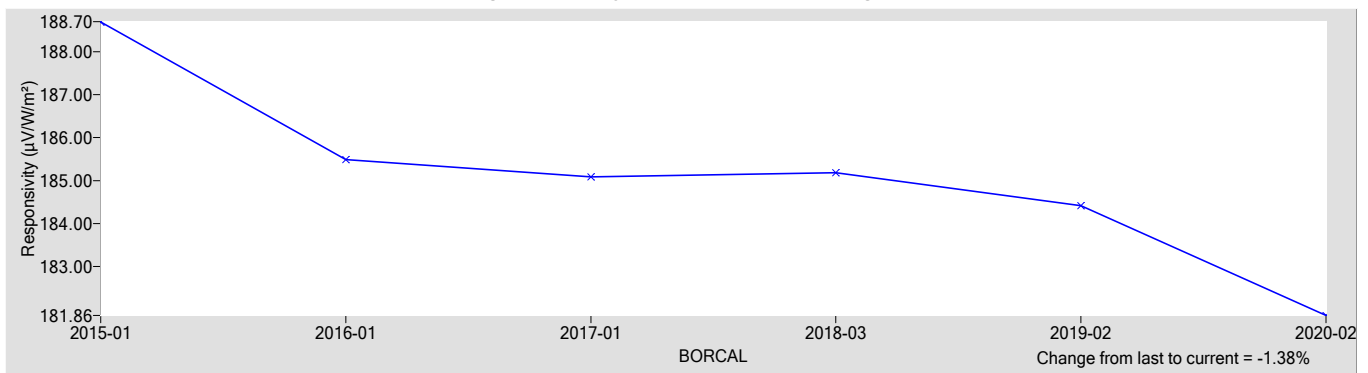
| | |
|----------------------------------|-------------------------------|
| $R @ 45^\circ$ ($\mu V/W/m^2$) | R_{net} ($\mu V/W/m^2$) † |
| 181.86 | 0 |

† R_{net} determination date: N/A

Table 5. Uncertainty using $R @ 45^\circ$

| | |
|---|----------------|
| Type-B Expanded Uncertainty, $U(B)$ (%) | ± 0.73 |
| Offset Uncertainty, $U(off)$ (%) | +1.3 / -1.1 |
| Expanded Uncertainty, U (%) | +2.0 / -1.8 |
| Effective degrees of freedom, DF | +Inf |
| Coverage factor, k | 1.96 |
| Valid zenith angle range | 30.0° to 60.0° |

Figure 5. History of instrument at Zenith Angle = 45°



References:

[1] Reda, I.; Hickey, J.; Long, C.; Myers, D.; Stoffel, T.; Wilcox, S.; Michalsky, J. J.; Dutton, E. G.; Nelson, D. (2005). "Using a Blackbody to Calculate Net Longwave Responsivity of Shortwave Solar Pyranometers to Correct for Their Thermal Offset Error During Outdoor Calibration Using the Component Sum Method." *Journal of Atmospheric and Oceanic Technology*, 2005; pp. 1531-1540; NREL Report No. JA-560-36646. doi:10.1175/JTECH1782.1

[2] Reda, I.; Myers, D.; Stoffel, T. (2008). "Uncertainty Estimate for the Outdoor Calibration of Solar Pyranometers: A Metrologist Perspective." *Measure*. (NCSLI Journal of Measurement Science). Vol. 3(4), December 2008; pp. 58-66; NREL Report No. JA-581-4137

[3] Reda, I.; Andreas, A. (2004). "Solar Position Algorithm for Solar Radiation Applications." *Solar Energy*. Vol. 76(5), 2004; pp. 577-589; NREL Report No. JA-560-35518. doi:10.1016/j.solener.2003.12.003

[4] Stoffel, T.; Reda, I. (2009). "NREL Pyrheliometer Comparisons: 22 September - 3 October 2008 (NPC-2008)." 54 pp.; NREL Report No. TP-550-45016.

[5] Reda, I.; Stoffel, T.; Myers, D. (2003). "Method to Calibrate a Solar Pyranometer for Measuring Reference Diffuse Irradiance." *Solar Energy*. Vol. 74, 2003; pp. 103-112; NREL Report No. JA-560-35025. doi:10.1016/S0038-092X(03)00124-5

[6] Reda, I. (1996). Calibration of a Solar Absolute Cavity Radiometer with Traceability to the World Radiometric Reference. 79 pp.; NREL Report No. TP-463-20619.

[7] Reda, I.; Gröbner, J.; Stoffel, T.; Myers, D.; Forgan, B. (2008). Improvements in the Blackbody Calibration of Pyrgometers. ARM 2008 Science Team Meeting (Poster).

National Renewable Energy Laboratory

Solar Radiation Research Laboratory

Metrology Laboratory

Calibration Certificate



Test Instrument: Pyrheliometer
Manufacturer: Hukseflux
Model: DR02
Serial Number: 9206
Calibration Date: 5/5/2020
Due Date: 5/5/2021
Customer: NREL-SRRL-BMS
Environmental Conditions: see page 4
Test Dates: 5/4-5

This certifies that the above product was calibrated in compliance with ISO/IEC 17025:2017. Measurement uncertainties at the time of calibration are consistent with the Guide to the Expression of Uncertainty in Measurement (GUM) using Reda et al., 2008. All nominal values are traceable to the International System (SI) Units of Measurement.

No statement of compliance with specifications is made or implied on this certificate. However, the estimated uncertainties are the uncertainties of the calibration process; users must add other uncertainties that are relevant to their measuring system, environmental and sky conditions, outdoor set-up, and site location.

The Type-B Standard Uncertainty of using the responsivity at each even zenith angle is reported, and the Expanded Uncertainty of the calibration is reported using two methods:

1. The Expanded Uncertainty of using the responsivity at zenith angle = 45°, within the zenith angle range from 30.0° to 60.0°
2. The Expanded Uncertainty of using Spline Interpolating Functions for the responsivity versus zenith angle.

This certificate applies only to the item identified above and shall not be reproduced other than in full, without specific written approval from the calibration facility. Certificate without signature is not valid.

Table 1. Traceability

| Measurement Type | Instrument | Calibration Date | Calibration Due Date |
|----------------------|--|------------------|----------------------|
| Beam Irradiance † | Eppley Absolute Cavity Radiometer Model HF, S/N 29219 | 09/27/2019 | 09/27/2020 |
| Diffuse Irradiance † | Hukseflux Pyranometer Model SR25, S/N 2541 | 04/17/2020 | 04/17/2021 |
| Diffuse Irradiance † | Hukseflux Pyranometer Model SR25, S/N 2542 | 04/17/2020 | 04/17/2021 |
| Data Acquisition | NREL Data Acquisition System Model RAP-DAQ, S/N 2005-998 | 02/14/2019 | 02/14/2021 |
| Data Acquisition | NREL Data Acquisition System Model RAP-DAQ, S/N 2005-999 | 02/14/2019 | 02/14/2021 |

† Through the World Radiometric Reference (WRR)

Number of pages of certificate: 4

Calibration Procedure: BORCAL-P00-Calibration and QA Procedure; available upon request.

Setup: Radiometers are calibrated outdoors, using the sun as the source. Pyranometers and pyrgeometers are installed for horizontal measurements, with their signal connectors oriented north, if their design permits.

The shading disk for the reference diffuse subtends a solid angle of 5°. Pyrheliometers are installed on solar trackers.

Calibrated by: Afshin Andreas, Ibrahim Reda, Peter Gotseff, and RCC

Ibrahim Reda, Technical Manager

Date

For questions or comments, please contact the technical manager at:

ibrahim.reda@nrel.gov; 303-384-6385; 15013 Denver West Parkway, Golden, CO 80401, USA

Calibration Results

9206 Hukseflux DR02

The responsivity (R , $\mu\text{V}/\text{W}/\text{m}^2$) of the test instrument during calibration is calculated using this Measurement Equation:

$$R = (V - R_{net} * W_{net}) / I \tag{1}$$

where,

- V = radiometer output voltage (microvolts),
 - R_{net} = radiometer net infrared responsivity ($\mu\text{V}/\text{W}/\text{m}^2$), see Table 4,
 - W_{net} = effective net infrared measured by pyrgeometer (W/m^2),
 - = $W_{in} - W_{out} = W_{in} - \sigma * T_c^4$
 - where, W_{in} = incoming infrared (W/m^2), $\sigma = 5.6704\text{e-}8 \text{ W}\cdot\text{m}^{-2}\cdot\text{K}^{-4}$,
 - T_c = case temperature of pyrgeometer (K).
- I = reference irradiance (W/m^2), beam (B) or global (G)
 - where, $G = B * \text{COS}(Z) + D$,
 - Z = zenith angle (degrees),
 - D = reference diffuse irradiance (W/m^2).

Figure 1. Responsivity vs Zenith Angle

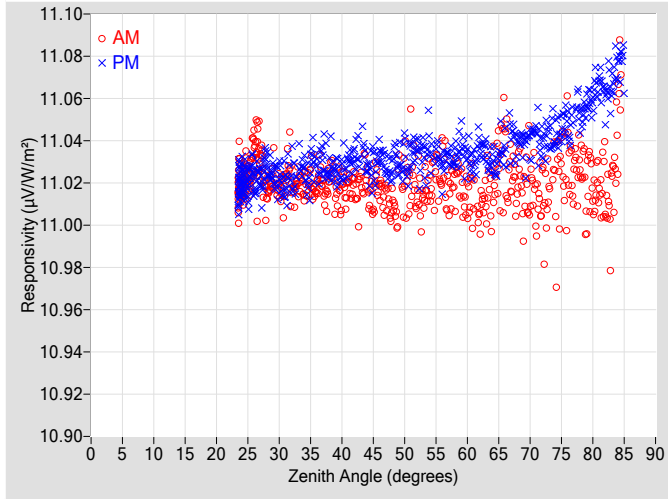


Figure 2. Responsivity vs Local Standard Time

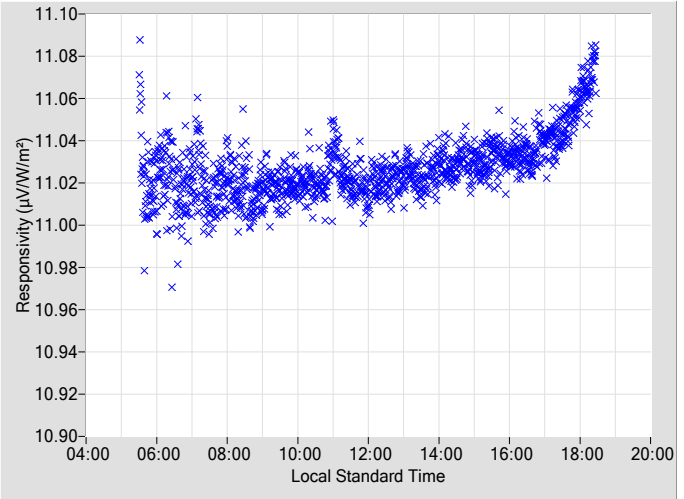


Table 2. Instrument Responsivity (R) and Calibration Type-B Standard Uncertainty, u(B)

| Zenith Angle (deg.) | R ($\mu\text{V}/\text{W}/\text{m}^2$) | AM u(B) \pm (%) | Azimuth Angle | R ($\mu\text{V}/\text{W}/\text{m}^2$) | PM u(B) \pm (%) | Azimuth Angle | Zenith Angle (deg.) | R ($\mu\text{V}/\text{W}/\text{m}^2$) | AM u(B) \pm (%) | Azimuth Angle | R ($\mu\text{V}/\text{W}/\text{m}^2$) | PM u(B) \pm (%) | Azimuth Angle |
|---------------------|---|-------------------|---------------|---|-------------------|---------------|---------------------|---|-------------------|---------------|---|-------------------|---------------|
| 0 | N/A | N/A | N/A | N/A | N/A | N/A | 46 | 11.018 | 0.29 | 106.76 | 11.034 | 0.29 | 252.81 |
| 2 | N/A | N/A | N/A | N/A | N/A | N/A | 48 | 11.009 | 0.29 | 104.54 | 11.026 | 0.29 | 255.07 |
| 4 | N/A | N/A | N/A | N/A | N/A | N/A | 50 | 11.019 | 0.33 | 102.40 | 11.034 | 0.30 | 257.22 |
| 6 | N/A | N/A | N/A | N/A | N/A | N/A | 52 | 11.014 | 0.30 | 100.37 | 11.038 | 0.29 | 259.28 |
| 8 | N/A | N/A | N/A | N/A | N/A | N/A | 54 | 11.020 | 0.31 | 98.49 | 11.038 | 0.29 | 261.27 |
| 10 | N/A | N/A | N/A | N/A | N/A | N/A | 56 | 11.028 | 0.30 | 96.57 | 11.027 | 0.29 | 263.14 |
| 12 | N/A | N/A | N/A | N/A | N/A | N/A | 58 | 11.022 | 0.30 | 94.78 | 11.032 | 0.29 | 264.91 |
| 14 | N/A | N/A | N/A | N/A | N/A | N/A | 60 | 11.013 | 0.29 | 93.05 | 11.034 | 0.29 | 266.71 |
| 16 | N/A | N/A | N/A | N/A | N/A | N/A | 62 | 11.006 | 0.30 | 91.34 | 11.038 | 0.30 | 268.39 |
| 18 | N/A | N/A | N/A | N/A | N/A | N/A | 64 | 11.016 | 0.30 | 89.67 | 11.031 | 0.30 | 270.08 |
| 20 | N/A | N/A | N/A | N/A | N/A | N/A | 66 | 11.037 | 0.31 | 88.03 | 11.035 | 0.30 | 271.71 |
| 22 | N/A | N/A | N/A | N/A | N/A | N/A | 68 | 11.018 | 0.30 | 86.42 | 11.039 | 0.30 | 273.35 |
| 24 | 11.018 | 0.29 | 166.98 | 11.020 | 0.30 | 192.98 | 70 | 11.019 | 0.31 | 84.81 | 11.039 | 0.30 | 274.98 |
| 26 | 11.037 | 0.31 | 151.03 | 11.021 | 0.30 | 209.21 | 72 | 11.009 | 0.30 | 83.22 | 11.039 | 0.30 | 276.59 |
| 28 | 11.015 | 0.29 | 140.80 | 11.029 | 0.30 | 218.18 | 74 | 11.027 | 0.31 | 81.63 | 11.041 | 0.31 | 278.19 |
| 30 | 11.017 | 0.31 | 134.48 | 11.022 | 0.31 | 224.76 | 76 | 11.031 | 0.31 | 79.99 | 11.047 | 0.31 | 279.83 |
| 32 | 11.017 | 0.29 | 129.23 | 11.024 | 0.29 | 230.12 | 78 | 11.030 | 0.31 | 78.38 | 11.051 | N/A | 281.44 |
| 34 | 11.018 | 0.31 | 124.81 | 11.026 | 0.30 | 234.54 | 80 | 11.015 | N/A | 76.74 | 11.059 | N/A | 283.08 |
| 36 | 11.018 | 0.30 | 120.99 | 11.028 | 0.29 | 238.48 | 82 | 11.019 | N/A | 75.12 | 11.061 | N/A | 284.73 |
| 38 | 11.023 | 0.30 | 117.64 | 11.028 | 0.31 | 241.91 | 84 | 11.057 | N/A | 73.41 | 11.076 | N/A | 286.38 |
| 40 | 11.017 | 0.29 | 114.49 | 11.028 | 0.30 | 244.98 | 86 | N/A | N/A | N/A | N/A | N/A | N/A |
| 42 | 11.020 | 0.30 | 111.81 | 11.033 | 0.29 | 247.80 | 88 | N/A | N/A | N/A | N/A | N/A | N/A |
| 44 | 11.019 | 0.29 | 109.14 | 11.027 | 0.31 | 250.44 | 90 | N/A | N/A | N/A | N/A | N/A | N/A |

N/A - Not Available

Figure 3. Type-B Standard Uncertainty vs Zenith Angle

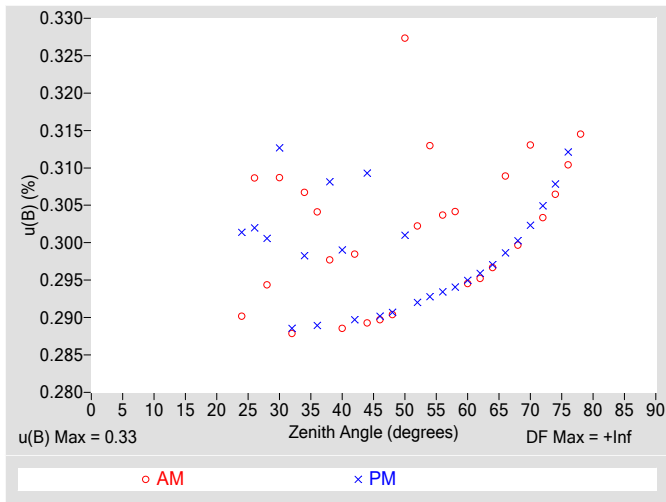


Figure 4. Residuals from Spline Interpolation

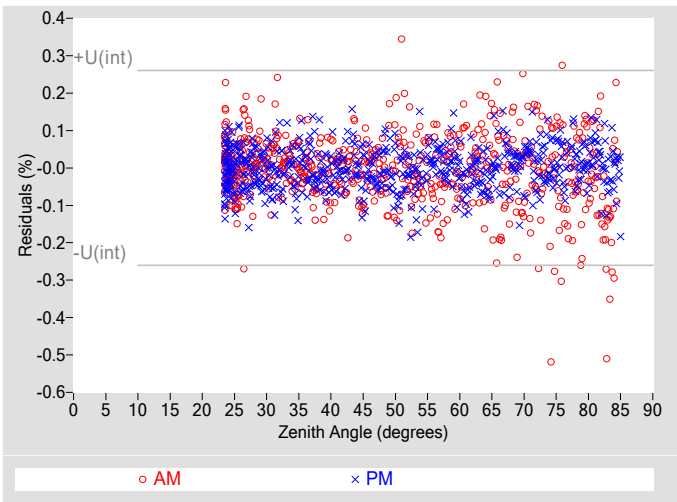


Table 3. Uncertainty using Spline Interpolation ‡

| | |
|---|------------|
| Type-B Standard Uncertainty, $u(B)$ (%) | ± 0.33 |
| Type-A Interpolating Function, $u(int)$ (%) | ± 0.13 |
| Combined Standard Uncertainty, $u(c)$ (%) | ± 0.35 |
| Effective degrees of freedom, $DF(c)$ | 61098 |
| Coverage factor, k | 1.96 |
| Expanded Uncertainty, U_{95} (%) | ± 0.69 |
| AM Valid zenith angle range | 24° to 78° |
| PM Valid zenith angle range | 24° to 76° |

‡ An illustration for how to reduce the uncertainty in calculating the irradiance using a function rather than $R@45^\circ$. Not accredited.

Table 4. Calibration Label Values

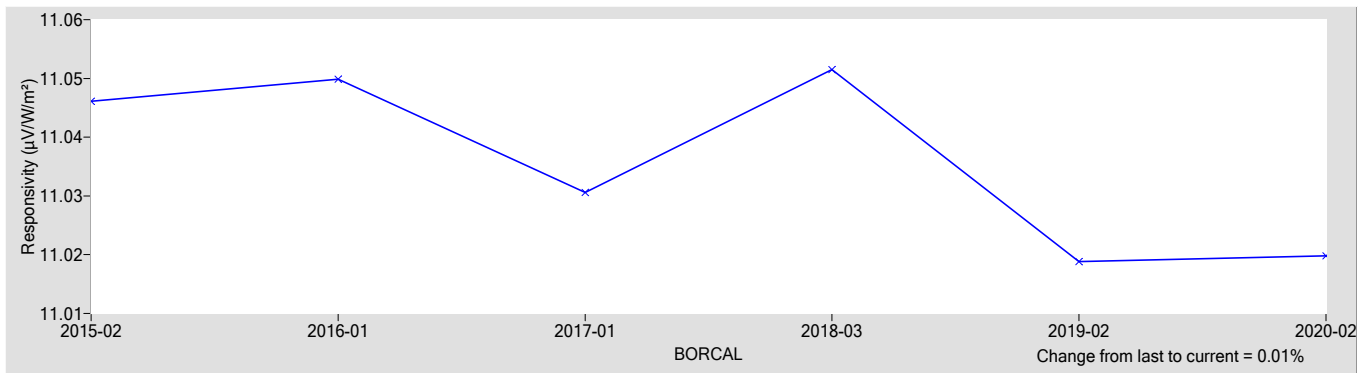
| | |
|----------------------------------|-------------------------------|
| $R @ 45^\circ$ ($\mu V/W/m^2$) | R_{net} ($\mu V/W/m^2$) † |
| 11.020 | 0 |

† R_{net} determination date: N/A

Table 5. Uncertainty using $R @ 45^\circ$

| | |
|---|----------------|
| Type-B Expanded Uncertainty, $U(B)$ (%) | ± 0.64 |
| Offset Uncertainty, $U(off)$ (%) | +0.16 / -0.10 |
| Expanded Uncertainty, U (%) | +0.80 / -0.74 |
| Effective degrees of freedom, DF | +Inf |
| Coverage factor, k | 1.96 |
| Valid zenith angle range | 30.0° to 60.0° |

Figure 5. History of instrument at Zenith Angle = 45°



References:

[1] Reda, I.; Hickey, J.; Long, C.; Myers, D.; Stoffel, T.; Wilcox, S.; Michalsky, J. J.; Dutton, E. G.; Nelson, D. (2005). "Using a Blackbody to Calculate Net Longwave Responsivity of Shortwave Solar Pyranometers to Correct for Their Thermal Offset Error During Outdoor Calibration Using the Component Sum Method." *Journal of Atmospheric and Oceanic Technology*, 2005; pp. 1531-1540; NREL Report No. JA-560-36646. doi:10.1175/JTECH1782.1

[2] Reda, I.; Myers, D.; Stoffel, T. (2008). "Uncertainty Estimate for the Outdoor Calibration of Solar Pyranometers: A Metrologist Perspective." *Measure.* (NCSLI Journal of Measurement Science). Vol. 3(4), December 2008; pp. 58-66; NREL Report No. JA-581-4137

[3] Reda, I.; Andreas, A. (2004). "Solar Position Algorithm for Solar Radiation Applications." *Solar Energy*. Vol. 76(5), 2004; pp. 577-589; NREL Report No. JA-560-35518. doi:10.1016/j.solener.2003.12.003

[4] Stoffel, T.; Reda, I. (2009). "NREL Pyrheliometer Comparisons: 22 September - 3 October 2008 (NPC-2008)." 54 pp.; NREL Report No. TP-550-45016.

[5] Reda, I.; Stoffel, T.; Myers, D. (2003). "Method to Calibrate a Solar Pyranometer for Measuring Reference Diffuse Irradiance." *Solar Energy*. Vol. 74, 2003; pp. 103-112; NREL Report No. JA-560-35025. doi:10.1016/S0038-092X(03)00124-5

[6] Reda, I. (1996). *Calibration of a Solar Absolute Cavity Radiometer with Traceability to the World Radiometric Reference*. 79 pp.; NREL Report No. TP-463-20619.

[7] Reda, I.; Gröbner, J.; Stoffel, T.; Myers, D.; Forgan, B. (2008). *Improvements in the Blackbody Calibration of Pyrgeometers*. ARM 2008 Science Team Meeting (Poster).



National Renewable Energy Laboratory

Solar Radiation Research Laboratory

Metrology Laboratory

Calibration Certificate



| | | | |
|--------------------------|---------------------|----------------------------------|--------------|
| Test Instrument: | Silicon Pyranometer | Manufacturer: | Kipp & Zonen |
| Model: | SP-LITE | Serial Number: | 970003 |
| Calibration Date: | 5/5/2020 | Due Date: | 5/5/2021 |
| Customer: | NREL-SRRL-BMS | Environmental Conditions: | see page 4 |
| Test Dates: | 5/4-5 | | |

This certifies that the above product was calibrated in compliance with ISO/IEC 17025:2017. Measurement uncertainties at the time of calibration are consistent with the Guide to the Expression of Uncertainty in Measurement (GUM) using Reda et al., 2008. All nominal values are traceable to the International System (SI) Units of Measurement.

No statement of compliance with specifications is made or implied on this certificate. However, the estimated uncertainties are the uncertainties of the calibration process; users must add other uncertainties that are relevant to their measuring system, environmental and sky conditions, outdoor set-up, and site location.

The Type-B Standard Uncertainty of using the responsivity at each even zenith angle is reported, and the Expanded Uncertainty of the calibration is reported using two methods:

1. The Expanded Uncertainty of using the responsivity at zenith angle = 45°, within the zenith angle range from 30.0° to 60.0°
2. The Expanded Uncertainty of using Spline Interpolating Functions for the responsivity versus zenith angle.

This certificate applies only to the item identified above and shall not be reproduced other than in full, without specific written approval from the calibration facility. Certificate without signature is not valid.

Table 1. Traceability

| Measurement Type | Instrument | Calibration Date | Calibration Due Date |
|----------------------|--|------------------|----------------------|
| Beam Irradiance † | Eppley Absolute Cavity Radiometer Model HF, S/N 29219 | 09/27/2019 | 09/27/2020 |
| Diffuse Irradiance † | Hukseflux Pyranometer Model SR25, S/N 2541 | 04/17/2020 | 04/17/2021 |
| Diffuse Irradiance † | Hukseflux Pyranometer Model SR25, S/N 2542 | 04/17/2020 | 04/17/2021 |
| Data Acquisition | NREL Data Acquisition System Model RAP-DAQ, S/N 2005-998 | 02/14/2019 | 02/14/2021 |
| Data Acquisition | NREL Data Acquisition System Model RAP-DAQ, S/N 2005-999 | 02/14/2019 | 02/14/2021 |

† Through the World Radiometric Reference (WRR)

Number of pages of certificate: 4

Calibration Procedure: BORCAL-P00-Calibration and QA Procedure; available upon request.

Setup: Radiometers are calibrated outdoors, using the sun as the source. Pyranometers and pyrgeometers are installed for horizontal measurements, with their signal connectors oriented north, if their design permits.
The shading disk for the reference diffuse subtends a solid angle of 5°. Pyrheliometers are installed on solar trackers.

Calibrated by: Afshin Andreas, Ibrahim Reda, Peter Gotseff, and RCC

Ibrahim Reda, Technical Manager

Date

For questions or comments, please contact the technical manager at:
ibrahim.reda@nrel.gov; 303-384-6385; 15013 Denver West Parkway, Golden, CO 80401, USA

Calibration Results

970003 Kipp & Zonen SP-LITE

The responsivity (R , $\mu\text{V}/\text{W}/\text{m}^2$) of the test instrument during calibration is calculated using this Measurement Equation:

$$R = (V - R_{net} * W_{net}) / I \tag{1}$$

where,

- V = radiometer output voltage (microvolts),
 - R_{net} = radiometer net infrared responsivity ($\mu\text{V}/\text{W}/\text{m}^2$), see Table 4,
 - W_{net} = effective net infrared measured by pyrgeometer (W/m^2),
 - = $W_{in} - W_{out} = W_{in} - \sigma * T_c^4$
 - where, W_{in} = incoming infrared (W/m^2), $\sigma = 5.6704\text{e-}8 \text{ W}\cdot\text{m}^{-2}\cdot\text{K}^{-4}$,
 - T_c = case temperature of pyrgeometer (K).
- I = reference irradiance (W/m^2), beam (B) or global (G)
 - where, $G = B * \text{COS}(Z) + D$,
 - Z = zenith angle (degrees),
 - D = reference diffuse irradiance (W/m^2).

Figure 1. Responsivity vs Zenith Angle

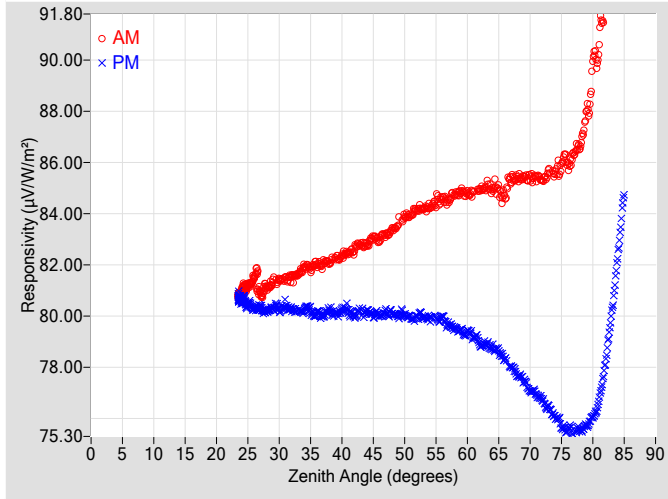


Figure 2. Responsivity vs Local Standard Time

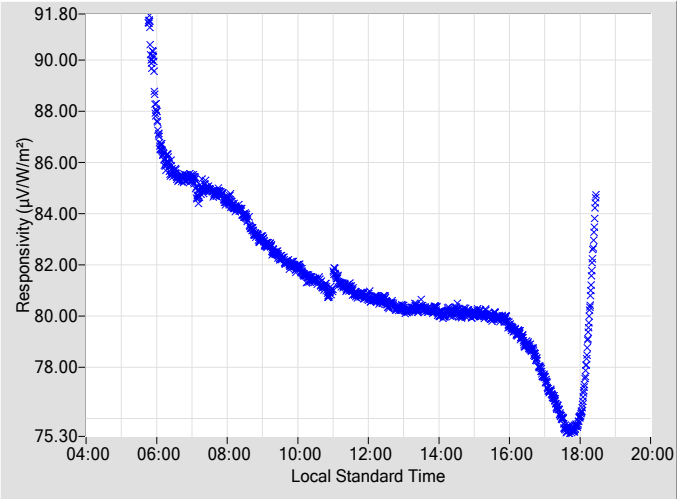


Table 2. Instrument Responsivity (R) and Calibration Type-B Standard Uncertainty, u(B)

| Zenith | | | AM | | | PM | | | Zenith | | | AM | | | PM | | |
|--------|---------------------------------------|-------|---------|---------------------------------------|-------|---------|--------|---------------------------------------|--------|---------|---------------------------------------|-------|---------|---------------------------------------|-------|---------|--|
| Angle | R | u(B) | Azimuth | R | u(B) | Azimuth | Angle | R | u(B) | Azimuth | R | u(B) | Azimuth | R | u(B) | Azimuth | |
| (deg.) | ($\mu\text{V}/\text{W}/\text{m}^2$) | ± (%) | Angle | ($\mu\text{V}/\text{W}/\text{m}^2$) | ± (%) | Angle | (deg.) | ($\mu\text{V}/\text{W}/\text{m}^2$) | ± (%) | Angle | ($\mu\text{V}/\text{W}/\text{m}^2$) | ± (%) | Angle | ($\mu\text{V}/\text{W}/\text{m}^2$) | ± (%) | Angle | |
| 0 | N/A | N/A | N/A | N/A | N/A | N/A | 46 | 82.978 | 0.31 | 106.77 | 80.032 | 0.32 | 252.82 | | | | |
| 2 | N/A | N/A | N/A | N/A | N/A | N/A | 48 | 83.380 | 0.31 | 104.55 | 80.126 | 0.32 | 255.08 | | | | |
| 4 | N/A | N/A | N/A | N/A | N/A | N/A | 50 | 83.868 | 0.33 | 102.41 | 80.032 | 0.33 | 257.23 | | | | |
| 6 | N/A | N/A | N/A | N/A | N/A | N/A | 52 | 84.141 | 0.35 | 100.38 | 80.006 | 0.32 | 259.29 | | | | |
| 8 | N/A | N/A | N/A | N/A | N/A | N/A | 54 | 84.256 | 0.34 | 98.45 | 79.937 | 0.32 | 261.22 | | | | |
| 10 | N/A | N/A | N/A | N/A | N/A | N/A | 56 | 84.587 | 0.36 | 96.58 | 79.955 | 0.33 | 263.10 | | | | |
| 12 | N/A | N/A | N/A | N/A | N/A | N/A | 58 | 84.751 | 0.38 | 94.75 | 79.519 | 0.33 | 264.91 | | | | |
| 14 | N/A | N/A | N/A | N/A | N/A | N/A | 60 | 84.767 | 0.34 | 93.05 | 79.385 | 0.34 | 266.67 | | | | |
| 16 | N/A | N/A | N/A | N/A | N/A | N/A | 62 | 84.945 | 0.35 | 91.35 | 78.888 | 0.35 | 268.39 | | | | |
| 18 | N/A | N/A | N/A | N/A | N/A | N/A | 64 | 84.929 | 0.36 | 89.68 | 78.754 | 0.36 | 270.09 | | | | |
| 20 | N/A | N/A | N/A | N/A | N/A | N/A | 66 | 84.763 | 0.40 | 88.03 | 78.297 | 0.38 | 271.72 | | | | |
| 22 | N/A | N/A | N/A | N/A | N/A | N/A | 68 | 85.412 | 0.39 | 86.42 | 77.658 | 0.40 | 273.36 | | | | |
| 24 | 80.920 | 0.31 | 167.16 | 80.628 | 0.31 | 193.01 | 70 | 85.432 | 0.42 | 84.82 | 77.075 | 0.42 | 274.99 | | | | |
| 26 | 81.505 | 0.32 | 151.05 | 80.287 | 0.31 | 209.06 | 72 | 85.317 | 0.45 | 83.18 | 76.700 | 0.45 | 276.60 | | | | |
| 28 | 81.148 | 0.33 | 140.91 | 80.212 | 0.31 | 218.07 | 74 | 85.581 | 0.49 | 81.61 | 76.052 | 0.49 | 278.20 | | | | |
| 30 | 81.399 | 0.31 | 134.42 | 80.230 | 0.29 | 224.61 | 76 | 85.910 | 0.54 | 79.99 | 75.564 | 0.55 | 279.83 | | | | |
| 32 | 81.494 | 0.30 | 129.21 | 80.269 | 0.32 | 230.02 | 78 | 86.697 | 0.61 | 78.39 | 75.533 | N/A | 281.44 | | | | |
| 34 | 81.921 | 0.31 | 124.83 | 80.265 | 0.32 | 234.61 | 80 | 89.826 | N/A | 76.74 | 76.094 | N/A | 283.09 | | | | |
| 36 | 82.035 | 0.31 | 121.06 | 80.125 | 0.31 | 238.40 | 82 | N/A | N/A | N/A | 78.271 | N/A | 284.73 | | | | |
| 38 | 82.080 | 0.31 | 117.65 | 80.228 | 0.31 | 241.82 | 84 | N/A | N/A | N/A | 82.386 | N/A | 286.39 | | | | |
| 40 | 82.377 | 0.31 | 114.46 | 80.229 | 0.33 | 244.99 | 86 | N/A | N/A | N/A | N/A | N/A | N/A | | | | |
| 42 | 82.567 | 0.31 | 111.82 | 79.993 | 0.33 | 247.81 | 88 | N/A | N/A | N/A | N/A | N/A | N/A | | | | |
| 44 | 82.764 | 0.30 | 109.15 | 80.184 | 0.36 | 250.45 | 90 | N/A | N/A | N/A | N/A | N/A | N/A | | | | |

N/A - Not Available

Figure 3. Type-B Standard Uncertainty vs Zenith Angle

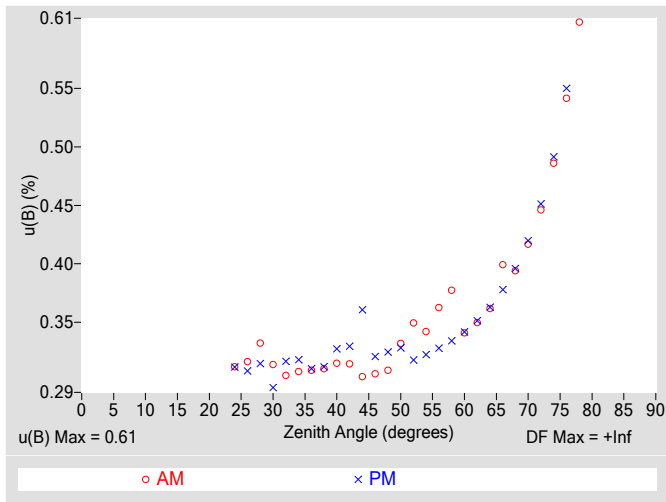


Figure 4. Residuals from Spline Interpolation

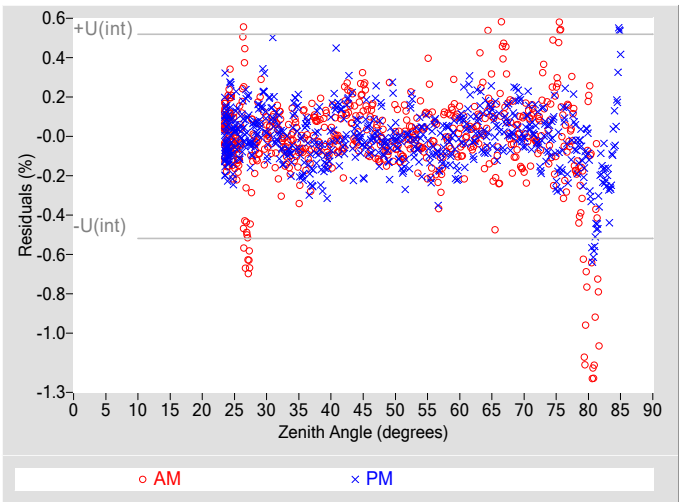


Table 3. Uncertainty using Spline Interpolation ‡

| | |
|---|------------|
| Type-B Standard Uncertainty, $u(B)$ (%) | ± 0.61 |
| Type-A Interpolating Function, $u(int)$ (%) | ± 0.26 |
| Combined Standard Uncertainty, $u(c)$ (%) | ± 0.66 |
| Effective degrees of freedom, $DF(c)$ | 48120 |
| Coverage factor, k | 1.96 |
| Expanded Uncertainty, $U95$ (%) | ± 1.3 |
| AM Valid zenith angle range | 24° to 78° |
| PM Valid zenith angle range | 24° to 76° |

‡ An illustration for how to reduce the uncertainty in calculating the irradiance using a function rather than $R@45^\circ$. Not accredited.

