

# Broadband Outdoor Radiometer Calibration Shortwave

## BORCAL-SW 2019-02

Generated by



*Radiometer Calibration and Characterization*

### Customer

**NREL-SRRL-BMS**

Organization: NREL

Address: BMS, SRRL, Golden, CO 80401 USA

Phone: 303-384-6326

### Calibration Facility

**Solar Radiation Research Laboratory**

Latitude: 39.742°N

Longitude: 105.180°W

Elevation: 1828.8 meters AMSL

Time Zone: -7.0

Calibration date

05/03/2019

Report Date

May 6, 2019



## **NOTICE**

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# Broadband Outdoor Radiometer Calibration Report

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# Introduction

This report compiles the calibration results from a Broadband Outdoor Radiometer Calibration (BORCAL). The work was accomplished at the Radiometer Calibration Facility shown on the front of this report. The calibration results reported here are traceable to the International System (SI) Units of Measurement.

This report includes these sections:

- Control Instruments - a group of instruments included in each BORCAL event that provides a measure of process consistency.
- Results Summary - a table of all instruments included in this report summarizing their calibration results and uncertainty.
- Instrument Details - the calibration certificates for each instrument.
- Environmental and Sky Conditions - meteorological conditions and reference irradiance during the calibration event.



# Control Instrument History

Figure 1. Eppley NIP Control Instrument History

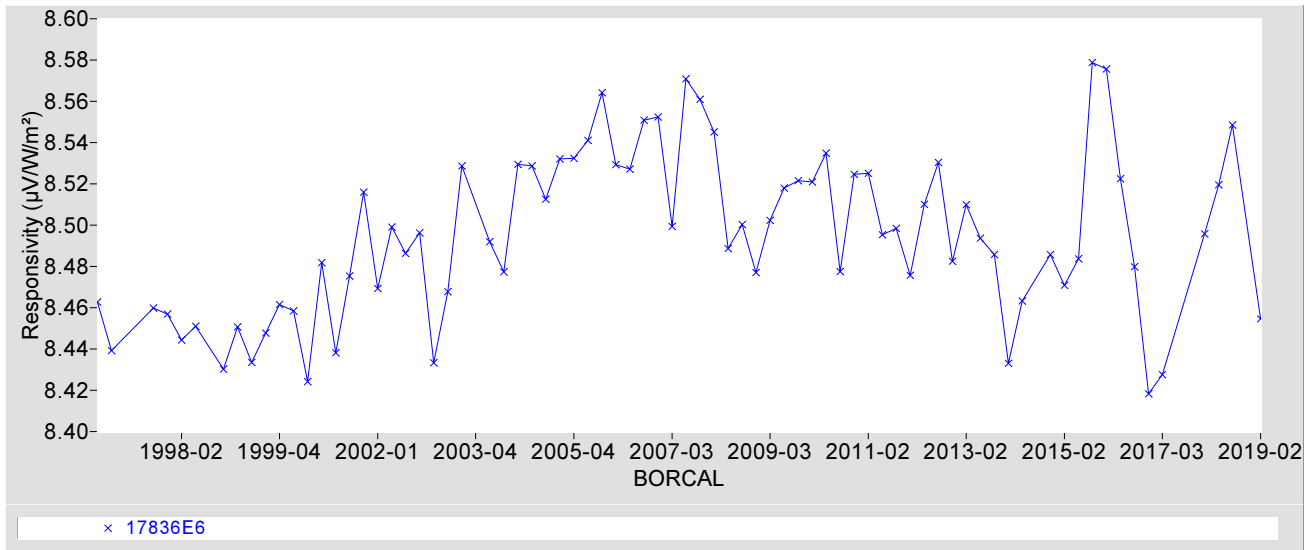
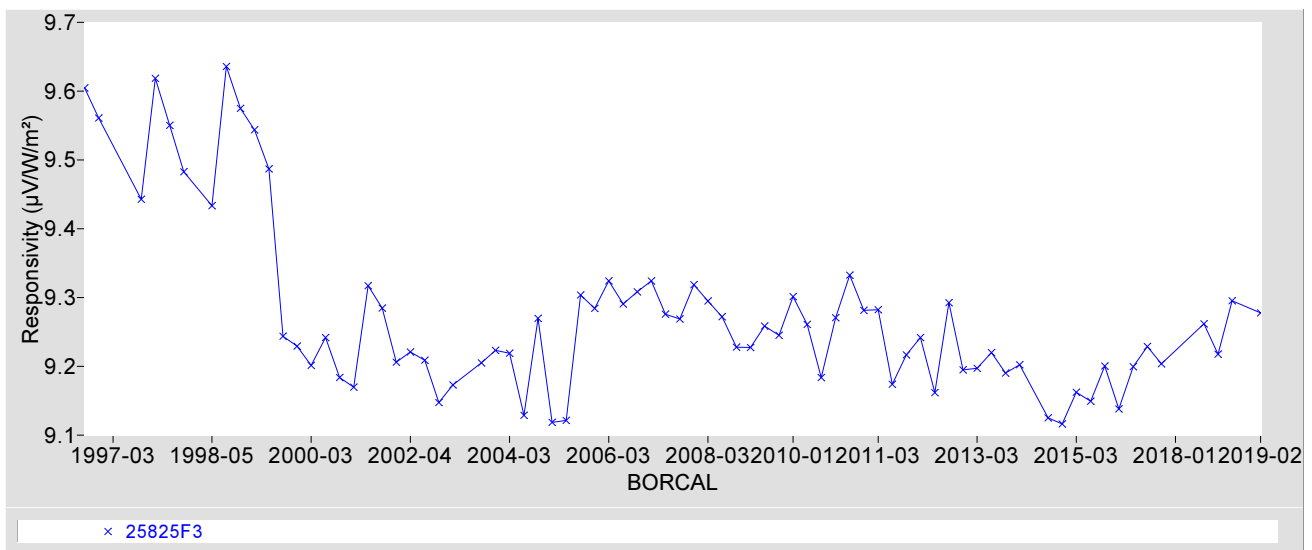


Figure 2. Eppley PSP Control Instrument History



# Results Summary

**Table 1. Results Summary**

Instrument	R@45 <sup>1</sup> ( $\mu\text{V}/\text{W}/\text{m}^2$ )	CF@45 <sup>1</sup> ( $\text{W}/\text{m}^2/\text{mV}$ )	U <sup>2</sup> (%)	Rnet <sup>3</sup> ( $\mu\text{V}/\text{W}/\text{m}^2$ )	Page
010047 Kipp & Zonen CM22	9.7805	102.24	+1.8 / -1.4	0.087000	A1-2
014261 Kipp & Zonen CM3	22.202	45.041	+2.9 / -2.8	0.40000	A1-5
015189 Kipp & Zonen CM6B	10.980	91.072	+2.3 / -2.1	0.30000	A1-8
0212-2 Yankee TSP-700	3003.2	0.33298	+2.2 / -2.3	0	A1-11
080009 Kipp & Zonen CHP1	7.9357	126.01	+1.2 / -0.76	0	A1-14
080017 Kipp & Zonen CMP22	10.547	94.818	+1.5 / -1.6	0.087000	A1-17
100174 Kipp & Zonen CMP22	9.8283	101.75	+2.1 / -1.5	0.087000	A1-20
1171 Apogee SP-510	53.551	18.674	+2.8 / -5.0	2.5000	A1-23
140043 Kipp & Zonen CMP22	9.0682	110.28	+2.3 / -1.4	0.087000	A1-26
140108 Kipp & Zonen CHP1	8.0759	123.82	+0.84 / -0.89	0	A1-29
140712 Kipp & Zonen CMP11	9.1157	109.70	+1.5 / -2.3	0.20500	A1-32
151027 Kipp & Zonen SP-LITE2	69.571	14.374	+3.6 / -2.4	0	A1-35
170535 Kipp & Zonen CMP22	9.5974	104.20	+2.0 / -2.4	0.087000	A1-38
2529 Hukseflux SR25	9.3822	106.59	+2.4 / -1.4	0.043000	A1-41
2543 Hukseflux SR25	9.5401	104.82	+2.1 / -1.4	0.043000	A1-44
28402F3 Eppley PSP	6.9865	143.13	+2.4 / -2.2	0.64000	A1-47
31137E6 Eppley NIP	8.4944	117.73	+1.4 / -1.5	0	A1-50
32331 Eppley 8-48	8.9438	111.81	+4.5 / -2.4	0	A1-53
34718 Eppley 8-48	9.3855	106.55	+3.7 / -2.1	0	A1-56
37831F3 Eppley GPP	8.4828	117.89	+2.2 / -2.9	0.15000	A1-59
37839F3 Eppley SPP	8.6758	115.26	+1.8 / -2.2	0.30000	A1-62
37882E6 Eppley sNIP	8.4047	118.98	+0.71 / -1.1	0	A1-65
40337 Apogee SP-110	184.41	5.4226	+2.5 / -2.4	0	A1-68
9206 Hukseflux DR02	11.019	90.754	+1.6 / -0.88	0	A1-71
A360 Delta-T SPN1	1027.5	0.97320	+8.3 / -3.8	0	A1-74
F14077R EKO MS-802	7.0776	141.29	+2.3 / -2.1	0.18000	A1-77
PY100360 Licor LI200R	10.882	91.897	+1.6 / -1.7	0	A1-80
PY102022 Licor LI200R	10.652	93.879	+1.5 / -1.8	0	A1-83
PY28257 Licor LI200	13.817	72.373	+2.1 / -2.9	0	A1-86
PYHR101 Licor LI201SB	6.7215	148.78	+4.7 / -1.9	0	A1-89
S13071483 EKO MS-602	7.0025	142.81	+2.0 / -4.1	0.30000	A1-92
S13135063 EKO ML-01	40.604	24.628	+2.3 / -1.3	0	A1-95
S13144.085R EKO MS-410	9.3100	107.41	+2.1 / -1.5	0.20000	A1-98
S17096005 EKO MS-80	10.646	93.929	+2.4 / -1.3	0.043000	A1-101
S18015.22 EKO MS-57	6.6849	149.59	+0.88 / -0.87	0	A1-104

<sup>1</sup> CF = 1000 / R

<sup>2</sup> See certificate for valid zenith angle range

<sup>3</sup> Instrument's Effective Net IR Response

Note: Environmental Conditions for BORCAL starts on page A1-107.

# Appendix 1

## Instrument Details

Calibration Certificates: 3 pages for each radiometer (4 including Environmental Conditions)

Environmental Conditions for BORCAL: Last Page of a Calibration Certificate. Note: This appears only once, at the end of Appendix 1.



# National Renewable Energy Laboratory

## Solar Radiation Research Laboratory

### Metrology Laboratory

### Calibration Certificate



<b>Test Instrument:</b>	Pyranometer (Ventilated)	<b>Manufacturer:</b>	Kipp & Zonen
<b>Model:</b>	CM22	<b>Serial Number:</b>	010047
<b>Calibration Date:</b>	5/3/2019	<b>Due Date:</b>	5/3/2020
<b>Customer:</b>	NREL-SRRL-BMS	<b>Environmental Conditions:</b>	see page 4
<b>Test Dates:</b>	5/3		

This certifies that the above product was calibrated in compliance with ISO/IEC 17025:2005. Measurement uncertainties at the time of calibration are consistent with the Guide to the Expression of Uncertainty in Measurement (GUM) using Reda et al., 2008. All nominal values are traceable to the International System (SI) Units of Measurement.

No statement of compliance with specifications is made or implied on this certificate. However, the estimated uncertainties are the uncertainties of the calibration process; users must add other uncertainties that are relevant to their measuring system, environmental and sky conditions, outdoor set-up, and site location.

The Type-B Standard Uncertainty of using the responsivity at each even zenith angle is reported, and the Expanded Uncertainty of the calibration is reported using two methods:

1. The Expanded Uncertainty of using the responsivity at zenith angle = 45°, within the zenith angle range from 30.0° to 60.0°
2. The Expanded Uncertainty of using Spline Interpolating Functions for the responsivity versus zenith angle.

This certificate applies only to the item identified above and shall not be reproduced other than in full, without specific written approval from the calibration facility. Certificate without signature is not valid.

**Table 1. Traceability**

Measurement Type	Instrument	Calibration Date	Calibration Due Date
Beam Irradiance †	Eppley Absolute Cavity Radiometer Model HF, S/N 29219	09/24/2018	09/24/2019
Diffuse Irradiance †	Hukseflux Pyranometer Model SR25, S/N 2541	04/19/2019	04/19/2020
Diffuse Irradiance †	Hukseflux Pyranometer Model SR25, S/N 2542	04/19/2019	04/19/2020
Data Acquisition	NREL Data Acquisition System Model RAP-DAQ, S/N 2005-998	02/14/2019	02/14/2021
Data Acquisition	NREL Data Acquisition System Model RAP-DAQ, S/N 2005-999	02/14/2019	02/14/2021
Infrared Irradiance ‡	Kipp & Zonen Pyrgeometer Model CGR4, S/N 140021	04/02/2019	04/02/2023

† Through the World Radiometric Reference (WRR)

‡ Through the World Infrared Standard Group (WISG)

**Number of pages of certificate:** 4

**Calibration Procedure:** BORCAL-P00-Calibration and QA Procedure; available upon request.

**Setup:** Radiometers are calibrated outdoors, using the sun as the source. Pyranometers and pyrgeometers are installed for horizontal measurements, with their signal connectors oriented north, if their design permits.

The shading disk for the reference diffuse subtends a solid angle of 5°. Pyrheliometers are installed on solar trackers.

**Calibrated by:** RCC

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Ibrahim Reda, Technical Manager

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Date

For questions or comments, please contact the technical manager at:

ibrahim.reda@nrel.gov; 303-384-6385; 15013 Denver West Parkway, Golden, CO 80401, USA

# Calibration Results

## 010047 Kipp & Zonen CM22

The responsivity ( $R$ ,  $\mu\text{V}/\text{W}/\text{m}^2$ ) of the test instrument during calibration is calculated using this Measurement Equation:

$$R = (V - R_{net} * W_{net}) / I \tag{1}$$

where,

- $V$  = radiometer output voltage (microvolts),
  - $R_{net}$  = radiometer net infrared responsivity ( $\mu\text{V}/\text{W}/\text{m}^2$ ), see Table 4,
  - $W_{net}$  = effective net infrared measured by pyrgeometer ( $\text{W}/\text{m}^2$ ),
  - =  $W_{in} - W_{out} = W_{in} - \sigma * T_c^4$
  - where,  $W_{in}$  = incoming infrared ( $\text{W}/\text{m}^2$ ),  $\sigma = 5.6704\text{e-}8 \text{ W}\cdot\text{m}^{-2}\cdot\text{K}^{-4}$ ,
  - $T_c$  = case temperature of pyrgeometer (K).
- $I$  = reference irradiance ( $\text{W}/\text{m}^2$ ), beam (B) or global (G)
  - where,  $G = B * \text{COS}(Z) + D$ ,
  - $Z$  = zenith angle (degrees),
  - $D$  = reference diffuse irradiance ( $\text{W}/\text{m}^2$ ).

Figure 1. Responsivity vs Zenith Angle

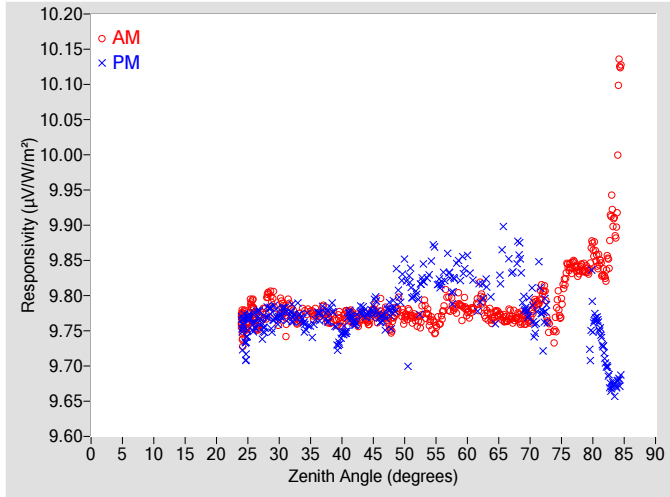


Figure 2. Responsivity vs Local Standard Time

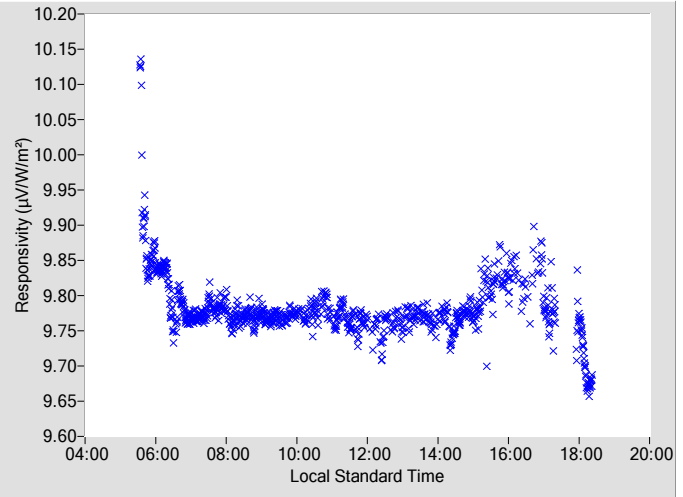


Table 2. Instrument Responsivity (R) and Calibration Type-B Standard Uncertainty, u(B)

Zenith Angle (deg.)	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	AM u(B) $\pm$ (%)	Azimuth Angle	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	PM u(B) $\pm$ (%)	Azimuth Angle	Zenith Angle (deg.)	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	AM u(B) $\pm$ (%)	Azimuth Angle	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	PM u(B) $\pm$ (%)	Azimuth Angle
0	N/A	N/A	N/A	N/A	N/A	N/A	46	9.7783	0.34	108.16	9.7673	0.38	251.95
2	N/A	N/A	N/A	N/A	N/A	N/A	48	9.7580	0.35	105.90	9.7751	0.39	254.15
4	N/A	N/A	N/A	N/A	N/A	N/A	50	9.7689	0.36	103.75	9.8361	0.44	256.52
6	N/A	N/A	N/A	N/A	N/A	N/A	52	9.7653	0.37	101.62	9.8009	0.44	258.41
8	N/A	N/A	N/A	N/A	N/A	N/A	54	9.7659	0.38	99.69	9.8393	0.47	260.51
10	N/A	N/A	N/A	N/A	N/A	N/A	56	9.7758	0.38	97.74	9.8229	0.50	262.26
12	N/A	N/A	N/A	N/A	N/A	N/A	58	9.7815	0.39	95.95	9.8317	0.51	264.15
14	N/A	N/A	N/A	N/A	N/A	N/A	60	9.7772	0.41	94.21	9.8572	N/A	265.93
16	N/A	N/A	N/A	N/A	N/A	N/A	62	9.7997	0.42	92.43	9.8038	0.51	267.64
18	N/A	N/A	N/A	N/A	N/A	N/A	64	9.7654	0.43	90.79	9.7981	0.53	269.13
20	N/A	N/A	N/A	N/A	N/A	N/A	66	9.7662	0.46	89.11	9.8982	N/A	270.80
22	N/A	N/A	N/A	N/A	N/A	N/A	68	9.7681	0.48	87.49	9.8603	N/A	272.71
24	9.7610	0.32	174.70	9.7565	0.32	187.00	70	9.7679	0.52	85.85	9.7930	N/A	274.28
26	9.7781	0.32	154.04	9.7591	0.32	206.09	72	9.8063	0.57	84.23	9.7647	N/A	275.91
28	9.7892	0.33	144.18	9.7742	0.33	215.96	74	9.7556	0.63	82.66	N/A	N/A	N/A
30	9.7743	0.34	137.18	9.7680	0.34	222.79	76	9.8396	0.69	81.05	N/A	N/A	N/A
32	9.7774	0.33	131.41	9.7728	0.34	228.40	78	9.8388	N/A	79.44	N/A	N/A	N/A
34	9.7803	0.33	127.26	9.7582	0.34	233.04	80	9.8695	N/A	77.79	9.7804	N/A	282.39
36	9.7754	0.33	123.03	9.7724	0.35	237.26	82	9.8324	N/A	76.13	9.7064	N/A	284.05
38	9.7661	0.33	119.43	9.7699	0.35	240.58	84	10.029	N/A	74.47	9.6782	N/A	285.73
40	9.7644	0.33	116.28	9.7450	0.36	243.96	86	N/A	N/A	N/A	N/A	N/A	N/A
42	9.7666	0.34	113.30	9.7608	0.39	246.76	88	N/A	N/A	N/A	N/A	N/A	N/A
44	9.7636	0.34	110.74	9.7737	0.39	249.50	90	N/A	N/A	N/A	N/A	N/A	N/A

N/A - Not Available

Figure 3. Type-B Standard Uncertainty vs Zenith Angle

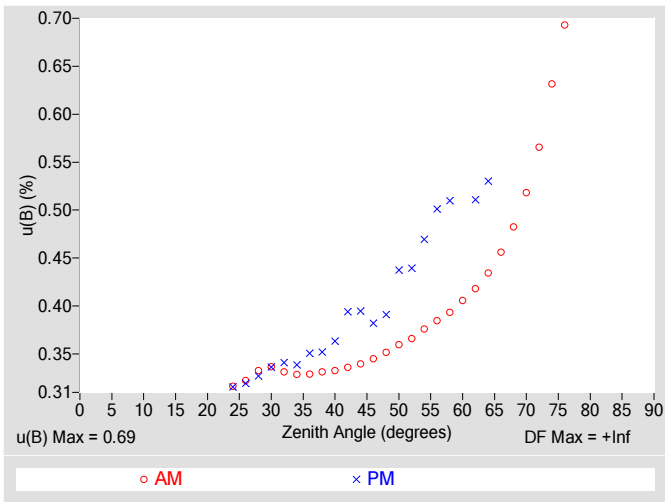


Figure 4. Residuals from Spline Interpolation

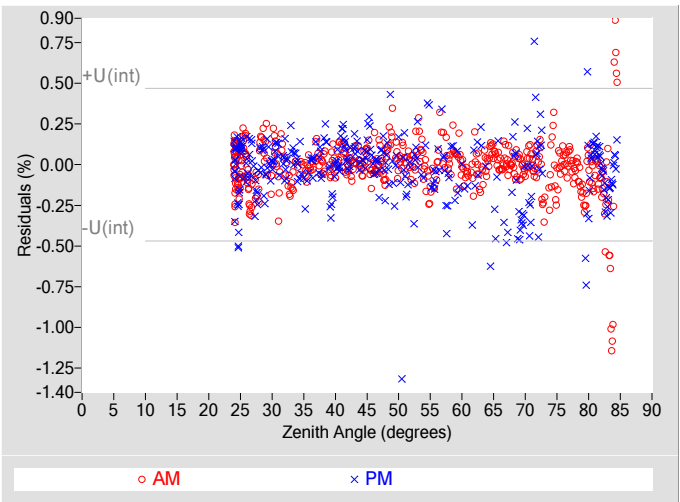


Table 3. Uncertainty using Spline Interpolation ‡

Type-B Standard Uncertainty, $u(B)$ (%)	$\pm 0.69$
Type-A Interpolating Function, $u(int)$ (%)	$\pm 0.23$
Combined Standard Uncertainty, $u(c)$ (%)	$\pm 0.73$
Effective degrees of freedom, $DF(c)$	66528
Coverage factor, $k$	1.96
Expanded Uncertainty, $U95$ (%)	$\pm 1.4$
AM Valid zenith angle range	24° to 76°
PM Valid zenith angle range	24° to 64°

‡ An illustration for how to reduce the uncertainty in calculating the irradiance using a function rather than  $R@45^\circ$ . Not accredited.

Table 4. Calibration Label Values

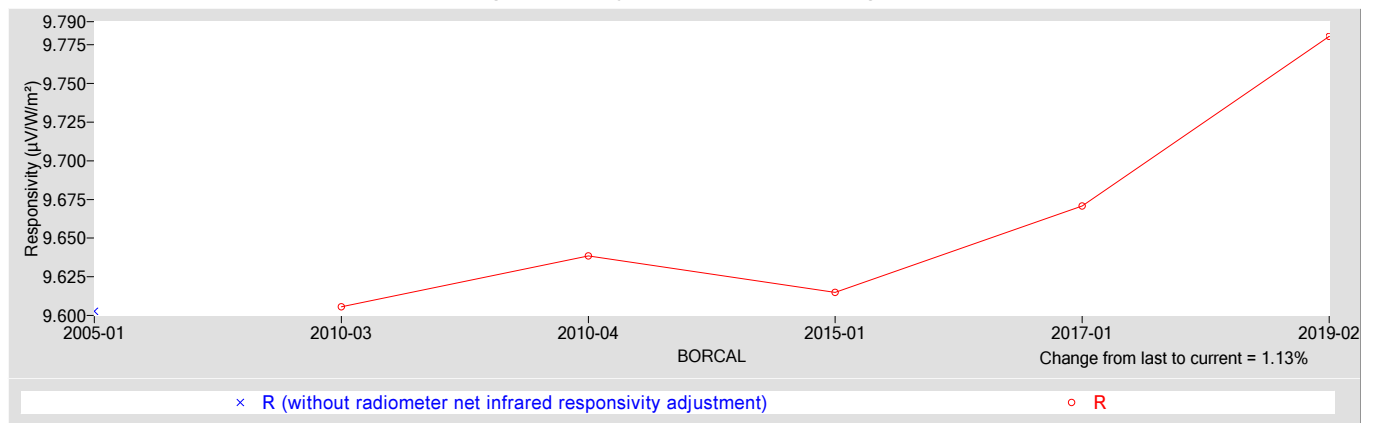
$R @ 45^\circ$ ( $\mu V/W/m^2$ )	$R_{net}$ ( $\mu V/W/m^2$ ) †
9.7805	0.087000

†  $R_{net}$  determination date: Estimated

Table 5. Uncertainty using  $R @ 45^\circ$

Type-B Expanded Uncertainty, $U(B)$ (%)	$\pm 1.00$
Offset Uncertainty, $U(off)$ (%)	+0.78 / -0.36
Expanded Uncertainty, $U$ (%)	+1.8 / -1.4
Effective degrees of freedom, $DF$	+Inf
Coverage factor, $k$	1.96
Valid zenith angle range	30.0° to 60.0°

Figure 5. History of instrument at Zenith Angle = 45°



## References:

- [1] Reda, I.; Hickey, J.; Long, C.; Myers, D.; Stoffel, T.; Wilcox, S.; Michalsky, J. J.; Dutton, E. G.; Nelson, D. (2005). "Using a Blackbody to Calculate Net Longwave Responsivity of Shortwave Solar Pyranometers to Correct for Their Thermal Offset Error During Outdoor Calibration Using the Component Sum Method." *Journal of Atmospheric and Oceanic Technology*, 2005; pp. 1531-1540; NREL Report No. JA-560-36646. doi:10.1175/JTECH1782.1
- [2] Reda, I.; Myers, D.; Stoffel, T. (2008). "Uncertainty Estimate for the Outdoor Calibration of Solar Pyranometers: A Metrologist Perspective." *Measure*. (NCSLI Journal of Measurement Science). Vol. 3(4), December 2008; pp. 58-66; NREL Report No. JA-581-4137
- [3] Reda, I.; Andreas, A. (2004). "Solar Position Algorithm for Solar Radiation Applications." *Solar Energy*. Vol. 76(5), 2004; pp. 577-589; NREL Report No. JA-560-35518. doi:10.1016/j.solener.2003.12.003
- [4] Stoffel, T.; Reda, I. (2009). "NREL Pyrheliometer Comparisons: 22 September - 3 October 2008 (NPC-2008)." 54 pp.; NREL Report No. TP-550-45016.
- [5] Reda, I.; Stoffel, T.; Myers, D. (2003). "Method to Calibrate a Solar Pyranometer for Measuring Reference Diffuse Irradiance." *Solar Energy*. Vol. 74, 2003; pp. 103-112; NREL Report No. JA-560-35025. doi:10.1016/S0038-092X(03)00124-5
- [6] Reda, I. (1996). *Calibration of a Solar Absolute Cavity Radiometer with Traceability to the World Radiometric Reference*. 79 pp.; NREL Report No. TP-463-20619.
- [7] Reda, I.; Gröbner, J.; Stoffel, T.; Myers, D.; Forgan, B. (2008). Improvements in the Blackbody Calibration of Pyrgometers. ARM 2008 Science Team Meeting (Poster).



# National Renewable Energy Laboratory

## Solar Radiation Research Laboratory

### Metrology Laboratory

### Calibration Certificate



<b>Test Instrument:</b>	Pyranometer	<b>Manufacturer:</b>	Kipp & Zonen
<b>Model:</b>	CM3	<b>Serial Number:</b>	014261
<b>Calibration Date:</b>	5/3/2019	<b>Due Date:</b>	5/3/2020
<b>Customer:</b>	NREL-SRRL-BMS	<b>Environmental Conditions:</b>	see page 4
<b>Test Dates:</b>	5/3		

This certifies that the above product was calibrated in compliance with ISO/IEC 17025:2005. Measurement uncertainties at the time of calibration are consistent with the Guide to the Expression of Uncertainty in Measurement (GUM) using Reda et al., 2008. All nominal values are traceable to the International System (SI) Units of Measurement.

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1. The Expanded Uncertainty of using the responsivity at zenith angle = 45°, within the zenith angle range from 30.0° to 60.0°
2. The Expanded Uncertainty of using Spline Interpolating Functions for the responsivity versus zenith angle.

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**Table 1. Traceability**

Measurement Type	Instrument	Calibration Date	Calibration Due Date
Beam Irradiance †	Eppley Absolute Cavity Radiometer Model HF, S/N 29219	09/24/2018	09/24/2019
Diffuse Irradiance †	Hukseflux Pyranometer Model SR25, S/N 2541	04/19/2019	04/19/2020
Diffuse Irradiance †	Hukseflux Pyranometer Model SR25, S/N 2542	04/19/2019	04/19/2020
Data Acquisition	NREL Data Acquisition System Model RAP-DAQ, S/N 2005-998	02/14/2019	02/14/2021
Data Acquisition	NREL Data Acquisition System Model RAP-DAQ, S/N 2005-999	02/14/2019	02/14/2021
Infrared Irradiance ‡	Kipp & Zonen Pyrgeometer Model CG4, S/N FT002	04/16/2018	04/16/2022

† Through the World Radiometric Reference (WRR)

‡ Through the World Infrared Standard Group (WISG)

**Number of pages of certificate:** 4

**Calibration Procedure:** BORCAL-P00-Calibration and QA Procedure; available upon request.

**Setup:** Radiometers are calibrated outdoors, using the sun as the source. Pyranometers and pyrgeometers are installed for horizontal measurements, with their signal connectors oriented north, if their design permits.

The shading disk for the reference diffuse subtends a solid angle of 5°. Pyrheliometers are installed on solar trackers.

**Calibrated by:** RCC

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Ibrahim Reda, Technical Manager

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Date

For questions or comments, please contact the technical manager at:

ibrahim.reda@nrel.gov; 303-384-6385; 15013 Denver West Parkway, Golden, CO 80401, USA

# Calibration Results

## 014261 Kipp & Zonen CM3

The responsivity ( $R$ ,  $\mu\text{V}/\text{W}/\text{m}^2$ ) of the test instrument during calibration is calculated using this Measurement Equation:

$$R = (V - R_{net} * W_{net}) / I \tag{1}$$

where,

- $V$  = radiometer output voltage (microvolts),
  - $R_{net}$  = radiometer net infrared responsivity ( $\mu\text{V}/\text{W}/\text{m}^2$ ), see Table 4,
  - $W_{net}$  = effective net infrared measured by pyrgeometer ( $\text{W}/\text{m}^2$ ),
  - =  $W_{in} - W_{out} = W_{in} - \sigma * T_c^4$
  - where,  $W_{in}$  = incoming infrared ( $\text{W}/\text{m}^2$ ),  $\sigma = 5.6704\text{e-}8 \text{ W}\cdot\text{m}^{-2}\cdot\text{K}^{-4}$ ,
  - $T_c$  = case temperature of pyrgeometer (K).
- $I$  = reference irradiance ( $\text{W}/\text{m}^2$ ), beam (B) or global (G)
  - where,  $G = B * \text{COS}(Z) + D$ ,
  - $Z$  = zenith angle (degrees),
  - $D$  = reference diffuse irradiance ( $\text{W}/\text{m}^2$ ).

Figure 1. Responsivity vs Zenith Angle

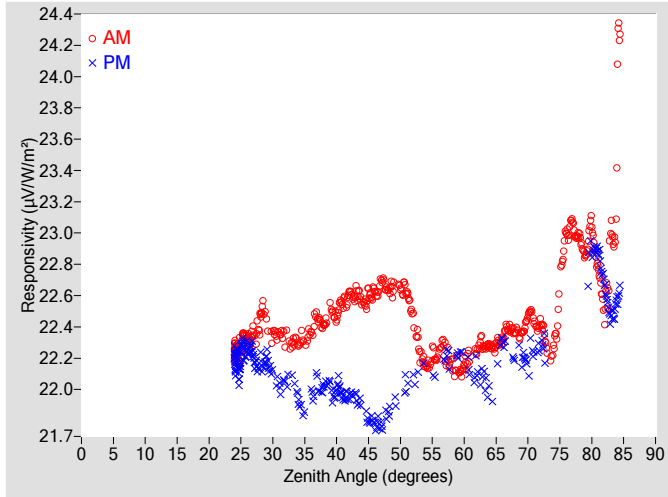


Figure 2. Responsivity vs Local Standard Time

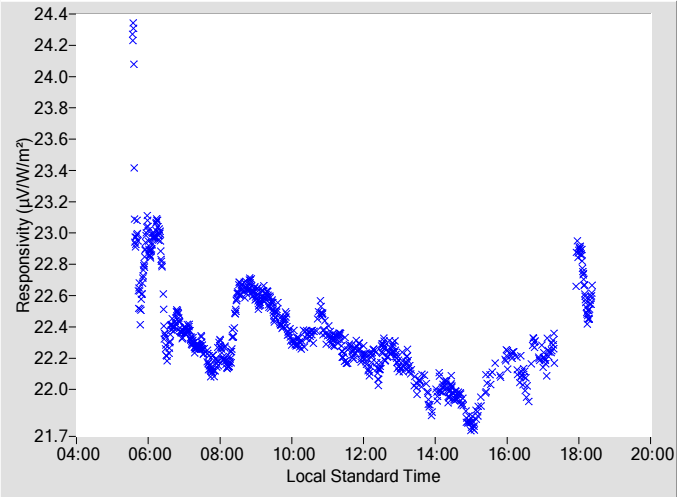


Table 2. Instrument Responsivity (R) and Calibration Type-B Standard Uncertainty, u(B)