Table 4. Calibration Label Values

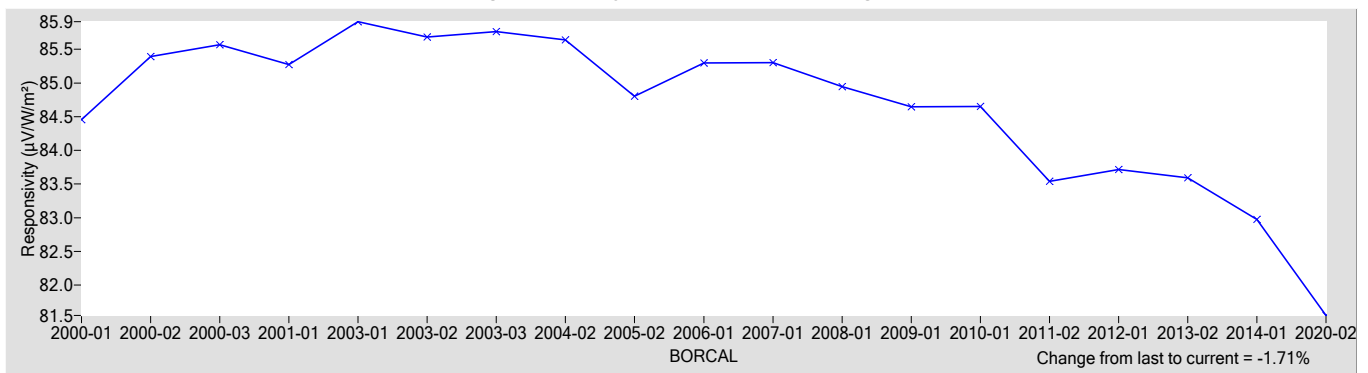
| | |
|----------------------------------|-------------------------------|
| $R @ 45^\circ$ ($\mu V/W/m^2$) | R_{net} ($\mu V/W/m^2$) † |
| 81.550 | 0 |

† R_{net} determination date: N/A

Table 5. Uncertainty using $R @ 45^\circ$

| | |
|---|----------------|
| Type-B Expanded Uncertainty, $U(B)$ (%) | ± 0.74 |
| Offset Uncertainty, $U(off)$ (%) | +3.9 / -2.7 |
| Expanded Uncertainty, U (%) | +4.7 / -3.4 |
| Effective degrees of freedom, DF | +Inf |
| Coverage factor, k | 1.96 |
| Valid zenith angle range | 30.0° to 60.0° |

Figure 5. History of instrument at Zenith Angle = 45°



References:

[1] Reda, I.; Hickey, J.; Long, C.; Myers, D.; Stoffel, T.; Wilcox, S.; Michalsky, J. J.; Dutton, E. G.; Nelson, D. (2005). "Using a Blackbody to Calculate Net Longwave Responsivity of Shortwave Solar Pyranometers to Correct for Their Thermal Offset Error During Outdoor Calibration Using the Component Sum Method." *Journal of Atmospheric and Oceanic Technology*, 2005; pp. 1531-1540; NREL Report No. JA-560-36646. doi:10.1175/JTECH1782.1

[2] Reda, I.; Myers, D.; Stoffel, T. (2008). "Uncertainty Estimate for the Outdoor Calibration of Solar Pyranometers: A Metrologist Perspective." *Measure*. (NCSLI Journal of Measurement Science). Vol. 3(4), December 2008; pp. 58-66; NREL Report No. JA-581-4137

[3] Reda, I.; Andreas, A. (2004). "Solar Position Algorithm for Solar Radiation Applications." *Solar Energy*. Vol. 76(5), 2004; pp. 577-589; NREL Report No. JA-560-35518. doi:10.1016/j.solener.2003.12.003

[4] Stoffel, T.; Reda, I. (2009). "NREL Pyrheliometer Comparisons: 22 September - 3 October 2008 (NPC-2008)." 54 pp.; NREL Report No. TP-550-45016.

[5] Reda, I.; Stoffel, T.; Myers, D. (2003). "Method to Calibrate a Solar Pyranometer for Measuring Reference Diffuse Irradiance." *Solar Energy*. Vol. 74, 2003; pp. 103-112; NREL Report No. JA-560-35025. doi:10.1016/S0038-092X(03)00124-5

[6] Reda, I. (1996). Calibration of a Solar Absolute Cavity Radiometer with Traceability to the World Radiometric Reference. 79 pp.; NREL Report No. TP-463-20619.

[7] Reda, I.; Gröbner, J.; Stoffel, T.; Myers, D.; Forgan, B. (2008). Improvements in the Blackbody Calibration of Pyrgometers. ARM 2008 Science Team Meeting (Poster).

National Renewable Energy Laboratory

Solar Radiation Research Laboratory

Metrology Laboratory

Calibration Certificate



Test Instrument: Sunshine Pyranometer - Global Output **Manufacturer:** Delta-T
Model: SPN1 **Serial Number:** A360
Calibration Date: 5/5/2020 **Due Date:** 5/5/2021
Customer: NREL-SRRL-BMS **Environmental Conditions:** see page 4
Test Dates: 5/4-5

This certifies that the above product was calibrated in compliance with ISO/IEC 17025:2017. Measurement uncertainties at the time of calibration are consistent with the Guide to the Expression of Uncertainty in Measurement (GUM) using Reda et al., 2008. All nominal values are traceable to the International System (SI) Units of Measurement.

No statement of compliance with specifications is made or implied on this certificate. However, the estimated uncertainties are the uncertainties of the calibration process; users must add other uncertainties that are relevant to their measuring system, environmental and sky conditions, outdoor set-up, and site location.

The Type-B Standard Uncertainty of using the responsivity at each even zenith angle is reported, and the Expanded Uncertainty of the calibration is reported using two methods:

1. The Expanded Uncertainty of using the responsivity at zenith angle = 45°, within the zenith angle range from 30.0° to 60.0°
2. The Expanded Uncertainty of using Spline Interpolating Functions for the responsivity versus zenith angle.

This certificate applies only to the item identified above and shall not be reproduced other than in full, without specific written approval from the calibration facility. Certificate without signature is not valid.

Table 1. Traceability

| Measurement Type | Instrument | Calibration Date | Calibration Due Date |
|----------------------|--|------------------|----------------------|
| Beam Irradiance † | Eppley Absolute Cavity Radiometer Model HF, S/N 29219 | 09/27/2019 | 09/27/2020 |
| Diffuse Irradiance † | Hukseflux Pyranometer Model SR25, S/N 2541 | 04/17/2020 | 04/17/2021 |
| Diffuse Irradiance † | Hukseflux Pyranometer Model SR25, S/N 2542 | 04/17/2020 | 04/17/2021 |
| Data Acquisition | NREL Data Acquisition System Model RAP-DAQ, S/N 2005-998 | 02/14/2019 | 02/14/2021 |
| Data Acquisition | NREL Data Acquisition System Model RAP-DAQ, S/N 2005-999 | 02/14/2019 | 02/14/2021 |

† Through the World Radiometric Reference (WRR)

Number of pages of certificate: 4

Calibration Procedure: BORCAL-P00-Calibration and QA Procedure; available upon request.

Setup: Radiometers are calibrated outdoors, using the sun as the source. Pyranometers and pyrgeometers are installed for horizontal measurements, with their signal connectors oriented north, if their design permits.

The shading disk for the reference diffuse subtends a solid angle of 5°. Pyrheliometers are installed on solar trackers.

Calibrated by: Afshin Andreas, Ibrahim Reda, Peter Gotseff, and RCC

Ibrahim Reda, Technical Manager

Date

For questions or comments, please contact the technical manager at:

ibrahim.reda@nrel.gov; 303-384-6385; 15013 Denver West Parkway, Golden, CO 80401, USA

Calibration Results

A360 Delta-T SPN1

The responsivity (R , $\mu\text{V}/\text{W}/\text{m}^2$) of the test instrument during calibration is calculated using this Measurement Equation:

$$R = (V - R_{net} * W_{net}) / I \quad [1]$$

where,

- V = radiometer output voltage (microvolts),
 - R_{net} = radiometer net infrared responsivity ($\mu\text{V}/\text{W}/\text{m}^2$), see Table 4,
 - W_{net} = effective net infrared measured by pyrgeometer (W/m^2),
 - = $W_{in} - W_{out} = W_{in} - \sigma * T_c^4$
 - where, W_{in} = incoming infrared (W/m^2), $\sigma = 5.6704\text{e-}8 \text{ W}\cdot\text{m}^{-2}\cdot\text{K}^{-4}$,
 - T_c = case temperature of pyrgeometer (K).
- I = reference irradiance (W/m^2), beam (B) or global (G)
 where, $G = B * \text{COS}(Z) + D$,
 Z = zenith angle (degrees),
 D = reference diffuse irradiance (W/m^2).

Figure 1. Responsivity vs Zenith Angle

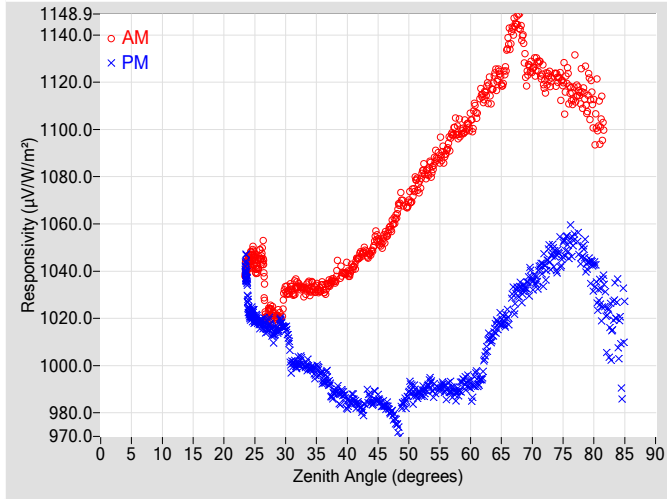


Figure 2. Responsivity vs Local Standard Time

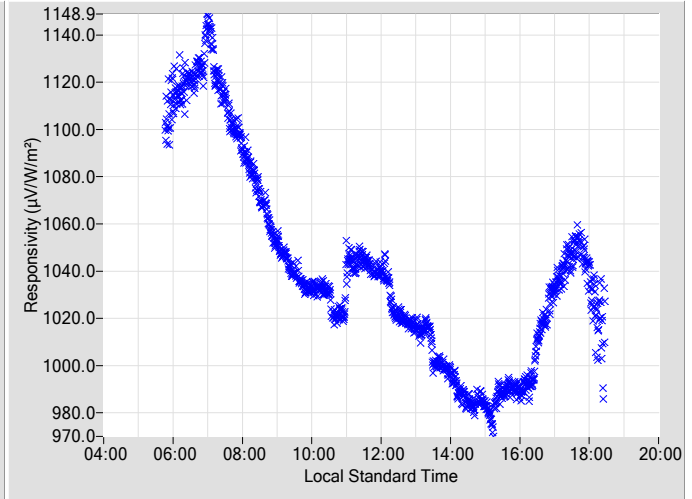


Table 2. Instrument Responsivity (R) and Calibration Type-B Standard Uncertainty, $u(B)$

| Zenith Angle (deg.) | R ($\mu\text{V}/\text{W}/\text{m}^2$) | AM $u(B)$ \pm (%) | Azimuth Angle | R ($\mu\text{V}/\text{W}/\text{m}^2$) | PM $u(B)$ \pm (%) | Azimuth Angle | Zenith Angle (deg.) | R ($\mu\text{V}/\text{W}/\text{m}^2$) | AM $u(B)$ \pm (%) | Azimuth Angle | R ($\mu\text{V}/\text{W}/\text{m}^2$) | PM $u(B)$ \pm (%) | Azimuth Angle |
|---------------------|---|---------------------|---------------|---|---------------------|---------------|---------------------|---|---------------------|---------------|---|---------------------|---------------|
| 0 | N/A | N/A | N/A | N/A | N/A | N/A | 46 | 1054.0 | 0.32 | 106.80 | 982.91 | 0.31 | 252.79 |
| 2 | N/A | N/A | N/A | N/A | N/A | N/A | 48 | 1063.2 | 0.31 | 104.58 | 974.85 | 0.31 | 255.11 |
| 4 | N/A | N/A | N/A | N/A | N/A | N/A | 50 | 1069.4 | 0.31 | 102.44 | 989.52 | 0.31 | 257.20 |
| 6 | N/A | N/A | N/A | N/A | N/A | N/A | 52 | 1079.3 | 0.32 | 100.41 | 988.81 | 0.32 | 259.27 |
| 8 | N/A | N/A | N/A | N/A | N/A | N/A | 54 | 1084.7 | 0.32 | 98.48 | 989.30 | 0.34 | 261.25 |
| 10 | N/A | N/A | N/A | N/A | N/A | N/A | 56 | 1090.0 | 0.33 | 96.61 | 989.21 | 0.33 | 263.13 |
| 12 | N/A | N/A | N/A | N/A | N/A | N/A | 58 | 1099.5 | 0.33 | 94.82 | 989.00 | 0.33 | 264.94 |
| 14 | N/A | N/A | N/A | N/A | N/A | N/A | 60 | 1102.4 | 0.34 | 93.03 | 989.70 | 0.34 | 266.70 |
| 16 | N/A | N/A | N/A | N/A | N/A | N/A | 62 | 1113.9 | 0.35 | 91.33 | 998.18 | 0.35 | 268.42 |
| 18 | N/A | N/A | N/A | N/A | N/A | N/A | 64 | 1121.6 | 0.36 | 89.70 | 1016.2 | 0.36 | 270.07 |
| 20 | N/A | N/A | N/A | N/A | N/A | N/A | 66 | 1135.0 | 0.40 | 88.02 | 1020.6 | 0.38 | 271.70 |
| 22 | N/A | N/A | N/A | N/A | N/A | N/A | 68 | 1144.1 | 0.39 | 86.40 | 1031.7 | 0.40 | 273.38 |
| 24 | 1043.4 | 0.31 | 167.06 | 1025.8 | 0.31 | 193.05 | 70 | 1125.9 | 0.42 | 84.80 | 1036.3 | 0.42 | 274.97 |
| 26 | 1046.3 | 0.30 | 150.99 | 1017.9 | 0.31 | 209.17 | 72 | 1120.7 | 0.45 | 83.21 | 1040.4 | 0.45 | 276.62 |
| 28 | 1021.2 | 0.32 | 140.86 | 1013.0 | 0.32 | 218.11 | 74 | 1121.6 | 0.49 | 81.59 | 1044.9 | 0.49 | 278.18 |
| 30 | 1031.7 | 0.35 | 134.40 | 1015.6 | 0.34 | 224.68 | 76 | 1118.7 | 0.54 | 80.01 | 1051.8 | 0.55 | 279.81 |
| 32 | 1033.9 | 0.34 | 129.23 | 1000.7 | 0.31 | 229.98 | 78 | 1115.8 | 0.61 | 78.37 | 1047.2 | N/A | 281.47 |
| 34 | 1032.5 | 0.31 | 124.79 | 998.82 | 0.30 | 234.57 | 80 | 1104.4 | N/A | 76.79 | 1039.4 | N/A | 283.07 |
| 36 | 1032.7 | 0.33 | 120.97 | 994.14 | 0.30 | 238.45 | 82 | N/A | N/A | N/A | 1021.4 | N/A | 284.71 |
| 38 | 1036.1 | 0.32 | 117.62 | 988.99 | 0.31 | 241.84 | 84 | N/A | N/A | N/A | 1018.9 | N/A | 286.37 |
| 40 | 1039.6 | 0.30 | 114.55 | 983.36 | 0.33 | 244.98 | 86 | N/A | N/A | N/A | N/A | N/A | N/A |
| 42 | 1046.3 | 0.33 | 111.79 | 982.95 | 0.32 | 247.78 | 88 | N/A | N/A | N/A | N/A | N/A | N/A |
| 44 | 1048.5 | 0.30 | 109.19 | 984.16 | 0.33 | 250.42 | 90 | N/A | N/A | N/A | N/A | N/A | N/A |

N/A - Not Available

Figure 3. Type-B Standard Uncertainty vs Zenith Angle

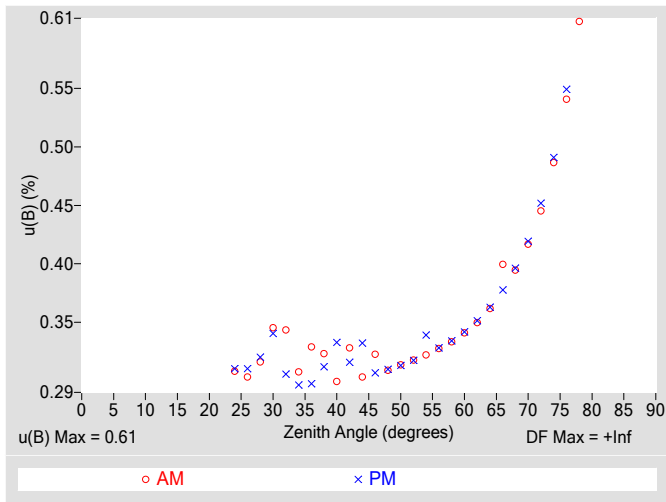


Figure 4. Residuals from Spline Interpolation

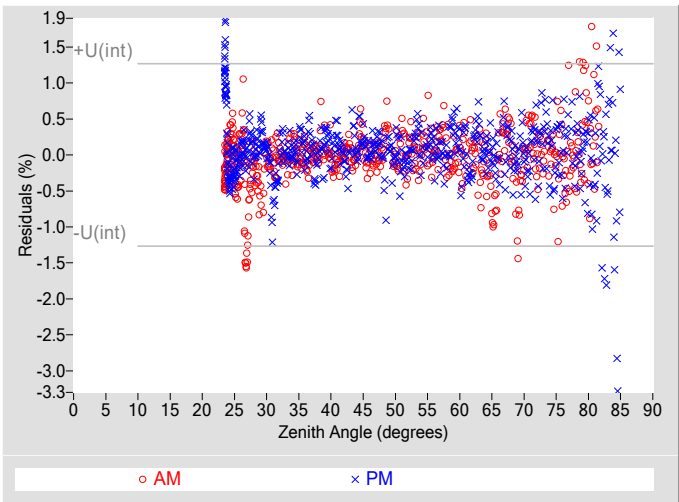


Table 3. Uncertainty using Spline Interpolation ‡

| | |
|---|------------|
| Type-B Standard Uncertainty, $u(B)$ (%) | ± 0.61 |
| Type-A Interpolating Function, $u(int)$ (%) | ± 0.63 |
| Combined Standard Uncertainty, $u(c)$ (%) | ± 0.88 |
| Effective degrees of freedom, $DF(c)$ | 4245 |
| Coverage factor, k | 1.96 |
| Expanded Uncertainty, U_{95} (%) | ± 1.7 |
| AM Valid zenith angle range | 24° to 78° |
| PM Valid zenith angle range | 24° to 76° |

‡ An illustration for how to reduce the uncertainty in calculating the irradiance using a function rather than $R@45^\circ$. Not accredited.

Table 4. Calibration Label Values

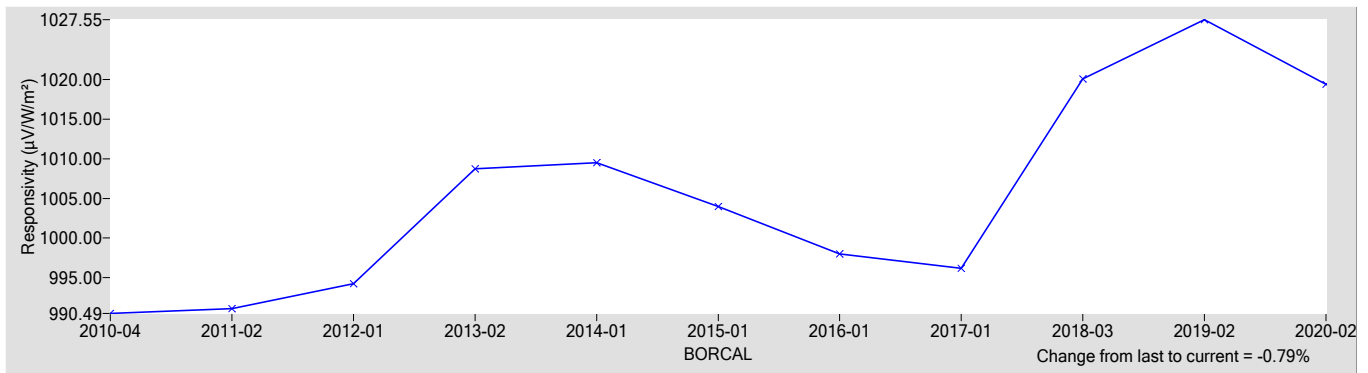
| | |
|----------------------------------|-------------------------------|
| $R @ 45^\circ$ ($\mu V/W/m^2$) | R_{net} ($\mu V/W/m^2$) † |
| 1019.4 | 0 |

† R_{net} determination date: N/A

Table 5. Uncertainty using $R @ 45^\circ$

| | |
|---|----------------|
| Type-B Expanded Uncertainty, $U(B)$ (%) | ± 0.68 |
| Offset Uncertainty, $U(off)$ (%) | +8.1 / -4.4 |
| Expanded Uncertainty, U (%) | +8.8 / -5.0 |
| Effective degrees of freedom, DF | +Inf |
| Coverage factor, k | 1.96 |
| Valid zenith angle range | 30.0° to 60.0° |

Figure 5. History of instrument at Zenith Angle = 45°



References:

- [1] Reda, I.; Hickey, J.; Long, C.; Myers, D.; Stoffel, T.; Wilcox, S.; Michalsky, J. J.; Dutton, E. G.; Nelson, D. (2005). "Using a Blackbody to Calculate Net Longwave Responsivity of Shortwave Solar Pyranometers to Correct for Their Thermal Offset Error During Outdoor Calibration Using the Component Sum Method." *Journal of Atmospheric and Oceanic Technology*, 2005; pp. 1531-1540; NREL Report No. JA-560-36646. doi:10.1175/JTECH1782.1
- [2] Reda, I.; Myers, D.; Stoffel, T. (2008). "Uncertainty Estimate for the Outdoor Calibration of Solar Pyranometers: A Metrologist Perspective." *Measure*. (NCSLI Journal of Measurement Science). Vol. 3(4), December 2008; pp. 58-66; NREL Report No. JA-581-4137
- [3] Reda, I.; Andreas, A. (2004). "Solar Position Algorithm for Solar Radiation Applications." *Solar Energy*. Vol. 76(5), 2004; pp. 577-589; NREL Report No. JA-560-35518. doi:10.1016/j.solener.2003.12.003
- [4] Stoffel, T.; Reda, I. (2009). "NREL Pyrheliometer Comparisons: 22 September - 3 October 2008 (NPC-2008)." 54 pp.; NREL Report No. TP-550-45016.
- [5] Reda, I.; Stoffel, T.; Myers, D. (2003). "Method to Calibrate a Solar Pyranometer for Measuring Reference Diffuse Irradiance." *Solar Energy*. Vol. 74, 2003; pp. 103-112; NREL Report No. JA-560-35025. doi:10.1016/S0038-092X(03)00124-5
- [6] Reda, I. (1996). Calibration of a Solar Absolute Cavity Radiometer with Traceability to the World Radiometric Reference. 79 pp.; NREL Report No. TP-463-20619.
- [7] Reda, I.; Gröbner, J.; Stoffel, T.; Myers, D.; Forgan, B. (2008). Improvements in the Blackbody Calibration of Pyrgometers. ARM 2008 Science Team Meeting (Poster).



National Renewable Energy Laboratory

Solar Radiation Research Laboratory

Metrology Laboratory

Calibration Certificate



| | | | |
|--------------------------|---------------|----------------------------------|------------|
| Test Instrument: | Pyranometer | Manufacturer: | EKO |
| Model: | MS-802 | Serial Number: | F14077R |
| Calibration Date: | 5/5/2020 | Due Date: | 5/5/2021 |
| Customer: | NREL-SRRL-BMS | Environmental Conditions: | see page 4 |
| Test Dates: | 5/4-5 | | |

This certifies that the above product was calibrated in compliance with ISO/IEC 17025:2017. Measurement uncertainties at the time of calibration are consistent with the Guide to the Expression of Uncertainty in Measurement (GUM) using Reda et al., 2008. All nominal values are traceable to the International System (SI) Units of Measurement.

No statement of compliance with specifications is made or implied on this certificate. However, the estimated uncertainties are the uncertainties of the calibration process; users must add other uncertainties that are relevant to their measuring system, environmental and sky conditions, outdoor set-up, and site location.

The Type-B Standard Uncertainty of using the responsivity at each even zenith angle is reported, and the Expanded Uncertainty of the calibration is reported using two methods:

1. The Expanded Uncertainty of using the responsivity at zenith angle = 45°, within the zenith angle range from 30.0° to 60.0°
2. The Expanded Uncertainty of using Spline Interpolating Functions for the responsivity versus zenith angle.

This certificate applies only to the item identified above and shall not be reproduced other than in full, without specific written approval from the calibration facility. Certificate without signature is not valid.

Table 1. Traceability

| Measurement Type | Instrument | Calibration Date | Calibration Due Date |
|-----------------------|--|------------------|----------------------|
| Beam Irradiance † | Eppley Absolute Cavity Radiometer Model HF, S/N 29219 | 09/27/2019 | 09/27/2020 |
| Diffuse Irradiance † | Hukseflux Pyranometer Model SR25, S/N 2541 | 04/17/2020 | 04/17/2021 |
| Diffuse Irradiance † | Hukseflux Pyranometer Model SR25, S/N 2542 | 04/17/2020 | 04/17/2021 |
| Data Acquisition | NREL Data Acquisition System Model RAP-DAQ, S/N 2005-998 | 02/14/2019 | 02/14/2021 |
| Data Acquisition | NREL Data Acquisition System Model RAP-DAQ, S/N 2005-999 | 02/14/2019 | 02/14/2021 |
| Infrared Irradiance ‡ | Kipp & Zonen Pyrgeometer Model CG4, S/N FT002 | 04/16/2018 | 04/16/2022 |

† Through the World Radiometric Reference (WRR)

‡ Through the World Infrared Standard Group (WISG)

Number of pages of certificate: 4

Calibration Procedure: BORCAL-P00-Calibration and QA Procedure; available upon request.

Setup: Radiometers are calibrated outdoors, using the sun as the source. Pyranometers and pyrgeometers are installed for horizontal measurements, with their signal connectors oriented north, if their design permits.

The shading disk for the reference diffuse subtends a solid angle of 5°. Pyrheliometers are installed on solar trackers.

Calibrated by: Afshin Andreas, Ibrahim Reda, Peter Gotseff, and RCC

Ibrahim Reda, Technical Manager

Date

For questions or comments, please contact the technical manager at:

ibrahim.reda@nrel.gov; 303-384-6385; 15013 Denver West Parkway, Golden, CO 80401, USA

Calibration Results

F14077R EKO MS-802

The responsivity (R , $\mu\text{V}/\text{W}/\text{m}^2$) of the test instrument during calibration is calculated using this Measurement Equation:

$$R = (V - R_{net} * W_{net}) / I \tag{1}$$

where,

- V = radiometer output voltage (microvolts),
 - R_{net} = radiometer net infrared responsivity ($\mu\text{V}/\text{W}/\text{m}^2$), see Table 4,
 - W_{net} = effective net infrared measured by pyrgeometer (W/m^2),
 - = $W_{in} - W_{out} = W_{in} - \sigma * T_c^4$
 - where, W_{in} = incoming infrared (W/m^2), $\sigma = 5.6704\text{e-}8 \text{ W}\cdot\text{m}^{-2}\cdot\text{K}^{-4}$,
 - T_c = case temperature of pyrgeometer (K).
- I = reference irradiance (W/m^2), beam (B) or global (G)
 - where, $G = B * \text{COS}(Z) + D$,
 - Z = zenith angle (degrees),
 - D = reference diffuse irradiance (W/m^2).