Zenith Angle (deg.)	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle	Zenith Angle (deg.)	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle
0	N/A	N/A	N/A	N/A	N/A	N/A	46	22.630	0.35	108.29	21.770	0.38	251.83
2	N/A	N/A	N/A	N/A	N/A	N/A	48	22.642	0.35	105.95	21.833	0.39	254.25
4	N/A	N/A	N/A	N/A	N/A	N/A	50	22.650	0.36	103.75	N/A	N/A	N/A
6	N/A	N/A	N/A	N/A	N/A	N/A	52	22.470	0.37	101.76	22.064	0.44	258.60
8	N/A	N/A	N/A	N/A	N/A	N/A	54	22.148	0.38	99.68	N/A	N/A	N/A
10	N/A	N/A	N/A	N/A	N/A	N/A	56	22.234	0.39	97.82	N/A	N/A	N/A
12	N/A	N/A	N/A	N/A	N/A	N/A	58	22.168	0.39	96.00	N/A	N/A	N/A
14	N/A	N/A	N/A	N/A	N/A	N/A	60	22.158	0.41	94.21	N/A	N/A	N/A
16	N/A	N/A	N/A	N/A	N/A	N/A	62	22.250	0.42	92.48	22.139	0.51	267.66
18	N/A	N/A	N/A	N/A	N/A	N/A	64	22.277	0.44	90.79	22.024	0.55	269.26
20	N/A	N/A	N/A	N/A	N/A	N/A	66	22.317	0.46	89.11	22.307	N/A	271.07
22	N/A	N/A	N/A	N/A	N/A	N/A	68	22.374	0.48	87.49	22.191	N/A	272.51
24	22.246	0.32	174.20	22.188	0.32	185.55	70	22.468	0.52	85.85	22.125	N/A	274.28
26	22.322	0.32	153.73	22.246	0.32	205.86	72	22.412	0.57	84.23	22.281	N/A	275.90
28	22.440	0.33	144.22	22.161	0.33	215.81	74	22.276	0.63	82.61	N/A	N/A	N/A
30	22.349	0.34	137.24	22.112	0.34	222.28	76	22.994	0.69	81.05	N/A	N/A	N/A
32	22.340	0.33	131.86	22.041	0.34	228.36	78	22.985	N/A	79.44	N/A	N/A	N/A
34	22.282	0.33	126.91	21.938	0.34	233.05	80	23.043	N/A	77.83	22.889	N/A	282.45
36	22.358	0.33	122.92	21.971	0.35	237.46	82	22.528	N/A	76.16	22.664	N/A	284.05
38	22.409	0.33	119.43	22.021	0.35	240.66	84	23.696	N/A	74.51	22.578	N/A	285.73
40	22.468	0.33	116.20	22.014	0.36	243.89	86	N/A	N/A	N/A	N/A	N/A	N/A
42	22.614	0.34	113.41	21.956	0.40	246.84	88	N/A	N/A	N/A	N/A	N/A	N/A
44	22.563	0.34	110.65	21.896	0.39	249.10	90	N/A	N/A	N/A	N/A	N/A	N/A

N/A - Not Available



Figure 3. Type-B Standard Uncertainty vs Zenith Angle

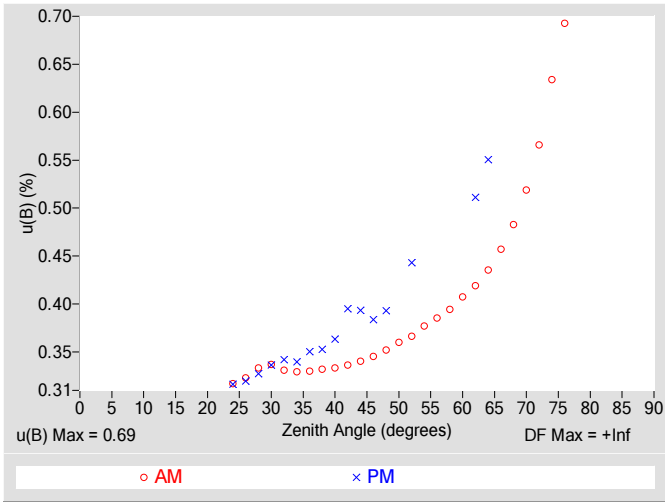


Figure 4. Residuals from Spline Interpolation

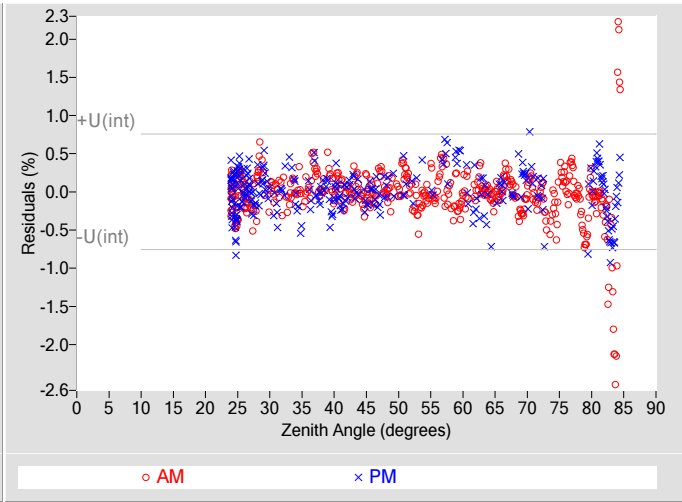


Table 3. Uncertainty using Spline Interpolation ‡

Type-B Standard Uncertainty, u(B) (%)	±0.69
Type-A Interpolating Function, u(int) (%)	±0.38
Combined Standard Uncertainty, u(c) (%)	±0.79
Effective degrees of freedom, DF(c)	12397
Coverage factor, k	1.96
Expanded Uncertainty, U95 (%)	±1.5
AM Valid zenith angle range	24° to 76°
PM Valid zenith angle range	24° to 64°

‡ An illustration for how to reduce the uncertainty in calculating the irradiance using a function rather than R@45°. Not accredited.

Table 4. Calibration Label Values

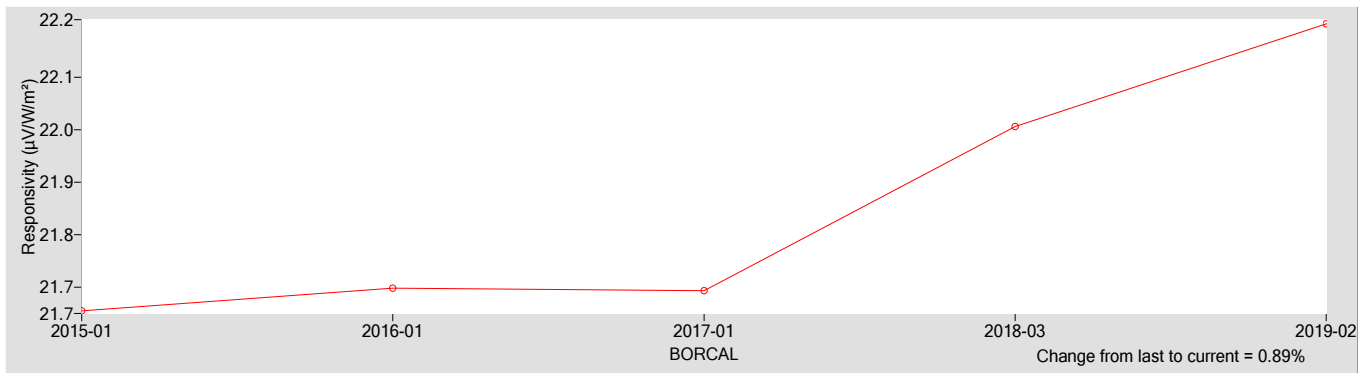
R @ 45° (μV/W/m²)	Rnet (μV/W/m²) †
22.202	0.40000

† Rnet determination date: Estimated

Table 5. Uncertainty using R @ 45°

Type-B Expanded Uncertainty, U(B) (%)	±0.87
Offset Uncertainty, U(off) (%)	+2.0 / -1.9
Expanded Uncertainty, U (%)	+2.9 / -2.8
Effective degrees of freedom, DF	+Inf
Coverage factor, k	1.96
Valid zenith angle range	30.0° to 60.0°

Figure 5. History of instrument at Zenith Angle = 45°



References:

[1] Reda, I.; Hickey, J.; Long, C.; Myers, D.; Stoffel, T.; Wilcox, S.; Michalsky, J. J.; Dutton, E. G.; Nelson, D. (2005). "Using a Blackbody to Calculate Net Longwave Responsivity of Shortwave Solar Pyranometers to Correct for Their Thermal Offset Error During Outdoor Calibration Using the Component Sum Method." Journal of Atmospheric and Oceanic Technology. , 2005; pp. 1531-1540; NREL Report No. JA-560-36646. doi:10.1175/JTECH1782.1

[2] Reda, I.; Myers, D.; Stoffel, T. (2008). "Uncertainty Estimate for the Outdoor Calibration of Solar Pyranometers: A Metrologist Perspective." Measure. (NCSLI Journal of Measurement Science). Vol. 3(4), December 2008; pp. 58-66; NREL Report No. JA-581-4137

[3] Reda, I.; Andreas, A. (2004). "Solar Position Algorithm for Solar Radiation Applications." Solar Energy. Vol. 76(5), 2004; pp. 577-589; NREL Report No. JA-560-35518. doi:10.1016/j.solener.2003.12.003

[4] Stoffel, T.; Reda, I. (2009). "NREL Pyrheliometer Comparisons: 22 September - 3 October 2008 (NPC-2008)." 54 pp.; NREL Report No. TP-550-45016.

[5] Reda, I.; Stoffel, T.; Myers, D. (2003). "Method to Calibrate a Solar Pyranometer for Measuring Reference Diffuse Irradiance." Solar Energy. Vol. 74, 2003; pp. 103-112; NREL Report No. JA-560-35025. doi:10.1016/S0038-092X(03)00124-5

[6] Reda, I. (1996). Calibration of a Solar Absolute Cavity Radiometer with Traceability to the World Radiometric Reference. 79 pp.; NREL Report No. TP-463-20619.

[7] Reda, I.; Gröbner, J.; Stoffel, T.; Myers, D.; Forgan, B. (2008). Improvements in the Blackbody Calibration of Pyrgeometers. ARM 2008 Science Team Meeting (Poster).



# National Renewable Energy Laboratory

## Solar Radiation Research Laboratory

### Metrology Laboratory

### Calibration Certificate



<b>Test Instrument:</b>	Pyranometer	<b>Manufacturer:</b>	Kipp & Zonen
<b>Model:</b>	CM6B	<b>Serial Number:</b>	015189
<b>Calibration Date:</b>	5/3/2019	<b>Due Date:</b>	5/3/2020
<b>Customer:</b>	NREL-SRRL-BMS	<b>Environmental Conditions:</b>	see page 4
<b>Test Dates:</b>	5/3		

This certifies that the above product was calibrated in compliance with ISO/IEC 17025:2005. Measurement uncertainties at the time of calibration are consistent with the Guide to the Expression of Uncertainty in Measurement (GUM) using Reda et al., 2008. All nominal values are traceable to the International System (SI) Units of Measurement.

No statement of compliance with specifications is made or implied on this certificate. However, the estimated uncertainties are the uncertainties of the calibration process; users must add other uncertainties that are relevant to their measuring system, environmental and sky conditions, outdoor set-up, and site location.

The Type-B Standard Uncertainty of using the responsivity at each even zenith angle is reported, and the Expanded Uncertainty of the calibration is reported using two methods:

1. The Expanded Uncertainty of using the responsivity at zenith angle = 45°, within the zenith angle range from 30.0° to 60.0°
2. The Expanded Uncertainty of using Spline Interpolating Functions for the responsivity versus zenith angle.

This certificate applies only to the item identified above and shall not be reproduced other than in full, without specific written approval from the calibration facility. Certificate without signature is not valid.

**Table 1. Traceability**

Measurement Type	Instrument	Calibration Date	Calibration Due Date
Beam Irradiance †	Eppley Absolute Cavity Radiometer Model HF, S/N 29219	09/24/2018	09/24/2019
Diffuse Irradiance †	Hukseflux Pyranometer Model SR25, S/N 2541	04/19/2019	04/19/2020
Diffuse Irradiance †	Hukseflux Pyranometer Model SR25, S/N 2542	04/19/2019	04/19/2020
Data Acquisition	NREL Data Acquisition System Model RAP-DAQ, S/N 2005-998	02/14/2019	02/14/2021
Data Acquisition	NREL Data Acquisition System Model RAP-DAQ, S/N 2005-999	02/14/2019	02/14/2021
Infrared Irradiance ‡	Kipp & Zonen Pyrgeometer Model CG4, S/N FT002	04/16/2018	04/16/2022

† Through the World Radiometric Reference (WRR)

‡ Through the World Infrared Standard Group (WISG)

**Number of pages of certificate:** 4

**Calibration Procedure:** BORCAL-P00-Calibration and QA Procedure; available upon request.

**Setup:** Radiometers are calibrated outdoors, using the sun as the source. Pyranometers and pyrgeometers are installed for horizontal measurements, with their signal connectors oriented north, if their design permits.

The shading disk for the reference diffuse subtends a solid angle of 5°. Pyrheliometers are installed on solar trackers.

**Calibrated by:** RCC

-----  
Ibrahim Reda, Technical Manager

-----  
Date

For questions or comments, please contact the technical manager at:

ibrahim.reda@nrel.gov; 303-384-6385; 15013 Denver West Parkway, Golden, CO 80401, USA

# Calibration Results

## 015189 Kipp & Zonen CM6B

The responsivity ( $R$ ,  $\mu\text{V}/\text{W}/\text{m}^2$ ) of the test instrument during calibration is calculated using this Measurement Equation:

$$R = (V - R_{net} * W_{net}) / I \tag{1}$$

where,

- $V$  = radiometer output voltage (microvolts),
  - $R_{net}$  = radiometer net infrared responsivity ( $\mu\text{V}/\text{W}/\text{m}^2$ ), see Table 4,
  - $W_{net}$  = effective net infrared measured by pyrgeometer ( $\text{W}/\text{m}^2$ ),
  - =  $W_{in} - W_{out} = W_{in} - \sigma * T_c^4$
  - where,  $W_{in}$  = incoming infrared ( $\text{W}/\text{m}^2$ ),  $\sigma = 5.6704\text{e-}8 \text{ W}\cdot\text{m}^{-2}\cdot\text{K}^{-4}$ ,
  - $T_c$  = case temperature of pyrgeometer (K).
- $I$  = reference irradiance ( $\text{W}/\text{m}^2$ ), beam (B) or global (G)
  - where,  $G = B * \text{COS}(Z) + D$ ,
  - $Z$  = zenith angle (degrees),
  - $D$  = reference diffuse irradiance ( $\text{W}/\text{m}^2$ ).

Figure 1. Responsivity vs Zenith Angle

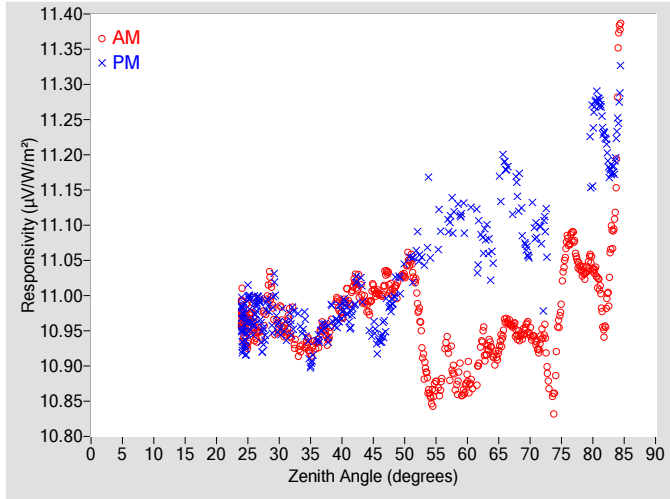


Figure 2. Responsivity vs Local Standard Time

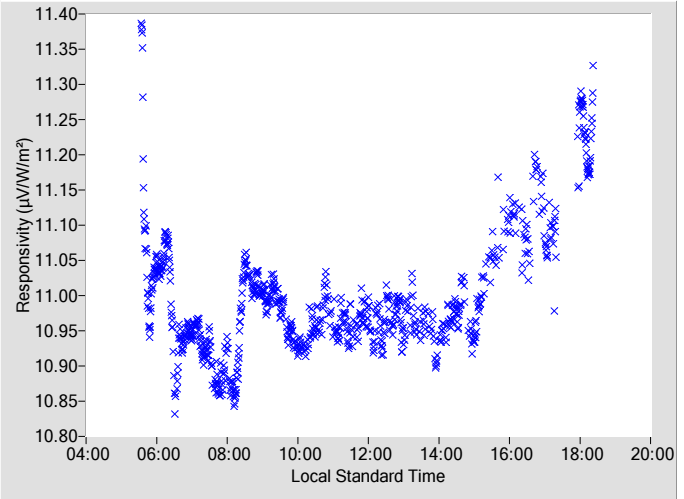


Table 2. Instrument Responsivity (R) and Calibration Type-B Standard Uncertainty, u(B)

Zenith Angle (deg.)	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	AM u(B) $\pm$ (%)	Azimuth Angle	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	PM u(B) $\pm$ (%)	Azimuth Angle	Zenith Angle (deg.)	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	AM u(B) $\pm$ (%)	Azimuth Angle	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	PM u(B) $\pm$ (%)	Azimuth Angle
0	N/A	N/A	N/A	N/A	N/A	N/A	46	11.004	0.35	108.44	10.937	0.39	251.92
2	N/A	N/A	N/A	N/A	N/A	N/A	48	11.007	0.36	106.02	10.987	0.40	254.16
4	N/A	N/A	N/A	N/A	N/A	N/A	50	11.028	0.36	103.81	11.045	0.44	256.29
6	N/A	N/A	N/A	N/A	N/A	N/A	52	10.998	0.37	101.71	11.068	0.45	258.50
8	N/A	N/A	N/A	N/A	N/A	N/A	54	10.858	0.38	99.69	11.111	0.48	260.35
10	N/A	N/A	N/A	N/A	N/A	N/A	56	10.880	0.39	97.94	N/A	N/A	N/A
12	N/A	N/A	N/A	N/A	N/A	N/A	58	10.882	0.40	95.98	11.119	0.51	264.04
14	N/A	N/A	N/A	N/A	N/A	N/A	60	10.880	0.41	94.21	N/A	N/A	N/A
16	N/A	N/A	N/A	N/A	N/A	N/A	62	10.917	0.43	92.48	11.096	0.52	267.64
18	N/A	N/A	N/A	N/A	N/A	N/A	64	10.920	0.44	90.78	11.054	0.56	269.36
20	N/A	N/A	N/A	N/A	N/A	N/A	66	10.962	0.46	89.13	11.185	N/A	271.07
22	N/A	N/A	N/A	N/A	N/A	N/A	68	10.945	0.49	87.49	11.153	N/A	272.68
24	10.968	0.32	174.39	10.960	0.32	185.12	70	10.945	0.53	85.81	11.055	N/A	274.10
26	10.958	0.33	153.74	10.971	0.32	206.20	72	10.944	0.58	84.26	11.053	N/A	275.94
28	10.996	0.34	144.07	10.972	0.33	215.58	74	10.875	0.64	82.66	N/A	N/A	N/A
30	10.961	0.34	137.48	10.953	0.34	222.75	76	11.076	0.71	81.05	N/A	N/A	N/A
32	10.953	0.33	131.94	10.963	0.35	228.30	78	11.038	N/A	79.39	N/A	N/A	N/A
34	10.927	0.33	126.60	10.959	0.34	233.26	80	11.040	N/A	77.79	11.239	N/A	282.44
36	10.930	0.33	122.88	10.939	0.35	237.40	82	10.964	N/A	76.18	11.221	N/A	284.06
38	10.944	0.33	119.52	10.955	0.36	240.54	84	11.290	N/A	74.52	11.253	N/A	285.73
40	10.976	0.34	116.18	10.977	0.37	243.78	86	N/A	N/A	N/A	N/A	N/A	N/A
42	11.019	0.34	113.38	11.000	0.40	246.85	88	N/A	N/A	N/A	N/A	N/A	N/A
44	10.985	0.34	110.64	N/A	N/A	N/A	90	N/A	N/A	N/A	N/A	N/A	N/A

N/A - Not Available

Figure 3. Type-B Standard Uncertainty vs Zenith Angle

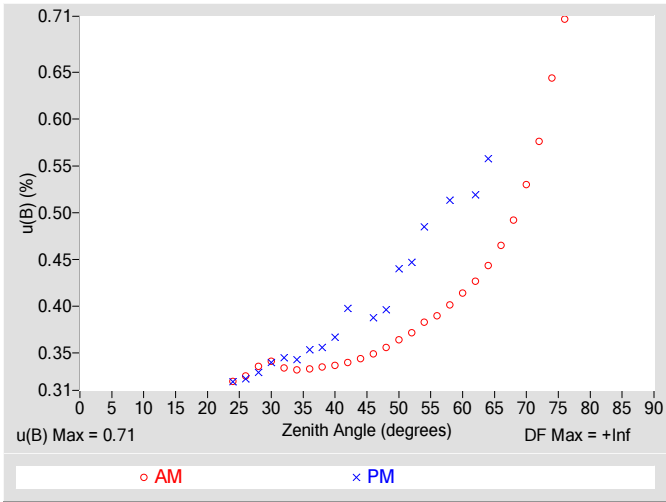


Figure 4. Residuals from Spline Interpolation

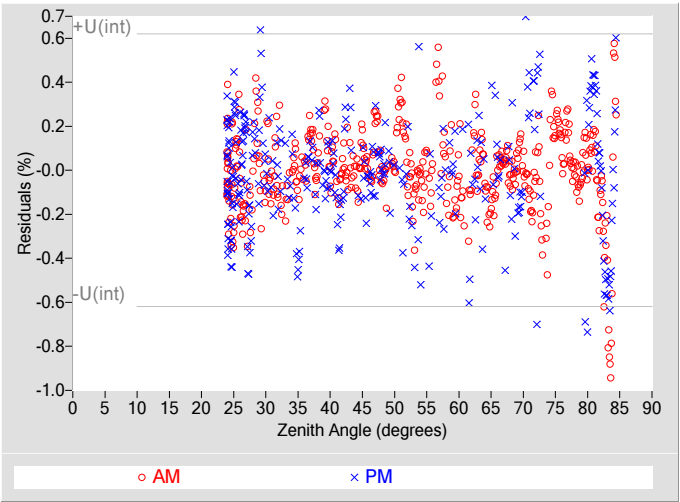


Table 3. Uncertainty using Spline Interpolation ‡

Type-B Standard Uncertainty, u(B) (%)	±0.71
Type-A Interpolating Function, u(int) (%)	±0.31
Combined Standard Uncertainty, u(c) (%)	±0.77
Effective degrees of freedom, DF(c)	26147
Coverage factor, k	1.96
Expanded Uncertainty, U95 (%)	±1.5
AM Valid zenith angle range	24° to 76°
PM Valid zenith angle range	24° to 64°

‡ An illustration for how to reduce the uncertainty in calculating the irradiance using a function rather than R@45°. Not accredited.

Table 4. Calibration Label Values

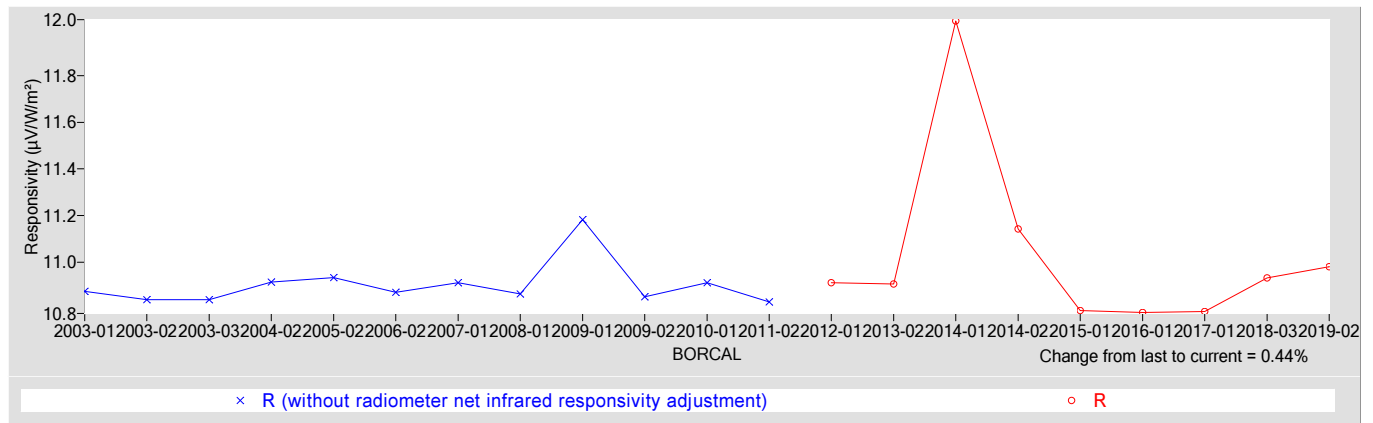
R @ 45° (μV/W/m²)	Rnet (μV/W/m²) †
10.980	0.30000

† Rnet determination date: Estimated

Table 5. Uncertainty using R @ 45°

Type-B Expanded Uncertainty, U(B) (%)	±1.0
Offset Uncertainty, U(off) (%)	+1.3 / -1.1
Expanded Uncertainty, U (%)	+2.3 / -2.1
Effective degrees of freedom, DF	+Inf
Coverage factor, k	1.96
Valid zenith angle range	30.0° to 60.0°

Figure 5. History of instrument at Zenith Angle = 45°



References:

[1] Reda, I.; Hickey, J.; Long, C.; Myers, D.; Stoffel, T.; Wilcox, S.; Michalsky, J. J.; Dutton, E. G.; Nelson, D. (2005). "Using a Blackbody to Calculate Net Longwave Responsivity of Shortwave Solar Pyranometers to Correct for Their Thermal Offset Error During Outdoor Calibration Using the Component Sum Method." Journal of Atmospheric and Oceanic Technology. , 2005; pp. 1531-1540; NREL Report No. JA-560-36646. doi:10.1175/JTECH1782.1

[2] Reda, I.; Myers, D.; Stoffel, T. (2008). "Uncertainty Estimate for the Outdoor Calibration of Solar Pyranometers: A Metrologist Perspective." Measure. (NCSLI Journal of Measurement Science). Vol. 3(4), December 2008; pp. 58-66; NREL Report No. JA-581-4137

[3] Reda, I.; Andreas, A. (2004). "Solar Position Algorithm for Solar Radiation Applications." Solar Energy. Vol. 76(5), 2004; pp. 577-589; NREL Report No. JA-560-35518. doi:10.1016/j.solener.2003.12.003

[4] Stoffel, T.; Reda, I. (2009). "NREL Pyrheliometer Comparisons: 22 September - 3 October 2008 (NPC-2008)." 54 pp.; NREL Report No. TP-550-45016.

[5] Reda, I.; Stoffel, T.; Myers, D. (2003). "Method to Calibrate a Solar Pyranometer for Measuring Reference Diffuse Irradiance." Solar Energy. Vol. 74, 2003; pp. 103-112; NREL Report No. JA-560-35025. doi:10.1016/S0038-092X(03)00124-5

[6] Reda, I. (1996). Calibration of a Solar Absolute Cavity Radiometer with Traceability to the World Radiometric Reference. 79 pp.; NREL Report No. TP-463-20619.

[7] Reda, I.; Gröbner, J.; Stoffel, T.; Myers, D.; Forgan, B. (2008). Improvements in the Blackbody Calibration of Pyrgeometers. ARM 2008 Science Team Meeting (Poster).

# National Renewable Energy Laboratory

## Solar Radiation Research Laboratory

### Metrology Laboratory

### Calibration Certificate



<b>Test Instrument:</b>	Pyranometer (Ventilated)	<b>Manufacturer:</b>	Yankee
<b>Model:</b>	TSP-700	<b>Serial Number:</b>	0212-2
<b>Calibration Date:</b>	5/3/2019	<b>Due Date:</b>	5/3/2020
<b>Customer:</b>	NREL-SRRL-BMS	<b>Environmental Conditions:</b>	see page 4
<b>Test Dates:</b>	5/3		

This certifies that the above product was calibrated in compliance with ISO/IEC 17025:2005. Measurement uncertainties at the time of calibration are consistent with the Guide to the Expression of Uncertainty in Measurement (GUM) using Reda et al., 2008. All nominal values are traceable to the International System (SI) Units of Measurement.

No statement of compliance with specifications is made or implied on this certificate. However, the estimated uncertainties are the uncertainties of the calibration process; users must add other uncertainties that are relevant to their measuring system, environmental and sky conditions, outdoor set-up, and site location.

The Type-B Standard Uncertainty of using the responsivity at each even zenith angle is reported, and the Expanded Uncertainty of the calibration is reported using two methods:

1. The Expanded Uncertainty of using the responsivity at zenith angle = 45°, within the zenith angle range from 30.0° to 60.0°
2. The Expanded Uncertainty of using Spline Interpolating Functions for the responsivity versus zenith angle.

This certificate applies only to the item identified above and shall not be reproduced other than in full, without specific written approval from the calibration facility. Certificate without signature is not valid.

**Table 1. Traceability**

Measurement Type	Instrument	Calibration Date	Calibration Due Date
Beam Irradiance †	Eppley Absolute Cavity Radiometer Model HF, S/N 29219	09/24/2018	09/24/2019
Diffuse Irradiance †	Hukseflux Pyranometer Model SR25, S/N 2541	04/19/2019	04/19/2020
Diffuse Irradiance †	Hukseflux Pyranometer Model SR25, S/N 2542	04/19/2019	04/19/2020
Data Acquisition	NREL Data Acquisition System Model RAP-DAQ, S/N 2005-998	02/14/2019	02/14/2021
Data Acquisition	NREL Data Acquisition System Model RAP-DAQ, S/N 2005-999	02/14/2019	02/14/2021

† Through the World Radiometric Reference (WRR)

**Number of pages of certificate:** 4

**Calibration Procedure:** BORCAL-P00-Calibration and QA Procedure; available upon request.

**Setup:** Radiometers are calibrated outdoors, using the sun as the source. Pyranometers and pyrgeometers are installed for horizontal measurements, with their signal connectors oriented north, if their design permits.  
The shading disk for the reference diffuse subtends a solid angle of 5°. Pyrheliometers are installed on solar trackers.

**Calibrated by:** RCC

-----  
Ibrahim Reda, Technical Manager

-----  
Date

For questions or comments, please contact the technical manager at:  
ibrahim.reda@nrel.gov; 303-384-6385; 15013 Denver West Parkway, Golden, CO 80401, USA

# Calibration Results

## 0212-2 Yankee TSP-700

The responsivity ( $R$ ,  $\mu\text{V}/\text{W}/\text{m}^2$ ) of the test instrument during calibration is calculated using this Measurement Equation:

$$R = (V - R_{net} * W_{net}) / I \tag{1}$$

where,

- $V$  = radiometer output voltage (microvolts),
  - $R_{net}$  = radiometer net infrared responsivity ( $\mu\text{V}/\text{W}/\text{m}^2$ ), see Table 4,
  - $W_{net}$  = effective net infrared measured by pyrgeometer ( $\text{W}/\text{m}^2$ ),
  - =  $W_{in} - W_{out} = W_{in} - \sigma * T_c^4$
  - where,  $W_{in}$  = incoming infrared ( $\text{W}/\text{m}^2$ ),  $\sigma = 5.6704\text{e-}8 \text{ W}\cdot\text{m}^{-2}\cdot\text{K}^{-4}$ ,
  - $T_c$  = case temperature of pyrgeometer (K).
- $I$  = reference irradiance ( $\text{W}/\text{m}^2$ ), beam (B) or global (G)
  - where,  $G = B * \text{COS}(Z) + D$ ,
  - $Z$  = zenith angle (degrees),
  - $D$  = reference diffuse irradiance ( $\text{W}/\text{m}^2$ ).

Figure 1. Responsivity vs Zenith Angle

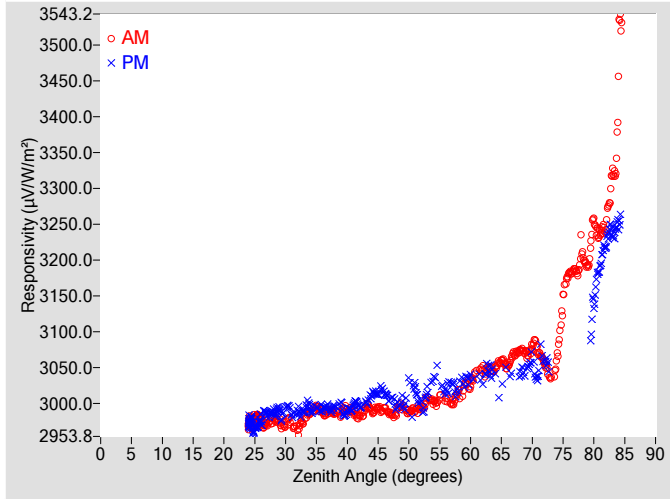


Figure 2. Responsivity vs Local Standard Time

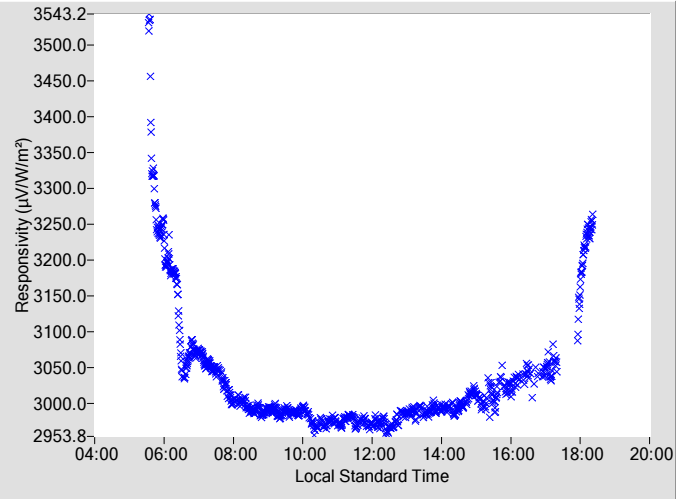


Table 2. Instrument Responsivity (R) and Calibration Type-B Standard Uncertainty, u(B)

Zenith Angle (deg.)	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle	Zenith Angle (deg.)	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle
0	N/A	N/A	N/A	N/A	N/A	N/A	46	2993.6	0.34	108.12	3013.5	0.38	252.04
2	N/A	N/A	N/A	N/A	N/A	N/A	48	2987.3	0.35	105.93	2996.4	0.39	254.12
4	N/A	N/A	N/A	N/A	N/A	N/A	50	2987.6	0.36	103.74	3032.1	0.43	256.46
6	N/A	N/A	N/A	N/A	N/A	N/A	52	2994.4	0.36	101.65	2996.9	0.44	258.58
8	N/A	N/A	N/A	N/A	N/A	N/A	54	3003.1	0.37	99.74	3034.6	0.47	260.48
10	N/A	N/A	N/A	N/A	N/A	N/A	56	3004.5	0.38	97.71	3019.3	0.50	262.40
12	N/A	N/A	N/A	N/A	N/A	N/A	58	3014.2	0.39	95.95	3022.2	0.51	264.15
14	N/A	N/A	N/A	N/A	N/A	N/A	60	3027.3	0.40	94.16	3038.3	N/A	265.83
16	N/A	N/A	N/A	N/A	N/A	N/A	62	3048.6	0.41	92.45	3026.4	0.51	267.64
18	N/A	N/A	N/A	N/A	N/A	N/A	64	3048.9	0.43	90.76	3041.4	0.54	269.40
20	N/A	N/A	N/A	N/A	N/A	N/A	66	3051.6	0.45	89.11	3050.4	N/A	270.80
22	N/A	N/A	N/A	N/A	N/A	N/A	68	3073.0	0.48	87.49	3039.8	N/A	272.71
24	2972.6	0.31	175.39	2972.6	0.31	185.93	70	3079.6	0.51	85.85	3062.0	N/A	274.28
26	2978.0	0.32	154.28	2976.4	0.32	205.69	72	3054.9	0.56	84.23	3057.2	N/A	275.93
28	2977.5	0.33	144.13	2987.7	0.32	215.63	74	3061.8	0.62	82.65	N/A	N/A	N/A
30	2969.5	0.34	137.46	2995.9	0.34	223.46	76	3180.7	0.68	81.05	N/A	N/A	N/A
32	2963.8	0.33	131.53	2988.3	0.34	228.51	78	3208.7	N/A	79.43	N/A	N/A	N/A
34	2985.0	0.33	127.25	2992.5	0.34	233.04	80	3252.7	N/A	77.78	3143.0	N/A	282.39
36	2986.6	0.33	122.91	2993.2	0.35	237.11	82	3256.8	N/A	76.10	3224.5	N/A	284.05
38	2985.4	0.33	119.67	2995.4	0.35	240.46	84	3473.2	N/A	74.46	3251.2	N/A	285.72
40	2990.6	0.33	116.22	2989.6	0.36	244.00	86	N/A	N/A	N/A	N/A	N/A	N/A
42	2981.5	0.33	113.44	2995.5	0.39	246.76	88	N/A	N/A	N/A	N/A	N/A	N/A
44	2989.4	0.34	110.74	3012.4	0.39	249.50	90	N/A	N/A	N/A	N/A	N/A	N/A