Figure 1. Responsivity vs Zenith Angle

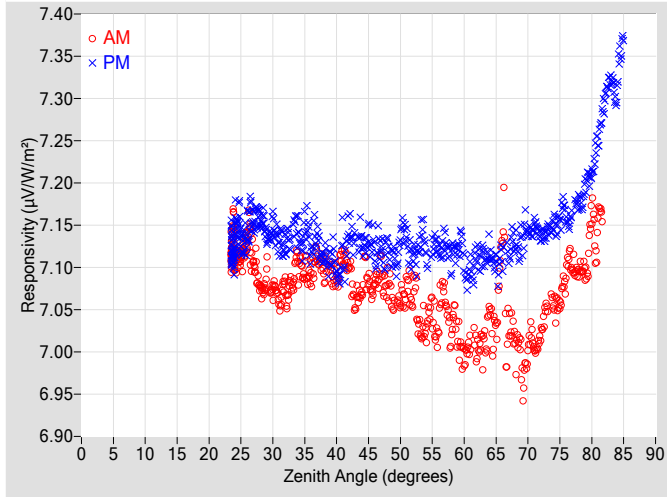


Figure 2. Responsivity vs Local Standard Time

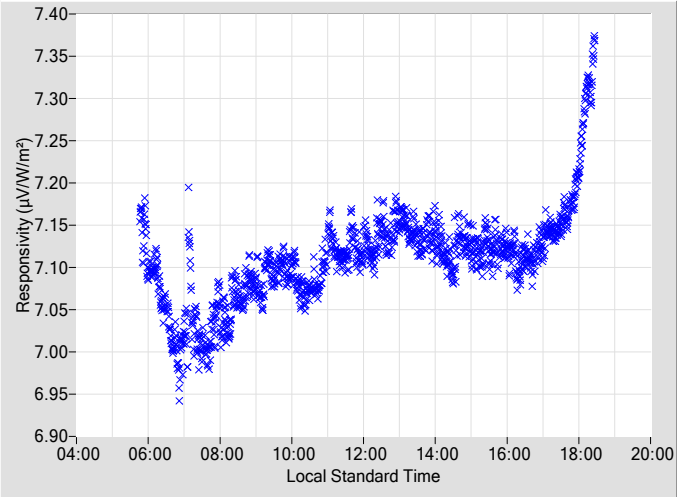


Table 2. Instrument Responsivity (R) and Calibration Type-B Standard Uncertainty, u(B)

| Zenith Angle (deg.) | R ($\mu\text{V}/\text{W}/\text{m}^2$) | u(B) \pm (%) | Azimuth Angle | R ($\mu\text{V}/\text{W}/\text{m}^2$) | u(B) \pm (%) | Azimuth Angle | Zenith Angle (deg.) | R ($\mu\text{V}/\text{W}/\text{m}^2$) | u(B) \pm (%) | Azimuth Angle | R ($\mu\text{V}/\text{W}/\text{m}^2$) | u(B) \pm (%) | Azimuth Angle |
|---------------------|---|----------------|---------------|---|----------------|---------------|---------------------|---|----------------|---------------|---|----------------|---------------|
| 0 | N/A | N/A | N/A | N/A | N/A | N/A | 46 | 7.0805 | 0.31 | 106.82 | 7.1145 | 0.33 | 252.87 |
| 2 | N/A | N/A | N/A | N/A | N/A | N/A | 48 | 7.0772 | 0.33 | 104.54 | 7.1251 | 0.32 | 255.12 |
| 4 | N/A | N/A | N/A | N/A | N/A | N/A | 50 | 7.0638 | 0.35 | 102.40 | 7.1397 | 0.34 | 257.27 |
| 6 | N/A | N/A | N/A | N/A | N/A | N/A | 52 | 7.0701 | 0.37 | 100.42 | 7.1174 | 0.35 | 259.28 |
| 8 | N/A | N/A | N/A | N/A | N/A | N/A | 54 | 7.0250 | 0.35 | 98.44 | 7.1164 | 0.35 | 261.21 |
| 10 | N/A | N/A | N/A | N/A | N/A | N/A | 56 | 7.0351 | 0.37 | 96.62 | 7.1225 | 0.34 | 263.09 |
| 12 | N/A | N/A | N/A | N/A | N/A | N/A | 58 | 7.0205 | 0.37 | 94.79 | 7.1123 | 0.35 | 264.95 |
| 14 | N/A | N/A | N/A | N/A | N/A | N/A | 60 | 6.9962 | 0.36 | 93.04 | 7.1064 | 0.36 | 266.66 |
| 16 | N/A | N/A | N/A | N/A | N/A | N/A | 62 | 7.0035 | 0.36 | 91.34 | 7.1128 | 0.37 | 268.39 |
| 18 | N/A | N/A | N/A | N/A | N/A | N/A | 64 | 7.0483 | 0.40 | 89.67 | 7.1169 | 0.38 | 270.08 |
| 20 | N/A | N/A | N/A | N/A | N/A | N/A | 66 | 7.1443 | 0.39 | 88.03 | 7.1148 | 0.40 | 271.67 |
| 22 | N/A | N/A | N/A | N/A | N/A | N/A | 68 | 7.0063 | 0.42 | 86.41 | 7.1298 | 0.42 | 273.35 |
| 24 | 7.1247 | 0.30 | 166.84 | 7.1215 | 0.31 | 193.06 | 70 | 6.9991 | 0.47 | 84.81 | 7.1430 | 0.45 | 274.98 |
| 26 | 7.1389 | 0.33 | 151.12 | 7.1392 | 0.31 | 209.06 | 72 | 7.0207 | 0.47 | 83.18 | 7.1380 | 0.48 | 276.59 |
| 28 | 7.0749 | 0.32 | 140.63 | 7.1562 | 0.32 | 218.05 | 74 | 7.0573 | 0.52 | 81.60 | 7.1538 | 0.53 | 278.19 |
| 30 | 7.0746 | 0.31 | 134.37 | 7.1481 | 0.32 | 224.60 | 76 | 7.0925 | 0.58 | 79.98 | 7.1604 | 0.59 | 279.78 |
| 32 | 7.0707 | 0.32 | 129.29 | 7.1284 | 0.33 | 230.04 | 78 | 7.0972 | 0.66 | 78.38 | 7.1777 | N/A | 281.39 |
| 34 | 7.1044 | 0.33 | 124.82 | 7.1395 | 0.31 | 234.42 | 80 | 7.1611 | N/A | 76.78 | 7.2112 | N/A | 283.04 |
| 36 | 7.0929 | 0.31 | 120.99 | 7.1211 | 0.30 | 238.39 | 82 | N/A | N/A | N/A | 7.2959 | N/A | 284.68 |
| 38 | 7.0963 | 0.32 | 117.56 | 7.1137 | 0.32 | 241.89 | 84 | N/A | N/A | N/A | 7.3192 | N/A | 286.42 |
| 40 | 7.0872 | 0.31 | 114.56 | 7.0927 | 0.34 | 244.98 | 86 | N/A | N/A | N/A | N/A | N/A | N/A |
| 42 | 7.1016 | 0.33 | 111.74 | 7.1439 | 0.31 | 247.86 | 88 | N/A | N/A | N/A | N/A | N/A | N/A |
| 44 | 7.0698 | 0.33 | 109.27 | 7.1321 | 0.34 | 250.37 | 90 | N/A | N/A | N/A | N/A | N/A | N/A |

N/A - Not Available

Figure 3. Type-B Standard Uncertainty vs Zenith Angle

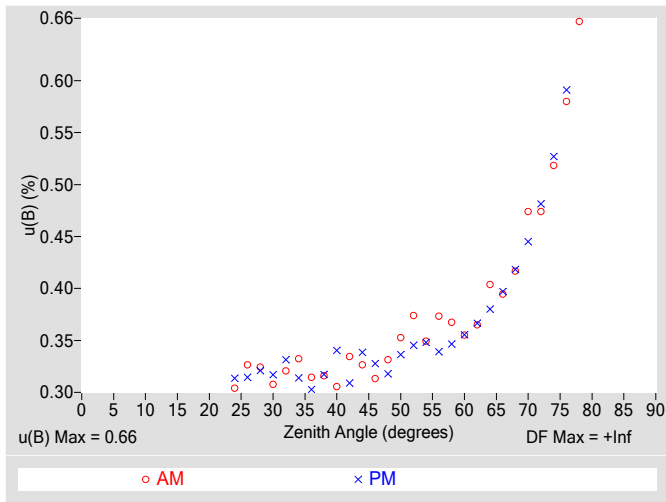


Figure 4. Residuals from Spline Interpolation

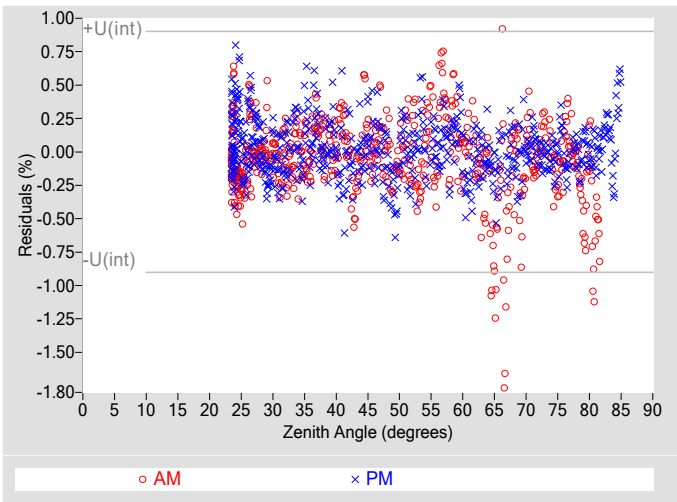


Table 3. Uncertainty using Spline Interpolation ‡

| | |
|---|------------|
| Type-B Standard Uncertainty, $u(B)$ (%) | ± 0.66 |
| Type-A Interpolating Function, $u(int)$ (%) | ± 0.45 |
| Combined Standard Uncertainty, $u(c)$ (%) | ± 0.80 |
| Effective degrees of freedom, $DF(c)$ | 11200 |
| Coverage factor, k | 1.96 |
| Expanded Uncertainty, $U95$ (%) | ± 1.6 |
| AM Valid zenith angle range | 24° to 78° |
| PM Valid zenith angle range | 24° to 76° |

‡ An illustration for how to reduce the uncertainty in calculating the irradiance using a function rather than $R@45^\circ$. Not accredited.

Table 4. Calibration Label Values

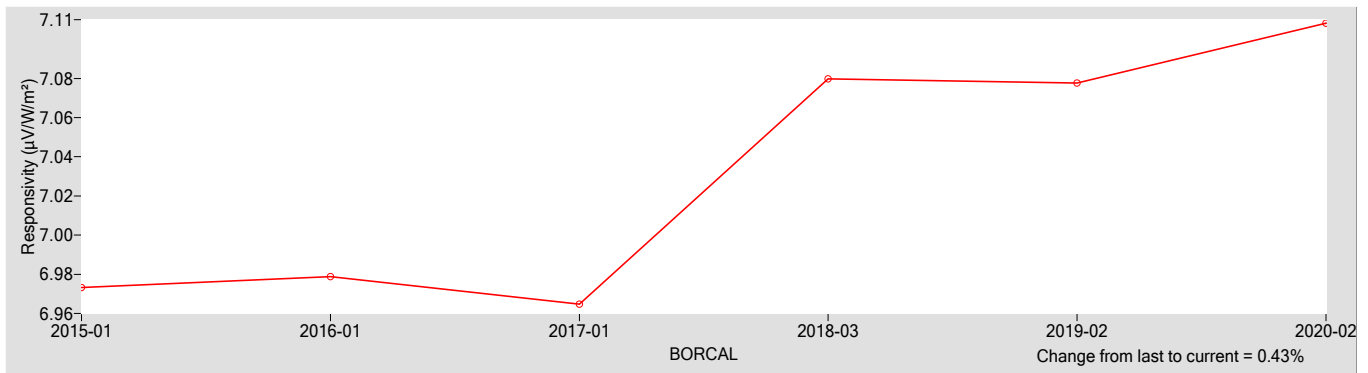
| | |
|----------------------------------|-------------------------------|
| $R @ 45^\circ$ ($\mu V/W/m^2$) | R_{net} ($\mu V/W/m^2$) † |
| 7.1082 | 0.18000 |

† R_{net} determination date: Estimated

Table 5. Uncertainty using $R @ 45^\circ$

| | |
|---|----------------|
| Type-B Expanded Uncertainty, $U(B)$ (%) | ± 0.73 |
| Offset Uncertainty, $U(off)$ (%) | +0.56 / -1.6 |
| Expanded Uncertainty, U (%) | +1.3 / -2.3 |
| Effective degrees of freedom, DF | +Inf |
| Coverage factor, k | 1.96 |
| Valid zenith angle range | 30.0° to 60.0° |

Figure 5. History of instrument at Zenith Angle = 45°



References:

[1] Reda, I.; Hickey, J.; Long, C.; Myers, D.; Stoffel, T.; Wilcox, S.; Michalsky, J. J.; Dutton, E. G.; Nelson, D. (2005). "Using a Blackbody to Calculate Net Longwave Responsivity of Shortwave Solar Pyranometers to Correct for Their Thermal Offset Error During Outdoor Calibration Using the Component Sum Method." *Journal of Atmospheric and Oceanic Technology*, 2005; pp. 1531-1540; NREL Report No. JA-560-36646. doi:10.1175/JTECH1782.1

[2] Reda, I.; Myers, D.; Stoffel, T. (2008). "Uncertainty Estimate for the Outdoor Calibration of Solar Pyranometers: A Metrologist Perspective." *Measure*. (NCSLI *Journal of Measurement Science*). Vol. 3(4), December 2008; pp. 58-66; NREL Report No. JA-581-4137

[3] Reda, I.; Andreas, A. (2004). "Solar Position Algorithm for Solar Radiation Applications." *Solar Energy*. Vol. 76(5), 2004; pp. 577-589; NREL Report No. JA-560-35518. doi:10.1016/j.solener.2003.12.003

[4] Stoffel, T.; Reda, I. (2009). "NREL Pyrheliometer Comparisons: 22 September - 3 October 2008 (NPC-2008)." 54 pp.; NREL Report No. TP-550-45016.

[5] Reda, I.; Stoffel, T.; Myers, D. (2003). "Method to Calibrate a Solar Pyranometer for Measuring Reference Diffuse Irradiance." *Solar Energy*. Vol. 74, 2003; pp. 103-112; NREL Report No. JA-560-35025. doi:10.1016/S0038-092X(03)00124-5

[6] Reda, I. (1996). *Calibration of a Solar Absolute Cavity Radiometer with Traceability to the World Radiometric Reference*. 79 pp.; NREL Report No. TP-463-20619.

[7] Reda, I.; Gröbner, J.; Stoffel, T.; Myers, D.; Forgan, B. (2008). *Improvements in the Blackbody Calibration of Pyrgometers*. ARM 2008 Science Team Meeting (Poster).



National Renewable Energy Laboratory

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Calibration Certificate



| | | | |
|--------------------------|-----------------------------|----------------------------------|------------|
| Test Instrument: | Revised Silicon Pyranometer | Manufacturer: | Licor |
| Model: | LI200R | Serial Number: | PY100360 |
| Calibration Date: | 5/5/2020 | Due Date: | 5/5/2021 |
| Customer: | NREL-SRRL-BMS | Environmental Conditions: | see page 4 |
| Test Dates: | 5/4-5 | | |

This certifies that the above product was calibrated in compliance with ISO/IEC 17025:2017. Measurement uncertainties at the time of calibration are consistent with the Guide to the Expression of Uncertainty in Measurement (GUM) using Reda et al., 2008. All nominal values are traceable to the International System (SI) Units of Measurement.

No statement of compliance with specifications is made or implied on this certificate. However, the estimated uncertainties are the uncertainties of the calibration process; users must add other uncertainties that are relevant to their measuring system, environmental and sky conditions, outdoor set-up, and site location.

The Type-B Standard Uncertainty of using the responsivity at each even zenith angle is reported, and the Expanded Uncertainty of the calibration is reported using two methods:

1. The Expanded Uncertainty of using the responsivity at zenith angle = 45°, within the zenith angle range from 30.0° to 60.0°
2. The Expanded Uncertainty of using Spline Interpolating Functions for the responsivity versus zenith angle.

This certificate applies only to the item identified above and shall not be reproduced other than in full, without specific written approval from the calibration facility. Certificate without signature is not valid.

Table 1. Traceability

| Measurement Type | Instrument | Calibration Date | Calibration Due Date |
|----------------------|--|------------------|----------------------|
| Beam Irradiance † | Eppley Absolute Cavity Radiometer Model HF, S/N 29219 | 09/27/2019 | 09/27/2020 |
| Diffuse Irradiance † | Hukseflux Pyranometer Model SR25, S/N 2541 | 04/17/2020 | 04/17/2021 |
| Diffuse Irradiance † | Hukseflux Pyranometer Model SR25, S/N 2542 | 04/17/2020 | 04/17/2021 |
| Data Acquisition | NREL Data Acquisition System Model RAP-DAQ, S/N 2005-998 | 02/14/2019 | 02/14/2021 |
| Data Acquisition | NREL Data Acquisition System Model RAP-DAQ, S/N 2005-999 | 02/14/2019 | 02/14/2021 |

† Through the World Radiometric Reference (WRR)

Number of pages of certificate: 4

Calibration Procedure: BORCAL-P00-Calibration and QA Procedure; available upon request.

Setup: Radiometers are calibrated outdoors, using the sun as the source. Pyranometers and pyrgeometers are installed for horizontal measurements, with their signal connectors oriented north, if their design permits.

The shading disk for the reference diffuse subtends a solid angle of 5°. Pyrheliometers are installed on solar trackers.

Calibrated by: Afshin Andreas, Ibrahim Reda, Peter Gotseff, and RCC

Ibrahim Reda, Technical Manager

Date

For questions or comments, please contact the technical manager at:

ibrahim.reda@nrel.gov; 303-384-6385; 15013 Denver West Parkway, Golden, CO 80401, USA

Calibration Results

PY100360 Licor LI200R

The responsivity (R , $\mu\text{V}/\text{W}/\text{m}^2$) of the test instrument during calibration is calculated using this Measurement Equation:

$$R = (V - R_{net} * W_{net}) / I \quad [1]$$

where,

- V = radiometer output voltage (microvolts),
 - R_{net} = radiometer net infrared responsivity ($\mu\text{V}/\text{W}/\text{m}^2$), see Table 4,
 - W_{net} = effective net infrared measured by pyrgeometer (W/m^2),
 - = $W_{in} - W_{out} = W_{in} - \sigma * T_c^4$
 - where, W_{in} = incoming infrared (W/m^2), $\sigma = 5.6704\text{e-}8 \text{ W}\cdot\text{m}^{-2}\cdot\text{K}^{-4}$,
 - T_c = case temperature of pyrgeometer (K).
- I = reference irradiance (W/m^2), beam (B) or global (G)
 where, $G = B * \text{COS}(Z) + D$,
 Z = zenith angle (degrees),
 D = reference diffuse irradiance (W/m^2).

Figure 1. Responsivity vs Zenith Angle

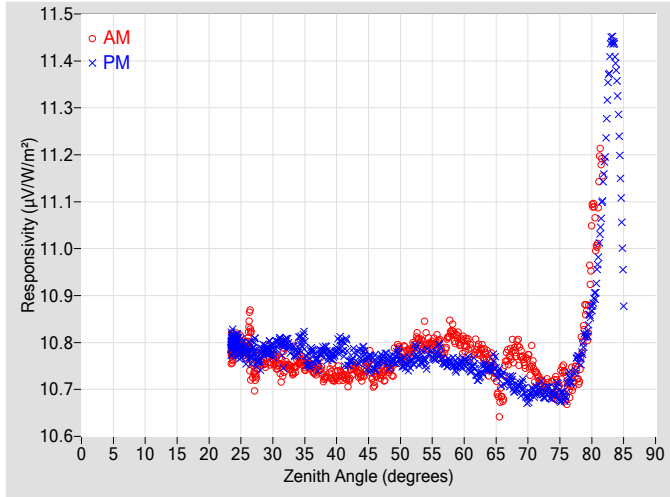


Figure 2. Responsivity vs Local Standard Time

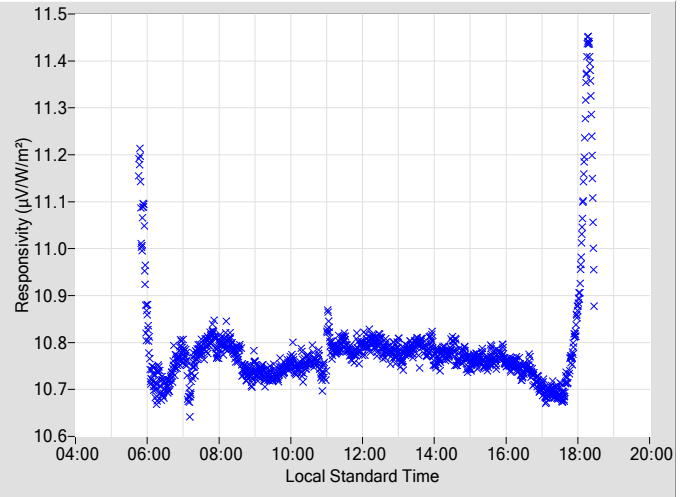


Table 2. Instrument Responsivity (R) and Calibration Type-B Standard Uncertainty, u(B)

| Zenith Angle (deg.) | R ($\mu\text{V}/\text{W}/\text{m}^2$) | AM u(B) \pm (%) | Azimuth Angle | R ($\mu\text{V}/\text{W}/\text{m}^2$) | PM u(B) \pm (%) | Azimuth Angle | Zenith Angle (deg.) | R ($\mu\text{V}/\text{W}/\text{m}^2$) | AM u(B) \pm (%) | Azimuth Angle | R ($\mu\text{V}/\text{W}/\text{m}^2$) | PM u(B) \pm (%) | Azimuth Angle |
|---------------------|---|-------------------|---------------|---|-------------------|---------------|---------------------|---|-------------------|---------------|---|-------------------|---------------|
| 0 | N/A | N/A | N/A | N/A | N/A | N/A | 46 | 10.719 | 0.31 | 106.77 | 10.750 | 0.31 | 252.82 |
| 2 | N/A | N/A | N/A | N/A | N/A | N/A | 48 | 10.746 | 0.33 | 104.55 | 10.763 | 0.33 | 255.08 |
| 4 | N/A | N/A | N/A | N/A | N/A | N/A | 50 | 10.774 | 0.35 | 102.42 | 10.764 | 0.33 | 257.23 |
| 6 | N/A | N/A | N/A | N/A | N/A | N/A | 52 | 10.790 | 0.33 | 100.38 | 10.767 | 0.33 | 259.30 |
| 8 | N/A | N/A | N/A | N/A | N/A | N/A | 54 | 10.807 | 0.34 | 98.46 | 10.761 | 0.34 | 261.22 |
| 10 | N/A | N/A | N/A | N/A | N/A | N/A | 56 | 10.799 | 0.33 | 96.58 | 10.786 | 0.33 | 263.10 |
| 12 | N/A | N/A | N/A | N/A | N/A | N/A | 58 | 10.830 | 0.37 | 94.80 | 10.758 | 0.34 | 264.92 |
| 14 | N/A | N/A | N/A | N/A | N/A | N/A | 60 | 10.796 | 0.34 | 93.05 | 10.757 | 0.34 | 266.67 |
| 16 | N/A | N/A | N/A | N/A | N/A | N/A | 62 | 10.789 | 0.35 | 91.35 | 10.730 | 0.35 | 268.39 |
| 18 | N/A | N/A | N/A | N/A | N/A | N/A | 64 | 10.754 | 0.41 | 89.68 | 10.745 | 0.37 | 270.09 |
| 20 | N/A | N/A | N/A | N/A | N/A | N/A | 66 | 10.693 | 0.43 | 88.03 | 10.723 | 0.38 | 271.72 |
| 22 | N/A | N/A | N/A | N/A | N/A | N/A | 68 | 10.780 | 0.40 | 86.42 | 10.700 | 0.40 | 273.36 |
| 24 | 10.788 | 0.32 | 166.97 | 10.800 | 0.32 | 193.02 | 70 | 10.765 | 0.42 | 84.74 | 10.680 | 0.42 | 274.99 |
| 26 | 10.804 | 0.33 | 150.85 | 10.779 | 0.31 | 209.04 | 72 | 10.709 | 0.45 | 83.19 | 10.702 | 0.46 | 276.60 |
| 28 | 10.767 | 0.29 | 141.03 | 10.768 | 0.31 | 218.08 | 74 | 10.698 | 0.49 | 81.61 | 10.690 | 0.50 | 278.20 |
| 30 | 10.765 | 0.29 | 134.16 | 10.783 | 0.30 | 224.62 | 76 | 10.696 | 0.65 | 79.99 | 10.702 | 0.56 | 279.83 |
| 32 | 10.755 | 0.32 | 129.22 | 10.800 | 0.32 | 229.97 | 78 | 10.730 | 0.62 | 78.39 | 10.765 | N/A | 281.45 |
| 34 | 10.770 | 0.31 | 124.84 | 10.790 | 0.30 | 234.53 | 80 | 11.034 | N/A | 76.75 | 10.872 | N/A | 283.05 |
| 36 | 10.747 | 0.30 | 121.07 | 10.773 | 0.30 | 238.41 | 82 | N/A | N/A | N/A | 11.199 | N/A | 284.74 |
| 38 | 10.726 | 0.31 | 117.65 | 10.785 | 0.31 | 241.83 | 84 | N/A | N/A | N/A | 11.331 | N/A | 286.39 |
| 40 | 10.734 | 0.33 | 114.51 | 10.787 | 0.33 | 245.00 | 86 | N/A | N/A | N/A | N/A | N/A | N/A |
| 42 | 10.723 | 0.30 | 111.82 | 10.756 | 0.32 | 247.81 | 88 | N/A | N/A | N/A | N/A | N/A | N/A |
| 44 | 10.726 | 0.34 | 109.17 | 10.779 | 0.35 | 250.45 | 90 | N/A | N/A | N/A | N/A | N/A | N/A |

N/A - Not Available

Figure 3. Type-B Standard Uncertainty vs Zenith Angle

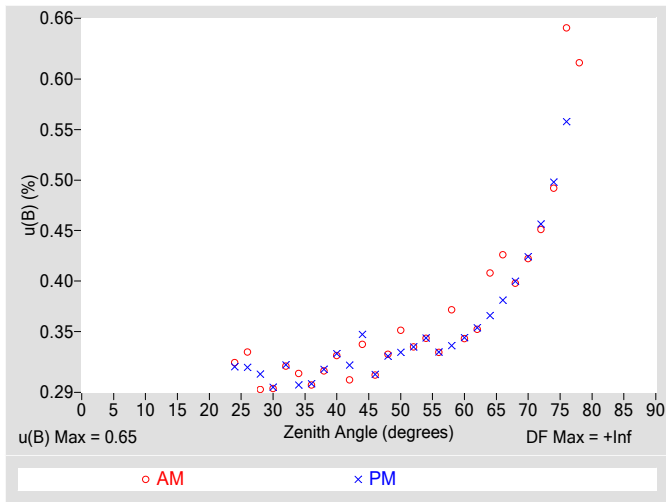


Figure 4. Residuals from Spline Interpolation

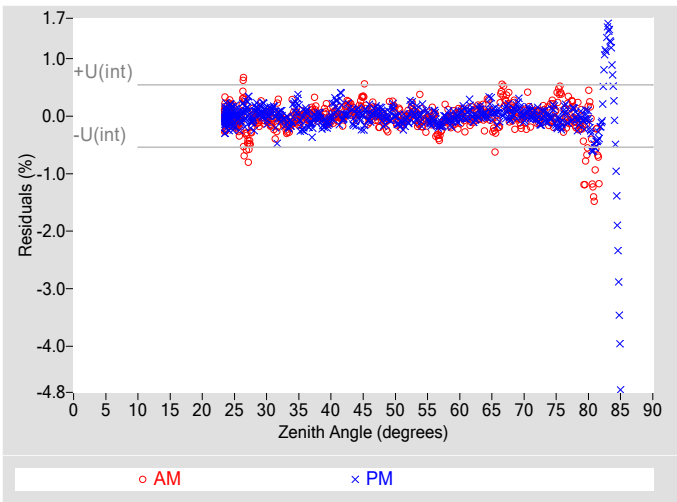


Table 3. Uncertainty using Spline Interpolation ‡

| | |
|---|------------|
| Type-B Standard Uncertainty, $u(B)$ (%) | ± 0.65 |
| Type-A Interpolating Function, $u(int)$ (%) | ± 0.27 |
| Combined Standard Uncertainty, $u(c)$ (%) | ± 0.70 |
| Effective degrees of freedom, $DF(c)$ | 52787 |
| Coverage factor, k | 1.96 |
| Expanded Uncertainty, U_{95} (%) | ± 1.4 |
| AM Valid zenith angle range | 24° to 78° |
| PM Valid zenith angle range | 24° to 76° |

‡ An illustration for how to reduce the uncertainty in calculating the irradiance using a function rather than $R@45^\circ$. Not accredited.

Table 4. Calibration Label Values

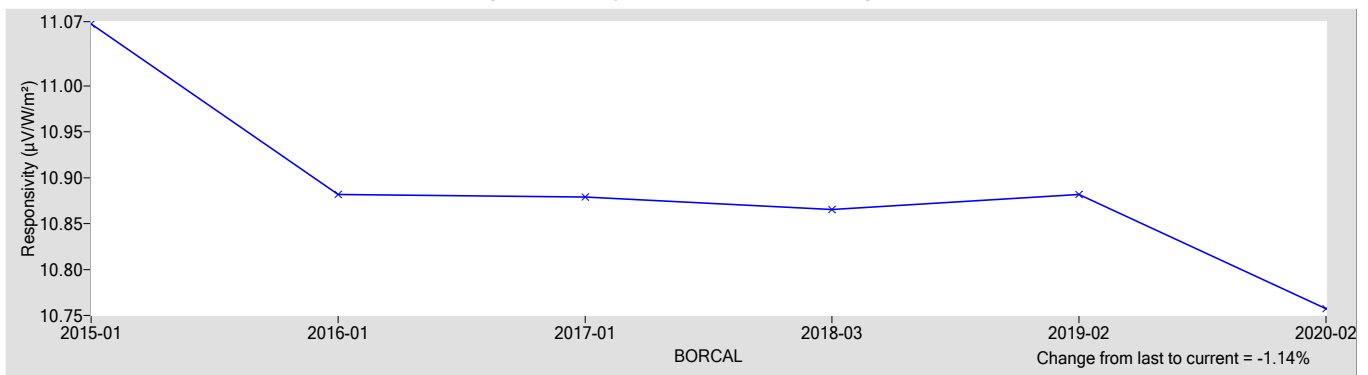
| | |
|----------------------------------|-------------------------------|
| $R @ 45^\circ$ ($\mu V/W/m^2$) | R_{net} ($\mu V/W/m^2$) † |
| 10.757 | 0 |

† R_{net} determination date: N/A

Table 5. Uncertainty using $R @ 45^\circ$

| | |
|---|----------------|
| Type-B Expanded Uncertainty, $U(B)$ (%) | ± 0.73 |
| Offset Uncertainty, $U(off)$ (%) | +0.67 / -0.35 |
| Expanded Uncertainty, U (%) | +1.4 / -1.1 |
| Effective degrees of freedom, DF | +Inf |
| Coverage factor, k | 1.96 |
| Valid zenith angle range | 30.0° to 60.0° |

Figure 5. History of instrument at Zenith Angle = 45°



References:

- [1] Reda, I.; Hickey, J.; Long, C.; Myers, D.; Stoffel, T.; Wilcox, S.; Michalsky, J. J.; Dutton, E. G.; Nelson, D. (2005). "Using a Blackbody to Calculate Net Longwave Responsivity of Shortwave Solar Pyranometers to Correct for Their Thermal Offset Error During Outdoor Calibration Using the Component Sum Method." *Journal of Atmospheric and Oceanic Technology*, 2005; pp. 1531-1540; NREL Report No. JA-560-36646. doi:10.1175/JTECH1782.1
- [2] Reda, I.; Myers, D.; Stoffel, T. (2008). "Uncertainty Estimate for the Outdoor Calibration of Solar Pyranometers: A Metrologist Perspective." *Measure*. (NCSLI Journal of Measurement Science). Vol. 3(4), December 2008; pp. 58-66; NREL Report No. JA-581-4137
- [3] Reda, I.; Andreas, A. (2004). "Solar Position Algorithm for Solar Radiation Applications." *Solar Energy*. Vol. 76(5), 2004; pp. 577-589; NREL Report No. JA-560-35518. doi:10.1016/j.solener.2003.12.003
- [4] Stoffel, T.; Reda, I. (2009). "NREL Pyrheliometer Comparisons: 22 September - 3 October 2008 (NPC-2008)." 54 pp.; NREL Report No. TP-550-45016.
- [5] Reda, I.; Stoffel, T.; Myers, D. (2003). "Method to Calibrate a Solar Pyranometer for Measuring Reference Diffuse Irradiance." *Solar Energy*. Vol. 74, 2003; pp. 103-112; NREL Report No. JA-560-35025. doi:10.1016/S0038-092X(03)00124-5
- [6] Reda, I. (1996). Calibration of a Solar Absolute Cavity Radiometer with Traceability to the World Radiometric Reference. 79 pp.; NREL Report No. TP-463-20619.
- [7] Reda, I.; Gröbner, J.; Stoffel, T.; Myers, D.; Forgan, B. (2008). Improvements in the Blackbody Calibration of Pyrgometers. ARM 2008 Science Team Meeting (Poster).



National Renewable Energy Laboratory

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Calibration Certificate



| | | | |
|--------------------------|-----------------------------|----------------------------------|------------|
| Test Instrument: | Revised Silicon Pyranometer | Manufacturer: | Licor |
| Model: | LI200R | Serial Number: | PY108623 |
| Calibration Date: | 5/5/2020 | Due Date: | 5/5/2021 |
| Customer: | NREL-SRRL-BMS | Environmental Conditions: | see page 4 |
| Test Dates: | 5/4-5 | | |

This certifies that the above product was calibrated in compliance with ISO/IEC 17025:2017. Measurement uncertainties at the time of calibration are consistent with the Guide to the Expression of Uncertainty in Measurement (GUM) using Reda et al., 2008. All nominal values are traceable to the International System (SI) Units of Measurement.

No statement of compliance with specifications is made or implied on this certificate. However, the estimated uncertainties are the uncertainties of the calibration process; users must add other uncertainties that are relevant to their measuring system, environmental and sky conditions, outdoor set-up, and site location.

The Type-B Standard Uncertainty of using the responsivity at each even zenith angle is reported, and the Expanded Uncertainty of the calibration is reported using two methods:

1. The Expanded Uncertainty of using the responsivity at zenith angle = 45°, within the zenith angle range from 30.0° to 60.0°
2. The Expanded Uncertainty of using Spline Interpolating Functions for the responsivity versus zenith angle.

This certificate applies only to the item identified above and shall not be reproduced other than in full, without specific written approval from the calibration facility. Certificate without signature is not valid.

Table 1. Traceability

| Measurement Type | Instrument | Calibration Date | Calibration Due Date |
|----------------------|--|------------------|----------------------|
| Beam Irradiance † | Eppley Absolute Cavity Radiometer Model HF, S/N 29219 | 09/27/2019 | 09/27/2020 |
| Diffuse Irradiance † | Hukseflux Pyranometer Model SR25, S/N 2541 | 04/17/2020 | 04/17/2021 |
| Diffuse Irradiance † | Hukseflux Pyranometer Model SR25, S/N 2542 | 04/17/2020 | 04/17/2021 |
| Data Acquisition | NREL Data Acquisition System Model RAP-DAQ, S/N 2005-998 | 02/14/2019 | 02/14/2021 |
| Data Acquisition | NREL Data Acquisition System Model RAP-DAQ, S/N 2005-999 | 02/14/2019 | 02/14/2021 |

† Through the World Radiometric Reference (WRR)

Number of pages of certificate: 4

Calibration Procedure: BORCAL-P00-Calibration and QA Procedure; available upon request.

Setup: Radiometers are calibrated outdoors, using the sun as the source. Pyranometers and pyrgeometers are installed for horizontal measurements, with their signal connectors oriented north, if their design permits.

The shading disk for the reference diffuse subtends a solid angle of 5°. Pyrheliometers are installed on solar trackers.

Calibrated by: Afshin Andreas, Ibrahim Reda, Peter Gotseff, and RCC

Ibrahim Reda, Technical Manager

Date

For questions or comments, please contact the technical manager at:

ibrahim.reda@nrel.gov; 303-384-6385; 15013 Denver West Parkway, Golden, CO 80401, USA

Calibration Results

PY108623 Licor LI200R

The responsivity (R , $\mu\text{V}/\text{W}/\text{m}^2$) of the test instrument during calibration is calculated using this Measurement Equation:

$$R = (V - R_{net} * W_{net}) / I \quad [1]$$

where,

- V = radiometer output voltage (microvolts),
 - R_{net} = radiometer net infrared responsivity ($\mu\text{V}/\text{W}/\text{m}^2$), see Table 4,
 - W_{net} = effective net infrared measured by pyrgeometer (W/m^2),
 - = $W_{in} - W_{out} = W_{in} - \sigma * T_c^4$
 - where, W_{in} = incoming infrared (W/m^2), $\sigma = 5.6704\text{e-}8 \text{ W}\cdot\text{m}^{-2}\cdot\text{K}^{-4}$,
 - T_c = case temperature of pyrgeometer (K).
- I = reference irradiance (W/m^2), beam (B) or global (G)
 where, $G = B * \text{COS}(Z) + D$,
 Z = zenith angle (degrees),
 D = reference diffuse irradiance (W/m^2).