N/A - Not Available

Figure 3. Type-B Standard Uncertainty vs Zenith Angle

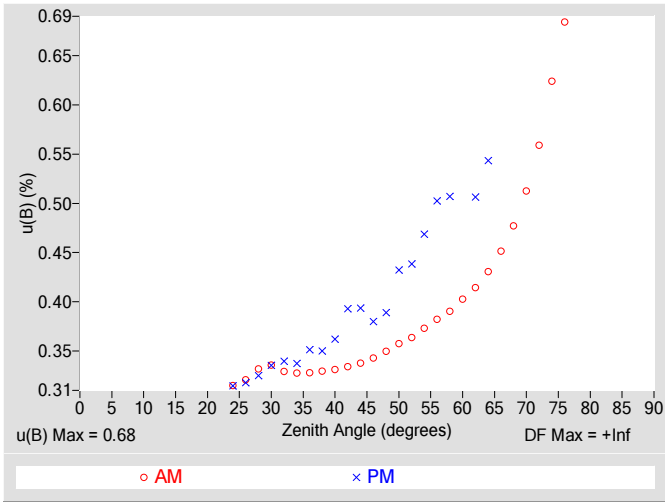


Figure 4. Residuals from Spline Interpolation

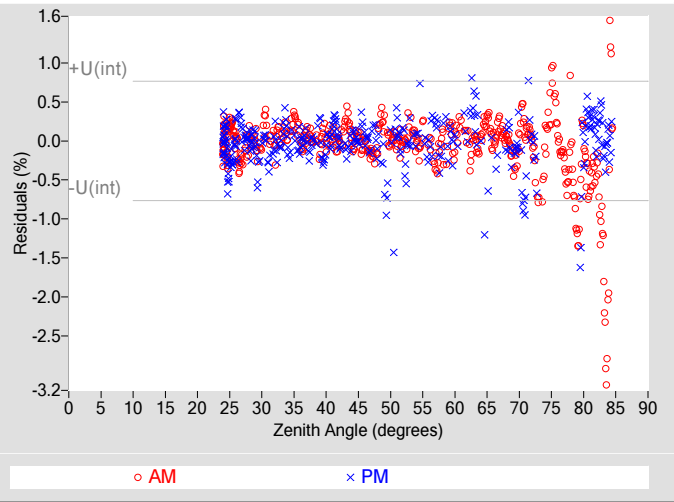


Table 3. Uncertainty using Spline Interpolation ‡

Type-B Standard Uncertainty, u(B) (%)	±0.68
Type-A Interpolating Function, u(int) (%)	±0.38
Combined Standard Uncertainty, u(c) (%)	±0.78
Effective degrees of freedom, DF(c)	12552
Coverage factor, k	1.96
Expanded Uncertainty, U95 (%)	±1.5
AM Valid zenith angle range	24° to 76°
PM Valid zenith angle range	24° to 64°

‡ An illustration for how to reduce the uncertainty in calculating the irradiance using a function rather than R@45°. Not accredited.

Table 4. Calibration Label Values

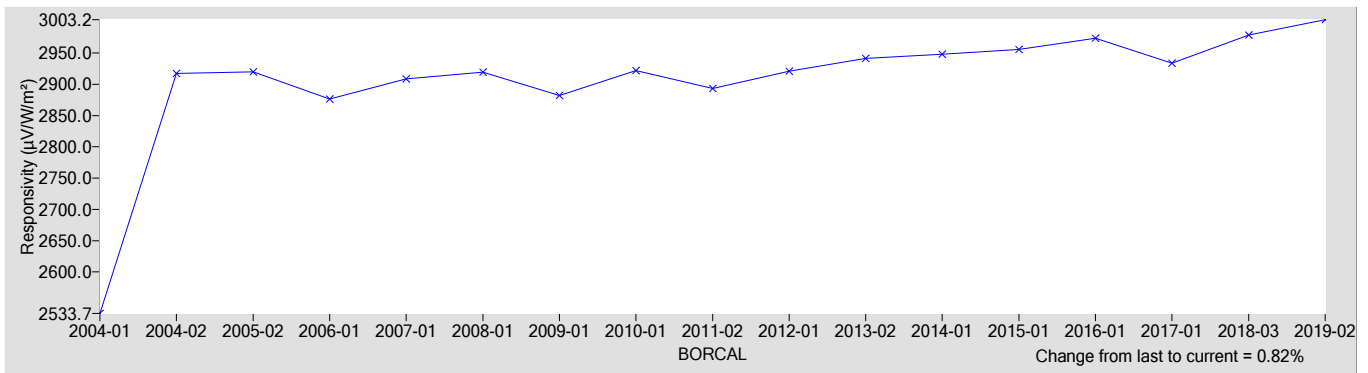
R @ 45° (μV/W/m²)	Rnet (μV/W/m²) †
3003.2	0

† Rnet determination date: N/A

Table 5. Uncertainty using R @ 45°

Type-B Expanded Uncertainty, U(B) (%)	±0.99
Offset Uncertainty, U(off) (%)	+1.2 / -1.3
Expanded Uncertainty, U (%)	+2.2 / -2.3
Effective degrees of freedom, DF	+Inf
Coverage factor, k	1.96
Valid zenith angle range	30.0° to 60.0°

Figure 5. History of instrument at Zenith Angle = 45°



References:

[1] Reda, I.; Hickey, J.; Long, C.; Myers, D.; Stoffel, T.; Wilcox, S.; Michalsky, J. J.; Dutton, E. G.; Nelson, D. (2005). "Using a Blackbody to Calculate Net Longwave Responsivity of Shortwave Solar Pyranometers to Correct for Their Thermal Offset Error During Outdoor Calibration Using the Component Sum Method." Journal of Atmospheric and Oceanic Technology. , 2005; pp. 1531-1540; NREL Report No. JA-560-36646. doi:10.1175/JTECH1782.1

[2] Reda, I.; Myers, D.; Stoffel, T. (2008). "Uncertainty Estimate for the Outdoor Calibration of Solar Pyranometers: A Metrologist Perspective." Measure. (NCSLI Journal of Measurement Science). Vol. 3(4), December 2008; pp. 58-66; NREL Report No. JA-581-4137

[3] Reda, I.; Andreas, A. (2004). "Solar Position Algorithm for Solar Radiation Applications." Solar Energy. Vol. 76(5), 2004; pp. 577-589; NREL Report No. JA-560-35518. doi:10.1016/j.solener.2003.12.003

[4] Stoffel, T.; Reda, I. (2009). "NREL Pyrheliometer Comparisons: 22 September - 3 October 2008 (NPC-2008)." 54 pp.; NREL Report No. TP-550-45016.

[5] Reda, I.; Stoffel, T.; Myers, D. (2003). "Method to Calibrate a Solar Pyranometer for Measuring Reference Diffuse Irradiance." Solar Energy. Vol. 74, 2003; pp. 103-112; NREL Report No. JA-560-35025. doi:10.1016/S0038-092X(03)00124-5

[6] Reda, I. (1996). Calibration of a Solar Absolute Cavity Radiometer with Traceability to the World Radiometric Reference. 79 pp.; NREL Report No. TP-463-20619.

[7] Reda, I.; Gröbner, J.; Stoffel, T.; Myers, D.; Forgan, B. (2008). Improvements in the Blackbody Calibration of Pyrgeometers. ARM 2008 Science Team Meeting (Poster).





# National Renewable Energy Laboratory

## Solar Radiation Research Laboratory

### Metrology Laboratory

### Calibration Certificate



<b>Test Instrument:</b>	Pyrheliometer	<b>Manufacturer:</b>	Kipp & Zonen
<b>Model:</b>	CHP1	<b>Serial Number:</b>	080009
<b>Calibration Date:</b>	5/3/2019	<b>Due Date:</b>	5/3/2020
<b>Customer:</b>	NREL-SRRL-BMS	<b>Environmental Conditions:</b>	see page 4
<b>Test Dates:</b>	5/3		

This certifies that the above product was calibrated in compliance with ISO/IEC 17025:2005. Measurement uncertainties at the time of calibration are consistent with the Guide to the Expression of Uncertainty in Measurement (GUM) using Reda et al., 2008. All nominal values are traceable to the International System (SI) Units of Measurement.

No statement of compliance with specifications is made or implied on this certificate. However, the estimated uncertainties are the uncertainties of the calibration process; users must add other uncertainties that are relevant to their measuring system, environmental and sky conditions, outdoor set-up, and site location.

The Type-B Standard Uncertainty of using the responsivity at each even zenith angle is reported, and the Expanded Uncertainty of the calibration is reported using two methods:

1. The Expanded Uncertainty of using the responsivity at zenith angle = 45°, within the zenith angle range from 30.0° to 60.0°
2. The Expanded Uncertainty of using Spline Interpolating Functions for the responsivity versus zenith angle.

This certificate applies only to the item identified above and shall not be reproduced other than in full, without specific written approval from the calibration facility. Certificate without signature is not valid.

**Table 1. Traceability**

Measurement Type	Instrument	Calibration Date	Calibration Due Date
Beam Irradiance †	Eppley Absolute Cavity Radiometer Model HF, S/N 29219	09/24/2018	09/24/2019
Diffuse Irradiance †	Hukseflux Pyranometer Model SR25, S/N 2541	04/19/2019	04/19/2020
Diffuse Irradiance †	Hukseflux Pyranometer Model SR25, S/N 2542	04/19/2019	04/19/2020
Data Acquisition	NREL Data Acquisition System Model RAP-DAQ, S/N 2005-998	02/14/2019	02/14/2021
Data Acquisition	NREL Data Acquisition System Model RAP-DAQ, S/N 2005-999	02/14/2019	02/14/2021

† Through the World Radiometric Reference (WRR)

**Number of pages of certificate:** 4

**Calibration Procedure:** BORCAL-P00-Calibration and QA Procedure; available upon request.

**Setup:** Radiometers are calibrated outdoors, using the sun as the source. Pyranometers and pyrgeometers are installed for horizontal measurements, with their signal connectors oriented north, if their design permits.

The shading disk for the reference diffuse subtends a solid angle of 5°. Pyrheliometers are installed on solar trackers.

**Calibrated by:** RCC

-----  
Ibrahim Reda, Technical Manager

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Date

For questions or comments, please contact the technical manager at:

ibrahim.reda@nrel.gov; 303-384-6385; 15013 Denver West Parkway, Golden, CO 80401, USA



# Calibration Results

## 080009 Kipp & Zonen CHP1

The responsivity ( $R$ ,  $\mu\text{V}/\text{W}/\text{m}^2$ ) of the test instrument during calibration is calculated using this Measurement Equation:

$$R = (V - R_{net} * W_{net}) / I \tag{1}$$

where,

- $V$  = radiometer output voltage (microvolts),
- $R_{net}$  = radiometer net infrared responsivity ( $\mu\text{V}/\text{W}/\text{m}^2$ ), see Table 4,
- $W_{net}$  = effective net infrared measured by pyrgeometer ( $\text{W}/\text{m}^2$ ),
- =  $W_{in} - W_{out} = W_{in} - \sigma * T_c^4$
- where,  $W_{in}$  = incoming infrared ( $\text{W}/\text{m}^2$ ),  $\sigma = 5.6704\text{e-}8 \text{ W}\cdot\text{m}^{-2}\cdot\text{K}^{-4}$ ,
- $T_c$  = case temperature of pyrgeometer (K).
- $I$  = reference irradiance ( $\text{W}/\text{m}^2$ ), beam (B) or global (G)
- where,  $G = B * \text{COS}(Z) + D$ ,
- $Z$  = zenith angle (degrees),
- $D$  = reference diffuse irradiance ( $\text{W}/\text{m}^2$ ).

Figure 1. Responsivity vs Zenith Angle

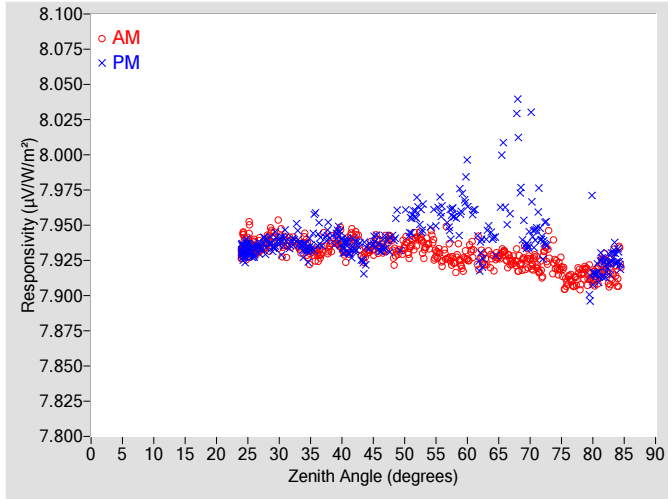


Figure 2. Responsivity vs Local Standard Time

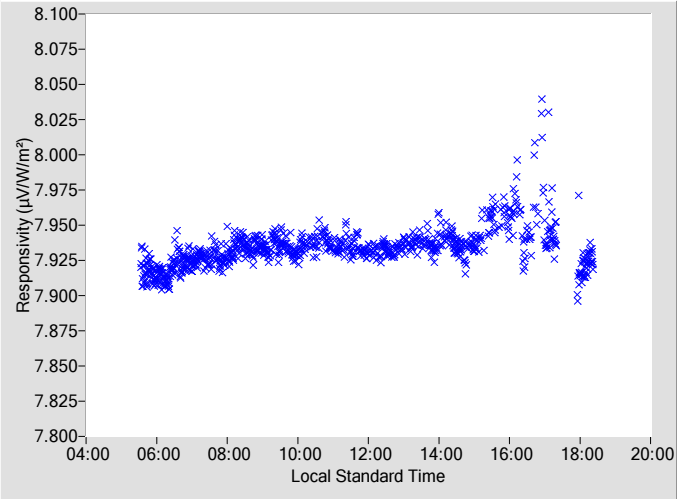


Table 2. Instrument Responsivity (R) and Calibration Type-B Standard Uncertainty, u(B)

Zenith			AM			PM			Zenith			AM			PM		
Angle	R	u(B)	Azimuth	R	u(B)	Azimuth	Angle	R	u(B)	Azimuth	R	u(B)	Azimuth	R	u(B)	Azimuth	
(deg.)	( $\mu\text{V}/\text{W}/\text{m}^2$ )	± (%)	Angle	( $\mu\text{V}/\text{W}/\text{m}^2$ )	± (%)	Angle	(deg.)	( $\mu\text{V}/\text{W}/\text{m}^2$ )	± (%)	Angle	( $\mu\text{V}/\text{W}/\text{m}^2$ )	± (%)	Angle	( $\mu\text{V}/\text{W}/\text{m}^2$ )	± (%)	Angle	
0	N/A	N/A	N/A	N/A	N/A	N/A	46	7.9334	0.28	108.27	7.9331	0.28	251.93				
2	N/A	N/A	N/A	N/A	N/A	N/A	48	7.9337	0.28	105.88	7.9410	0.29	254.21				
4	N/A	N/A	N/A	N/A	N/A	N/A	50	7.9372	0.28	103.73	7.9609	0.30	256.55				
6	N/A	N/A	N/A	N/A	N/A	N/A	52	7.9393	0.28	101.79	7.9620	0.29	258.37				
8	N/A	N/A	N/A	N/A	N/A	N/A	54	7.9381	0.28	99.77	7.9486	0.30	260.54				
10	N/A	N/A	N/A	N/A	N/A	N/A	56	7.9231	0.28	97.82	7.9595	0.30	262.18				
12	N/A	N/A	N/A	N/A	N/A	N/A	58	7.9227	0.28	95.93	7.9556	0.30	264.14				
14	N/A	N/A	N/A	N/A	N/A	N/A	60	7.9254	0.29	94.15	7.9813	N/A	265.88				
16	N/A	N/A	N/A	N/A	N/A	N/A	62	7.9300	0.29	92.49	7.9301	0.30	267.72				
18	N/A	N/A	N/A	N/A	N/A	N/A	64	7.9252	0.29	90.77	7.9420	0.30	269.35				
20	N/A	N/A	N/A	N/A	N/A	N/A	66	7.9288	0.29	89.10	7.9627	N/A	271.06				
22	N/A	N/A	N/A	N/A	N/A	N/A	68	7.9236	0.29	87.47	8.0270	N/A	272.67				
24	7.9338	0.28	174.40	7.9317	0.28	185.29	70	7.9233	0.29	85.88	7.9690	N/A	274.32				
26	7.9350	0.28	153.95	7.9314	0.28	205.72	72	7.9206	0.30	84.26	7.9368	N/A	275.94				
28	7.9377	0.28	144.37	7.9359	0.28	215.69	74	7.9254	0.30	82.64	N/A	N/A	N/A				
30	7.9430	0.28	137.22	7.9390	0.28	223.11	76	7.9103	0.30	81.04	N/A	N/A	N/A				
32	7.9383	0.28	131.86	7.9378	0.28	228.47	78	7.9128	N/A	79.42	N/A	N/A	N/A				
34	7.9379	0.28	126.98	7.9337	0.28	233.02	80	7.9112	N/A	77.77	7.9139	N/A	282.51				
36	7.9288	0.28	122.98	7.9460	0.28	237.23	82	7.9219	N/A	76.16	7.9200	N/A	284.04				
38	7.9327	0.28	119.44	7.9465	0.28	240.44	84	7.9192	N/A	74.45	7.9262	N/A	285.76				
40	7.9388	0.28	116.30	7.9356	0.28	243.86	86	N/A	N/A	N/A	N/A	N/A	N/A				
42	7.9406	0.28	113.46	7.9350	0.28	246.74	88	N/A	N/A	N/A	N/A	N/A	N/A				
44	7.9306	0.28	110.66	7.9298	0.28	249.41	90	N/A	N/A	N/A	N/A	N/A	N/A				

N/A - Not Available

Figure 3. Type-B Standard Uncertainty vs Zenith Angle

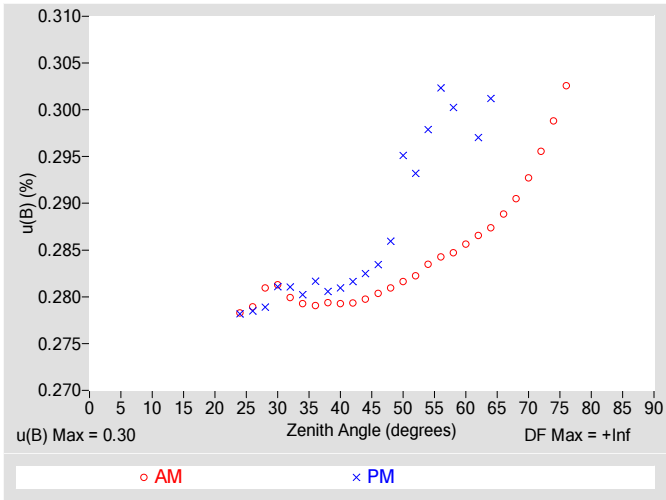


Figure 4. Residuals from Spline Interpolation

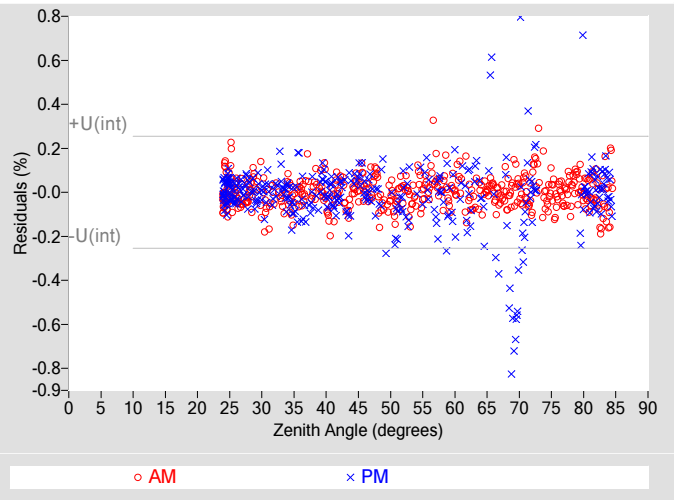


Table 3. Uncertainty using Spline Interpolation ‡

Type-B Standard Uncertainty, u(B) (%)	±0.30
Type-A Interpolating Function, u(int) (%)	±0.13
Combined Standard Uncertainty, u(c) (%)	±0.33
Effective degrees of freedom, DF(c)	30753
Coverage factor, k	1.96
Expanded Uncertainty, U95 (%)	±0.64
AM Valid zenith angle range	24° to 76°
PM Valid zenith angle range	24° to 64°

‡ An illustration for how to reduce the uncertainty in calculating the irradiance using a function rather than R@45°. Not accredited.

Table 4. Calibration Label Values

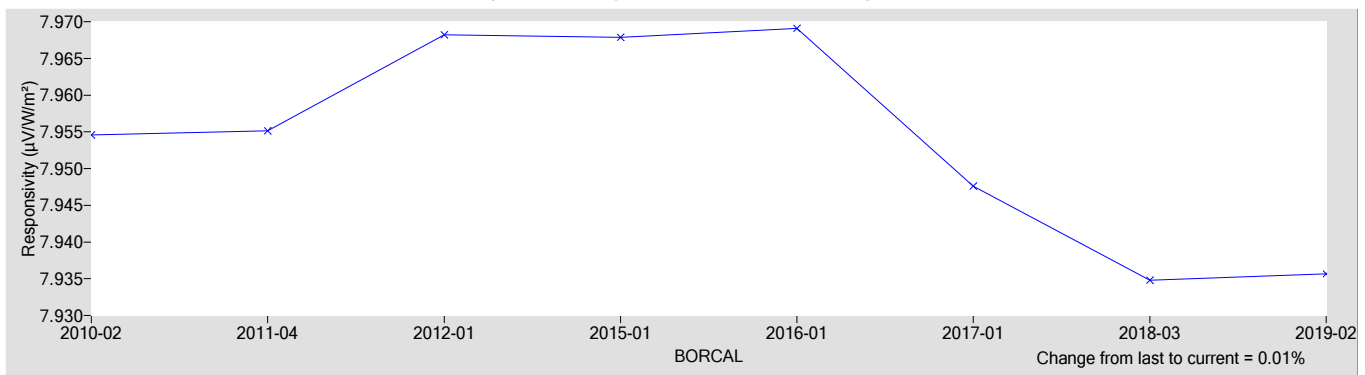
R @ 45° (μV/W/m²)	Rnet (μV/W/m²) †
7.9357	0

† Rnet determination date: N/A

Table 5. Uncertainty using R @ 45°

Type-B Expanded Uncertainty, U(B) (%)	±0.59
Offset Uncertainty, U(off) (%)	+0.58 / -0.16
Expanded Uncertainty, U (%)	+1.2 / -0.76
Effective degrees of freedom, DF	+Inf
Coverage factor, k	1.96
Valid zenith angle range	30.0° to 60.0°

Figure 5. History of instrument at Zenith Angle = 45°



References:

[1] Reda, I.; Hickey, J.; Long, C.; Myers, D.; Stoffel, T.; Wilcox, S.; Michalsky, J. J.; Dutton, E. G.; Nelson, D. (2005). "Using a Blackbody to Calculate Net Longwave Responsivity of Shortwave Solar Pyranometers to Correct for Their Thermal Offset Error During Outdoor Calibration Using the Component Sum Method." Journal of Atmospheric and Oceanic Technology. , 2005; pp. 1531-1540; NREL Report No. JA-560-36646. doi:10.1175/JTECH1782.1

[2] Reda, I.; Myers, D.; Stoffel, T. (2008). "Uncertainty Estimate for the Outdoor Calibration of Solar Pyranometers: A Metrologist Perspective." Measure. (NCSLI Journal of Measurement Science). Vol. 3(4), December 2008; pp. 58-66; NREL Report No. JA-581-4137

[3] Reda, I.; Andreas, A. (2004). "Solar Position Algorithm for Solar Radiation Applications." Solar Energy. Vol. 76(5), 2004; pp. 577-589; NREL Report No. JA-560-35518. doi:10.1016/j.solener.2003.12.003

[4] Stoffel, T.; Reda, I. (2009). "NREL Pyrheliometer Comparisons: 22 September - 3 October 2008 (NPC-2008)." 54 pp.; NREL Report No. TP-550-45016.

[5] Reda, I.; Stoffel, T.; Myers, D. (2003). "Method to Calibrate a Solar Pyranometer for Measuring Reference Diffuse Irradiance." Solar Energy. Vol. 74, 2003; pp. 103-112; NREL Report No. JA-560-35025. doi:10.1016/S0038-092X(03)00124-5

[6] Reda, I. (1996). Calibration of a Solar Absolute Cavity Radiometer with Traceability to the World Radiometric Reference. 79 pp.; NREL Report No. TP-463-20619.

[7] Reda, I.; Gröbner, J.; Stoffel, T.; Myers, D.; Forgan, B. (2008). Improvements in the Blackbody Calibration of Pyrgeometers. ARM 2008 Science Team Meeting (Poster).



# National Renewable Energy Laboratory

## Solar Radiation Research Laboratory

### Metrology Laboratory

### Calibration Certificate



<b>Test Instrument:</b>	Pyranometer (Ventilated)	<b>Manufacturer:</b>	Kipp & Zonen
<b>Model:</b>	CMP22	<b>Serial Number:</b>	080017
<b>Calibration Date:</b>	5/3/2019	<b>Due Date:</b>	5/3/2020
<b>Customer:</b>	NREL-SRRL-BMS	<b>Environmental Conditions:</b>	see page 4
<b>Test Dates:</b>	5/3		

This certifies that the above product was calibrated in compliance with ISO/IEC 17025:2005. Measurement uncertainties at the time of calibration are consistent with the Guide to the Expression of Uncertainty in Measurement (GUM) using Reda et al., 2008. All nominal values are traceable to the International System (SI) Units of Measurement.

No statement of compliance with specifications is made or implied on this certificate. However, the estimated uncertainties are the uncertainties of the calibration process; users must add other uncertainties that are relevant to their measuring system, environmental and sky conditions, outdoor set-up, and site location.

The Type-B Standard Uncertainty of using the responsivity at each even zenith angle is reported, and the Expanded Uncertainty of the calibration is reported using two methods:

1. The Expanded Uncertainty of using the responsivity at zenith angle = 45°, within the zenith angle range from 30.0° to 60.0°
2. The Expanded Uncertainty of using Spline Interpolating Functions for the responsivity versus zenith angle.

This certificate applies only to the item identified above and shall not be reproduced other than in full, without specific written approval from the calibration facility. Certificate without signature is not valid.

**Table 1. Traceability**

Measurement Type	Instrument	Calibration Date	Calibration Due Date
Beam Irradiance †	Eppley Absolute Cavity Radiometer Model HF, S/N 29219	09/24/2018	09/24/2019
Diffuse Irradiance †	Hukseflux Pyranometer Model SR25, S/N 2541	04/19/2019	04/19/2020
Diffuse Irradiance †	Hukseflux Pyranometer Model SR25, S/N 2542	04/19/2019	04/19/2020
Data Acquisition	NREL Data Acquisition System Model RAP-DAQ, S/N 2005-998	02/14/2019	02/14/2021
Data Acquisition	NREL Data Acquisition System Model RAP-DAQ, S/N 2005-999	02/14/2019	02/14/2021
Infrared Irradiance ‡	Kipp & Zonen Pyrgeometer Model CGR4, S/N 140021	04/02/2019	04/02/2023

† Through the World Radiometric Reference (WRR)

‡ Through the World Infrared Standard Group (WISG)

**Number of pages of certificate:** 4

**Calibration Procedure:** BORCAL-P00-Calibration and QA Procedure; available upon request.

**Setup:** Radiometers are calibrated outdoors, using the sun as the source. Pyranometers and pyrgeometers are installed for horizontal measurements, with their signal connectors oriented north, if their design permits.

The shading disk for the reference diffuse subtends a solid angle of 5°. Pyrheliometers are installed on solar trackers.

**Calibrated by:** RCC

-----  
Ibrahim Reda, Technical Manager

-----  
Date

For questions or comments, please contact the technical manager at:

ibrahim.reda@nrel.gov; 303-384-6385; 15013 Denver West Parkway, Golden, CO 80401, USA

# Calibration Results

## 080017 Kipp & Zonen CMP22

The responsivity ( $R$ ,  $\mu\text{V}/\text{W}/\text{m}^2$ ) of the test instrument during calibration is calculated using this Measurement Equation:

$$R = (V - R_{net} * W_{net}) / I \tag{1}$$

where,

- $V$  = radiometer output voltage (microvolts),
  - $R_{net}$  = radiometer net infrared responsivity ( $\mu\text{V}/\text{W}/\text{m}^2$ ), see Table 4,
  - $W_{net}$  = effective net infrared measured by pyrgeometer ( $\text{W}/\text{m}^2$ ),
  - =  $W_{in} - W_{out} = W_{in} - \sigma * T_c^4$
  - where,  $W_{in}$  = incoming infrared ( $\text{W}/\text{m}^2$ ),  $\sigma = 5.6704\text{e-}8 \text{ W}\cdot\text{m}^{-2}\cdot\text{K}^{-4}$ ,
  - $T_c$  = case temperature of pyrgeometer (K).
- $I$  = reference irradiance ( $\text{W}/\text{m}^2$ ), beam (B) or global (G)
  - where,  $G = B * \text{COS}(Z) + D$ ,
  - $Z$  = zenith angle (degrees),
  - $D$  = reference diffuse irradiance ( $\text{W}/\text{m}^2$ ).

Figure 1. Responsivity vs Zenith Angle

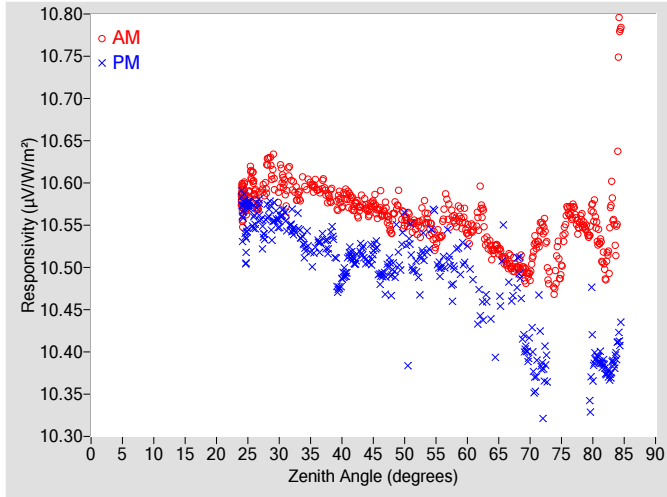


Figure 2. Responsivity vs Local Standard Time

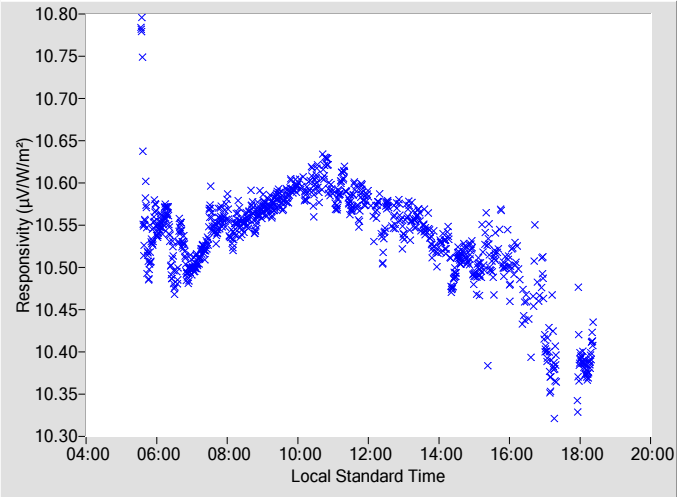


Table 2. Instrument Responsivity (R) and Calibration Type-B Standard Uncertainty,  $u(B)$

Zenith Angle (deg.)	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	AM $u(B)$ $\pm$ (%)	Azimuth Angle	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	PM $u(B)$ $\pm$ (%)	Azimuth Angle	Zenith Angle (deg.)	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	AM $u(B)$ $\pm$ (%)	Azimuth Angle	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	PM $u(B)$ $\pm$ (%)	Azimuth Angle
0	N/A	N/A	N/A	N/A	N/A	N/A	46	10.572	0.34	108.16	10.489	0.38	251.95
2	N/A	N/A	N/A	N/A	N/A	N/A	48	10.551	0.35	105.90	10.490	0.39	254.15
4	N/A	N/A	N/A	N/A	N/A	N/A	50	10.556	0.36	103.75	10.546	0.44	256.52
6	N/A	N/A	N/A	N/A	N/A	N/A	52	10.548	0.37	101.62	10.497	0.44	258.41
8	N/A	N/A	N/A	N/A	N/A	N/A	54	10.548	0.38	99.69	10.534	0.47	260.51
10	N/A	N/A	N/A	N/A	N/A	N/A	56	10.551	0.38	97.74	10.504	0.50	262.26
12	N/A	N/A	N/A	N/A	N/A	N/A	58	10.555	0.39	95.95	10.507	0.51	264.15
14	N/A	N/A	N/A	N/A	N/A	N/A	60	10.543	0.41	94.21	10.525	N/A	265.93
16	N/A	N/A	N/A	N/A	N/A	N/A	62	10.571	0.42	92.43	10.458	0.51	267.64
18	N/A	N/A	N/A	N/A	N/A	N/A	64	10.517	0.43	90.79	10.439	0.53	269.13
20	N/A	N/A	N/A	N/A	N/A	N/A	66	10.507	0.46	89.11	10.550	N/A	270.80
22	N/A	N/A	N/A	N/A	N/A	N/A	68	10.498	0.48	87.49	10.493	N/A	272.71
24	10.578	0.32	174.57	10.569	0.32	187.00	70	10.494	0.52	85.85	10.413	N/A	274.28
26	10.596	0.32	154.04	10.556	0.32	206.09	72	10.549	0.56	84.23	10.369	N/A	275.91
28	10.612	0.33	144.18	10.563	0.33	215.96	74	10.485	0.63	82.66	N/A	N/A	N/A
30	10.596	0.34	137.18	10.555	0.34	222.79	76	10.566	0.69	81.05	N/A	N/A	N/A
32	10.599	0.33	131.41	10.549	0.34	228.40	78	10.555	N/A	79.44	N/A	N/A	N/A
34	10.601	0.33	127.26	10.524	0.34	233.04	80	10.569	N/A	77.79	10.407	N/A	282.39
36	10.596	0.33	123.03	10.529	0.35	237.26	82	10.500	N/A	76.13	10.377	N/A	284.05
38	10.583	0.33	119.43	10.527	0.35	240.58	84	10.677	N/A	74.47	10.410	N/A	285.73
40	10.578	0.33	116.28	10.487	0.36	243.96	86	N/A	N/A	N/A	N/A	N/A	N/A
42	10.573	0.34	113.30	10.507	0.39	246.76	88	N/A	N/A	N/A	N/A	N/A	N/A
44	10.568	0.34	110.74	10.507	0.39	249.50	90	N/A	N/A	N/A	N/A	N/A	N/A