Figure 1. Responsivity vs Zenith Angle

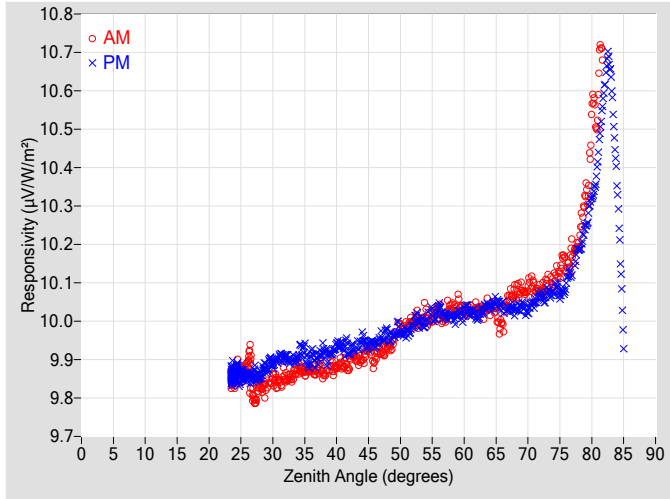


Figure 2. Responsivity vs Local Standard Time

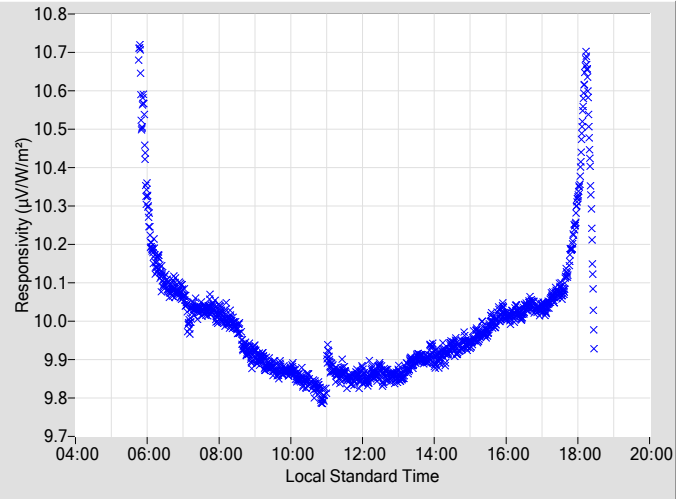


Table 2. Instrument Responsivity (R) and Calibration Type-B Standard Uncertainty, u(B)

| Zenith Angle (deg.) | R ($\mu\text{V}/\text{W}/\text{m}^2$) | AM u(B) \pm (%) | Azimuth Angle | R ($\mu\text{V}/\text{W}/\text{m}^2$) | PM u(B) \pm (%) | Azimuth Angle | Zenith Angle (deg.) | R ($\mu\text{V}/\text{W}/\text{m}^2$) | AM u(B) \pm (%) | Azimuth Angle | R ($\mu\text{V}/\text{W}/\text{m}^2$) | PM u(B) \pm (%) | Azimuth Angle |
|---------------------|---|-------------------|---------------|---|-------------------|---------------|---------------------|---|-------------------|---------------|---|-------------------|---------------|
| 0 | N/A | N/A | N/A | N/A | N/A | N/A | 46 | 9.8976 | 0.31 | 106.77 | 9.9386 | 0.31 | 252.82 |
| 2 | N/A | N/A | N/A | N/A | N/A | N/A | 48 | 9.9353 | 0.33 | 104.55 | 9.9677 | 0.33 | 255.08 |
| 4 | N/A | N/A | N/A | N/A | N/A | N/A | 50 | 9.9778 | 0.35 | 102.42 | 9.9718 | 0.33 | 257.23 |
| 6 | N/A | N/A | N/A | N/A | N/A | N/A | 52 | 9.9936 | 0.34 | 100.38 | 9.9947 | 0.34 | 259.30 |
| 8 | N/A | N/A | N/A | N/A | N/A | N/A | 54 | 10.014 | 0.34 | 98.46 | 9.9971 | 0.34 | 261.22 |
| 10 | N/A | N/A | N/A | N/A | N/A | N/A | 56 | 10.030 | 0.33 | 96.58 | 10.037 | 0.33 | 263.10 |
| 12 | N/A | N/A | N/A | N/A | N/A | N/A | 58 | 10.038 | 0.37 | 94.80 | 10.015 | 0.34 | 264.92 |
| 14 | N/A | N/A | N/A | N/A | N/A | N/A | 60 | 10.025 | 0.34 | 93.05 | 10.022 | 0.34 | 266.67 |
| 16 | N/A | N/A | N/A | N/A | N/A | N/A | 62 | 10.033 | 0.35 | 91.35 | 10.010 | 0.35 | 268.39 |
| 18 | N/A | N/A | N/A | N/A | N/A | N/A | 64 | 10.031 | 0.41 | 89.68 | 10.035 | 0.37 | 270.09 |
| 20 | N/A | N/A | N/A | N/A | N/A | N/A | 66 | 9.9973 | 0.43 | 88.03 | 10.037 | 0.38 | 271.72 |
| 22 | N/A | N/A | N/A | N/A | N/A | N/A | 68 | 10.076 | 0.40 | 86.42 | 10.028 | 0.40 | 273.36 |
| 24 | 9.8547 | 0.32 | 166.97 | 9.8632 | 0.32 | 193.02 | 70 | 10.096 | 0.42 | 84.74 | 10.027 | 0.42 | 274.99 |
| 26 | 9.8883 | 0.33 | 150.85 | 9.8567 | 0.31 | 209.04 | 72 | 10.078 | 0.45 | 83.19 | 10.068 | 0.46 | 276.60 |
| 28 | 9.8285 | 0.29 | 141.03 | 9.8567 | 0.31 | 218.08 | 74 | 10.101 | 0.49 | 81.61 | 10.077 | 0.50 | 278.20 |
| 30 | 9.8500 | 0.29 | 134.16 | 9.8878 | 0.30 | 224.62 | 76 | 10.143 | 0.65 | 79.99 | 10.101 | 0.56 | 279.83 |
| 32 | 9.8505 | 0.32 | 129.22 | 9.9061 | 0.32 | 229.97 | 78 | 10.211 | 0.62 | 78.39 | 10.188 | N/A | 281.45 |
| 34 | 9.8777 | 0.31 | 124.84 | 9.9114 | 0.30 | 234.53 | 80 | 10.524 | N/A | 76.75 | 10.321 | N/A | 283.05 |
| 36 | 9.8734 | 0.30 | 121.07 | 9.9100 | 0.30 | 238.41 | 82 | N/A | N/A | N/A | 10.620 | N/A | 284.74 |
| 38 | 9.8604 | 0.31 | 117.65 | 9.9228 | 0.31 | 241.83 | 84 | N/A | N/A | N/A | 10.341 | N/A | 286.39 |
| 40 | 9.8813 | 0.33 | 114.51 | 9.9388 | 0.33 | 245.00 | 86 | N/A | N/A | N/A | N/A | N/A | N/A |
| 42 | 9.8835 | 0.30 | 111.82 | 9.9167 | 0.32 | 247.81 | 88 | N/A | N/A | N/A | N/A | N/A | N/A |
| 44 | 9.8958 | 0.34 | 109.17 | 9.9536 | 0.35 | 250.45 | 90 | N/A | N/A | N/A | N/A | N/A | N/A |

N/A - Not Available

Figure 3. Type-B Standard Uncertainty vs Zenith Angle

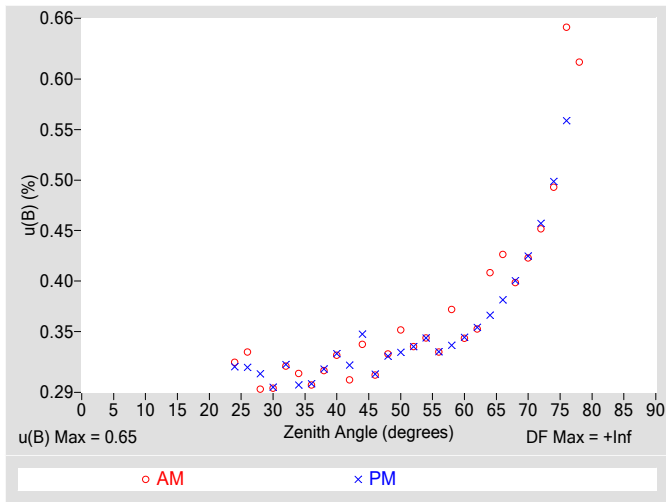


Figure 4. Residuals from Spline Interpolation

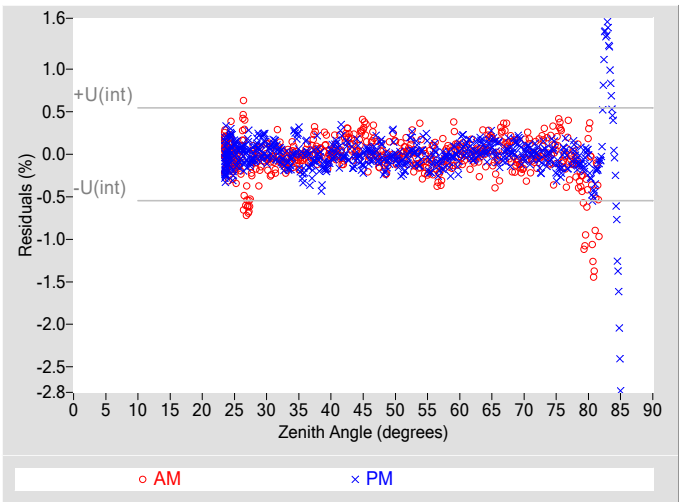


Table 3. Uncertainty using Spline Interpolation ‡

| | |
|---|------------|
| Type-B Standard Uncertainty, $u(B)$ (%) | ± 0.65 |
| Type-A Interpolating Function, $u(int)$ (%) | ± 0.27 |
| Combined Standard Uncertainty, $u(c)$ (%) | ± 0.71 |
| Effective degrees of freedom, $DF(c)$ | 51844 |
| Coverage factor, k | 1.96 |
| Expanded Uncertainty, $U95$ (%) | ± 1.4 |
| AM Valid zenith angle range | 24° to 78° |
| PM Valid zenith angle range | 24° to 76° |

‡ An illustration for how to reduce the uncertainty in calculating the irradiance using a function rather than $R@45^\circ$. Not accredited.

Table 4. Calibration Label Values

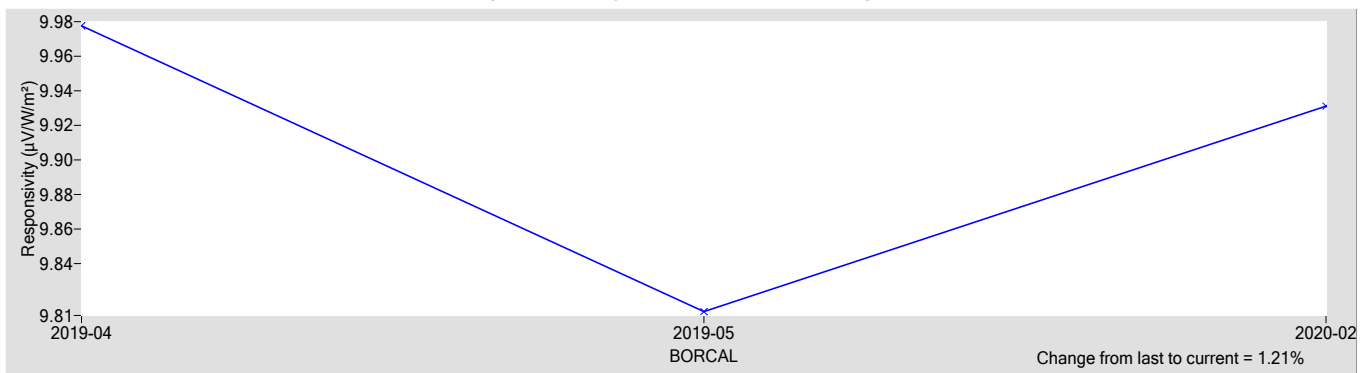
| | |
|----------------------------------|-------------------------------|
| $R @ 45^\circ$ ($\mu V/W/m^2$) | R_{net} ($\mu V/W/m^2$) † |
| 9.9311 | 0 |

† R_{net} determination date: N/A

Table 5. Uncertainty using $R @ 45^\circ$

| | |
|---|----------------|
| Type-B Expanded Uncertainty, $U(B)$ (%) | ± 0.73 |
| Offset Uncertainty, $U(off)$ (%) | +1.1 / -0.82 |
| Expanded Uncertainty, U (%) | +1.8 / -1.5 |
| Effective degrees of freedom, DF | +Inf |
| Coverage factor, k | 1.96 |
| Valid zenith angle range | 30.0° to 60.0° |

Figure 5. History of instrument at Zenith Angle = 45°



References:

[1] Reda, I.; Hickey, J.; Long, C.; Myers, D.; Stoffel, T.; Wilcox, S.; Michalsky, J. J.; Dutton, E. G.; Nelson, D. (2005). "Using a Blackbody to Calculate Net Longwave Responsivity of Shortwave Solar Pyranometers to Correct for Their Thermal Offset Error During Outdoor Calibration Using the Component Sum Method." *Journal of Atmospheric and Oceanic Technology*, 2005; pp. 1531-1540; NREL Report No. JA-560-36646. doi:10.1175/JTECH1782.1

[2] Reda, I.; Myers, D.; Stoffel, T. (2008). "Uncertainty Estimate for the Outdoor Calibration of Solar Pyranometers: A Metrologist Perspective." *Measure*. (NCSLI Journal of Measurement Science). Vol. 3(4), December 2008; pp. 58-66; NREL Report No. JA-581-4137

[3] Reda, I.; Andreas, A. (2004). "Solar Position Algorithm for Solar Radiation Applications." *Solar Energy*. Vol. 76(5), 2004; pp. 577-589; NREL Report No. JA-560-35518. doi:10.1016/j.solener.2003.12.003

[4] Stoffel, T.; Reda, I. (2009). "NREL Pyrheliometer Comparisons: 22 September - 3 October 2008 (NPC-2008)." 54 pp.; NREL Report No. TP-550-45016.

[5] Reda, I.; Stoffel, T.; Myers, D. (2003). "Method to Calibrate a Solar Pyranometer for Measuring Reference Diffuse Irradiance." *Solar Energy*. Vol. 74, 2003; pp. 103-112; NREL Report No. JA-560-35025. doi:10.1016/S0038-092X(03)00124-5

[6] Reda, I. (1996). Calibration of a Solar Absolute Cavity Radiometer with Traceability to the World Radiometric Reference. 79 pp.; NREL Report No. TP-463-20619.

[7] Reda, I.; Gröbner, J.; Stoffel, T.; Myers, D.; Forgan, B. (2008). Improvements in the Blackbody Calibration of Pyrgometers. ARM 2008 Science Team Meeting (Poster).



National Renewable Energy Laboratory

Solar Radiation Research Laboratory

Metrology Laboratory

Calibration Certificate



| | | | |
|--------------------------|---------------------|----------------------------------|------------|
| Test Instrument: | Silicon Pyranometer | Manufacturer: | Licor |
| Model: | LI200 | Serial Number: | PY1750 |
| Calibration Date: | 5/5/2020 | Due Date: | 5/5/2021 |
| Customer: | NREL-SRRL-BMS | Environmental Conditions: | see page 4 |
| Test Dates: | 5/4-5 | | |

This certifies that the above product was calibrated in compliance with ISO/IEC 17025:2017. Measurement uncertainties at the time of calibration are consistent with the Guide to the Expression of Uncertainty in Measurement (GUM) using Reda et al., 2008. All nominal values are traceable to the International System (SI) Units of Measurement.

No statement of compliance with specifications is made or implied on this certificate. However, the estimated uncertainties are the uncertainties of the calibration process; users must add other uncertainties that are relevant to their measuring system, environmental and sky conditions, outdoor set-up, and site location.

The Type-B Standard Uncertainty of using the responsivity at each even zenith angle is reported, and the Expanded Uncertainty of the calibration is reported using two methods:

1. The Expanded Uncertainty of using the responsivity at zenith angle = 45°, within the zenith angle range from 30.0° to 60.0°
2. The Expanded Uncertainty of using Spline Interpolating Functions for the responsivity versus zenith angle.

This certificate applies only to the item identified above and shall not be reproduced other than in full, without specific written approval from the calibration facility. Certificate without signature is not valid.

Table 1. Traceability

| Measurement Type | Instrument | Calibration Date | Calibration Due Date |
|----------------------|--|------------------|----------------------|
| Beam Irradiance † | Eppley Absolute Cavity Radiometer Model HF, S/N 29219 | 09/27/2019 | 09/27/2020 |
| Diffuse Irradiance † | Hukseflux Pyranometer Model SR25, S/N 2541 | 04/17/2020 | 04/17/2021 |
| Diffuse Irradiance † | Hukseflux Pyranometer Model SR25, S/N 2542 | 04/17/2020 | 04/17/2021 |
| Data Acquisition | NREL Data Acquisition System Model RAP-DAQ, S/N 2005-998 | 02/14/2019 | 02/14/2021 |
| Data Acquisition | NREL Data Acquisition System Model RAP-DAQ, S/N 2005-999 | 02/14/2019 | 02/14/2021 |

† Through the World Radiometric Reference (WRR)

Number of pages of certificate: 4

Calibration Procedure: BORCAL-P00-Calibration and QA Procedure; available upon request.

Setup: Radiometers are calibrated outdoors, using the sun as the source. Pyranometers and pyrgeometers are installed for horizontal measurements, with their signal connectors oriented north, if their design permits.

The shading disk for the reference diffuse subtends a solid angle of 5°. Pyrheliometers are installed on solar trackers.

Calibrated by: Afshin Andreas, Ibrahim Reda, Peter Gotseff, and RCC

Ibrahim Reda, Technical Manager

Date

For questions or comments, please contact the technical manager at:

ibrahim.reda@nrel.gov; 303-384-6385; 15013 Denver West Parkway, Golden, CO 80401, USA

Calibration Results

PY1750 Licor LI200

The responsivity (R , $\mu\text{V}/\text{W}/\text{m}^2$) of the test instrument during calibration is calculated using this Measurement Equation:

$$R = (V - R_{net} * W_{net}) / I \quad [1]$$

where,

- V = radiometer output voltage (microvolts),
 - R_{net} = radiometer net infrared responsivity ($\mu\text{V}/\text{W}/\text{m}^2$), see Table 4,
 - W_{net} = effective net infrared measured by pyrgeometer (W/m^2),
 - = $W_{in} - W_{out} = W_{in} - \sigma * T_c^4$
 - where, W_{in} = incoming infrared (W/m^2), $\sigma = 5.6704\text{e-}8 \text{ W}\cdot\text{m}^{-2}\cdot\text{K}^{-4}$,
 - T_c = case temperature of pyrgeometer (K).
- I = reference irradiance (W/m^2), beam (B) or global (G)
 where, $G = B * \text{COS}(Z) + D$,
 Z = zenith angle (degrees),
 D = reference diffuse irradiance (W/m^2).

Figure 1. Responsivity vs Zenith Angle

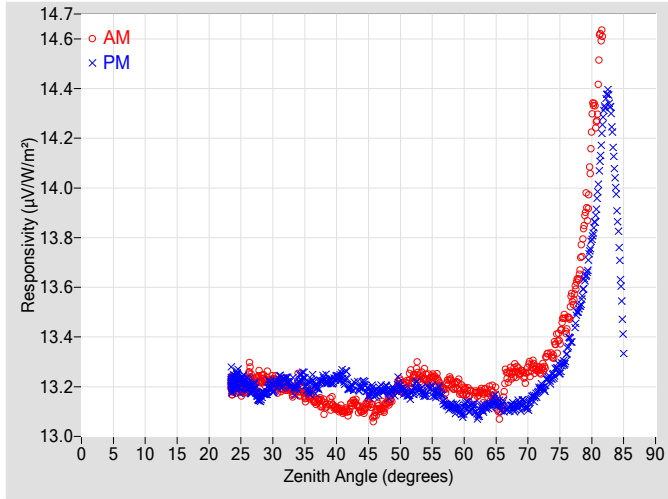


Figure 2. Responsivity vs Local Standard Time

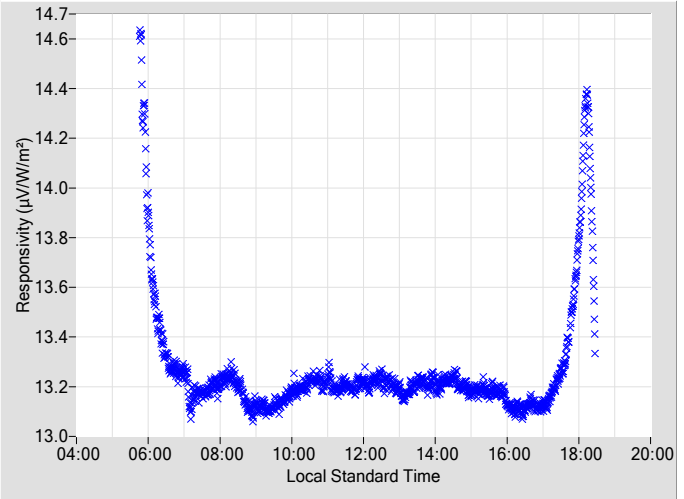


Table 2. Instrument Responsivity (R) and Calibration Type-B Standard Uncertainty, u(B)

| Zenith Angle (deg.) | R ($\mu\text{V}/\text{W}/\text{m}^2$) | u(B) \pm (%) | Azimuth Angle | R ($\mu\text{V}/\text{W}/\text{m}^2$) | u(B) \pm (%) | Azimuth Angle | Zenith Angle (deg.) | R ($\mu\text{V}/\text{W}/\text{m}^2$) | u(B) \pm (%) | Azimuth Angle | R ($\mu\text{V}/\text{W}/\text{m}^2$) | u(B) \pm (%) | Azimuth Angle |
|---------------------|---|----------------|---------------|---|----------------|---------------|---------------------|---|----------------|---------------|---|----------------|---------------|
| 0 | N/A | N/A | N/A | N/A | N/A | N/A | 46 | 13.084 | 0.31 | 106.77 | 13.174 | 0.31 | 252.82 |
| 2 | N/A | N/A | N/A | N/A | N/A | N/A | 48 | 13.138 | 0.33 | 104.55 | 13.190 | 0.33 | 255.04 |
| 4 | N/A | N/A | N/A | N/A | N/A | N/A | 50 | 13.208 | 0.35 | 102.42 | 13.198 | 0.33 | 257.23 |
| 6 | N/A | N/A | N/A | N/A | N/A | N/A | 52 | 13.233 | 0.33 | 100.38 | 13.188 | 0.33 | 259.30 |
| 8 | N/A | N/A | N/A | N/A | N/A | N/A | 54 | 13.237 | 0.34 | 98.46 | 13.175 | 0.34 | 261.22 |
| 10 | N/A | N/A | N/A | N/A | N/A | N/A | 56 | 13.221 | 0.33 | 96.58 | 13.184 | 0.33 | 263.10 |
| 12 | N/A | N/A | N/A | N/A | N/A | N/A | 58 | 13.216 | 0.37 | 94.80 | 13.125 | 0.34 | 264.92 |
| 14 | N/A | N/A | N/A | N/A | N/A | N/A | 60 | 13.181 | 0.34 | 93.05 | 13.109 | 0.34 | 266.67 |
| 16 | N/A | N/A | N/A | N/A | N/A | N/A | 62 | 13.173 | 0.35 | 91.35 | 13.087 | 0.35 | 268.39 |
| 18 | N/A | N/A | N/A | N/A | N/A | N/A | 64 | 13.171 | 0.41 | 89.68 | 13.123 | 0.36 | 270.09 |
| 20 | N/A | N/A | N/A | N/A | N/A | N/A | 66 | 13.138 | 0.43 | 88.03 | 13.120 | 0.38 | 271.72 |
| 22 | N/A | N/A | N/A | N/A | N/A | N/A | 68 | 13.264 | 0.40 | 86.42 | 13.115 | 0.40 | 273.36 |
| 24 | 13.200 | 0.32 | 166.97 | 13.227 | 0.32 | 193.02 | 70 | 13.282 | 0.42 | 84.74 | 13.121 | 0.42 | 274.99 |
| 26 | 13.214 | 0.33 | 150.85 | 13.203 | 0.31 | 209.04 | 72 | 13.266 | 0.45 | 83.19 | 13.198 | 0.45 | 276.60 |
| 28 | 13.237 | 0.29 | 141.03 | 13.153 | 0.31 | 218.08 | 74 | 13.339 | 0.49 | 81.61 | 13.247 | 0.50 | 278.20 |
| 30 | 13.228 | 0.29 | 134.16 | 13.187 | 0.29 | 224.62 | 76 | 13.445 | 0.65 | 79.99 | 13.329 | 0.55 | 279.83 |
| 32 | 13.197 | 0.32 | 129.22 | 13.230 | 0.32 | 229.97 | 78 | 13.657 | 0.61 | 78.39 | 13.516 | N/A | 281.45 |
| 34 | 13.186 | 0.31 | 124.82 | 13.217 | 0.30 | 234.53 | 80 | 14.235 | N/A | 76.75 | 13.792 | N/A | 283.05 |
| 36 | 13.164 | 0.30 | 121.07 | 13.212 | 0.30 | 238.41 | 82 | N/A | N/A | N/A | 14.331 | N/A | 284.74 |
| 38 | 13.123 | 0.31 | 117.65 | 13.230 | 0.31 | 241.83 | 84 | N/A | N/A | N/A | 13.889 | N/A | 286.39 |
| 40 | 13.113 | 0.33 | 114.51 | 13.238 | 0.33 | 245.00 | 86 | N/A | N/A | N/A | N/A | N/A | N/A |
| 42 | 13.105 | 0.30 | 111.82 | 13.193 | 0.32 | 247.81 | 88 | N/A | N/A | N/A | N/A | N/A | N/A |
| 44 | 13.100 | 0.34 | 109.17 | 13.206 | 0.35 | 250.45 | 90 | N/A | N/A | N/A | N/A | N/A | N/A |

N/A - Not Available

Figure 3. Type-B Standard Uncertainty vs Zenith Angle

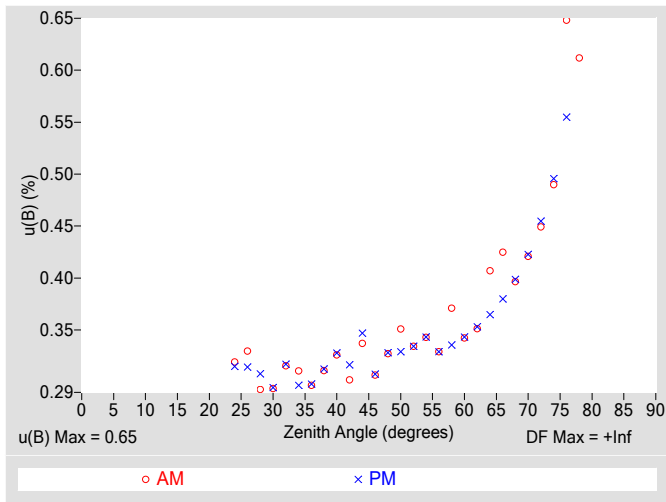


Figure 4. Residuals from Spline Interpolation

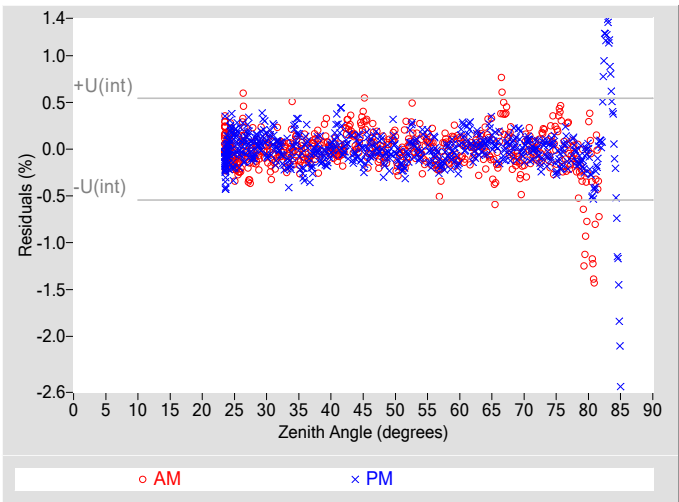


Table 3. Uncertainty using Spline Interpolation ‡

| | |
|---|------------|
| Type-B Standard Uncertainty, $u(B)$ (%) | ± 0.65 |
| Type-A Interpolating Function, $u(int)$ (%) | ± 0.27 |
| Combined Standard Uncertainty, $u(c)$ (%) | ± 0.70 |
| Effective degrees of freedom, $DF(c)$ | 51099 |
| Coverage factor, k | 1.96 |
| Expanded Uncertainty, $U95$ (%) | ± 1.4 |
| AM Valid zenith angle range | 24° to 78° |
| PM Valid zenith angle range | 24° to 76° |

‡ An illustration for how to reduce the uncertainty in calculating the irradiance using a function rather than $R@45^\circ$. Not accredited.

Table 4. Calibration Label Values

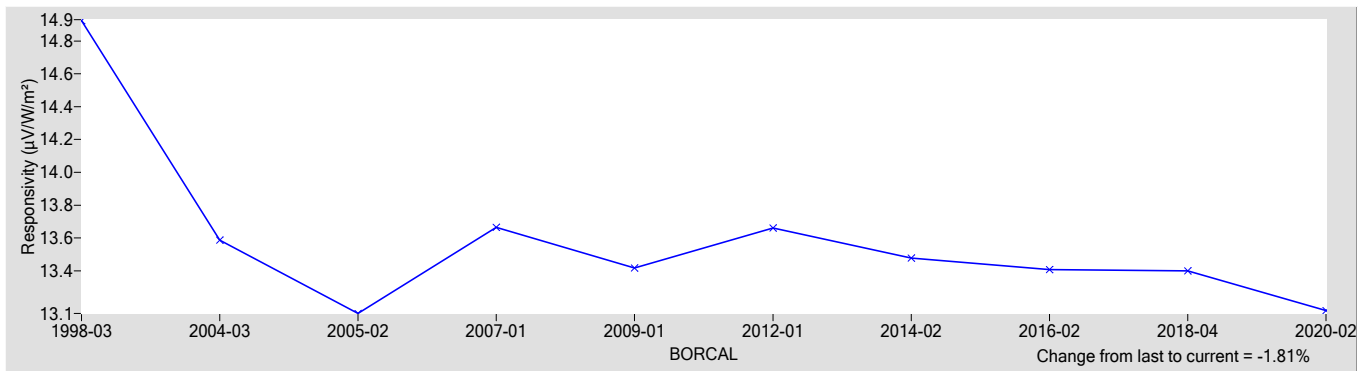
| | |
|----------------------------------|-------------------------------|
| $R @ 45^\circ$ ($\mu V/W/m^2$) | R_{net} ($\mu V/W/m^2$) † |
| 13.157 | 0 |

† R_{net} determination date: N/A

Table 5. Uncertainty using $R @ 45^\circ$

| | |
|---|----------------|
| Type-B Expanded Uncertainty, $U(B)$ (%) | ± 0.73 |
| Offset Uncertainty, $U(off)$ (%) | +0.62 / -0.55 |
| Expanded Uncertainty, U (%) | +1.3 / -1.3 |
| Effective degrees of freedom, DF | +Inf |
| Coverage factor, k | 1.96 |
| Valid zenith angle range | 30.0° to 60.0° |

Figure 5. History of instrument at Zenith Angle = 45°



References:

[1] Reda, I.; Hickey, J.; Long, C.; Myers, D.; Stoffel, T.; Wilcox, S.; Michalsky, J. J.; Dutton, E. G.; Nelson, D. (2005). "Using a Blackbody to Calculate Net Longwave Responsivity of Shortwave Solar Pyranometers to Correct for Their Thermal Offset Error During Outdoor Calibration Using the Component Sum Method." *Journal of Atmospheric and Oceanic Technology*, 2005; pp. 1531-1540; NREL Report No. JA-560-36646. doi:10.1175/JTECH1782.1

[2] Reda, I.; Myers, D.; Stoffel, T. (2008). "Uncertainty Estimate for the Outdoor Calibration of Solar Pyranometers: A Metrologist Perspective." *Measure*. (NCSLI Journal of Measurement Science). Vol. 3(4), December 2008; pp. 58-66; NREL Report No. JA-581-4137

[3] Reda, I.; Andreas, A. (2004). "Solar Position Algorithm for Solar Radiation Applications." *Solar Energy*. Vol. 76(5), 2004; pp. 577-589; NREL Report No. JA-560-35518. doi:10.1016/j.solener.2003.12.003

[4] Stoffel, T.; Reda, I. (2009). "NREL Pyrheliometer Comparisons: 22 September - 3 October 2008 (NPC-2008)." 54 pp.; NREL Report No. TP-550-45016.

[5] Reda, I.; Stoffel, T.; Myers, D. (2003). "Method to Calibrate a Solar Pyranometer for Measuring Reference Diffuse Irradiance." *Solar Energy*. Vol. 74, 2003; pp. 103-112; NREL Report No. JA-560-35025. doi:10.1016/S0038-092X(03)00124-5

[6] Reda, I. (1996). Calibration of a Solar Absolute Cavity Radiometer with Traceability to the World Radiometric Reference. 79 pp.; NREL Report No. TP-463-20619.

[7] Reda, I.; Gröbner, J.; Stoffel, T.; Myers, D.; Forgan, B. (2008). Improvements in the Blackbody Calibration of Pyrgeometers. ARM 2008 Science Team Meeting (Poster).



National Renewable Energy Laboratory

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Calibration Certificate



| | | | |
|--------------------------|---------------------|----------------------------------|------------|
| Test Instrument: | Silicon Pyranometer | Manufacturer: | Licor |
| Model: | LI200 | Serial Number: | PY28257 |
| Calibration Date: | 5/5/2020 | Due Date: | 5/5/2021 |
| Customer: | NREL-SRRL-BMS | Environmental Conditions: | see page 4 |
| Test Dates: | 5/4-5 | | |

This certifies that the above product was calibrated in compliance with ISO/IEC 17025:2017. Measurement uncertainties at the time of calibration are consistent with the Guide to the Expression of Uncertainty in Measurement (GUM) using Reda et al., 2008. All nominal values are traceable to the International System (SI) Units of Measurement.

No statement of compliance with specifications is made or implied on this certificate. However, the estimated uncertainties are the uncertainties of the calibration process; users must add other uncertainties that are relevant to their measuring system, environmental and sky conditions, outdoor set-up, and site location.

The Type-B Standard Uncertainty of using the responsivity at each even zenith angle is reported, and the Expanded Uncertainty of the calibration is reported using two methods:

1. The Expanded Uncertainty of using the responsivity at zenith angle = 45°, within the zenith angle range from 30.0° to 60.0°
2. The Expanded Uncertainty of using Spline Interpolating Functions for the responsivity versus zenith angle.

This certificate applies only to the item identified above and shall not be reproduced other than in full, without specific written approval from the calibration facility. Certificate without signature is not valid.