N/A - Not Available

Figure 3. Type-B Standard Uncertainty vs Zenith Angle

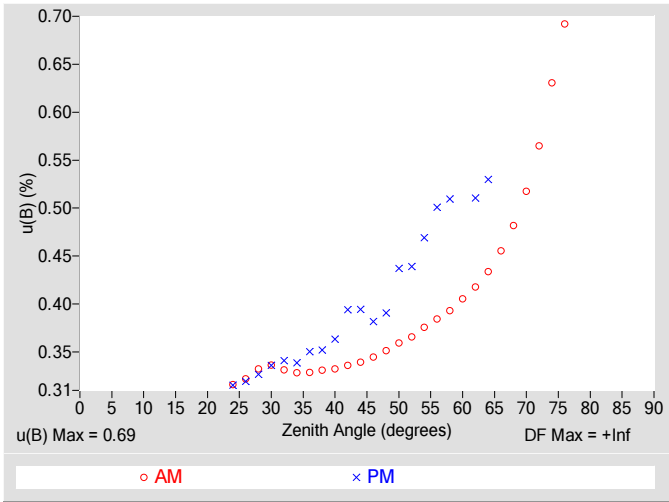


Figure 4. Residuals from Spline Interpolation

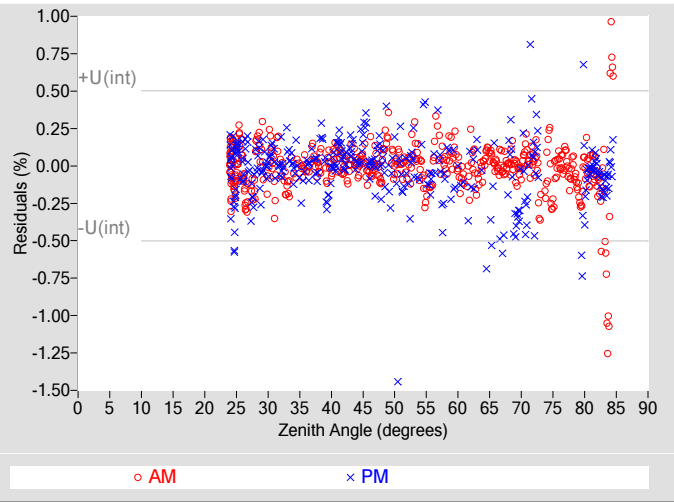


Table 3. Uncertainty using Spline Interpolation ‡

Type-B Standard Uncertainty, u(B) (%)	±0.69
Type-A Interpolating Function, u(int) (%)	±0.25
Combined Standard Uncertainty, u(c) (%)	±0.74
Effective degrees of freedom, DF(c)	52439
Coverage factor, k	1.96
Expanded Uncertainty, U95 (%)	±1.4
AM Valid zenith angle range	24° to 76°
PM Valid zenith angle range	24° to 64°

‡ An illustration for how to reduce the uncertainty in calculating the irradiance using a function rather than R@45°. Not accredited.

Table 4. Calibration Label Values

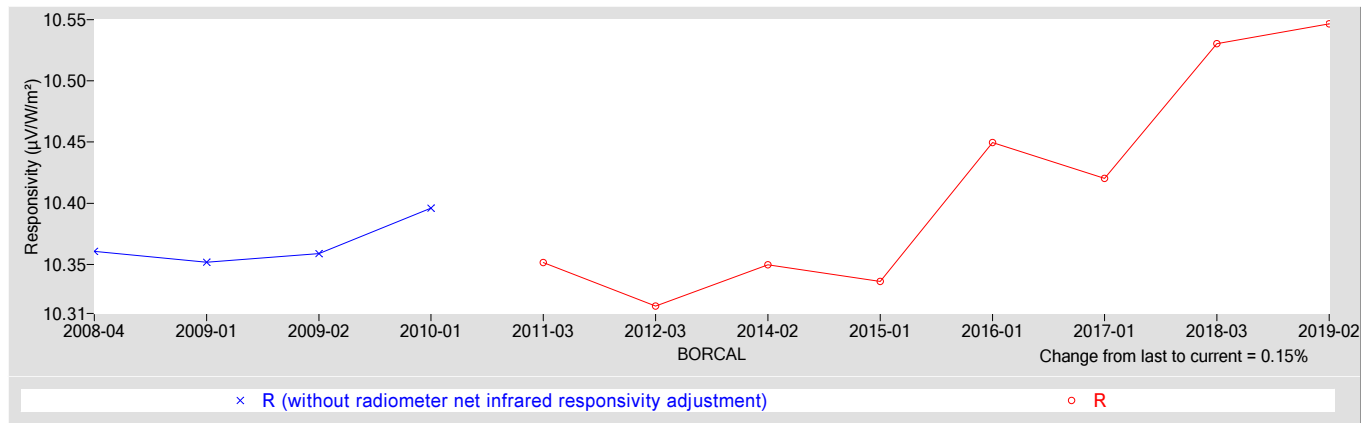
R @ 45° (μV/W/m²)	Rnet (μV/W/m²) †
10.547	0.087000

† Rnet determination date: Estimated

Table 5. Uncertainty using R @ 45°

Type-B Expanded Uncertainty, U(B) (%)	±1.00
Offset Uncertainty, U(off) (%)	+0.52 / -0.57
Expanded Uncertainty, U (%)	+1.5 / -1.6
Effective degrees of freedom, DF	+Inf
Coverage factor, k	1.96
Valid zenith angle range	30.0° to 60.0°

Figure 5. History of instrument at Zenith Angle = 45°



References:

[1] Reda, I.; Hickey, J.; Long, C.; Myers, D.; Stoffel, T.; Wilcox, S.; Michalsky, J. J.; Dutton, E. G.; Nelson, D. (2005). "Using a Blackbody to Calculate Net Longwave Responsivity of Shortwave Solar Pyranometers to Correct for Their Thermal Offset Error During Outdoor Calibration Using the Component Sum Method." Journal of Atmospheric and Oceanic Technology. , 2005; pp. 1531-1540; NREL Report No. JA-560-36646. doi:10.1175/JTECH1782.1

[2] Reda, I.; Myers, D.; Stoffel, T. (2008). "Uncertainty Estimate for the Outdoor Calibration of Solar Pyranometers: A Metrologist Perspective." Measure. (NCSLI Journal of Measurement Science). Vol. 3(4), December 2008; pp. 58-66; NREL Report No. JA-581-4137

[3] Reda, I.; Andreas, A. (2004). "Solar Position Algorithm for Solar Radiation Applications." Solar Energy. Vol. 76(5), 2004; pp. 577-589; NREL Report No. JA-560-35518. doi:10.1016/j.solener.2003.12.003

[4] Stoffel, T.; Reda, I. (2009). "NREL Pyrheliometer Comparisons: 22 September - 3 October 2008 (NPC-2008)." 54 pp.; NREL Report No. TP-550-45016.

[5] Reda, I.; Stoffel, T.; Myers, D. (2003). "Method to Calibrate a Solar Pyranometer for Measuring Reference Diffuse Irradiance." Solar Energy. Vol. 74, 2003; pp. 103-112; NREL Report No. JA-560-35025. doi:10.1016/S0038-092X(03)00124-5

[6] Reda, I. (1996). Calibration of a Solar Absolute Cavity Radiometer with Traceability to the World Radiometric Reference. 79 pp.; NREL Report No. TP-463-20619.

[7] Reda, I.; Gröbner, J.; Stoffel, T.; Myers, D.; Forgan, B. (2008). Improvements in the Blackbody Calibration of Pyrgometers. ARM 2008 Science Team Meeting (Poster).



# National Renewable Energy Laboratory

## Solar Radiation Research Laboratory

### Metrology Laboratory

### Calibration Certificate



<b>Test Instrument:</b>	Pyranometer	<b>Manufacturer:</b>	Kipp & Zonen
<b>Model:</b>	CMP22	<b>Serial Number:</b>	100174
<b>Calibration Date:</b>	5/3/2019	<b>Due Date:</b>	5/3/2020
<b>Customer:</b>	NREL-SRRL-BMS	<b>Environmental Conditions:</b>	see page 4
<b>Test Dates:</b>	5/3		

This certifies that the above product was calibrated in compliance with ISO/IEC 17025:2005. Measurement uncertainties at the time of calibration are consistent with the Guide to the Expression of Uncertainty in Measurement (GUM) using Reda et al., 2008. All nominal values are traceable to the International System (SI) Units of Measurement.

No statement of compliance with specifications is made or implied on this certificate. However, the estimated uncertainties are the uncertainties of the calibration process; users must add other uncertainties that are relevant to their measuring system, environmental and sky conditions, outdoor set-up, and site location.

The Type-B Standard Uncertainty of using the responsivity at each even zenith angle is reported, and the Expanded Uncertainty of the calibration is reported using two methods:

1. The Expanded Uncertainty of using the responsivity at zenith angle = 45°, within the zenith angle range from 30.0° to 60.0°
2. The Expanded Uncertainty of using Spline Interpolating Functions for the responsivity versus zenith angle.

This certificate applies only to the item identified above and shall not be reproduced other than in full, without specific written approval from the calibration facility. Certificate without signature is not valid.

**Table 1. Traceability**

Measurement Type	Instrument	Calibration Date	Calibration Due Date
Beam Irradiance †	Eppley Absolute Cavity Radiometer Model HF, S/N 29219	09/24/2018	09/24/2019
Diffuse Irradiance †	Hukseflux Pyranometer Model SR25, S/N 2541	04/19/2019	04/19/2020
Diffuse Irradiance †	Hukseflux Pyranometer Model SR25, S/N 2542	04/19/2019	04/19/2020
Data Acquisition	NREL Data Acquisition System Model RAP-DAQ, S/N 2005-998	02/14/2019	02/14/2021
Data Acquisition	NREL Data Acquisition System Model RAP-DAQ, S/N 2005-999	02/14/2019	02/14/2021
Infrared Irradiance ‡	Kipp & Zonen Pyrgeometer Model CG4, S/N FT002	04/16/2018	04/16/2022

† Through the World Radiometric Reference (WRR)

‡ Through the World Infrared Standard Group (WISG)

**Number of pages of certificate:** 4

**Calibration Procedure:** BORCAL-P00-Calibration and QA Procedure; available upon request.

**Setup:** Radiometers are calibrated outdoors, using the sun as the source. Pyranometers and pyrgeometers are installed for horizontal measurements, with their signal connectors oriented north, if their design permits.

The shading disk for the reference diffuse subtends a solid angle of 5°. Pyrheliometers are installed on solar trackers.

**Calibrated by:** RCC

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Ibrahim Reda, Technical Manager

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Date

For questions or comments, please contact the technical manager at:

ibrahim.reda@nrel.gov; 303-384-6385; 15013 Denver West Parkway, Golden, CO 80401, USA

# Calibration Results

## 100174 Kipp & Zonen CMP22

The responsivity ( $R$ ,  $\mu\text{V}/\text{W}/\text{m}^2$ ) of the test instrument during calibration is calculated using this Measurement Equation:

$$R = (V - R_{net} * W_{net}) / I \tag{1}$$

where,

- $V$  = radiometer output voltage (microvolts),
  - $R_{net}$  = radiometer net infrared responsivity ( $\mu\text{V}/\text{W}/\text{m}^2$ ), see Table 4,
  - $W_{net}$  = effective net infrared measured by pyrgeometer ( $\text{W}/\text{m}^2$ ),
  - =  $W_{in} - W_{out} = W_{in} - \sigma * T_c^4$
  - where,  $W_{in}$  = incoming infrared ( $\text{W}/\text{m}^2$ ),  $\sigma = 5.6704\text{e-}8 \text{ W}\cdot\text{m}^{-2}\cdot\text{K}^{-4}$ ,
  - $T_c$  = case temperature of pyrgeometer (K).
- $I$  = reference irradiance ( $\text{W}/\text{m}^2$ ), beam (B) or global (G)
  - where,  $G = B * \text{COS}(Z) + D$ ,
  - $Z$  = zenith angle (degrees),
  - $D$  = reference diffuse irradiance ( $\text{W}/\text{m}^2$ ).

Figure 1. Responsivity vs Zenith Angle

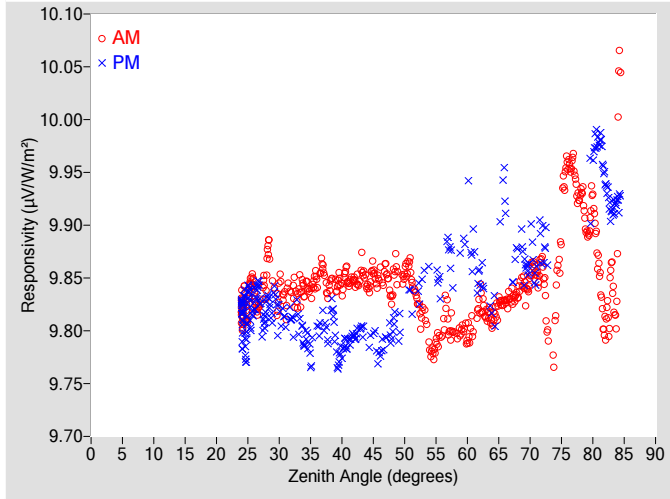


Figure 2. Responsivity vs Local Standard Time

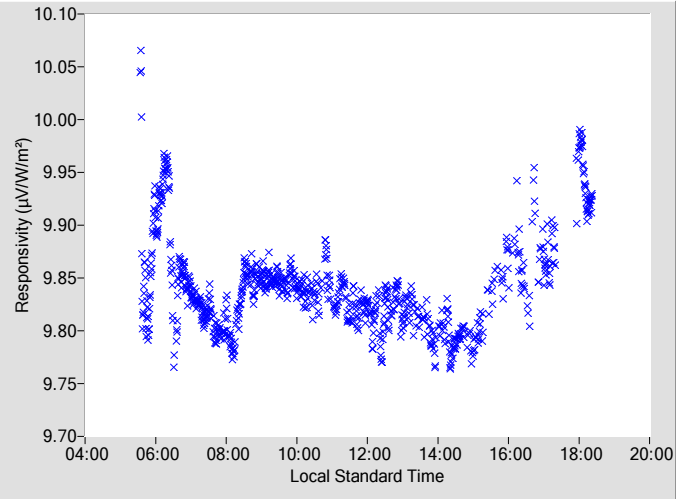


Table 2. Instrument Responsivity (R) and Calibration Type-B Standard Uncertainty, u(B)

Zenith Angle (deg.)	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle	Zenith Angle (deg.)	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle
0	N/A	N/A	N/A	N/A	N/A	N/A	46	9.8526	0.34	108.34	9.7747	0.38	251.79
2	N/A	N/A	N/A	N/A	N/A	N/A	48	9.8361	0.35	105.95	9.7981	0.39	254.21
4	N/A	N/A	N/A	N/A	N/A	N/A	50	9.8557	0.36	103.74	N/A	N/A	N/A
6	N/A	N/A	N/A	N/A	N/A	N/A	52	9.8303	0.37	101.75	9.8414	0.44	258.65
8	N/A	N/A	N/A	N/A	N/A	N/A	54	9.7817	0.38	99.63	9.8610	0.47	260.29
10	N/A	N/A	N/A	N/A	N/A	N/A	56	9.8002	0.38	97.78	N/A	N/A	N/A
12	N/A	N/A	N/A	N/A	N/A	N/A	58	9.7992	0.39	96.09	N/A	N/A	N/A
14	N/A	N/A	N/A	N/A	N/A	N/A	60	9.7959	0.41	94.20	9.9422	N/A	266.07
16	N/A	N/A	N/A	N/A	N/A	N/A	62	9.8275	0.42	92.45	9.8525	0.51	267.59
18	N/A	N/A	N/A	N/A	N/A	N/A	64	9.8088	0.43	90.79	9.8250	0.55	269.45
20	N/A	N/A	N/A	N/A	N/A	N/A	66	9.8276	0.46	89.10	9.9295	N/A	271.02
22	N/A	N/A	N/A	N/A	N/A	N/A	68	9.8351	0.48	87.49	9.8782	N/A	272.60
24	9.8193	0.32	174.60	9.8146	0.32	185.66	70	9.8498	0.52	85.85	9.8824	N/A	274.28
26	9.8353	0.32	153.77	9.8248	0.32	206.06	72	9.8593	0.56	84.27	9.8759	N/A	275.91
28	9.8598	0.33	144.08	9.8222	0.33	215.43	74	9.8082	0.63	82.63	N/A	N/A	N/A
30	9.8377	0.34	137.37	9.8127	0.34	222.58	76	9.9586	0.69	81.04	N/A	N/A	N/A
32	9.8390	0.33	131.78	9.8087	0.34	228.46	78	9.9281	N/A	79.43	N/A	N/A	N/A
34	9.8399	0.33	127.08	9.7898	0.34	233.16	80	9.9225	N/A	77.83	9.9682	N/A	282.52
36	9.8476	0.33	123.17	9.8044	0.35	237.42	82	9.8059	N/A	76.17	9.9406	N/A	284.05
38	9.8399	0.33	119.47	9.8036	0.35	240.73	84	9.9362	N/A	74.51	9.9226	N/A	285.72
40	9.8402	0.33	116.28	9.7809	0.36	243.88	86	N/A	N/A	N/A	N/A	N/A	N/A
42	9.8472	0.34	113.44	9.7945	0.39	246.90	88	N/A	N/A	N/A	N/A	N/A	N/A
44	9.8438	0.34	110.71	N/A	N/A	N/A	90	N/A	N/A	N/A	N/A	N/A	N/A