Table 1. Traceability

| Measurement Type | Instrument | Calibration Date | Calibration Due Date |
|----------------------|--|------------------|----------------------|
| Beam Irradiance † | Eppley Absolute Cavity Radiometer Model HF, S/N 29219 | 09/27/2019 | 09/27/2020 |
| Diffuse Irradiance † | Hukseflux Pyranometer Model SR25, S/N 2541 | 04/17/2020 | 04/17/2021 |
| Diffuse Irradiance † | Hukseflux Pyranometer Model SR25, S/N 2542 | 04/17/2020 | 04/17/2021 |
| Data Acquisition | NREL Data Acquisition System Model RAP-DAQ, S/N 2005-998 | 02/14/2019 | 02/14/2021 |
| Data Acquisition | NREL Data Acquisition System Model RAP-DAQ, S/N 2005-999 | 02/14/2019 | 02/14/2021 |

† Through the World Radiometric Reference (WRR)

Number of pages of certificate: 4

Calibration Procedure: BORCAL-P00-Calibration and QA Procedure; available upon request.

Setup: Radiometers are calibrated outdoors, using the sun as the source. Pyranometers and pyrgeometers are installed for horizontal measurements, with their signal connectors oriented north, if their design permits.

The shading disk for the reference diffuse subtends a solid angle of 5°. Pyrhemometers are installed on solar trackers.

Calibrated by: Afshin Andreas, Ibrahim Reda, Peter Gotseff, and RCC

Ibrahim Reda, Technical Manager

Date

For questions or comments, please contact the technical manager at:

ibrahim.reda@nrel.gov; 303-384-6385; 15013 Denver West Parkway, Golden, CO 80401, USA

Calibration Results

PY28257 Licor LI200

The responsivity (R , $\mu\text{V}/\text{W}/\text{m}^2$) of the test instrument during calibration is calculated using this Measurement Equation:

$$R = (V - R_{net} * W_{net}) / I \quad [1]$$

where,

- V = radiometer output voltage (microvolts),
 - R_{net} = radiometer net infrared responsivity ($\mu\text{V}/\text{W}/\text{m}^2$), see Table 4,
 - W_{net} = effective net infrared measured by pyrgeometer (W/m^2),
 - = $W_{in} - W_{out} = W_{in} - \sigma * T_c^4$
 - where, W_{in} = incoming infrared (W/m^2), $\sigma = 5.6704\text{e-}8 \text{ W}\cdot\text{m}^{-2}\cdot\text{K}^{-4}$,
 - T_c = case temperature of pyrgeometer (K).
- I = reference irradiance (W/m^2), beam (B) or global (G)
 where, $G = B * \text{COS}(Z) + D$,
 Z = zenith angle (degrees),
 D = reference diffuse irradiance (W/m^2).

Figure 1. Responsivity vs Zenith Angle

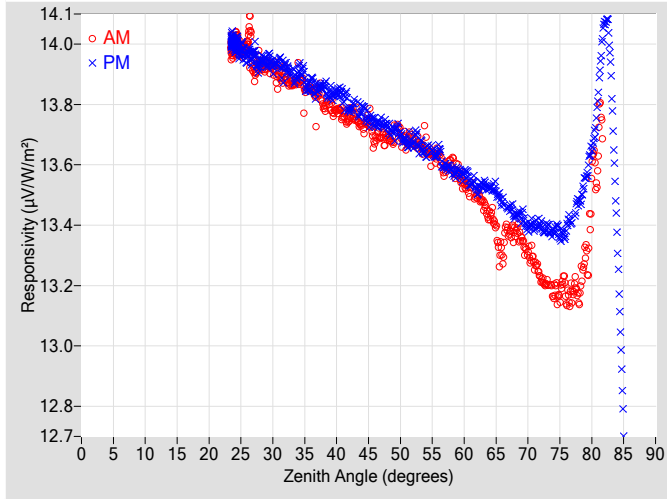


Figure 2. Responsivity vs Local Standard Time

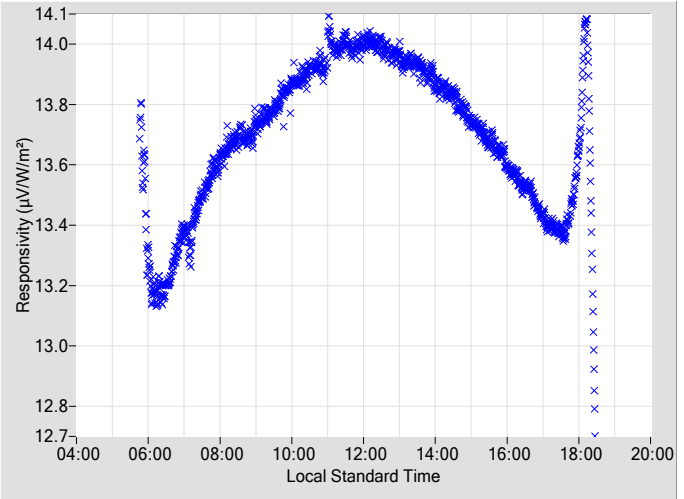


Table 2. Instrument Responsivity (R) and Calibration Type-B Standard Uncertainty, u(B)

| Zenith Angle (deg.) | R ($\mu\text{V}/\text{W}/\text{m}^2$) | u(B) \pm (%) | Azimuth Angle | R ($\mu\text{V}/\text{W}/\text{m}^2$) | u(B) \pm (%) | Azimuth Angle | Zenith Angle (deg.) | R ($\mu\text{V}/\text{W}/\text{m}^2$) | u(B) \pm (%) | Azimuth Angle | R ($\mu\text{V}/\text{W}/\text{m}^2$) | u(B) \pm (%) | Azimuth Angle |
|---------------------|---|----------------|---------------|---|----------------|---------------|---------------------|---|----------------|---------------|---|----------------|---------------|
| 0 | N/A | N/A | N/A | N/A | N/A | N/A | 46 | 13.678 | 0.31 | 106.77 | 13.740 | 0.31 | 252.82 |
| 2 | N/A | N/A | N/A | N/A | N/A | N/A | 48 | 13.695 | 0.33 | 104.55 | 13.728 | 0.33 | 255.08 |
| 4 | N/A | N/A | N/A | N/A | N/A | N/A | 50 | 13.698 | 0.35 | 102.42 | 13.697 | 0.33 | 257.23 |
| 6 | N/A | N/A | N/A | N/A | N/A | N/A | 52 | 13.676 | 0.33 | 100.38 | 13.677 | 0.33 | 259.30 |
| 8 | N/A | N/A | N/A | N/A | N/A | N/A | 54 | 13.671 | 0.34 | 98.46 | 13.642 | 0.34 | 261.22 |
| 10 | N/A | N/A | N/A | N/A | N/A | N/A | 56 | 13.633 | 0.33 | 96.58 | 13.649 | 0.33 | 263.10 |
| 12 | N/A | N/A | N/A | N/A | N/A | N/A | 58 | 13.610 | 0.37 | 94.80 | 13.585 | 0.34 | 264.92 |
| 14 | N/A | N/A | N/A | N/A | N/A | N/A | 60 | 13.532 | 0.34 | 93.05 | 13.570 | 0.34 | 266.67 |
| 16 | N/A | N/A | N/A | N/A | N/A | N/A | 62 | 13.502 | 0.35 | 91.35 | 13.517 | 0.35 | 268.39 |
| 18 | N/A | N/A | N/A | N/A | N/A | N/A | 64 | 13.431 | 0.41 | 89.68 | 13.523 | 0.36 | 270.09 |
| 20 | N/A | N/A | N/A | N/A | N/A | N/A | 66 | 13.313 | 0.42 | 88.03 | 13.475 | 0.38 | 271.72 |
| 22 | N/A | N/A | N/A | N/A | N/A | N/A | 68 | 13.375 | 0.40 | 86.42 | 13.429 | 0.40 | 273.36 |
| 24 | 13.996 | 0.32 | 166.97 | 14.001 | 0.31 | 193.02 | 70 | 13.309 | 0.42 | 84.74 | 13.393 | 0.42 | 274.99 |
| 26 | 14.008 | 0.33 | 150.85 | 13.963 | 0.31 | 209.04 | 72 | 13.221 | 0.45 | 83.19 | 13.400 | 0.45 | 276.60 |
| 28 | 13.945 | 0.29 | 141.03 | 13.936 | 0.31 | 218.08 | 74 | 13.176 | 0.49 | 81.61 | 13.378 | 0.50 | 278.20 |
| 30 | 13.923 | 0.29 | 134.16 | 13.928 | 0.29 | 224.62 | 76 | 13.166 | 0.65 | 79.99 | 13.387 | 0.55 | 279.83 |
| 32 | 13.892 | 0.32 | 129.22 | 13.926 | 0.32 | 229.97 | 78 | 13.166 | 0.61 | 78.39 | 13.478 | N/A | 281.45 |
| 34 | 13.887 | 0.31 | 124.84 | 13.911 | 0.30 | 234.53 | 80 | 13.543 | N/A | 76.75 | 13.654 | N/A | 283.05 |
| 36 | 13.849 | 0.30 | 121.07 | 13.872 | 0.30 | 238.41 | 82 | N/A | N/A | N/A | 14.069 | N/A | 284.74 |
| 38 | 13.793 | 0.31 | 117.65 | 13.861 | 0.31 | 241.83 | 84 | N/A | N/A | N/A | 13.338 | N/A | 286.39 |
| 40 | 13.781 | 0.33 | 114.51 | 13.842 | 0.33 | 245.00 | 86 | N/A | N/A | N/A | N/A | N/A | N/A |
| 42 | 13.756 | 0.30 | 111.82 | 13.781 | 0.32 | 247.81 | 88 | N/A | N/A | N/A | N/A | N/A | N/A |
| 44 | 13.724 | 0.34 | 109.17 | 13.786 | 0.35 | 250.45 | 90 | N/A | N/A | N/A | N/A | N/A | N/A |

N/A - Not Available

Figure 3. Type-B Standard Uncertainty vs Zenith Angle

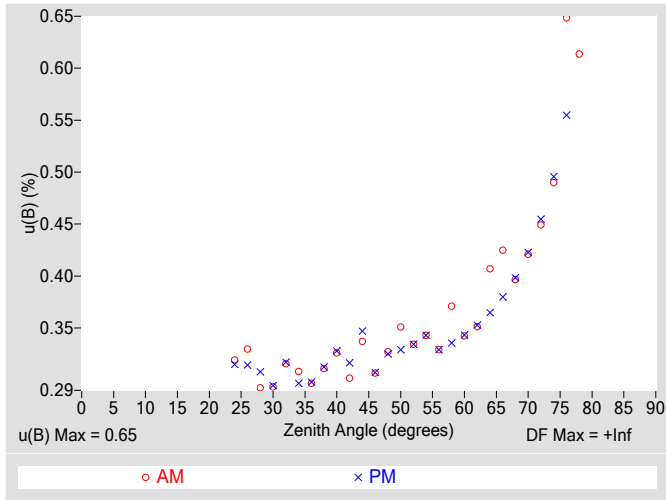


Figure 4. Residuals from Spline Interpolation

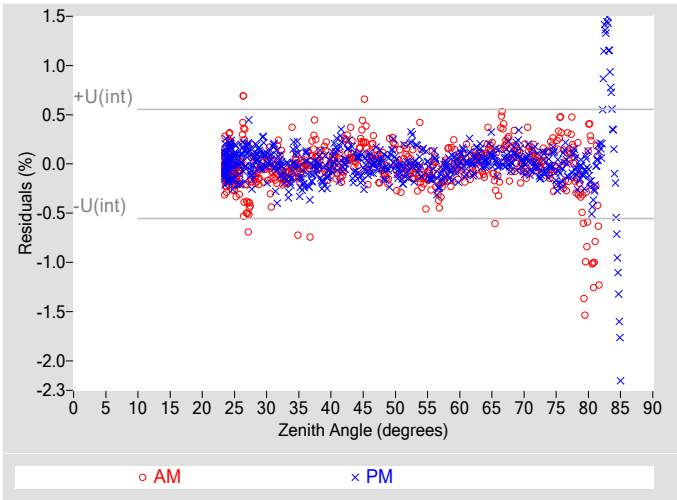


Table 3. Uncertainty using Spline Interpolation ‡

| | |
|---|------------|
| Type-B Standard Uncertainty, $u(B)$ (%) | ± 0.65 |
| Type-A Interpolating Function, $u(int)$ (%) | ± 0.28 |
| Combined Standard Uncertainty, $u(c)$ (%) | ± 0.70 |
| Effective degrees of freedom, $DF(c)$ | 48327 |
| Coverage factor, k | 1.96 |
| Expanded Uncertainty, U_{95} (%) | ± 1.4 |
| AM Valid zenith angle range | 24° to 78° |
| PM Valid zenith angle range | 24° to 76° |

‡ An illustration for how to reduce the uncertainty in calculating the irradiance using a function rather than $R@45^\circ$. Not accredited.

Table 4. Calibration Label Values

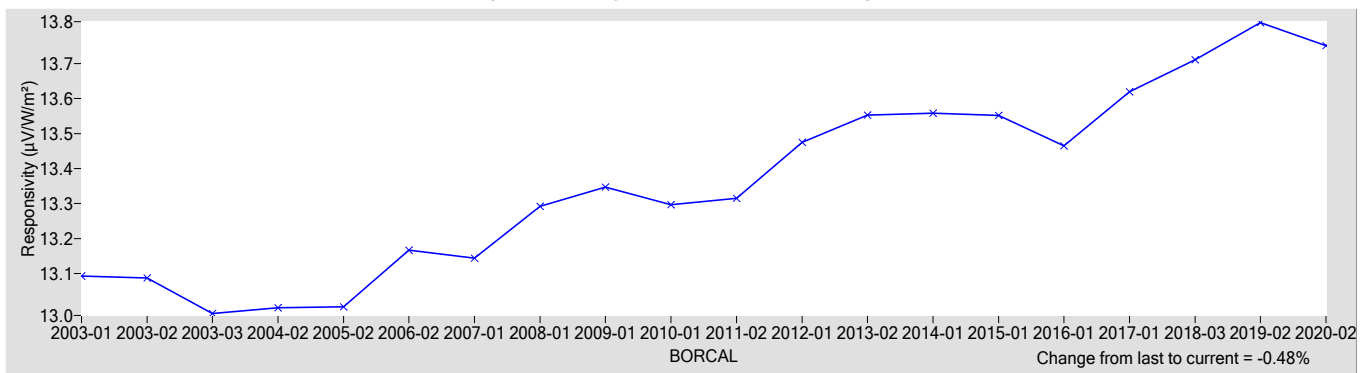
| | |
|----------------------------------|-------------------------------|
| $R @ 45^\circ$ ($\mu V/W/m^2$) | R_{net} ($\mu V/W/m^2$) † |
| 13.751 | 0 |

† R_{net} determination date: N/A

Table 5. Uncertainty using $R @ 45^\circ$

| | |
|---|----------------|
| Type-B Expanded Uncertainty, $U(B)$ (%) | ± 0.73 |
| Offset Uncertainty, $U(off)$ (%) | +1.3 / -1.6 |
| Expanded Uncertainty, U (%) | +2.0 / -2.3 |
| Effective degrees of freedom, DF | +Inf |
| Coverage factor, k | 1.96 |
| Valid zenith angle range | 30.0° to 60.0° |

Figure 5. History of instrument at Zenith Angle = 45°



References:

- [1] Reda, I.; Hickey, J.; Long, C.; Myers, D.; Stoffel, T.; Wilcox, S.; Michalsky, J. J.; Dutton, E. G.; Nelson, D. (2005). "Using a Blackbody to Calculate Net Longwave Responsivity of Shortwave Solar Pyranometers to Correct for Their Thermal Offset Error During Outdoor Calibration Using the Component Sum Method." *Journal of Atmospheric and Oceanic Technology*, 2005; pp. 1531-1540; NREL Report No. JA-560-36646. doi:10.1175/JTECH1782.1
- [2] Reda, I.; Myers, D.; Stoffel, T. (2008). "Uncertainty Estimate for the Outdoor Calibration of Solar Pyranometers: A Metrologist Perspective." *Measure*. (NCSLI Journal of Measurement Science). Vol. 3(4), December 2008; pp. 58-66; NREL Report No. JA-581-4137
- [3] Reda, I.; Andreas, A. (2004). "Solar Position Algorithm for Solar Radiation Applications." *Solar Energy*. Vol. 76(5), 2004; pp. 577-589; NREL Report No. JA-560-35518. doi:10.1016/j.solener.2003.12.003
- [4] Stoffel, T.; Reda, I. (2009). "NREL Pyrheliometer Comparisons: 22 September - 3 October 2008 (NPC-2008)." 54 pp.; NREL Report No. TP-550-45016.
- [5] Reda, I.; Stoffel, T.; Myers, D. (2003). "Method to Calibrate a Solar Pyranometer for Measuring Reference Diffuse Irradiance." *Solar Energy*. Vol. 74, 2003; pp. 103-112; NREL Report No. JA-560-35025. doi:10.1016/S0038-092X(03)00124-5
- [6] Reda, I. (1996). Calibration of a Solar Absolute Cavity Radiometer with Traceability to the World Radiometric Reference. 79 pp.; NREL Report No. TP-463-20619.
- [7] Reda, I.; Gröbner, J.; Stoffel, T.; Myers, D.; Forgan, B. (2008). Improvements in the Blackbody Calibration of Pyrgometers. ARM 2008 Science Team Meeting (Poster).



National Renewable Energy Laboratory

Solar Radiation Research Laboratory

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Calibration Certificate



| | | | |
|--------------------------|-----------------------------|----------------------------------|------------|
| Test Instrument: | Semiconductor Pyrheliometer | Manufacturer: | Licor |
| Model: | LI201SB | Serial Number: | PYHR101 |
| Calibration Date: | 5/5/2020 | Due Date: | 5/5/2021 |
| Customer: | NREL-SRRL-BMS | Environmental Conditions: | see page 4 |
| Test Dates: | 5/4-5 | | |

This certifies that the above product was calibrated in compliance with ISO/IEC 17025:2017. Measurement uncertainties at the time of calibration are consistent with the Guide to the Expression of Uncertainty in Measurement (GUM) using Reda et al., 2008. All nominal values are traceable to the International System (SI) Units of Measurement.

No statement of compliance with specifications is made or implied on this certificate. However, the estimated uncertainties are the uncertainties of the calibration process; users must add other uncertainties that are relevant to their measuring system, environmental and sky conditions, outdoor set-up, and site location.

The Type-B Standard Uncertainty of using the responsivity at each even zenith angle is reported, and the Expanded Uncertainty of the calibration is reported using two methods:

1. The Expanded Uncertainty of using the responsivity at zenith angle = 45°, within the zenith angle range from 30.0° to 60.0°
2. The Expanded Uncertainty of using Spline Interpolating Functions for the responsivity versus zenith angle.

This certificate applies only to the item identified above and shall not be reproduced other than in full, without specific written approval from the calibration facility. Certificate without signature is not valid.

Table 1. Traceability

| Measurement Type | Instrument | Calibration Date | Calibration Due Date |
|----------------------|--|------------------|----------------------|
| Beam Irradiance † | Eppley Absolute Cavity Radiometer Model HF, S/N 29219 | 09/27/2019 | 09/27/2020 |
| Diffuse Irradiance † | Hukseflux Pyranometer Model SR25, S/N 2541 | 04/17/2020 | 04/17/2021 |
| Diffuse Irradiance † | Hukseflux Pyranometer Model SR25, S/N 2542 | 04/17/2020 | 04/17/2021 |
| Data Acquisition | NREL Data Acquisition System Model RAP-DAQ, S/N 2005-998 | 02/14/2019 | 02/14/2021 |
| Data Acquisition | NREL Data Acquisition System Model RAP-DAQ, S/N 2005-999 | 02/14/2019 | 02/14/2021 |

† Through the World Radiometric Reference (WRR)

Number of pages of certificate: 4

Calibration Procedure: BORCAL-P00-Calibration and QA Procedure; available upon request.

Setup: Radiometers are calibrated outdoors, using the sun as the source. Pyranometers and pyrgeometers are installed for horizontal measurements, with their signal connectors oriented north, if their design permits.

The shading disk for the reference diffuse subtends a solid angle of 5°. Pyrheliometers are installed on solar trackers.

Calibrated by: Afshin Andreas, Ibrahim Reda, Peter Gotseff, and RCC

Ibrahim Reda, Technical Manager

Date

For questions or comments, please contact the technical manager at:

ibrahim.reda@nrel.gov; 303-384-6385; 15013 Denver West Parkway, Golden, CO 80401, USA

Calibration Results

PYHR101 Licor LI201SB

The responsivity (R , $\mu\text{V}/\text{W}/\text{m}^2$) of the test instrument during calibration is calculated using this Measurement Equation:

$$R = (V - R_{net} * W_{net}) / I \tag{1}$$

where,

- V = radiometer output voltage (microvolts),
 - R_{net} = radiometer net infrared responsivity ($\mu\text{V}/\text{W}/\text{m}^2$), see Table 4,
 - W_{net} = effective net infrared measured by pyrgeometer (W/m^2),
 - = $W_{in} - W_{out} = W_{in} - \sigma * T_c^4$
 - where, W_{in} = incoming infrared (W/m^2), $\sigma = 5.6704\text{e-}8 \text{ W}\cdot\text{m}^{-2}\cdot\text{K}^{-4}$,
 - T_c = case temperature of pyrgeometer (K).
- I = reference irradiance (W/m^2), beam (B) or global (G)
 - where, $G = B * \text{COS}(Z) + D$,
 - Z = zenith angle (degrees),
 - D = reference diffuse irradiance (W/m^2).

Figure 1. Responsivity vs Zenith Angle

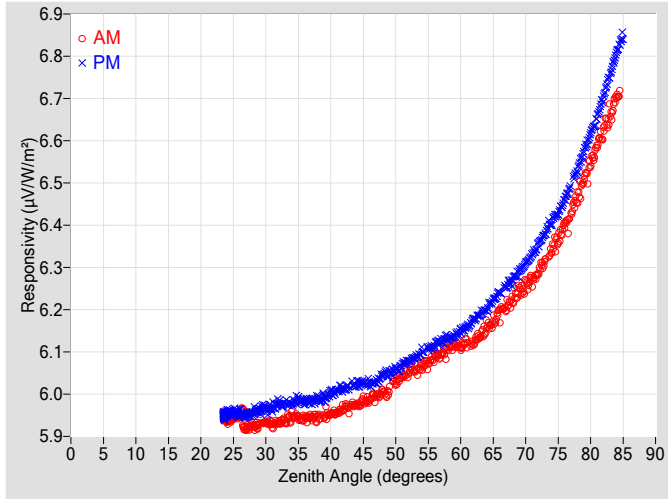


Figure 2. Responsivity vs Local Standard Time

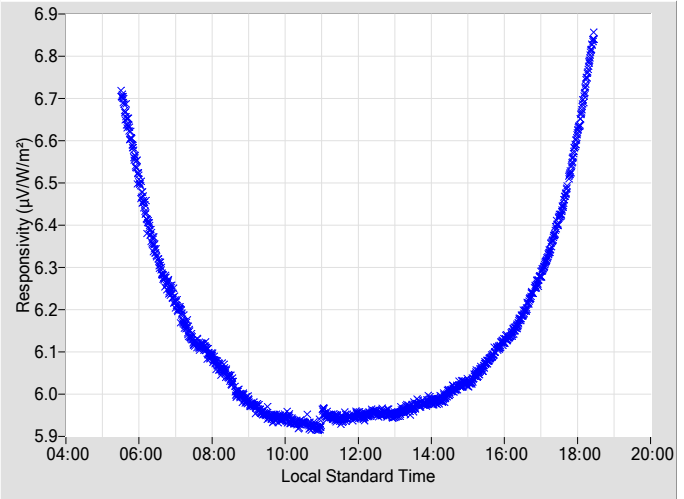


Table 2. Instrument Responsivity (R) and Calibration Type-B Standard Uncertainty, u(B)

| Zenith Angle (deg.) | R ($\mu\text{V}/\text{W}/\text{m}^2$) | u(B) \pm (%) | Azimuth Angle | R ($\mu\text{V}/\text{W}/\text{m}^2$) | u(B) \pm (%) | Azimuth Angle | Zenith Angle (deg.) | R ($\mu\text{V}/\text{W}/\text{m}^2$) | u(B) \pm (%) | Azimuth Angle | R ($\mu\text{V}/\text{W}/\text{m}^2$) | u(B) \pm (%) | Azimuth Angle |
|---------------------|---|----------------|---------------|---|----------------|---------------|---------------------|---|----------------|---------------|---|----------------|---------------|
| 0 | N/A | N/A | N/A | N/A | N/A | N/A | 46 | 5.9852 | 0.29 | 106.77 | 6.0261 | 0.29 | 252.82 |
| 2 | N/A | N/A | N/A | N/A | N/A | N/A | 48 | 6.0071 | 0.29 | 104.55 | 6.0459 | 0.31 | 255.08 |
| 4 | N/A | N/A | N/A | N/A | N/A | N/A | 50 | 6.0272 | 0.33 | 102.42 | 6.0605 | 0.31 | 257.24 |
| 6 | N/A | N/A | N/A | N/A | N/A | N/A | 52 | 6.0519 | 0.31 | 100.38 | 6.0779 | 0.29 | 259.30 |
| 8 | N/A | N/A | N/A | N/A | N/A | N/A | 54 | 6.0661 | 0.31 | 98.46 | 6.0994 | 0.31 | 261.23 |
| 10 | N/A | N/A | N/A | N/A | N/A | N/A | 56 | 6.0874 | 0.31 | 96.59 | 6.1171 | 0.30 | 263.11 |
| 12 | N/A | N/A | N/A | N/A | N/A | N/A | 58 | 6.1064 | 0.32 | 94.80 | 6.1316 | 0.30 | 264.92 |
| 14 | N/A | N/A | N/A | N/A | N/A | N/A | 60 | 6.1101 | 0.31 | 93.06 | 6.1502 | 0.30 | 266.68 |
| 16 | N/A | N/A | N/A | N/A | N/A | N/A | 62 | 6.1214 | 0.30 | 91.35 | 6.1773 | 0.30 | 268.40 |
| 18 | N/A | N/A | N/A | N/A | N/A | N/A | 64 | 6.1579 | 0.32 | 89.68 | 6.2000 | 0.30 | 270.10 |
| 20 | N/A | N/A | N/A | N/A | N/A | N/A | 66 | 6.1939 | 0.31 | 88.04 | 6.2402 | 0.30 | 271.72 |
| 22 | N/A | N/A | N/A | N/A | N/A | N/A | 68 | 6.2235 | 0.30 | 86.42 | 6.2709 | 0.30 | 273.36 |
| 24 | 5.9419 | 0.31 | 167.11 | 5.9538 | 0.31 | 192.94 | 70 | 6.2605 | 0.32 | 84.78 | 6.3105 | 0.30 | 274.99 |
| 26 | 5.9537 | 0.31 | 150.89 | 5.9542 | 0.30 | 208.97 | 72 | 6.2889 | 0.31 | 83.19 | 6.3581 | 0.31 | 276.60 |
| 28 | 5.9260 | 0.31 | 140.89 | 5.9543 | 0.31 | 217.98 | 74 | 6.3400 | 0.31 | 81.61 | 6.4064 | 0.32 | 278.20 |
| 30 | 5.9325 | 0.29 | 134.31 | 5.9650 | 0.30 | 224.74 | 76 | 6.4027 | 0.31 | 80.00 | 6.4621 | 0.31 | 279.80 |
| 32 | 5.9318 | 0.29 | 129.22 | 5.9795 | 0.31 | 229.97 | 78 | 6.4661 | 0.32 | 78.39 | 6.5337 | N/A | 281.45 |
| 34 | 5.9433 | 0.31 | 124.84 | 5.9768 | 0.29 | 234.53 | 80 | 6.5480 | N/A | 76.75 | 6.6185 | N/A | 283.05 |
| 36 | 5.9449 | 0.31 | 121.01 | 5.9826 | 0.31 | 238.41 | 82 | 6.6247 | N/A | 75.09 | 6.7073 | N/A | 284.74 |
| 38 | 5.9423 | 0.30 | 117.66 | 5.9897 | 0.30 | 241.83 | 84 | 6.7022 | N/A | 73.42 | 6.8091 | N/A | 286.39 |
| 40 | 5.9522 | 0.32 | 114.51 | 6.0040 | 0.31 | 245.01 | 86 | N/A | N/A | N/A | N/A | N/A | N/A |
| 42 | 5.9661 | 0.29 | 111.82 | 6.0118 | 0.29 | 247.82 | 88 | N/A | N/A | N/A | N/A | N/A | N/A |
| 44 | 5.9753 | 0.31 | 109.16 | 6.0236 | 0.29 | 250.46 | 90 | N/A | N/A | N/A | N/A | N/A | N/A |

N/A - Not Available

Figure 3. Type-B Standard Uncertainty vs Zenith Angle

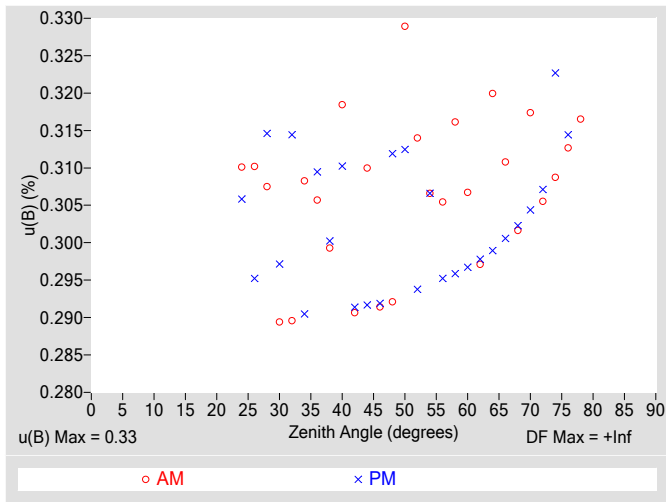


Figure 4. Residuals from Spline Interpolation

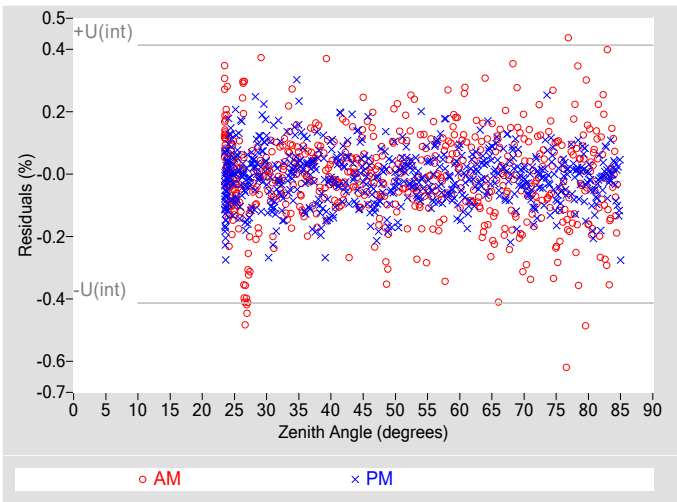


Table 3. Uncertainty using Spline Interpolation ‡

| | |
|---|------------|
| Type-B Standard Uncertainty, $u(B)$ (%) | ± 0.33 |
| Type-A Interpolating Function, $u(int)$ (%) | ± 0.21 |
| Combined Standard Uncertainty, $u(c)$ (%) | ± 0.39 |
| Effective degrees of freedom, $DF(c)$ | 14290 |
| Coverage factor, k | 1.96 |
| Expanded Uncertainty, U_{95} (%) | ± 0.76 |
| AM Valid zenith angle range | 24° to 78° |
| PM Valid zenith angle range | 24° to 76° |

‡ An illustration for how to reduce the uncertainty in calculating the irradiance using a function rather than $R@45^\circ$. Not accredited.

Table 4. Calibration Label Values

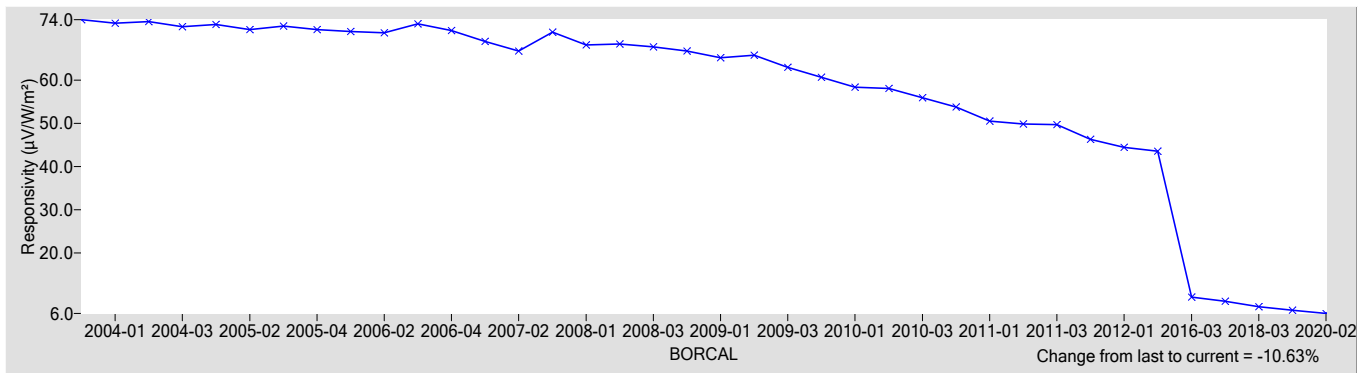
| | |
|----------------------------------|-------------------------------|
| $R @ 45^\circ$ ($\mu V/W/m^2$) | R_{net} ($\mu V/W/m^2$) † |
| 6.0067 | 0 |

† R_{net} determination date: N/A

Table 5. Uncertainty using $R @ 45^\circ$

| | |
|---|----------------|
| Type-B Expanded Uncertainty, $U(B)$ (%) | ± 0.64 |
| Offset Uncertainty, $U(off)$ (%) | +2.4 / -1.2 |
| Expanded Uncertainty, U (%) | +3.0 / -1.9 |
| Effective degrees of freedom, DF | +Inf |
| Coverage factor, k | 1.96 |
| Valid zenith angle range | 30.0° to 60.0° |

Figure 5. History of instrument at Zenith Angle = 45°



References:

[1] Reda, I.; Hickey, J.; Long, C.; Myers, D.; Stoffel, T.; Wilcox, S.; Michalsky, J. J.; Dutton, E. G.; Nelson, D. (2005). "Using a Blackbody to Calculate Net Longwave Responsivity of Shortwave Solar Pyranometers to Correct for Their Thermal Offset Error During Outdoor Calibration Using the Component Sum Method." *Journal of Atmospheric and Oceanic Technology*, 2005; pp. 1531-1540; NREL Report No. JA-560-36646. doi:10.1175/JTECH1782.1

[2] Reda, I.; Myers, D.; Stoffel, T. (2008). "Uncertainty Estimate for the Outdoor Calibration of Solar Pyranometers: A Metrologist Perspective." *Measure*. (NCSLI *Journal of Measurement Science*). Vol. 3(4), December 2008; pp. 58-66; NREL Report No. JA-581-4137

[3] Reda, I.; Andreas, A. (2004). "Solar Position Algorithm for Solar Radiation Applications." *Solar Energy*. Vol. 76(5), 2004; pp. 577-589; NREL Report No. JA-560-35518. doi:10.1016/j.solener.2003.12.003

[4] Stoffel, T.; Reda, I. (2009). "NREL Pyrheliometer Comparisons: 22 September - 3 October 2008 (NPC-2008)." 54 pp.; NREL Report No. TP-550-45016.

[5] Reda, I.; Stoffel, T.; Myers, D. (2003). "Method to Calibrate a Solar Pyranometer for Measuring Reference Diffuse Irradiance." *Solar Energy*. Vol. 74, 2003; pp. 103-112; NREL Report No. JA-560-35025. doi:10.1016/S0038-092X(03)00124-5

[6] Reda, I. (1996). *Calibration of a Solar Absolute Cavity Radiometer with Traceability to the World Radiometric Reference*. 79 pp.; NREL Report No. TP-463-20619.

[7] Reda, I.; Gröbner, J.; Stoffel, T.; Myers, D.; Forgan, B. (2008). *Improvements in the Blackbody Calibration of Pyrgometers*. ARM 2008 Science Team Meeting (Poster).



National Renewable Energy Laboratory

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Calibration Certificate



| | | | |
|--------------------------|---------------|----------------------------------|------------|
| Test Instrument: | Pyranometer | Manufacturer: | EKO |
| Model: | MS-602 | Serial Number: | S13071483 |
| Calibration Date: | 5/5/2020 | Due Date: | 5/5/2021 |
| Customer: | NREL-SRRL-BMS | Environmental Conditions: | see page 4 |
| Test Dates: | 5/4-5 | | |

This certifies that the above product was calibrated in compliance with ISO/IEC 17025:2017. Measurement uncertainties at the time of calibration are consistent with the Guide to the Expression of Uncertainty in Measurement (GUM) using Reda et al., 2008. All nominal values are traceable to the International System (SI) Units of Measurement.

No statement of compliance with specifications is made or implied on this certificate. However, the estimated uncertainties are the uncertainties of the calibration process; users must add other uncertainties that are relevant to their measuring system, environmental and sky conditions, outdoor set-up, and site location.

The Type-B Standard Uncertainty of using the responsivity at each even zenith angle is reported, and the Expanded Uncertainty of the calibration is reported using two methods:

1. The Expanded Uncertainty of using the responsivity at zenith angle = 45°, within the zenith angle range from 30.0° to 60.0°
2. The Expanded Uncertainty of using Spline Interpolating Functions for the responsivity versus zenith angle.

This certificate applies only to the item identified above and shall not be reproduced other than in full, without specific written approval from the calibration facility. Certificate without signature is not valid.

Table 1. Traceability

| Measurement Type | Instrument | Calibration Date | Calibration Due Date |
|-----------------------|--|------------------|----------------------|
| Beam Irradiance † | Eppley Absolute Cavity Radiometer Model HF, S/N 29219 | 09/27/2019 | 09/27/2020 |
| Diffuse Irradiance † | Hukseflux Pyranometer Model SR25, S/N 2541 | 04/17/2020 | 04/17/2021 |
| Diffuse Irradiance † | Hukseflux Pyranometer Model SR25, S/N 2542 | 04/17/2020 | 04/17/2021 |
| Data Acquisition | NREL Data Acquisition System Model RAP-DAQ, S/N 2005-998 | 02/14/2019 | 02/14/2021 |
| Data Acquisition | NREL Data Acquisition System Model RAP-DAQ, S/N 2005-999 | 02/14/2019 | 02/14/2021 |
| Infrared Irradiance ‡ | Kipp & Zonen Pyrgeometer Model CG4, S/N FT002 | 04/16/2018 | 04/16/2022 |

† Through the World Radiometric Reference (WRR)

‡ Through the World Infrared Standard Group (WISG)

Number of pages of certificate: 4

Calibration Procedure: BORCAL-P00-Calibration and QA Procedure; available upon request.

Setup: Radiometers are calibrated outdoors, using the sun as the source. Pyranometers and pyrgeometers are installed for horizontal measurements, with their signal connectors oriented north, if their design permits.

The shading disk for the reference diffuse subtends a solid angle of 5°. Pyrheliometers are installed on solar trackers.

Calibrated by: Afshin Andreas, Ibrahim Reda, Peter Gotseff, and RCC

Ibrahim Reda, Technical Manager

Date

For questions or comments, please contact the technical manager at:

ibrahim.reda@nrel.gov; 303-384-6385; 15013 Denver West Parkway, Golden, CO 80401, USA

Calibration Results

S13071483 EKO MS-602

The responsivity (R , $\mu\text{V}/\text{W}/\text{m}^2$) of the test instrument during calibration is calculated using this Measurement Equation:

$$R = (V - R_{net} * W_{net}) / I \quad [1]$$

where,

- V = radiometer output voltage (microvolts),
 - R_{net} = radiometer net infrared responsivity ($\mu\text{V}/\text{W}/\text{m}^2$), see Table 4,
 - W_{net} = effective net infrared measured by pyrgeometer (W/m^2),
 - = $W_{in} - W_{out} = W_{in} - \sigma * T_c^4$
 - where, W_{in} = incoming infrared (W/m^2), $\sigma = 5.6704\text{e-}8 \text{ W}\cdot\text{m}^{-2}\cdot\text{K}^{-4}$,
 - T_c = case temperature of pyrgeometer (K).
- I = reference irradiance (W/m^2), beam (B) or global (G)
 - where, $G = B * \text{COS}(Z) + D$,
 - Z = zenith angle (degrees),
 - D = reference diffuse irradiance (W/m^2).

Figure 1. Responsivity vs Zenith Angle

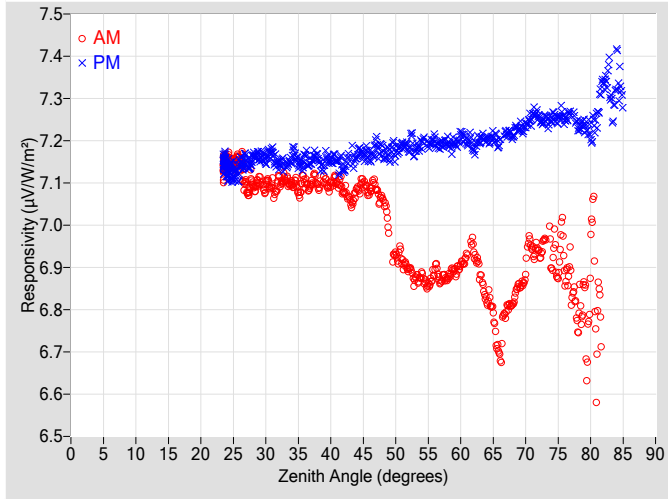


Figure 2. Responsivity vs Local Standard Time

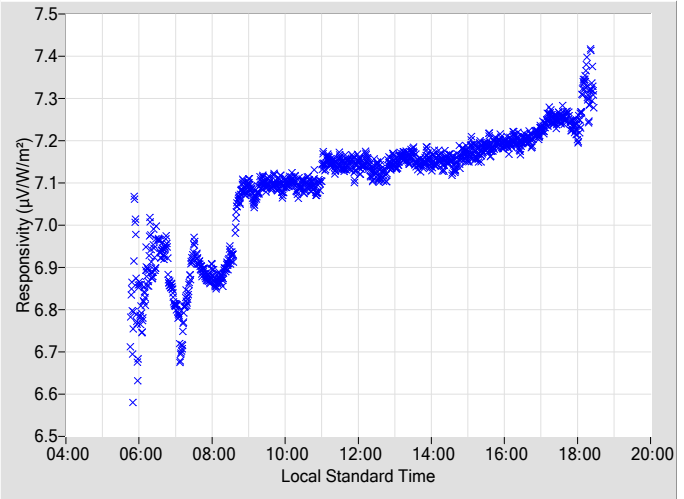


Table 2. Instrument Responsivity (R) and Calibration Type-B Standard Uncertainty, u(B)

| Zenith Angle (deg.) | R ($\mu\text{V}/\text{W}/\text{m}^2$) | u(B) \pm (%) | Azimuth Angle | R ($\mu\text{V}/\text{W}/\text{m}^2$) | u(B) \pm (%) | Azimuth Angle | Zenith Angle (deg.) | R ($\mu\text{V}/\text{W}/\text{m}^2$) | u(B) \pm (%) | Azimuth Angle | R ($\mu\text{V}/\text{W}/\text{m}^2$) | u(B) \pm (%) | Azimuth Angle |
|---------------------|---|----------------|---------------|---|----------------|---------------|---------------------|---|----------------|---------------|---|----------------|---------------|
| 0 | N/A | N/A | N/A | N/A | N/A | N/A | 46 | 7.0779 | 0.34 | 106.81 | 7.1605 | 0.32 | 252.86 |
| 2 | N/A | N/A | N/A | N/A | N/A | N/A | 48 | 7.0606 | 0.34 | 104.56 | 7.1739 | 0.35 | 255.11 |
| 4 | N/A | N/A | N/A | N/A | N/A | N/A | 50 | 6.9277 | 0.35 | 102.39 | 7.1690 | 0.36 | 257.27 |
| 6 | N/A | N/A | N/A | N/A | N/A | N/A | 52 | 6.8965 | 0.40 | 100.41 | 7.1800 | 0.34 | 259.28 |
| 8 | N/A | N/A | N/A | N/A | N/A | N/A | 54 | 6.8800 | 0.37 | 98.47 | 7.1945 | 0.34 | 261.21 |
| 10 | N/A | N/A | N/A | N/A | N/A | N/A | 56 | 6.8945 | 0.39 | 96.61 | 7.2003 | 0.37 | 263.08 |
| 12 | N/A | N/A | N/A | N/A | N/A | N/A | 58 | 6.8758 | 0.38 | 94.83 | 7.1942 | 0.36 | 264.95 |
| 14 | N/A | N/A | N/A | N/A | N/A | N/A | 60 | 6.9067 | 0.39 | 93.03 | 7.2119 | 0.37 | 266.66 |
| 16 | N/A | N/A | N/A | N/A | N/A | N/A | 62 | 6.9426 | 0.41 | 91.33 | 7.1795 | 0.38 | 268.42 |
| 18 | N/A | N/A | N/A | N/A | N/A | N/A | 64 | 6.8207 | 0.47 | 89.66 | 7.2033 | 0.40 | 270.07 |
| 20 | N/A | N/A | N/A | N/A | N/A | N/A | 66 | 6.6896 | 0.45 | 88.02 | 7.1952 | 0.42 | 271.70 |
| 22 | N/A | N/A | N/A | N/A | N/A | N/A | 68 | 6.8131 | 0.44 | 86.41 | 7.2108 | 0.44 | 273.35 |
| 24 | 7.1473 | 0.32 | 166.92 | 7.1368 | 0.32 | 193.02 | 70 | 6.8847 | 0.47 | 84.85 | 7.2373 | 0.47 | 274.97 |
| 26 | 7.1461 | 0.32 | 150.78 | 7.1381 | 0.31 | 209.24 | 72 | 6.9380 | 0.54 | 83.21 | 7.2564 | 0.51 | 276.58 |
| 28 | 7.0977 | 0.34 | 140.87 | 7.1595 | 0.32 | 218.03 | 74 | 6.9161 | 0.56 | 81.59 | 7.2544 | 0.57 | 278.23 |
| 30 | 7.0945 | 0.34 | 134.35 | 7.1538 | 0.31 | 224.80 | 76 | 6.9021 | 0.62 | 79.98 | 7.2495 | 0.64 | 279.82 |
| 32 | 7.1017 | 0.31 | 129.35 | 7.1442 | 0.33 | 230.03 | 78 | 6.7766 | 0.71 | 78.42 | 7.2351 | N/A | 281.39 |
| 34 | 7.0960 | 0.35 | 124.80 | 7.1620 | 0.32 | 234.50 | 80 | 6.9058 | N/A | 76.77 | 7.2165 | N/A | 283.03 |
| 36 | 7.1037 | 0.33 | 120.98 | 7.1609 | 0.32 | 238.38 | 82 | N/A | N/A | N/A | 7.3377 | N/A | 284.68 |
| 38 | 7.0907 | 0.31 | 117.47 | 7.1594 | 0.32 | 241.88 | 84 | N/A | N/A | N/A | 7.3548 | N/A | 286.42 |
| 40 | 7.0952 | 0.35 | 114.55 | 7.1508 | 0.32 | 244.97 | 86 | N/A | N/A | N/A | N/A | N/A | N/A |
| 42 | 7.0795 | 0.32 | 111.72 | 7.1313 | 0.33 | 247.85 | 88 | N/A | N/A | N/A | N/A | N/A | N/A |
| 44 | 7.0816 | 0.32 | 109.20 | 7.1630 | 0.35 | 250.36 | 90 | N/A | N/A | N/A | N/A | N/A | N/A |

N/A - Not Available

Figure 3. Type-B Standard Uncertainty vs Zenith Angle

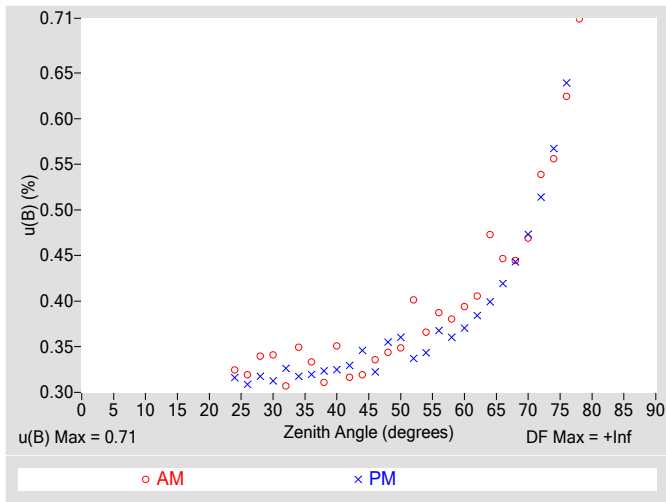


Figure 4. Residuals from Spline Interpolation

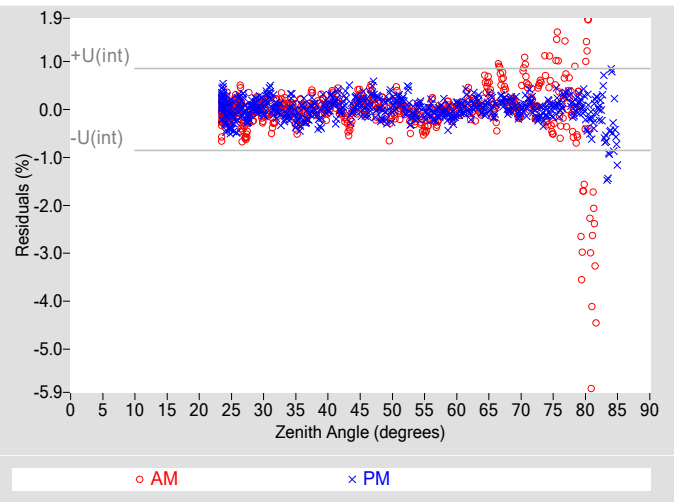


Table 3. Uncertainty using Spline Interpolation ‡

| | |
|---|------------|
| Type-B Standard Uncertainty, $u(B)$ (%) | ± 0.71 |
| Type-A Interpolating Function, $u(int)$ (%) | ± 0.43 |
| Combined Standard Uncertainty, $u(c)$ (%) | ± 0.83 |
| Effective degrees of freedom, $DF(c)$ | 16212 |
| Coverage factor, k | 1.96 |
| Expanded Uncertainty, U_{95} (%) | ± 1.6 |
| AM Valid zenith angle range | 24° to 78° |
| PM Valid zenith angle range | 24° to 76° |

‡ An illustration for how to reduce the uncertainty in calculating the irradiance using a function rather than $R@45^\circ$. Not accredited.

Table 4. Calibration Label Values

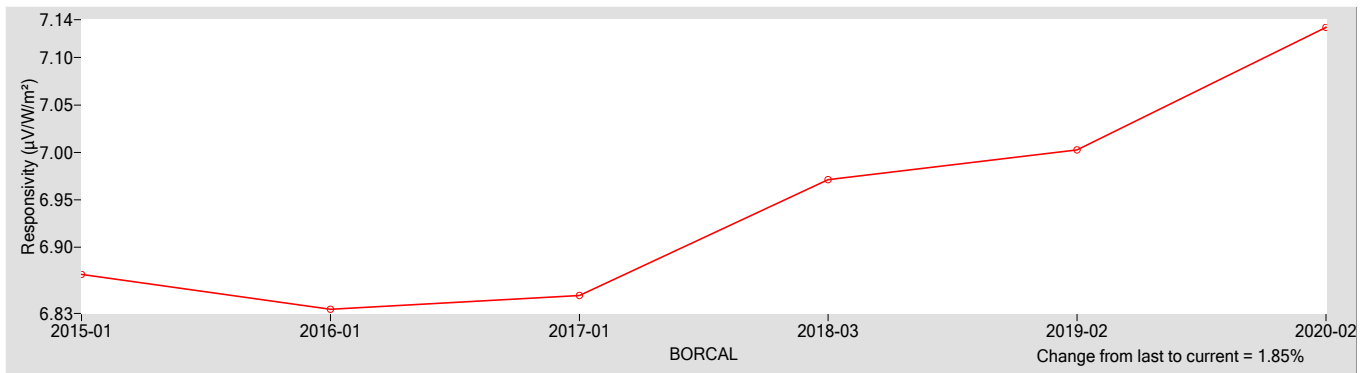
| | |
|----------------------------------|-------------------------------|
| $R @ 45^\circ$ ($\mu V/W/m^2$) | R_{net} ($\mu V/W/m^2$) † |
| 7.1318 | 0.30000 |

† R_{net} determination date: Estimated

Table 5. Uncertainty using $R @ 45^\circ$

| | |
|---|----------------|
| Type-B Expanded Uncertainty, $U(B)$ (%) | ± 0.79 |
| Offset Uncertainty, $U(off)$ (%) | +1.1 / -3.6 |
| Expanded Uncertainty, U (%) | +1.9 / -4.4 |
| Effective degrees of freedom, DF | +Inf |
| Coverage factor, k | 1.96 |
| Valid zenith angle range | 30.0° to 60.0° |

Figure 5. History of instrument at Zenith Angle = 45°



References:

- [1] Reda, I.; Hickey, J.; Long, C.; Myers, D.; Stoffel, T.; Wilcox, S.; Michalsky, J. J.; Dutton, E. G.; Nelson, D. (2005). "Using a Blackbody to Calculate Net Longwave Responsivity of Shortwave Solar Pyranometers to Correct for Their Thermal Offset Error During Outdoor Calibration Using the Component Sum Method." *Journal of Atmospheric and Oceanic Technology*, 2005; pp. 1531-1540; NREL Report No. JA-560-36646. doi:10.1175/JTECH1782.1
- [2] Reda, I.; Myers, D.; Stoffel, T. (2008). "Uncertainty Estimate for the Outdoor Calibration of Solar Pyranometers: A Metrologist Perspective." *Measure*. (NCSLI *Journal of Measurement Science*). Vol. 3(4), December 2008; pp. 58-66; NREL Report No. JA-581-4137
- [3] Reda, I.; Andreas, A. (2004). "Solar Position Algorithm for Solar Radiation Applications." *Solar Energy*. Vol. 76(5), 2004; pp. 577-589; NREL Report No. JA-560-35518. doi:10.1016/j.solener.2003.12.003
- [4] Stoffel, T.; Reda, I. (2009). "NREL Pyrheliometer Comparisons: 22 September - 3 October 2008 (NPC-2008)." 54 pp.; NREL Report No. TP-550-45016.
- [5] Reda, I.; Stoffel, T.; Myers, D. (2003). "Method to Calibrate a Solar Pyranometer for Measuring Reference Diffuse Irradiance." *Solar Energy*. Vol. 74, 2003; pp. 103-112; NREL Report No. JA-560-35025. doi:10.1016/S0038-092X(03)00124-5
- [6] Reda, I. (1996). *Calibration of a Solar Absolute Cavity Radiometer with Traceability to the World Radiometric Reference*. 79 pp.; NREL Report No. TP-463-20619.
- [7] Reda, I.; Gröbner, J.; Stoffel, T.; Myers, D.; Forgan, B. (2008). *Improvements in the Blackbody Calibration of Pyrgometers*. ARM 2008 Science Team Meeting (Poster).



National Renewable Energy Laboratory

Solar Radiation Research Laboratory

Metrology Laboratory

Calibration Certificate



| | | | |
|--------------------------|---------------------|----------------------------------|------------|
| Test Instrument: | Silicon Pyranometer | Manufacturer: | EKO |
| Model: | ML-01 | Serial Number: | S13135063 |
| Calibration Date: | 5/5/2020 | Due Date: | 5/5/2021 |
| Customer: | NREL-SRRL-BMS | Environmental Conditions: | see page 4 |
| Test Dates: | 5/4-5 | | |

This certifies that the above product was calibrated in compliance with ISO/IEC 17025:2017. Measurement uncertainties at the time of calibration are consistent with the Guide to the Expression of Uncertainty in Measurement (GUM) using Reda et al., 2008. All nominal values are traceable to the International System (SI) Units of Measurement.

No statement of compliance with specifications is made or implied on this certificate. However, the estimated uncertainties are the uncertainties of the calibration process; users must add other uncertainties that are relevant to their measuring system, environmental and sky conditions, outdoor set-up, and site location.

The Type-B Standard Uncertainty of using the responsivity at each even zenith angle is reported, and the Expanded Uncertainty of the calibration is reported using two methods:

1. The Expanded Uncertainty of using the responsivity at zenith angle = 45°, within the zenith angle range from 30.0° to 60.0°
2. The Expanded Uncertainty of using Spline Interpolating Functions for the responsivity versus zenith angle.

This certificate applies only to the item identified above and shall not be reproduced other than in full, without specific written approval from the calibration facility. Certificate without signature is not valid.

Table 1. Traceability

| Measurement Type | Instrument | Calibration Date | Calibration Due Date |
|----------------------|--|------------------|----------------------|
| Beam Irradiance † | Eppley Absolute Cavity Radiometer Model HF, S/N 29219 | 09/27/2019 | 09/27/2020 |
| Diffuse Irradiance † | Hukseflux Pyranometer Model SR25, S/N 2541 | 04/17/2020 | 04/17/2021 |
| Diffuse Irradiance † | Hukseflux Pyranometer Model SR25, S/N 2542 | 04/17/2020 | 04/17/2021 |
| Data Acquisition | NREL Data Acquisition System Model RAP-DAQ, S/N 2005-998 | 02/14/2019 | 02/14/2021 |
| Data Acquisition | NREL Data Acquisition System Model RAP-DAQ, S/N 2005-999 | 02/14/2019 | 02/14/2021 |

† Through the World Radiometric Reference (WRR)

Number of pages of certificate: 4

Calibration Procedure: BORCAL-P00-Calibration and QA Procedure; available upon request.

Setup: Radiometers are calibrated outdoors, using the sun as the source. Pyranometers and pyrgeometers are installed for horizontal measurements, with their signal connectors oriented north, if their design permits.

The shading disk for the reference diffuse subtends a solid angle of 5°. Pyrheliometers are installed on solar trackers.

Calibrated by: Afshin Andreas, Ibrahim Reda, Peter Gotseff, and RCC

Ibrahim Reda, Technical Manager

Date

For questions or comments, please contact the technical manager at:

ibrahim.reda@nrel.gov; 303-384-6385; 15013 Denver West Parkway, Golden, CO 80401, USA

Calibration Results

S13135063 EKO ML-01

The responsivity (R , $\mu\text{V}/\text{W}/\text{m}^2$) of the test instrument during calibration is calculated using this Measurement Equation:

$$R = (V - R_{net} * W_{net}) / I \quad [1]$$

where,

- V = radiometer output voltage (microvolts),
 - R_{net} = radiometer net infrared responsivity ($\mu\text{V}/\text{W}/\text{m}^2$), see Table 4,
 - W_{net} = effective net infrared measured by pyrgeometer (W/m^2),
 - = $W_{in} - W_{out} = W_{in} - \sigma * T_c^4$
 - where, W_{in} = incoming infrared (W/m^2), $\sigma = 5.6704\text{e-}8 \text{ W}\cdot\text{m}^{-2}\cdot\text{K}^{-4}$,
 - T_c = case temperature of pyrgeometer (K).
- I = reference irradiance (W/m^2), beam (B) or global (G)
 where, $G = B * \text{COS}(Z) + D$,
 Z = zenith angle (degrees),
 D = reference diffuse irradiance (W/m^2).

Figure 1. Responsivity vs Zenith Angle

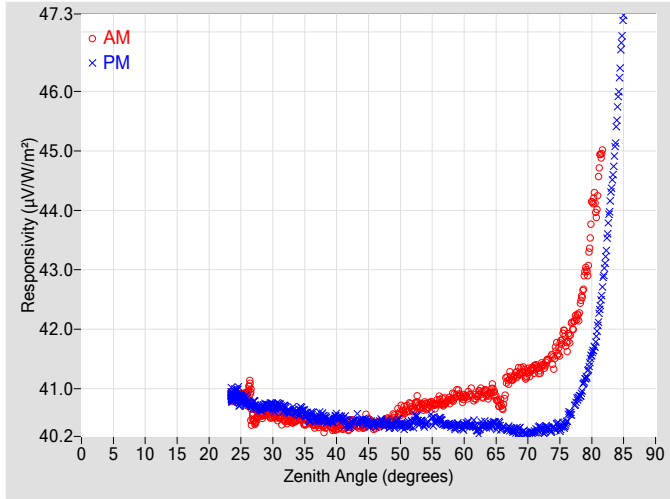


Figure 2. Responsivity vs Local Standard Time

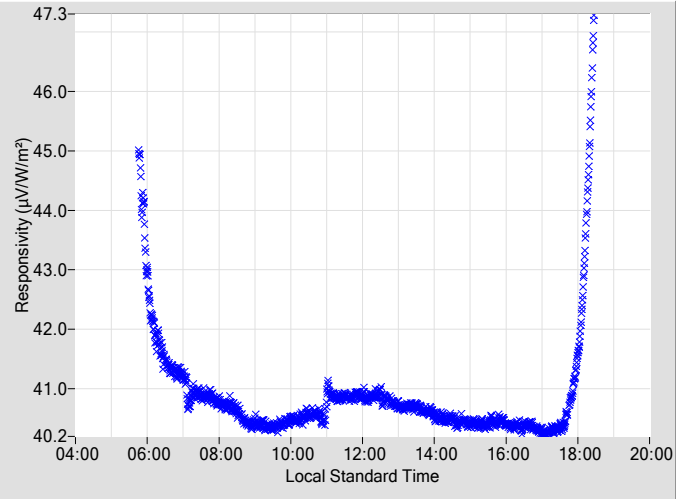


Table 2. Instrument Responsivity (R) and Calibration Type-B Standard Uncertainty, $u(B)$

| Zenith Angle (deg.) | R ($\mu\text{V}/\text{W}/\text{m}^2$) | AM $u(B)$ \pm (%) | Azimuth Angle | R ($\mu\text{V}/\text{W}/\text{m}^2$) | PM $u(B)$ \pm (%) | Azimuth Angle | Zenith Angle (deg.) | R ($\mu\text{V}/\text{W}/\text{m}^2$) | AM $u(B)$ \pm (%) | Azimuth Angle | R ($\mu\text{V}/\text{W}/\text{m}^2$) | PM $u(B)$ \pm (%) | Azimuth Angle |
|---------------------|---|---------------------|---------------|---|---------------------|---------------|---------------------|---|---------------------|---------------|---|---------------------|---------------|
| 0 | N/A | N/A | N/A | N/A | N/A | N/A | 46 | 40.355 | 0.32 | 106.80 | 40.399 | 0.31 | 252.80 |
| 2 | N/A | N/A | N/A | N/A | N/A | N/A | 48 | 40.462 | 0.31 | 104.58 | 40.412 | 0.33 | 255.11 |
| 4 | N/A | N/A | N/A | N/A | N/A | N/A | 50 | 40.593 | 0.33 | 102.44 | 40.402 | 0.31 | 257.21 |
| 6 | N/A | N/A | N/A | N/A | N/A | N/A | 52 | 40.640 | 0.34 | 100.41 | 40.440 | 0.32 | 259.27 |
| 8 | N/A | N/A | N/A | N/A | N/A | N/A | 54 | 40.717 | 0.37 | 98.48 | 40.410 | 0.34 | 261.25 |
| 10 | N/A | N/A | N/A | N/A | N/A | N/A | 56 | 40.801 | 0.35 | 96.61 | 40.486 | 0.33 | 263.13 |
| 12 | N/A | N/A | N/A | N/A | N/A | N/A | 58 | 40.823 | 0.36 | 94.82 | 40.391 | 0.33 | 264.89 |
| 14 | N/A | N/A | N/A | N/A | N/A | N/A | 60 | 40.851 | 0.36 | 93.03 | 40.372 | 0.34 | 266.70 |
| 16 | N/A | N/A | N/A | N/A | N/A | N/A | 62 | 40.889 | 0.35 | 91.33 | 40.296 | 0.35 | 268.42 |
| 18 | N/A | N/A | N/A | N/A | N/A | N/A | 64 | 40.919 | 0.38 | 89.66 | 40.391 | 0.36 | 270.07 |
| 20 | N/A | N/A | N/A | N/A | N/A | N/A | 66 | 40.738 | 0.38 | 88.02 | 40.338 | 0.38 | 271.70 |
| 22 | N/A | N/A | N/A | N/A | N/A | N/A | 68 | 41.227 | 0.39 | 86.40 | 40.282 | 0.40 | 273.39 |
| 24 | 40.866 | 0.30 | 167.14 | 40.887 | 0.31 | 193.11 | 70 | 41.247 | 0.50 | 84.81 | 40.231 | 0.42 | 274.97 |
| 26 | 40.918 | 0.31 | 150.99 | 40.767 | 0.31 | 209.17 | 72 | 41.337 | 0.45 | 83.21 | 40.350 | 0.45 | 276.58 |
| 28 | 40.584 | 0.30 | 140.90 | 40.667 | 0.33 | 218.11 | 74 | 41.510 | 0.49 | 81.59 | 40.334 | 0.49 | 278.18 |
| 30 | 40.559 | 0.31 | 134.53 | 40.695 | 0.33 | 224.68 | 76 | 41.795 | 0.54 | 80.02 | 40.444 | 0.55 | 279.82 |
| 32 | 40.506 | 0.34 | 129.24 | 40.660 | 0.33 | 230.02 | 78 | 42.305 | 0.61 | 78.37 | 40.862 | N/A | 281.43 |
| 34 | 40.523 | 0.31 | 124.79 | 40.600 | 0.32 | 234.58 | 80 | 43.940 | N/A | 76.77 | 41.588 | N/A | 283.07 |
| 36 | 40.436 | 0.31 | 121.06 | 40.542 | 0.30 | 238.40 | 82 | N/A | N/A | N/A | 43.077 | N/A | 284.72 |
| 38 | 40.352 | 0.32 | 117.62 | 40.517 | 0.31 | 241.87 | 84 | N/A | N/A | N/A | 45.617 | N/A | 286.37 |
| 40 | 40.353 | 0.30 | 114.55 | 40.533 | 0.35 | 244.97 | 86 | N/A | N/A | N/A | N/A | N/A | N/A |
| 42 | 40.360 | 0.32 | 111.72 | 40.379 | 0.30 | 247.78 | 88 | N/A | N/A | N/A | N/A | N/A | N/A |
| 44 | 40.388 | 0.34 | 109.19 | 40.468 | 0.32 | 250.42 | 90 | N/A | N/A | N/A | N/A | N/A | N/A |

N/A - Not Available

Figure 3. Type-B Standard Uncertainty vs Zenith Angle

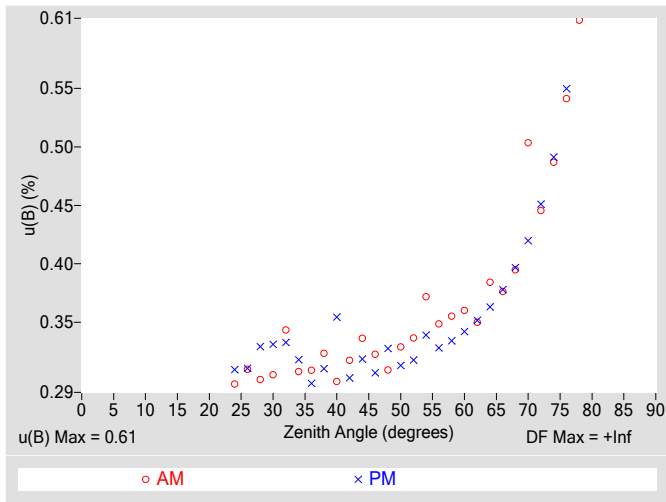


Figure 4. Residuals from Spline Interpolation

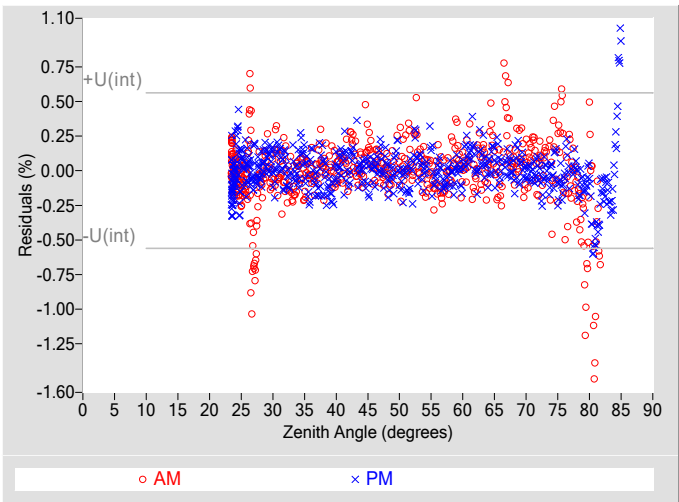


Table 3. Uncertainty using Spline Interpolation ‡

| | |
|---|------------|
| Type-B Standard Uncertainty, $u(B)$ (%) | ± 0.61 |
| Type-A Interpolating Function, $u(int)$ (%) | ± 0.28 |
| Combined Standard Uncertainty, $u(c)$ (%) | ± 0.67 |
| Effective degrees of freedom, $DF(c)$ | 37749 |
| Coverage factor, k | 1.96 |
| Expanded Uncertainty, $U95$ (%) | ± 1.3 |
| AM Valid zenith angle range | 24° to 78° |
| PM Valid zenith angle range | 24° to 76° |

‡ An illustration for how to reduce the uncertainty in calculating the irradiance using a function rather than $R@45^\circ$. Not accredited.

Table 4. Calibration Label Values

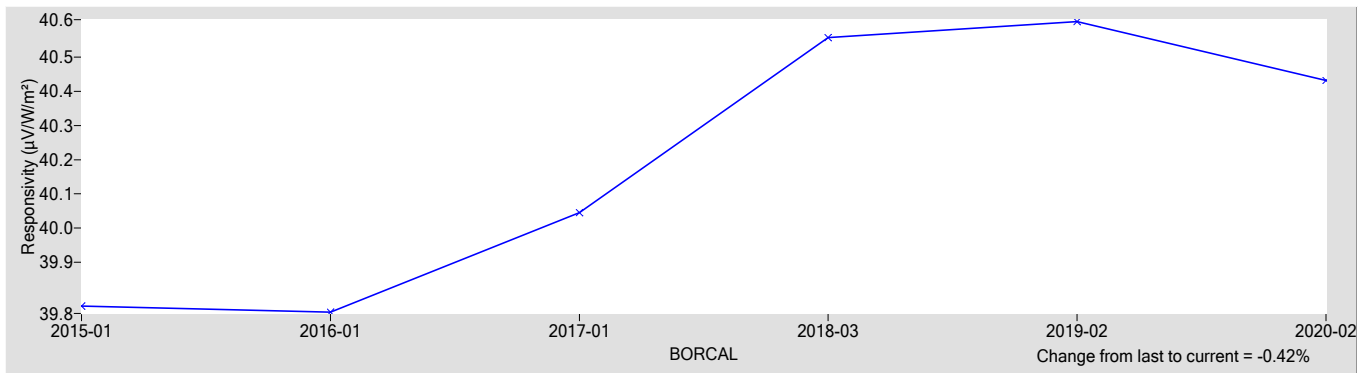
| | |
|----------------------------------|-------------------------------|
| $R @ 45^\circ$ ($\mu V/W/m^2$) | R_{net} ($\mu V/W/m^2$) † |
| 40.432 | 0 |

† R_{net} determination date: N/A

Table 5. Uncertainty using $R @ 45^\circ$

| | |
|---|----------------|
| Type-B Expanded Uncertainty, $U(B)$ (%) | ± 0.73 |
| Offset Uncertainty, $U(off)$ (%) | +1.0 / -0.20 |
| Expanded Uncertainty, U (%) | +1.8 / -0.93 |
| Effective degrees of freedom, DF | +Inf |
| Coverage factor, k | 1.96 |
| Valid zenith angle range | 30.0° to 60.0° |

Figure 5. History of instrument at Zenith Angle = 45°



References:

[1] Reda, I.; Hickey, J.; Long, C.; Myers, D.; Stoffel, T.; Wilcox, S.; Michalsky, J. J.; Dutton, E. G.; Nelson, D. (2005). "Using a Blackbody to Calculate Net Longwave Responsivity of Shortwave Solar Pyranometers to Correct for Their Thermal Offset Error During Outdoor Calibration Using the Component Sum Method." *Journal of Atmospheric and Oceanic Technology*, 2005; pp. 1531-1540; NREL Report No. JA-560-36646. doi:10.1175/JTECH1782.1

[2] Reda, I.; Myers, D.; Stoffel, T. (2008). "Uncertainty Estimate for the Outdoor Calibration of Solar Pyranometers: A Metrologist Perspective." *Measure*. (NCSLI *Journal of Measurement Science*). Vol. 3(4), December 2008; pp. 58-66; NREL Report No. JA-581-4137

[3] Reda, I.; Andreas, A. (2004). "Solar Position Algorithm for Solar Radiation Applications." *Solar Energy*. Vol. 76(5), 2004; pp. 577-589; NREL Report No. JA-560-35518. doi:10.1016/j.solener.2003.12.003

[4] Stoffel, T.; Reda, I. (2009). "NREL Pyrheliometer Comparisons: 22 September - 3 October 2008 (NPC-2008)." 54 pp.; NREL Report No. TP-550-45016.

[5] Reda, I.; Stoffel, T.; Myers, D. (2003). "Method to Calibrate a Solar Pyranometer for Measuring Reference Diffuse Irradiance." *Solar Energy*. Vol. 74, 2003; pp. 103-112; NREL Report No. JA-560-35025. doi:10.1016/S0038-092X(03)00124-5

[6] Reda, I. (1996). *Calibration of a Solar Absolute Cavity Radiometer with Traceability to the World Radiometric Reference*. 79 pp.; NREL Report No. TP-463-20619.

[7] Reda, I.; Gröbner, J.; Stoffel, T.; Myers, D.; Forgan, B. (2008). *Improvements in the Blackbody Calibration of Pyrheliometers*. ARM 2008 Science Team Meeting (Poster).



National Renewable Energy Laboratory

Solar Radiation Research Laboratory

Metrology Laboratory

Calibration Certificate



| | | | |
|--------------------------|---------------|----------------------------------|-------------|
| Test Instrument: | Pyranometer | Manufacturer: | EKO |
| Model: | MS-410 | Serial Number: | S13144.085R |
| Calibration Date: | 5/5/2020 | Due Date: | 5/5/2021 |
| Customer: | NREL-SRRL-BMS | Environmental Conditions: | see page 4 |
| Test Dates: | 5/4-5 | | |

This certifies that the above product was calibrated in compliance with ISO/IEC 17025:2017. Measurement uncertainties at the time of calibration are consistent with the Guide to the Expression of Uncertainty in Measurement (GUM) using Reda et al., 2008. All nominal values are traceable to the International System (SI) Units of Measurement.

No statement of compliance with specifications is made or implied on this certificate. However, the estimated uncertainties are the uncertainties of the calibration process; users must add other uncertainties that are relevant to their measuring system, environmental and sky conditions, outdoor set-up, and site location.

The Type-B Standard Uncertainty of using the responsivity at each even zenith angle is reported, and the Expanded Uncertainty of the calibration is reported using two methods:

1. The Expanded Uncertainty of using the responsivity at zenith angle = 45°, within the zenith angle range from 30.0° to 60.0°
2. The Expanded Uncertainty of using Spline Interpolating Functions for the responsivity versus zenith angle.

This certificate applies only to the item identified above and shall not be reproduced other than in full, without specific written approval from the calibration facility. Certificate without signature is not valid.

Table 1. Traceability

| Measurement Type | Instrument | Calibration Date | Calibration Due Date |
|-----------------------|--|------------------|----------------------|
| Beam Irradiance † | Eppley Absolute Cavity Radiometer Model HF, S/N 29219 | 09/27/2019 | 09/27/2020 |
| Diffuse Irradiance † | Hukseflux Pyranometer Model SR25, S/N 2541 | 04/17/2020 | 04/17/2021 |
| Diffuse Irradiance † | Hukseflux Pyranometer Model SR25, S/N 2542 | 04/17/2020 | 04/17/2021 |
| Data Acquisition | NREL Data Acquisition System Model RAP-DAQ, S/N 2005-998 | 02/14/2019 | 02/14/2021 |
| Data Acquisition | NREL Data Acquisition System Model RAP-DAQ, S/N 2005-999 | 02/14/2019 | 02/14/2021 |
| Infrared Irradiance ‡ | Kipp & Zonen Pyrgeometer Model CG4, S/N FT002 | 04/16/2018 | 04/16/2022 |

† Through the World Radiometric Reference (WRR)

‡ Through the World Infrared Standard Group (WISG)

Number of pages of certificate: 4

Calibration Procedure: BORCAL-P00-Calibration and QA Procedure; available upon request.

Setup: Radiometers are calibrated outdoors, using the sun as the source. Pyranometers and pyrgeometers are installed for horizontal measurements, with their signal connectors oriented north, if their design permits.

The shading disk for the reference diffuse subtends a solid angle of 5°. Pyrheliometers are installed on solar trackers.

Calibrated by: Afshin Andreas, Ibrahim Reda, Peter Gotseff, and RCC

Ibrahim Reda, Technical Manager

Date

For questions or comments, please contact the technical manager at:

ibrahim.reda@nrel.gov; 303-384-6385; 15013 Denver West Parkway, Golden, CO 80401, USA

Calibration Results

S13144.085R EKO MS-410

The responsivity (R , $\mu\text{V}/\text{W}/\text{m}^2$) of the test instrument during calibration is calculated using this Measurement Equation:

$$R = (V - R_{net} * W_{net}) / I \tag{1}$$

where,

- V = radiometer output voltage (microvolts),
 - R_{net} = radiometer net infrared responsivity ($\mu\text{V}/\text{W}/\text{m}^2$), see Table 4,
 - W_{net} = effective net infrared measured by pyrgeometer (W/m^2),
 - = $W_{in} - W_{out} = W_{in} - \sigma * T_c^4$
 - where, W_{in} = incoming infrared (W/m^2), $\sigma = 5.6704\text{e-}8 \text{ W}\cdot\text{m}^{-2}\cdot\text{K}^{-4}$,
 - T_c = case temperature of pyrgeometer (K).
- I = reference irradiance (W/m^2), beam (B) or global (G)
 - where, $G = B * \text{COS}(Z) + D$,
 - Z = zenith angle (degrees),
 - D = reference diffuse irradiance (W/m^2).

Figure 1. Responsivity vs Zenith Angle

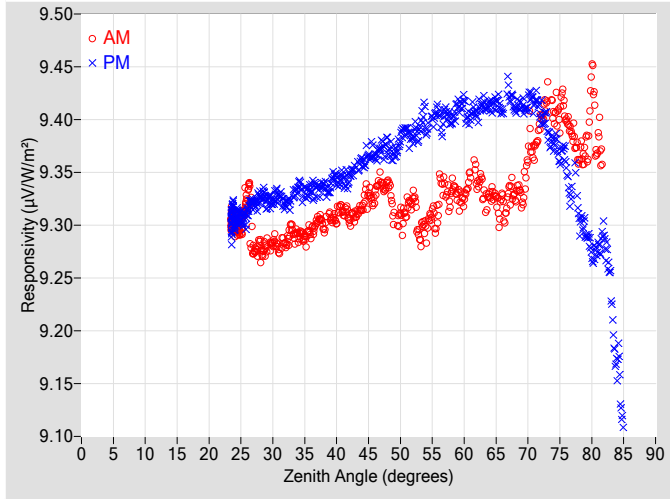


Figure 2. Responsivity vs Local Standard Time

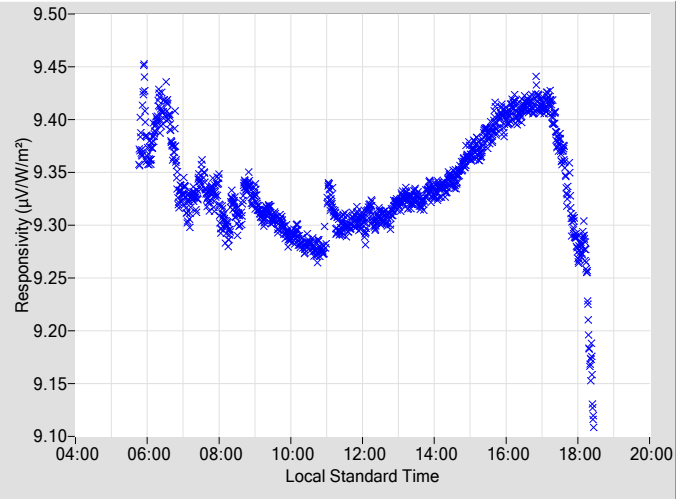


Table 2. Instrument Responsivity (R) and Calibration Type-B Standard Uncertainty, u(B)

| Zenith Angle (deg.) | R ($\mu\text{V}/\text{W}/\text{m}^2$) | u(B) \pm (%) | Azimuth Angle | R ($\mu\text{V}/\text{W}/\text{m}^2$) | u(B) \pm (%) | Azimuth Angle | Zenith Angle (deg.) | R ($\mu\text{V}/\text{W}/\text{m}^2$) | u(B) \pm (%) | Azimuth Angle | R ($\mu\text{V}/\text{W}/\text{m}^2$) | u(B) \pm (%) | Azimuth Angle |
|---------------------|---|----------------|---------------|---|----------------|---------------|---------------------|---|----------------|---------------|---|----------------|---------------|
| 0 | N/A | N/A | N/A | N/A | N/A | N/A | 46 | 9.3273 | 0.31 | 106.80 | 9.3645 | 0.31 | 252.85 |
| 2 | N/A | N/A | N/A | N/A | N/A | N/A | 48 | 9.3392 | 0.34 | 104.53 | 9.3755 | 0.32 | 255.11 |
| 4 | N/A | N/A | N/A | N/A | N/A | N/A | 50 | 9.3062 | 0.32 | 102.39 | 9.3819 | 0.33 | 257.26 |
| 6 | N/A | N/A | N/A | N/A | N/A | N/A | 52 | 9.3241 | 0.34 | 100.41 | 9.3833 | 0.34 | 259.27 |
| 8 | N/A | N/A | N/A | N/A | N/A | N/A | 54 | 9.2952 | 0.35 | 98.46 | 9.3973 | 0.33 | 261.20 |
| 10 | N/A | N/A | N/A | N/A | N/A | N/A | 56 | 9.3238 | 0.34 | 96.61 | 9.4081 | 0.35 | 263.08 |
| 12 | N/A | N/A | N/A | N/A | N/A | N/A | 58 | 9.3299 | 0.36 | 94.82 | 9.3985 | 0.34 | 264.94 |
| 14 | N/A | N/A | N/A | N/A | N/A | N/A | 60 | 9.3256 | 0.39 | 93.08 | 9.4147 | 0.35 | 266.70 |
| 16 | N/A | N/A | N/A | N/A | N/A | N/A | 62 | 9.3418 | 0.38 | 91.33 | 9.4067 | 0.36 | 268.42 |
| 18 | N/A | N/A | N/A | N/A | N/A | N/A | 64 | 9.3273 | 0.42 | 89.66 | 9.4145 | 0.37 | 270.07 |
| 20 | N/A | N/A | N/A | N/A | N/A | N/A | 66 | 9.3219 | 0.47 | 88.02 | 9.4070 | 0.39 | 271.70 |
| 22 | N/A | N/A | N/A | N/A | N/A | N/A | 68 | 9.3274 | 0.41 | 86.40 | 9.4097 | 0.41 | 273.34 |
| 24 | 9.3003 | 0.31 | 166.89 | 9.3073 | 0.31 | 193.02 | 70 | 9.3722 | 0.43 | 84.80 | 9.4160 | 0.44 | 274.97 |
| 26 | 9.3260 | 0.30 | 150.99 | 9.3103 | 0.32 | 209.18 | 72 | 9.3990 | 0.46 | 83.21 | 9.4054 | 0.47 | 276.58 |
| 28 | 9.2822 | 0.32 | 140.68 | 9.3257 | 0.31 | 218.11 | 74 | 9.4060 | 0.51 | 81.59 | 9.3778 | 0.52 | 278.22 |
| 30 | 9.2830 | 0.32 | 134.45 | 9.3232 | 0.32 | 224.80 | 76 | 9.3999 | 0.57 | 79.97 | 9.3565 | 0.58 | 279.82 |
| 32 | 9.2818 | 0.30 | 129.21 | 9.3193 | 0.31 | 230.02 | 78 | 9.3659 | 0.64 | 78.41 | 9.3053 | N/A | 281.43 |
| 34 | 9.2908 | 0.31 | 124.79 | 9.3365 | 0.31 | 234.49 | 80 | 9.4339 | N/A | 76.77 | 9.2731 | N/A | 283.03 |
| 36 | 9.2939 | 0.33 | 120.99 | 9.3363 | 0.34 | 238.46 | 82 | N/A | N/A | N/A | 9.2858 | N/A | 284.67 |
| 38 | 9.2985 | 0.30 | 117.62 | 9.3380 | 0.32 | 241.92 | 84 | N/A | N/A | N/A | 9.1719 | N/A | 286.41 |
| 40 | 9.3070 | 0.32 | 114.55 | 9.3433 | 0.31 | 244.97 | 86 | N/A | N/A | N/A | N/A | N/A | N/A |
| 42 | 9.3050 | 0.32 | 111.72 | 9.3456 | 0.32 | 247.85 | 88 | N/A | N/A | N/A | N/A | N/A | N/A |
| 44 | 9.3161 | 0.32 | 109.19 | 9.3610 | 0.32 | 250.36 | 90 | N/A | N/A | N/A | N/A | N/A | N/A |

N/A - Not Available

Figure 3. Type-B Standard Uncertainty vs Zenith Angle

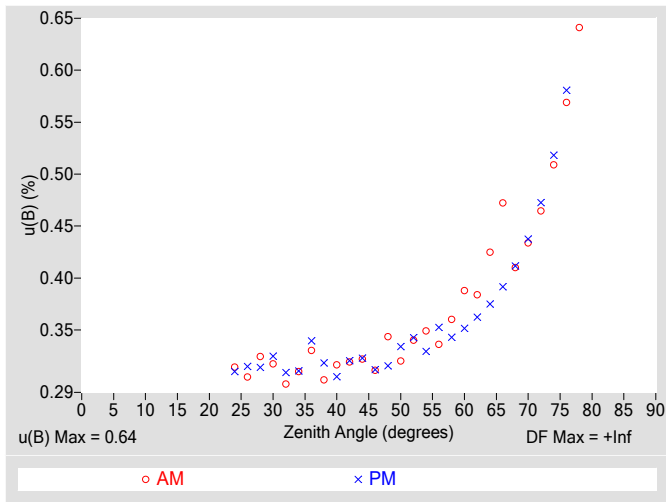


Figure 4. Residuals from Spline Interpolation

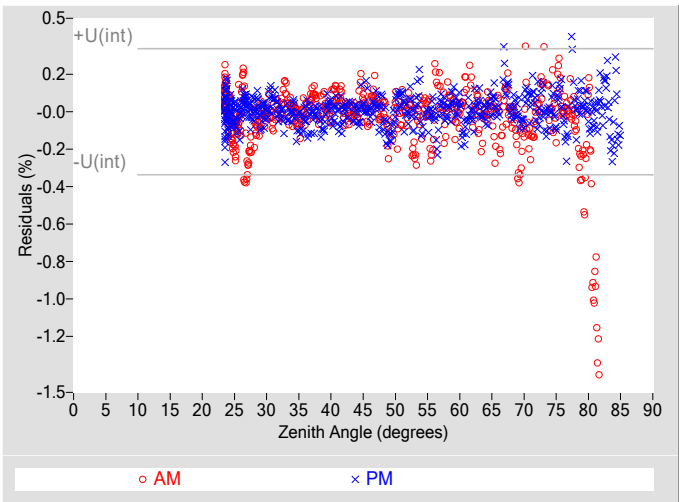


Table 3. Uncertainty using Spline Interpolation ‡

| | |
|---|------------|
| Type-B Standard Uncertainty, $u(B)$ (%) | ± 0.64 |
| Type-A Interpolating Function, $u(int)$ (%) | ± 0.17 |
| Combined Standard Uncertainty, $u(c)$ (%) | ± 0.66 |
| Effective degrees of freedom, $DF(c)$ | 273164 |
| Coverage factor, k | 1.96 |
| Expanded Uncertainty, U_{95} (%) | ± 1.3 |
| AM Valid zenith angle range | 24° to 78° |
| PM Valid zenith angle range | 24° to 76° |

‡ An illustration for how to reduce the uncertainty in calculating the irradiance using a function rather than $R@45^\circ$. Not accredited.

Table 4. Calibration Label Values

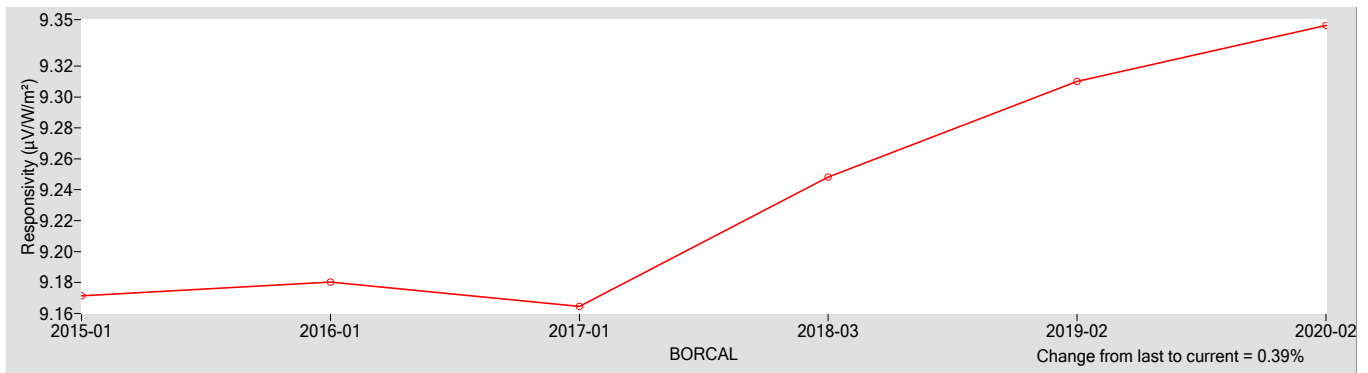
| | |
|----------------------------------|-------------------------------|
| $R @ 45^\circ$ ($\mu V/W/m^2$) | R_{net} ($\mu V/W/m^2$) † |
| 9.3463 | 0.20000 |

† R_{net} determination date: Estimated

Table 5. Uncertainty using $R @ 45^\circ$

| | |
|---|----------------|
| Type-B Expanded Uncertainty, $U(B)$ (%) | ± 0.76 |
| Offset Uncertainty, $U(off)$ (%) | +0.73 / -0.69 |
| Expanded Uncertainty, U (%) | +1.5 / -1.5 |
| Effective degrees of freedom, DF | +Inf |
| Coverage factor, k | 1.96 |
| Valid zenith angle range | 30.0° to 60.0° |

Figure 5. History of instrument at Zenith Angle = 45°



References:

- [1] Reda, I.; Hickey, J.; Long, C.; Myers, D.; Stoffel, T.; Wilcox, S.; Michalsky, J. J.; Dutton, E. G.; Nelson, D. (2005). "Using a Blackbody to Calculate Net Longwave Responsivity of Shortwave Solar Pyranometers to Correct for Their Thermal Offset Error During Outdoor Calibration Using the Component Sum Method." *Journal of Atmospheric and Oceanic Technology*, 2005; pp. 1531-1540; NREL Report No. JA-560-36646. doi:10.1175/JTECH1782.1
- [2] Reda, I.; Myers, D.; Stoffel, T. (2008). "Uncertainty Estimate for the Outdoor Calibration of Solar Pyranometers: A Metrologist Perspective." *Measure*. (NCSLI *Journal of Measurement Science*). Vol. 3(4), December 2008; pp. 58-66; NREL Report No. JA-581-4137
- [3] Reda, I.; Andreas, A. (2004). "Solar Position Algorithm for Solar Radiation Applications." *Solar Energy*. Vol. 76(5), 2004; pp. 577-589; NREL Report No. JA-560-35518. doi:10.1016/j.solener.2003.12.003
- [4] Stoffel, T.; Reda, I. (2009). "NREL Pyrheliometer Comparisons: 22 September - 3 October 2008 (NPC-2008)." 54 pp.; NREL Report No. TP-550-45016.
- [5] Reda, I.; Stoffel, T.; Myers, D. (2003). "Method to Calibrate a Solar Pyranometer for Measuring Reference Diffuse Irradiance." *Solar Energy*. Vol. 74, 2003; pp. 103-112; NREL Report No. JA-560-35025. doi:10.1016/S0038-092X(03)00124-5
- [6] Reda, I. (1996). *Calibration of a Solar Absolute Cavity Radiometer with Traceability to the World Radiometric Reference*. 79 pp.; NREL Report No. TP-463-20619.
- [7] Reda, I.; Gröbner, J.; Stoffel, T.; Myers, D.; Forgan, B. (2008). *Improvements in the Blackbody Calibration of Pyrgometers*. ARM 2008 Science Team Meeting (Poster).



National Renewable Energy Laboratory

Solar Radiation Research Laboratory

Metrology Laboratory

Calibration Certificate



| | | | |
|--------------------------|---------------|----------------------------------|------------|
| Test Instrument: | Pyranometer | Manufacturer: | EKO |
| Model: | MS-80 | Serial Number: | S17096005 |
| Calibration Date: | 5/5/2020 | Due Date: | 5/5/2021 |
| Customer: | NREL-SRRL-BMS | Environmental Conditions: | see page 4 |
| Test Dates: | 5/4-5 | | |

This certifies that the above product was calibrated in compliance with ISO/IEC 17025:2017. Measurement uncertainties at the time of calibration are consistent with the Guide to the Expression of Uncertainty in Measurement (GUM) using Reda et al., 2008. All nominal values are traceable to the International System (SI) Units of Measurement.

No statement of compliance with specifications is made or implied on this certificate. However, the estimated uncertainties are the uncertainties of the calibration process; users must add other uncertainties that are relevant to their measuring system, environmental and sky conditions, outdoor set-up, and site location.

The Type-B Standard Uncertainty of using the responsivity at each even zenith angle is reported, and the Expanded Uncertainty of the calibration is reported using two methods:

1. The Expanded Uncertainty of using the responsivity at zenith angle = 45°, within the zenith angle range from 30.0° to 60.0°
2. The Expanded Uncertainty of using Spline Interpolating Functions for the responsivity versus zenith angle.

This certificate applies only to the item identified above and shall not be reproduced other than in full, without specific written approval from the calibration facility. Certificate without signature is not valid.

Table 1. Traceability

| Measurement Type | Instrument | Calibration Date | Calibration Due Date |
|-----------------------|--|------------------|----------------------|
| Beam Irradiance † | Eppley Absolute Cavity Radiometer Model HF, S/N 29219 | 09/27/2019 | 09/27/2020 |
| Diffuse Irradiance † | Hukseflux Pyranometer Model SR25, S/N 2541 | 04/17/2020 | 04/17/2021 |
| Diffuse Irradiance † | Hukseflux Pyranometer Model SR25, S/N 2542 | 04/17/2020 | 04/17/2021 |
| Data Acquisition | NREL Data Acquisition System Model RAP-DAQ, S/N 2005-998 | 02/14/2019 | 02/14/2021 |
| Data Acquisition | NREL Data Acquisition System Model RAP-DAQ, S/N 2005-999 | 02/14/2019 | 02/14/2021 |
| Infrared Irradiance ‡ | Kipp & Zonen Pyrgeometer Model CG4, S/N FT002 | 04/16/2018 | 04/16/2022 |

† Through the World Radiometric Reference (WRR)

‡ Through the World Infrared Standard Group (WISG)

Number of pages of certificate: 4

Calibration Procedure: BORCAL-P00-Calibration and QA Procedure; available upon request.

Setup: Radiometers are calibrated outdoors, using the sun as the source. Pyranometers and pyrgeometers are installed for horizontal measurements, with their signal connectors oriented north, if their design permits.

The shading disk for the reference diffuse subtends a solid angle of 5°. Pyrheliometers are installed on solar trackers.

Calibrated by: Afshin Andreas, Ibrahim Reda, Peter Gotseff, and RCC

Ibrahim Reda, Technical Manager

Date

For questions or comments, please contact the technical manager at:

ibrahim.reda@nrel.gov; 303-384-6385; 15013 Denver West Parkway, Golden, CO 80401, USA

Calibration Results

S17096005 EKO MS-80

The responsivity (R , $\mu\text{V}/\text{W}/\text{m}^2$) of the test instrument during calibration is calculated using this Measurement Equation:

$$R = (V - R_{net} * W_{net}) / I \tag{1}$$

where,

- V = radiometer output voltage (microvolts),
 - R_{net} = radiometer net infrared responsivity ($\mu\text{V}/\text{W}/\text{m}^2$), see Table 4,
 - W_{net} = effective net infrared measured by pyrgeometer (W/m^2),
 - = $W_{in} - W_{out} = W_{in} - \sigma * T_c^4$
 - where, W_{in} = incoming infrared (W/m^2), $\sigma = 5.6704\text{e-}8 \text{ W}\cdot\text{m}^{-2}\cdot\text{K}^{-4}$,
 - T_c = case temperature of pyrgeometer (K).
- I = reference irradiance (W/m^2), beam (B) or global (G)
 - where, $G = B * \text{COS}(Z) + D$,
 - Z = zenith angle (degrees),
 - D = reference diffuse irradiance (W/m^2).

Figure 1. Responsivity vs Zenith Angle

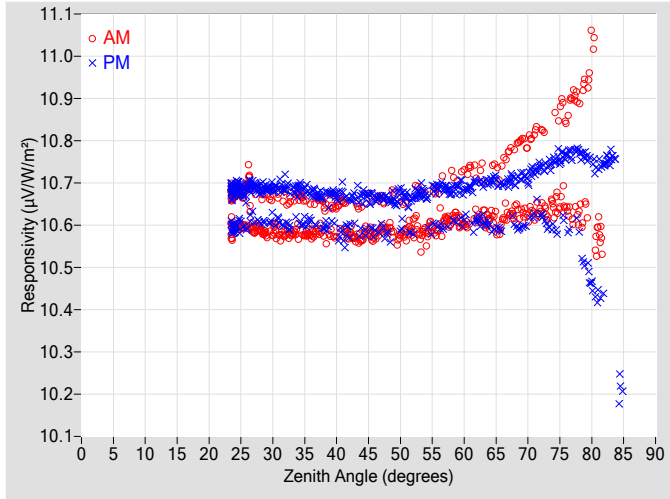


Figure 2. Responsivity vs Local Standard Time

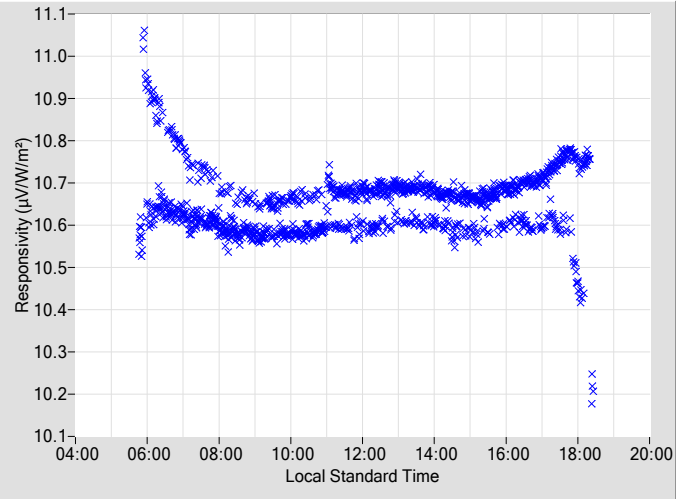


Table 2. Instrument Responsivity (R) and Calibration Type-B Standard Uncertainty, u(B)

| Zenith Angle (deg.) | R ($\mu\text{V}/\text{W}/\text{m}^2$) | u(B) \pm (%) | Azimuth Angle | R ($\mu\text{V}/\text{W}/\text{m}^2$) | u(B) \pm (%) | Azimuth Angle | Zenith Angle (deg.) | R ($\mu\text{V}/\text{W}/\text{m}^2$) | u(B) \pm (%) | Azimuth Angle | R ($\mu\text{V}/\text{W}/\text{m}^2$) | u(B) \pm (%) | Azimuth Angle |
|---------------------|---|----------------|---------------|---|----------------|---------------|---------------------|---|----------------|---------------|---|----------------|---------------|
| 0 | N/A | N/A | N/A | N/A | N/A | N/A | 46 | 10.574 | 0.31 | 106.81 | 10.635 | 0.32 | 252.87 |
| 2 | N/A | N/A | N/A | N/A | N/A | N/A | 48 | 10.602 | 0.33 | 104.57 | 10.635 | 0.31 | 255.12 |
| 4 | N/A | N/A | N/A | N/A | N/A | N/A | 50 | 10.592 | 0.33 | 102.40 | 10.639 | 0.31 | 257.27 |
| 6 | N/A | N/A | N/A | N/A | N/A | N/A | 52 | 10.594 | 0.32 | 100.41 | 10.648 | 0.34 | 259.28 |
| 8 | N/A | N/A | N/A | N/A | N/A | N/A | 54 | 10.594 | 0.34 | 98.44 | 10.668 | 0.34 | 261.21 |
| 10 | N/A | N/A | N/A | N/A | N/A | N/A | 56 | 10.614 | 0.36 | 96.62 | 10.659 | 0.33 | 263.09 |
| 12 | N/A | N/A | N/A | N/A | N/A | N/A | 58 | 10.633 | 0.34 | 94.78 | 10.670 | 0.34 | 264.95 |
| 14 | N/A | N/A | N/A | N/A | N/A | N/A | 60 | 10.627 | 0.34 | 93.04 | 10.646 | 0.34 | 266.66 |
| 16 | N/A | N/A | N/A | N/A | N/A | N/A | 62 | 10.638 | 0.35 | 91.34 | 10.632 | 0.35 | 268.38 |
| 18 | N/A | N/A | N/A | N/A | N/A | N/A | 64 | 10.614 | 0.42 | 89.66 | 10.686 | 0.37 | 270.08 |
| 20 | N/A | N/A | N/A | N/A | N/A | N/A | 66 | 10.667 | 0.38 | 88.02 | 10.669 | 0.38 | 271.70 |
| 22 | N/A | N/A | N/A | N/A | N/A | N/A | 68 | 10.659 | 0.40 | 86.41 | 10.669 | 0.40 | 273.35 |
| 24 | 10.653 | 0.30 | 167.05 | 10.637 | 0.31 | 193.13 | 70 | 10.722 | 0.46 | 84.81 | 10.709 | 0.42 | 274.98 |
| 26 | 10.684 | 0.30 | 151.01 | 10.666 | 0.31 | 209.20 | 72 | 10.676 | 0.45 | 83.22 | 10.683 | 0.46 | 276.59 |
| 28 | 10.622 | 0.34 | 140.63 | 10.666 | 0.32 | 218.04 | 74 | 10.687 | 0.49 | 81.59 | 10.691 | 0.50 | 278.19 |
| 30 | 10.599 | 0.34 | 134.24 | 10.681 | 0.30 | 224.70 | 76 | 10.744 | 0.59 | 79.98 | 10.733 | 0.56 | 279.78 |
| 32 | 10.606 | 0.32 | 129.36 | 10.681 | 0.32 | 230.04 | 78 | 10.715 | 0.62 | 78.42 | 10.744 | N/A | 281.39 |
| 34 | 10.634 | 0.33 | 124.81 | 10.675 | 0.30 | 234.50 | 80 | 11.039 | N/A | 76.69 | 10.557 | N/A | 283.04 |
| 36 | 10.589 | 0.32 | 120.99 | 10.656 | 0.30 | 238.41 | 82 | N/A | N/A | N/A | 10.684 | N/A | 284.72 |
| 38 | 10.635 | 0.32 | 117.55 | 10.619 | 0.34 | 241.88 | 84 | N/A | N/A | N/A | 10.178 | N/A | 286.64 |
| 40 | 10.621 | 0.34 | 114.56 | 10.653 | 0.31 | 244.98 | 86 | N/A | N/A | N/A | N/A | N/A | N/A |
| 42 | 10.582 | 0.32 | 111.73 | 10.625 | 0.30 | 247.86 | 88 | N/A | N/A | N/A | N/A | N/A | N/A |
| 44 | 10.580 | 0.30 | 109.26 | 10.657 | 0.31 | 250.37 | 90 | N/A | N/A | N/A | N/A | N/A | N/A |

N/A - Not Available

Figure 3. Type-B Standard Uncertainty vs Zenith Angle

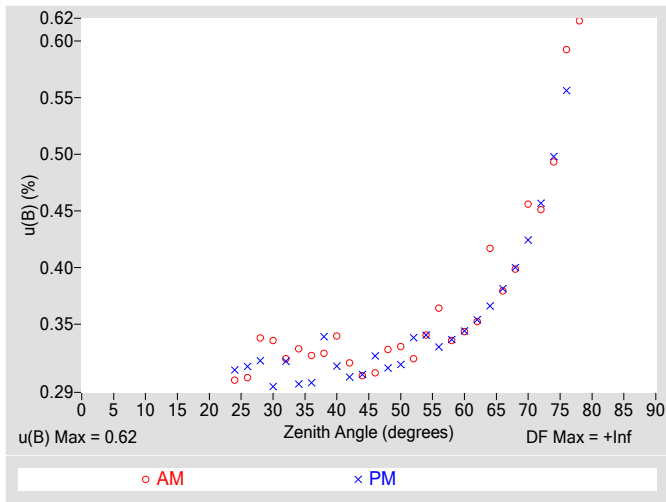


Figure 4. Residuals from Spline Interpolation

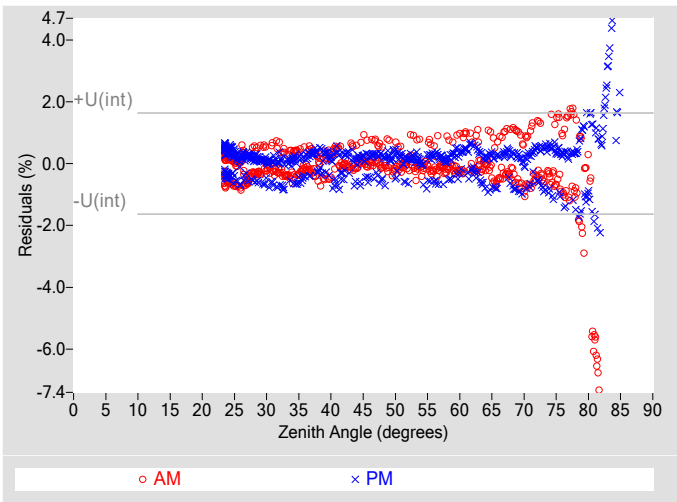


Table 3. Uncertainty using Spline Interpolation ‡

| | |
|---|------------|
| Type-B Standard Uncertainty, $u(B)$ (%) | ± 0.62 |
| Type-A Interpolating Function, $u(int)$ (%) | ± 0.82 |
| Combined Standard Uncertainty, $u(c)$ (%) | ± 1.0 |
| Effective degrees of freedom, $DF(c)$ | 2831 |
| Coverage factor, k | 1.96 |
| Expanded Uncertainty, $U95$ (%) | ± 2.0 |
| AM Valid zenith angle range | 24° to 78° |
| PM Valid zenith angle range | 24° to 76° |

‡ An illustration for how to reduce the uncertainty in calculating the irradiance using a function rather than $R@45^\circ$. Not accredited.

Table 4. Calibration Label Values

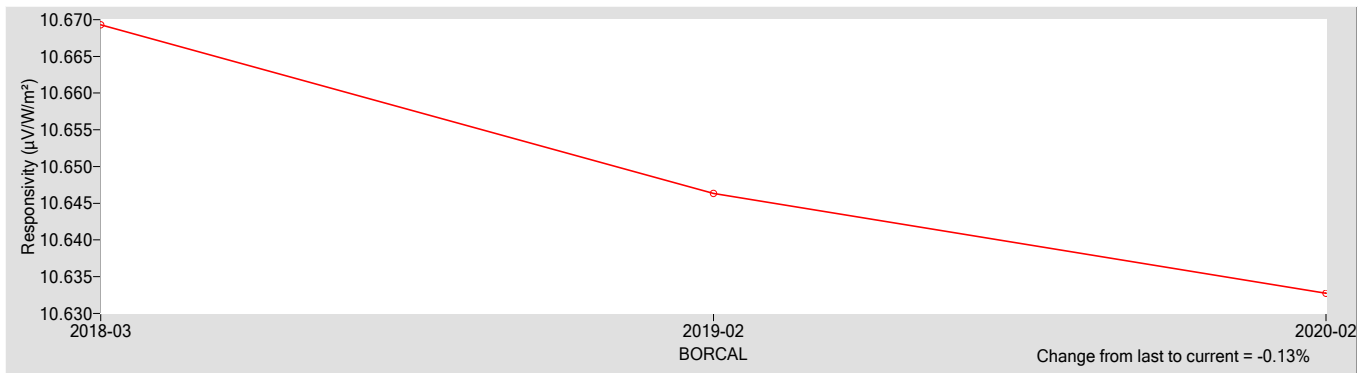
| | |
|----------------------------------|-------------------------------|
| $R @ 45^\circ$ ($\mu V/W/m^2$) | R_{net} ($\mu V/W/m^2$) † |
| 10.633 | 0.043000 |

† R_{net} determination date: Estimated

Table 5. Uncertainty using $R @ 45^\circ$

| | |
|---|----------------|
| Type-B Expanded Uncertainty, $U(B)$ (%) | ± 0.71 |
| Offset Uncertainty, $U(off)$ (%) | +0.45 / -0.56 |
| Expanded Uncertainty, U (%) | +1.2 / -1.3 |
| Effective degrees of freedom, DF | +Inf |
| Coverage factor, k | 1.96 |
| Valid zenith angle range | 30.0° to 60.0° |

Figure 5. History of instrument at Zenith Angle = 45°



References:

- [1] Reda, I.; Hickey, J.; Long, C.; Myers, D.; Stoffel, T.; Wilcox, S.; Michalsky, J. J.; Dutton, E. G.; Nelson, D. (2005). "Using a Blackbody to Calculate Net Longwave Responsivity of Shortwave Solar Pyranometers to Correct for Their Thermal Offset Error During Outdoor Calibration Using the Component Sum Method." *Journal of Atmospheric and Oceanic Technology*, 2005; pp. 1531-1540; NREL Report No. JA-560-36646. doi:10.1175/JTECH1782.1
- [2] Reda, I.; Myers, D.; Stoffel, T. (2008). "Uncertainty Estimate for the Outdoor Calibration of Solar Pyranometers: A Metrologist Perspective." *Measure*. (NCSLI Journal of Measurement Science). Vol. 3(4), December 2008; pp. 58-66; NREL Report No. JA-581-4137
- [3] Reda, I.; Andreas, A. (2004). "Solar Position Algorithm for Solar Radiation Applications." *Solar Energy*. Vol. 76(5), 2004; pp. 577-589; NREL Report No. JA-560-35518. doi:10.1016/j.solener.2003.12.003
- [4] Stoffel, T.; Reda, I. (2009). "NREL Pyrheliometer Comparisons: 22 September - 3 October 2008 (NPC-2008)." 54 pp.; NREL Report No. TP-550-45016.
- [5] Reda, I.; Stoffel, T.; Myers, D. (2003). "Method to Calibrate a Solar Pyranometer for Measuring Reference Diffuse Irradiance." *Solar Energy*. Vol. 74, 2003; pp. 103-112; NREL Report No. JA-560-35025. doi:10.1016/S0038-092X(03)00124-5
- [6] Reda, I. (1996). Calibration of a Solar Absolute Cavity Radiometer with Traceability to the World Radiometric Reference. 79 pp.; NREL Report No. TP-463-20619.
- [7] Reda, I.; Gröbner, J.; Stoffel, T.; Myers, D.; Forgan, B. (2008). Improvements in the Blackbody Calibration of Pyrgometers. ARM 2008 Science Team Meeting (Poster).



National Renewable Energy Laboratory

Solar Radiation Research Laboratory

Metrology Laboratory

Calibration Certificate



| | | | |
|--------------------------|---------------|----------------------------------|------------|
| Test Instrument: | Pyrheliometer | Manufacturer: | EKO |
| Model: | MS-57 | Serial Number: | S18015.22 |
| Calibration Date: | 5/5/2020 | Due Date: | 5/5/2021 |
| Customer: | NREL-SRRL-BMS | Environmental Conditions: | see page 4 |
| Test Dates: | 5/4-5 | | |

This certifies that the above product was calibrated in compliance with ISO/IEC 17025:2017. Measurement uncertainties at the time of calibration are consistent with the Guide to the Expression of Uncertainty in Measurement (GUM) using Reda et al., 2008. All nominal values are traceable to the International System (SI) Units of Measurement.

No statement of compliance with specifications is made or implied on this certificate. However, the estimated uncertainties are the uncertainties of the calibration process; users must add other uncertainties that are relevant to their measuring system, environmental and sky conditions, outdoor set-up, and site location.

The Type-B Standard Uncertainty of using the responsivity at each even zenith angle is reported, and the Expanded Uncertainty of the calibration is reported using two methods:

1. The Expanded Uncertainty of using the responsivity at zenith angle = 45°, within the zenith angle range from 30.0° to 60.0°
2. The Expanded Uncertainty of using Spline Interpolating Functions for the responsivity versus zenith angle.

This certificate applies only to the item identified above and shall not be reproduced other than in full, without specific written approval from the calibration facility. Certificate without signature is not valid.

Table 1. Traceability

| Measurement Type | Instrument | Calibration Date | Calibration Due Date |
|----------------------|--|------------------|----------------------|
| Beam Irradiance † | Eppley Absolute Cavity Radiometer Model HF, S/N 29219 | 09/27/2019 | 09/27/2020 |
| Diffuse Irradiance † | Hukseflux Pyranometer Model SR25, S/N 2541 | 04/17/2020 | 04/17/2021 |
| Diffuse Irradiance † | Hukseflux Pyranometer Model SR25, S/N 2542 | 04/17/2020 | 04/17/2021 |
| Data Acquisition | NREL Data Acquisition System Model RAP-DAQ, S/N 2005-998 | 02/14/2019 | 02/14/2021 |
| Data Acquisition | NREL Data Acquisition System Model RAP-DAQ, S/N 2005-999 | 02/14/2019 | 02/14/2021 |

† Through the World Radiometric Reference (WRR)

Number of pages of certificate: 4

Calibration Procedure: BORCAL-P00-Calibration and QA Procedure; available upon request.

Setup: Radiometers are calibrated outdoors, using the sun as the source. Pyranometers and pyrgeometers are installed for horizontal measurements, with their signal connectors oriented north, if their design permits.

The shading disk for the reference diffuse subtends a solid angle of 5°. Pyrheliometers are installed on solar trackers.

Calibrated by: Afshin Andreas, Ibrahim Reda, Peter Gotseff, and RCC

Ibrahim Reda, Technical Manager

Date

For questions or comments, please contact the technical manager at:

ibrahim.reda@nrel.gov; 303-384-6385; 15013 Denver West Parkway, Golden, CO 80401, USA

Calibration Results

S18015.22 EKO MS-57

The responsivity (R , $\mu\text{V}/\text{W}/\text{m}^2$) of the test instrument during calibration is calculated using this Measurement Equation:

$$R = (V - R_{net} * W_{net}) / I \tag{1}$$

where,

- V = radiometer output voltage (microvolts),
 - R_{net} = radiometer net infrared responsivity ($\mu\text{V}/\text{W}/\text{m}^2$), see Table 4,
 - W_{net} = effective net infrared measured by pyrgeometer (W/m^2),
 - = $W_{in} - W_{out} = W_{in} - \sigma * T_c^4$
 - where, W_{in} = incoming infrared (W/m^2), $\sigma = 5.6704\text{e-}8 \text{ W}\cdot\text{m}^{-2}\cdot\text{K}^{-4}$,
 - T_c = case temperature of pyrgeometer (K).
- I = reference irradiance (W/m^2), beam (B) or global (G)
 - where, $G = B * \text{COS}(Z) + D$,
 - Z = zenith angle (degrees),
 - D = reference diffuse irradiance (W/m^2).

Figure 1. Responsivity vs Zenith Angle

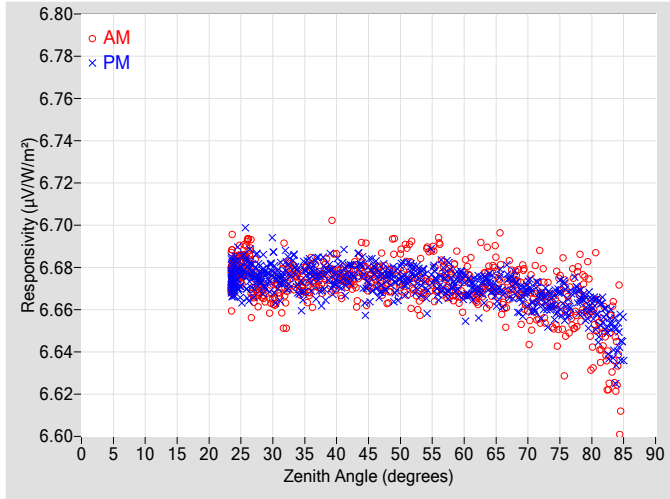


Figure 2. Responsivity vs Local Standard Time

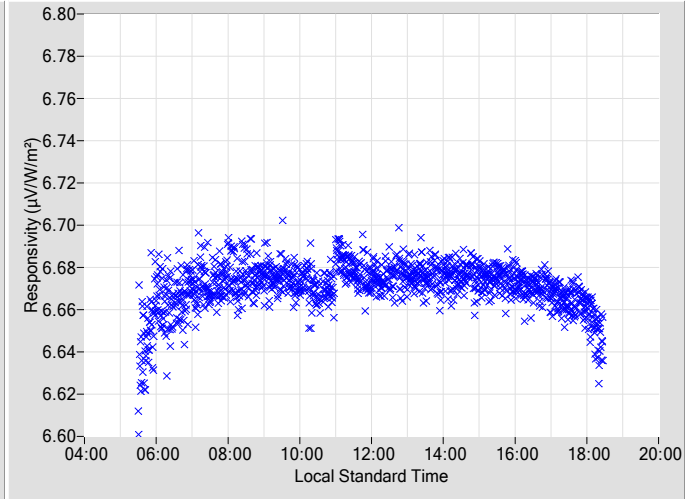


Table 2. Instrument Responsivity (R) and Calibration Type-B Standard Uncertainty, u(B)

| Zenith Angle (deg.) | R ($\mu\text{V}/\text{W}/\text{m}^2$) | u(B) \pm (%) | Azimuth Angle | R ($\mu\text{V}/\text{W}/\text{m}^2$) | u(B) \pm (%) | Azimuth Angle | Zenith Angle (deg.) | R ($\mu\text{V}/\text{W}/\text{m}^2$) | u(B) \pm (%) | Azimuth Angle | R ($\mu\text{V}/\text{W}/\text{m}^2$) | u(B) \pm (%) | Azimuth Angle |
|---------------------|---|----------------|---------------|---|----------------|---------------|---------------------|---|----------------|---------------|---|----------------|---------------|
| 0 | N/A | N/A | N/A | N/A | N/A | N/A | 46 | 6.6780 | 0.29 | 106.81 | 6.6780 | 0.30 | 252.80 |
| 2 | N/A | N/A | N/A | N/A | N/A | N/A | 48 | 6.6682 | 0.29 | 104.53 | 6.6753 | 0.30 | 255.05 |
| 4 | N/A | N/A | N/A | N/A | N/A | N/A | 50 | 6.6768 | 0.30 | 102.45 | 6.6773 | 0.29 | 257.21 |
| 6 | N/A | N/A | N/A | N/A | N/A | N/A | 52 | 6.6759 | 0.31 | 100.41 | 6.6763 | 0.29 | 259.27 |
| 8 | N/A | N/A | N/A | N/A | N/A | N/A | 54 | 6.6771 | 0.30 | 98.49 | 6.6688 | 0.29 | 261.26 |
| 10 | N/A | N/A | N/A | N/A | N/A | N/A | 56 | 6.6833 | 0.29 | 96.61 | 6.6695 | 0.29 | 263.13 |
| 12 | N/A | N/A | N/A | N/A | N/A | N/A | 58 | 6.6714 | 0.32 | 94.78 | 6.6728 | 0.30 | 264.90 |
| 14 | N/A | N/A | N/A | N/A | N/A | N/A | 60 | 6.6724 | 0.32 | 93.04 | 6.6687 | 0.30 | 266.70 |
| 16 | N/A | N/A | N/A | N/A | N/A | N/A | 62 | 6.6649 | 0.31 | 91.33 | 6.6720 | 0.30 | 268.33 |
| 18 | N/A | N/A | N/A | N/A | N/A | N/A | 64 | 6.6714 | 0.31 | 89.66 | 6.6720 | 0.30 | 270.08 |
| 20 | N/A | N/A | N/A | N/A | N/A | N/A | 66 | 6.6660 | 0.32 | 88.02 | 6.6685 | 0.30 | 271.70 |
| 22 | N/A | N/A | N/A | N/A | N/A | N/A | 68 | 6.6739 | 0.30 | 86.40 | 6.6732 | 0.30 | 273.39 |
| 24 | 6.6766 | 0.29 | 166.93 | 6.6737 | 0.30 | 192.72 | 70 | 6.6613 | 0.30 | 84.81 | 6.6702 | 0.30 | 274.97 |
| 26 | 6.6876 | 0.30 | 151.14 | 6.6756 | 0.30 | 209.18 | 72 | 6.6659 | 0.30 | 83.21 | 6.6636 | 0.31 | 276.58 |
| 28 | 6.6686 | 0.30 | 140.90 | 6.6767 | 0.30 | 218.15 | 74 | 6.6596 | 0.31 | 81.59 | 6.6634 | 0.31 | 278.18 |
| 30 | 6.6678 | 0.31 | 134.48 | 6.6817 | 0.30 | 224.69 | 76 | 6.6571 | 0.31 | 80.02 | 6.6610 | 0.31 | 279.82 |
| 32 | 6.6693 | 0.31 | 129.18 | 6.6779 | 0.29 | 230.13 | 78 | 6.6726 | 0.32 | 78.37 | 6.6646 | N/A | 281.43 |
| 34 | 6.6739 | 0.30 | 124.80 | 6.6732 | 0.29 | 234.40 | 80 | 6.6425 | N/A | 76.77 | 6.6616 | N/A | 283.07 |
| 36 | 6.6726 | 0.31 | 120.98 | 6.6767 | 0.31 | 238.46 | 82 | 6.6479 | N/A | 75.12 | 6.6567 | N/A | 284.72 |
| 38 | 6.6768 | 0.31 | 117.62 | 6.6743 | 0.32 | 241.82 | 84 | 6.6391 | N/A | 73.41 | 6.6422 | N/A | 286.37 |
| 40 | 6.6755 | 0.29 | 114.48 | 6.6773 | 0.29 | 244.97 | 86 | N/A | N/A | N/A | N/A | N/A | N/A |
| 42 | 6.6754 | 0.31 | 111.80 | 6.6775 | 0.29 | 247.78 | 88 | N/A | N/A | N/A | N/A | N/A | N/A |
| 44 | 6.6812 | 0.30 | 109.13 | 6.6783 | 0.29 | 250.43 | 90 | N/A | N/A | N/A | N/A | N/A | N/A |

N/A - Not Available

Figure 3. Type-B Standard Uncertainty vs Zenith Angle

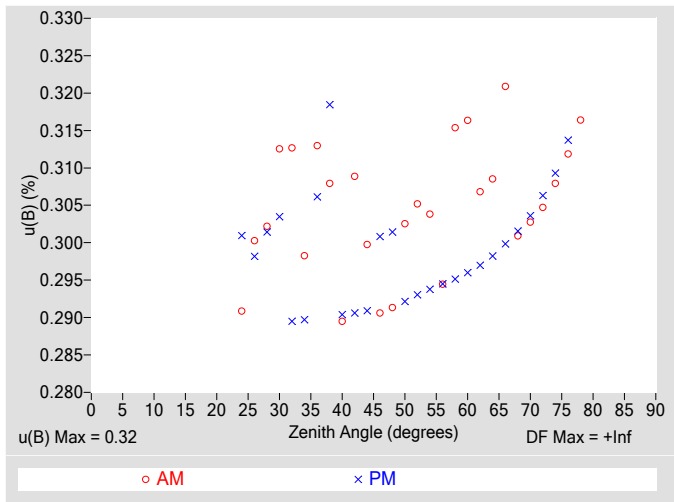


Figure 4. Residuals from Spline Interpolation

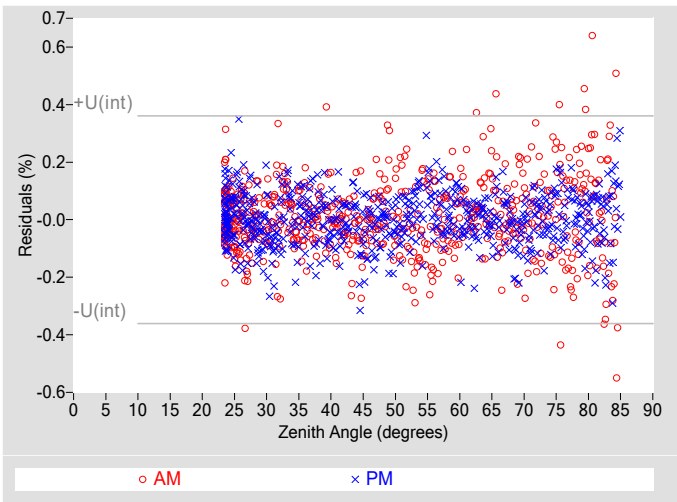


Table 3. Uncertainty using Spline Interpolation ‡

| | |
|---|------------|
| Type-B Standard Uncertainty, $u(B)$ (%) | ± 0.32 |
| Type-A Interpolating Function, $u(int)$ (%) | ± 0.18 |
| Combined Standard Uncertainty, $u(c)$ (%) | ± 0.37 |
| Effective degrees of freedom, $DF(c)$ | 19866 |
| Coverage factor, k | 1.96 |
| Expanded Uncertainty, U_{95} (%) | ± 0.72 |
| AM Valid zenith angle range | 24° to 78° |
| PM Valid zenith angle range | 24° to 76° |

‡ An illustration for how to reduce the uncertainty in calculating the irradiance using a function rather than $R@45^\circ$. Not accredited.

Table 4. Calibration Label Values

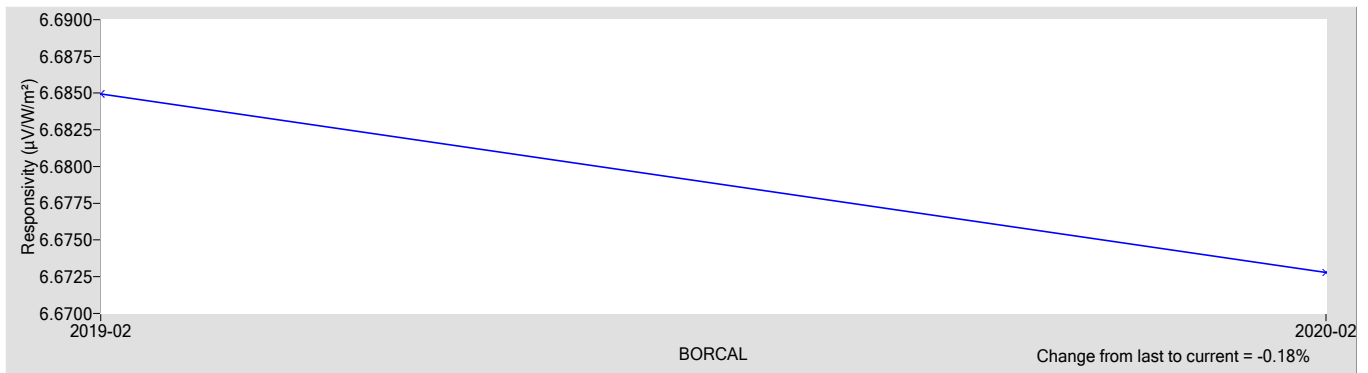
| | |
|----------------------------------|-------------------------------|
| $R @ 45^\circ$ ($\mu V/W/m^2$) | R_{net} ($\mu V/W/m^2$) † |
| 6.6728 | 0 |

† R_{net} determination date: N/A

Table 5. Uncertainty using $R @ 45^\circ$

| | |
|---|----------------|
| Type-B Expanded Uncertainty, $U(B)$ (%) | ± 0.62 |
| Offset Uncertainty, $U(off)$ (%) | +0.16 / -0.075 |
| Expanded Uncertainty, U (%) | +0.78 / -0.70 |
| Effective degrees of freedom, DF | +Inf |
| Coverage factor, k | 1.96 |
| Valid zenith angle range | 30.0° to 60.0° |

Figure 5. History of instrument at Zenith Angle = 45°



References:

- [1] Reda, I.; Hickey, J.; Long, C.; Myers, D.; Stoffel, T.; Wilcox, S.; Michalsky, J. J.; Dutton, E. G.; Nelson, D. (2005). "Using a Blackbody to Calculate Net Longwave Responsivity of Shortwave Solar Pyranometers to Correct for Their Thermal Offset Error During Outdoor Calibration Using the Component Sum Method." *Journal of Atmospheric and Oceanic Technology*, 2005; pp. 1531-1540; NREL Report No. JA-560-36646. doi:10.1175/JTECH1782.1
- [2] Reda, I.; Myers, D.; Stoffel, T. (2008). "Uncertainty Estimate for the Outdoor Calibration of Solar Pyranometers: A Metrologist Perspective." *Measure*. (NCSLI *Journal of Measurement Science*). Vol. 3(4), December 2008; pp. 58-66; NREL Report No. JA-581-4137
- [3] Reda, I.; Andreas, A. (2004). "Solar Position Algorithm for Solar Radiation Applications." *Solar Energy*. Vol. 76(5), 2004; pp. 577-589; NREL Report No. JA-560-35518. doi:10.1016/j.solener.2003.12.003
- [4] Stoffel, T.; Reda, I. (2009). "NREL Pyrheliometer Comparisons: 22 September - 3 October 2008 (NPC-2008)." 54 pp.; NREL Report No. TP-550-45016.
- [5] Reda, I.; Stoffel, T.; Myers, D. (2003). "Method to Calibrate a Solar Pyranometer for Measuring Reference Diffuse Irradiance." *Solar Energy*. Vol. 74, 2003; pp. 103-112; NREL Report No. JA-560-35025. doi:10.1016/S0038-092X(03)00124-5
- [6] Reda, I. (1996). *Calibration of a Solar Absolute Cavity Radiometer with Traceability to the World Radiometric Reference*. 79 pp.; NREL Report No. TP-463-20619.
- [7] Reda, I.; Gröbner, J.; Stoffel, T.; Myers, D.; Forgan, B. (2008). *Improvements in the Blackbody Calibration of Pyrgometers*. ARM 2008 Science Team Meeting (Poster).

Environmental and Sky Conditions for BORCAL-SW 2020-02

Calibration Facility: Solar Radiation Research Laboratory

Latitude: 39.742°N

Longitude: 105.180°W

Elevation: 1828.8 meters AMSL

Time Zone: -7.0

Reference Irradiance:

Figure 6. Reference Irradiance

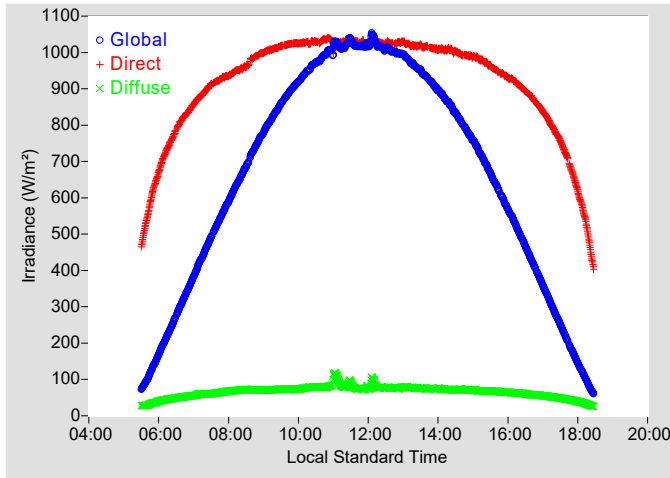
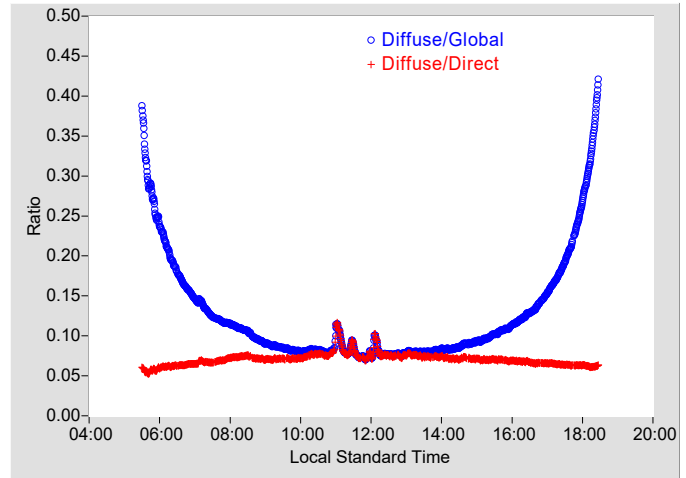


Figure 7. Diffuse Ratios



Meteorological Observations:

Figure 8. Temperature

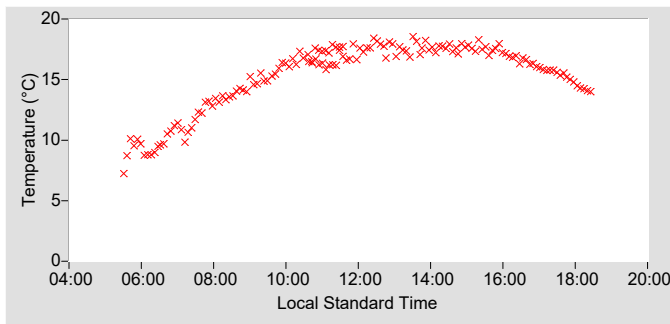


Figure 9. Humidity

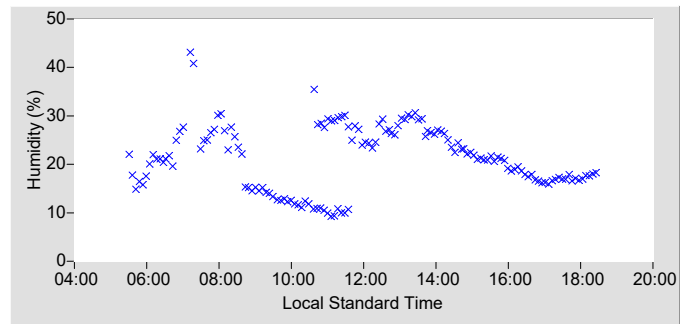


Figure 10. Pressure

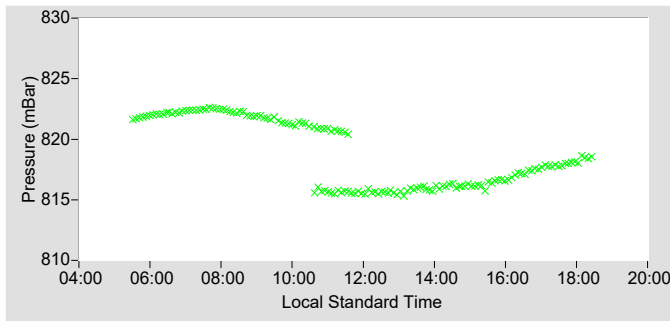


Figure 11. Effective Net Infrared

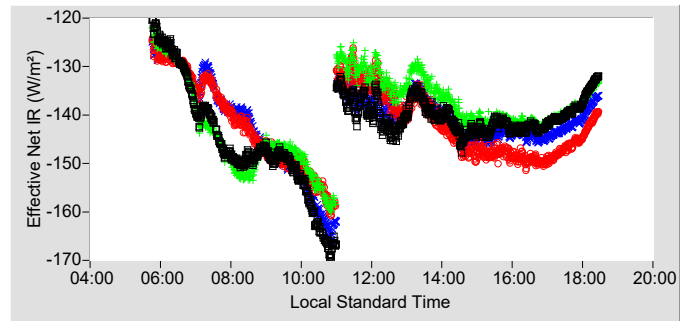
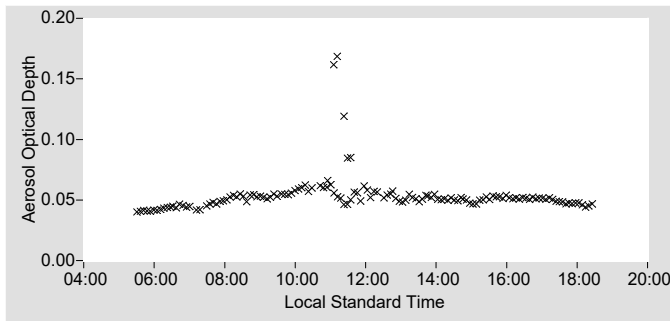


Figure 12. Estimated Broadband Aerosol Optical Depth



× 140021 ○ 31203F3 + 32309F3 □ FT002

Table 6. Meteorological Observations

| Observations | Mean | Min | Max |
|---------------------------------|-------|-------|-------|
| Temperature (°C) | 15.40 | 7.23 | 18.54 |
| Humidity (%) | 21.22 | 9.24 | 43.11 |
| Pressure (mBar) | 818.7 | 815.3 | 822.6 |
| Est. Aerosol Optical Depth (BB) | 0.053 | 0.040 | 0.168 |

For other information about the calibration facility visit: <http://www.nrel.gov/esif/solar-radiation-research-laboratory.html>

Appendix 2

BORCAL Notes

Instrument, Configuration, and Session Notes for the BORCAL

BORCAL Notes

Facility: Solar Radiation Research Laboratory

Comments:

Avg. Station Pressure & Temperature is for Denver, CO, which is used for the Solar Position Algorithm (SPA).

010284-DW-CM3 Kipp & Zonen CM3

Comments:

Retro-fitted from CNR1

Session Config: 1171 Apogee SP-510; Number: 2

Comments:

30K Thermistor measured by spare SP-510 pyrgeometer mounted next to pyranometer.