N/A - Not Available



Figure 3. Type-B Standard Uncertainty vs Zenith Angle

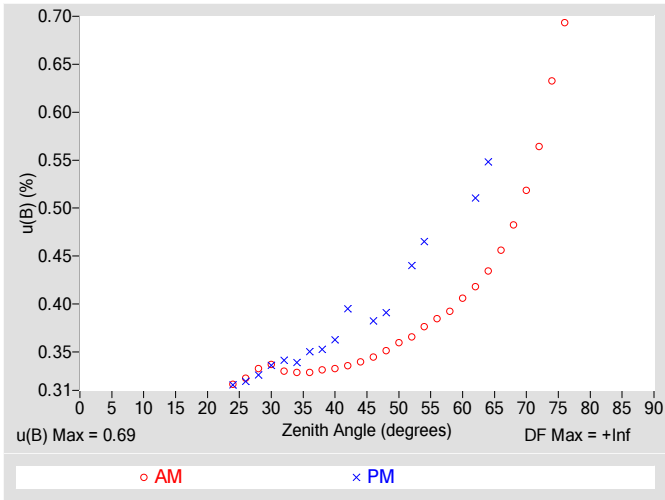


Figure 4. Residuals from Spline Interpolation

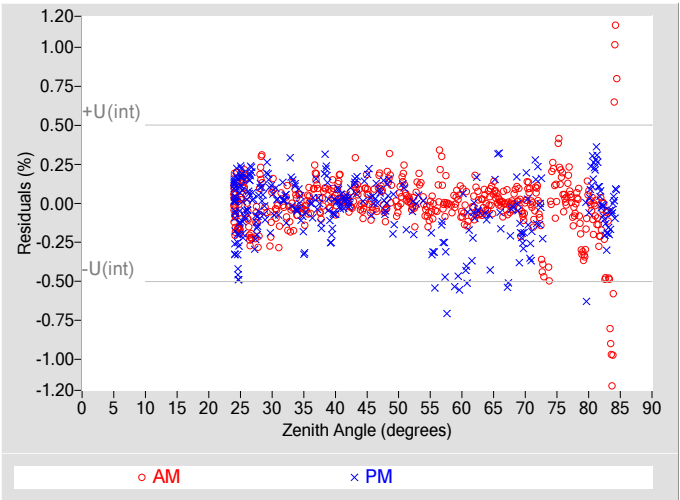


Table 3. Uncertainty using Spline Interpolation ‡

Type-B Standard Uncertainty, u(B) (%)	±0.69
Type-A Interpolating Function, u(int) (%)	±0.25
Combined Standard Uncertainty, u(c) (%)	±0.74
Effective degrees of freedom, DF(c)	50869
Coverage factor, k	1.96
Expanded Uncertainty, U95 (%)	±1.4
AM Valid zenith angle range	24° to 76°
PM Valid zenith angle range	24° to 64°

‡ An illustration for how to reduce the uncertainty in calculating the irradiance using a function rather than R@45°. Not accredited.

Table 4. Calibration Label Values

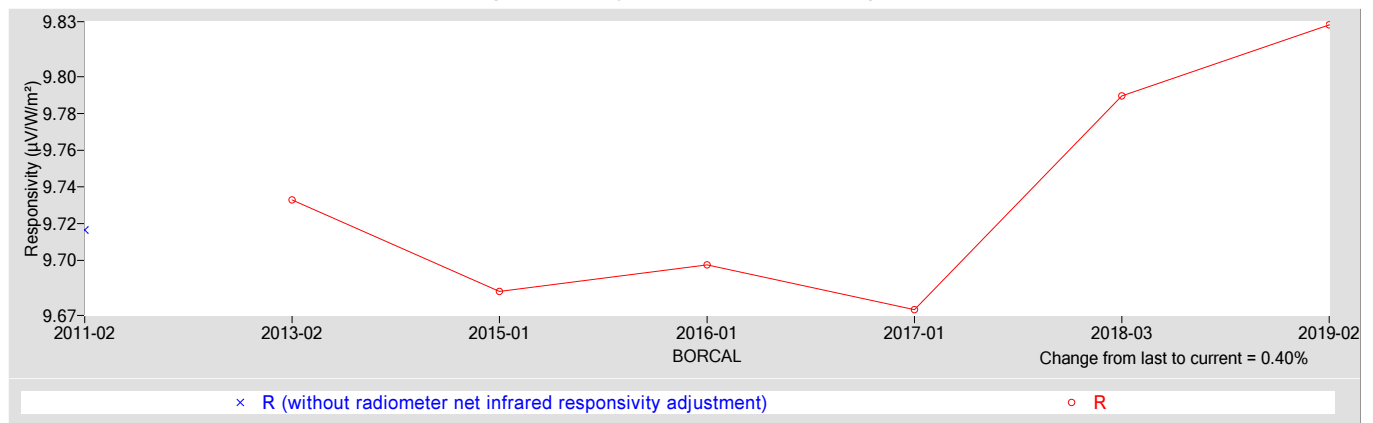
R @ 45° (μV/W/m²)	Rnet (μV/W/m²) †
9.8283	0.087000

† Rnet determination date: Estimated

Table 5. Uncertainty using R @ 45°

Type-B Expanded Uncertainty, U(B) (%)	±0.91
Offset Uncertainty, U(off) (%)	+1.2 / -0.55
Expanded Uncertainty, U (%)	+2.1 / -1.5
Effective degrees of freedom, DF	+Inf
Coverage factor, k	1.96
Valid zenith angle range	30.0° to 60.0°

Figure 5. History of instrument at Zenith Angle = 45°



References:

[1] Reda, I.; Hickey, J.; Long, C.; Myers, D.; Stoffel, T.; Wilcox, S.; Michalsky, J. J.; Dutton, E. G.; Nelson, D. (2005). "Using a Blackbody to Calculate Net Longwave Responsivity of Shortwave Solar Pyranometers to Correct for Their Thermal Offset Error During Outdoor Calibration Using the Component Sum Method." Journal of Atmospheric and Oceanic Technology. , 2005; pp. 1531-1540; NREL Report No. JA-560-36646. doi:10.1175/JTECH1782.1

[2] Reda, I.; Myers, D.; Stoffel, T. (2008). "Uncertainty Estimate for the Outdoor Calibration of Solar Pyranometers: A Metrologist Perspective." Measure. (NCSLI Journal of Measurement Science). Vol. 3(4), December 2008; pp. 58-66; NREL Report No. JA-581-4137

[3] Reda, I.; Andreas, A. (2004). "Solar Position Algorithm for Solar Radiation Applications." Solar Energy. Vol. 76(5), 2004; pp. 577-589; NREL Report No. JA-560-35518. doi:10.1016/j.solener.2003.12.003

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[5] Reda, I.; Stoffel, T.; Myers, D. (2003). "Method to Calibrate a Solar Pyranometer for Measuring Reference Diffuse Irradiance." Solar Energy. Vol. 74, 2003; pp. 103-112; NREL Report No. JA-560-35025. doi:10.1016/S0038-092X(03)00124-5

[6] Reda, I. (1996). Calibration of a Solar Absolute Cavity Radiometer with Traceability to the World Radiometric Reference. 79 pp.; NREL Report No. TP-463-20619.

[7] Reda, I.; Gröbner, J.; Stoffel, T.; Myers, D.; Forgan, B. (2008). Improvements in the Blackbody Calibration of Pyrgeometers. ARM 2008 Science Team Meeting (Poster).





# National Renewable Energy Laboratory

## Solar Radiation Research Laboratory

### Metrology Laboratory

### Calibration Certificate



<b>Test Instrument:</b>	Thermopile Pyranometer	<b>Manufacturer:</b>	Apogee
<b>Model:</b>	SP-510	<b>Serial Number:</b>	1171
<b>Calibration Date:</b>	5/3/2019	<b>Due Date:</b>	5/3/2020
<b>Customer:</b>	NREL-SRRL-BMS	<b>Environmental Conditions:</b>	see page 4
<b>Test Dates:</b>	5/3		

This certifies that the above product was calibrated in compliance with ISO/IEC 17025:2005. Measurement uncertainties at the time of calibration are consistent with the Guide to the Expression of Uncertainty in Measurement (GUM) using Reda et al., 2008. All nominal values are traceable to the International System (SI) Units of Measurement.

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The Type-B Standard Uncertainty of using the responsivity at each even zenith angle is reported, and the Expanded Uncertainty of the calibration is reported using two methods:

1. The Expanded Uncertainty of using the responsivity at zenith angle = 45°, within the zenith angle range from 30.0° to 60.0°
2. The Expanded Uncertainty of using Spline Interpolating Functions for the responsivity versus zenith angle.

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**Table 1. Traceability**

Measurement Type	Instrument	Calibration Date	Calibration Due Date
Beam Irradiance †	Eppley Absolute Cavity Radiometer Model HF, S/N 29219	09/24/2018	09/24/2019
Diffuse Irradiance †	Hukseflux Pyranometer Model SR25, S/N 2541	04/19/2019	04/19/2020
Diffuse Irradiance †	Hukseflux Pyranometer Model SR25, S/N 2542	04/19/2019	04/19/2020
Data Acquisition	NREL Data Acquisition System Model RAP-DAQ, S/N 2005-998	02/14/2019	02/14/2021
Data Acquisition	NREL Data Acquisition System Model RAP-DAQ, S/N 2005-999	02/14/2019	02/14/2021
Infrared Irradiance ‡	Kipp & Zonen Pyrgeometer Model CG4, S/N FT002	04/16/2018	04/16/2022

† Through the World Radiometric Reference (WRR)

‡ Through the World Infrared Standard Group (WISG)

**Number of pages of certificate:** 4

**Calibration Procedure:** BORCAL-P00-Calibration and QA Procedure; available upon request.

**Setup:** Radiometers are calibrated outdoors, using the sun as the source. Pyranometers and pyrgeometers are installed for horizontal measurements, with their signal connectors oriented north, if their design permits.

The shading disk for the reference diffuse subtends a solid angle of 5°. Pyrheliometers are installed on solar trackers.

**Calibrated by:** RCC

-----  
Ibrahim Reda, Technical Manager

-----  
Date

For questions or comments, please contact the technical manager at:

ibrahim.reda@nrel.gov; 303-384-6385; 15013 Denver West Parkway, Golden, CO 80401, USA

# Calibration Results

## 1171 Apogee SP-510

The responsivity ( $R$ ,  $\mu\text{V}/\text{W}/\text{m}^2$ ) of the test instrument during calibration is calculated using this Measurement Equation:

$$R = (V - R_{net} * W_{net}) / I \tag{1}$$

where,

- $V$  = radiometer output voltage (microvolts),
  - $R_{net}$  = radiometer net infrared responsivity ( $\mu\text{V}/\text{W}/\text{m}^2$ ), see Table 4,
  - $W_{net}$  = effective net infrared measured by pyrgeometer ( $\text{W}/\text{m}^2$ ),
  - =  $W_{in} - W_{out} = W_{in} - \sigma * T_c^4$
  - where,  $W_{in}$  = incoming infrared ( $\text{W}/\text{m}^2$ ),  $\sigma = 5.6704\text{e-}8 \text{ W}\cdot\text{m}^{-2}\cdot\text{K}^{-4}$ ,
  - $T_c$  = case temperature of radiometer (K).
- $I$  = reference irradiance ( $\text{W}/\text{m}^2$ ), beam (B) or global (G)
  - where,  $G = B * \text{COS}(Z) + D$ ,
  - $Z$  = zenith angle (degrees),
  - $D$  = reference diffuse irradiance ( $\text{W}/\text{m}^2$ ).

Figure 1. Responsivity vs Zenith Angle

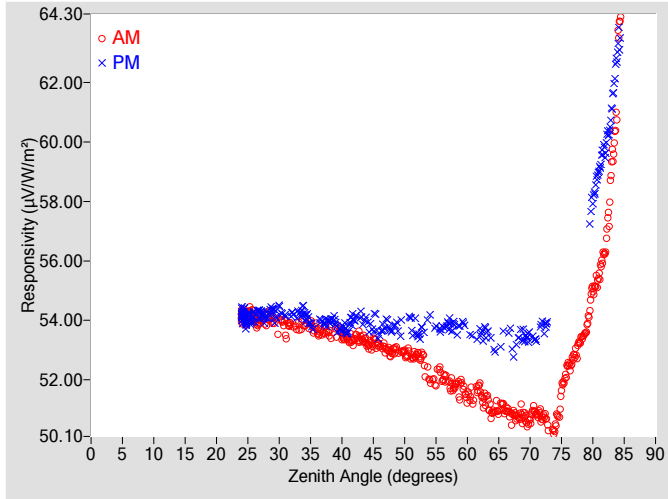


Figure 2. Responsivity vs Local Standard Time

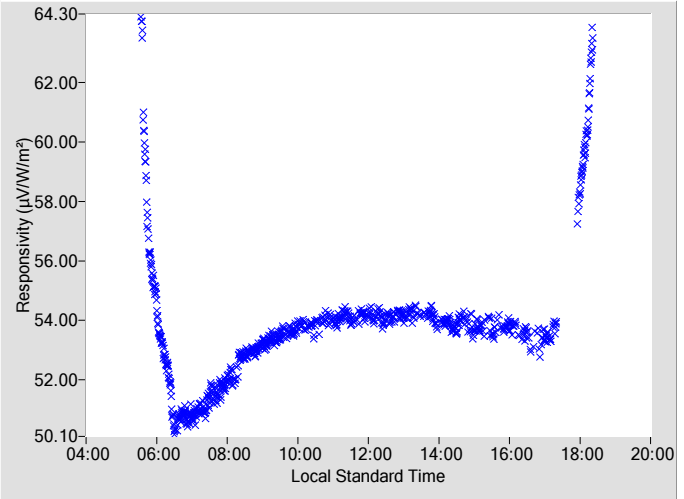


Table 2. Instrument Responsivity (R) and Calibration Type-B Standard Uncertainty, u(B)

Zenith			AM			PM			Zenith			AM			PM		
Angle	R	u(B)	Azimuth	R	u(B)	Azimuth	Angle	R	u(B)	Azimuth	R	u(B)	Azimuth	R	u(B)	Azimuth	
(deg.)	( $\mu\text{V}/\text{W}/\text{m}^2$ )	± (%)	Angle	( $\mu\text{V}/\text{W}/\text{m}^2$ )	± (%)	Angle	(deg.)	( $\mu\text{V}/\text{W}/\text{m}^2$ )	± (%)	Angle	( $\mu\text{V}/\text{W}/\text{m}^2$ )	± (%)	Angle	( $\mu\text{V}/\text{W}/\text{m}^2$ )	± (%)	Angle	
0	N/A	N/A	N/A	N/A	N/A	N/A	46	53.172	0.36	108.30	53.509	0.40	251.91				
2	N/A	N/A	N/A	N/A	N/A	N/A	48	52.937	0.37	105.92	53.630	0.41	254.11				
4	N/A	N/A	N/A	N/A	N/A	N/A	50	52.898	0.37	103.76	N/A	N/A	N/A				
6	N/A	N/A	N/A	N/A	N/A	N/A	52	52.833	0.38	101.67	53.509	0.46	258.46				
8	N/A	N/A	N/A	N/A	N/A	N/A	54	51.969	0.40	99.70	54.192	0.50	260.47				
10	N/A	N/A	N/A	N/A	N/A	N/A	56	52.080	0.41	97.77	53.753	0.53	262.34				
12	N/A	N/A	N/A	N/A	N/A	N/A	58	51.781	0.43	95.96	53.901	0.53	264.01				
14	N/A	N/A	N/A	N/A	N/A	N/A	60	51.450	0.44	94.22	N/A	N/A	N/A				
16	N/A	N/A	N/A	N/A	N/A	N/A	62	51.720	0.46	92.47	53.599	0.54	267.75				
18	N/A	N/A	N/A	N/A	N/A	N/A	64	50.877	0.48	90.80	53.218	0.56	269.37				
20	N/A	N/A	N/A	N/A	N/A	N/A	66	51.005	0.50	89.12	53.641	N/A	270.81				
22	N/A	N/A	N/A	N/A	N/A	N/A	68	50.718	0.53	87.53	53.340	N/A	272.73				
24	54.183	0.33	175.30	54.157	0.33	185.06	70	50.641	0.57	85.87	53.433	N/A	274.16				
26	54.112	0.33	154.13	54.144	0.33	205.45	72	50.707	0.61	84.24	53.798	N/A	275.91				
28	53.978	0.34	144.74	54.159	0.34	216.35	74	50.426	0.69	82.67	N/A	N/A	N/A				
30	53.770	0.35	137.11	54.490	0.35	222.79	76	52.440	0.76	81.02	N/A	N/A	N/A				
32	53.851	0.34	131.79	54.227	0.35	228.43	78	53.316	N/A	79.45	N/A	N/A	N/A				
34	53.815	0.34	126.91	54.240	0.35	233.17	80	55.013	N/A	77.80	58.052	N/A	282.37				
36	53.676	0.34	122.81	N/A	N/A	N/A	82	56.471	N/A	76.14	59.845	N/A	284.02				
38	53.549	0.34	119.43	53.983	0.37	240.70	84	62.605	N/A	74.47	63.130	N/A	285.70				
40	53.475	0.35	116.20	53.721	0.38	243.84	86	N/A	N/A	N/A	N/A	N/A	N/A				
42	53.390	0.35	113.31	54.043	0.41	246.75	88	N/A	N/A	N/A	N/A	N/A	N/A				
44	53.232	0.35	110.76	54.019	0.41	249.39	90	N/A	N/A	N/A	N/A	N/A	N/A				

N/A - Not Available

Figure 3. Type-B Standard Uncertainty vs Zenith Angle

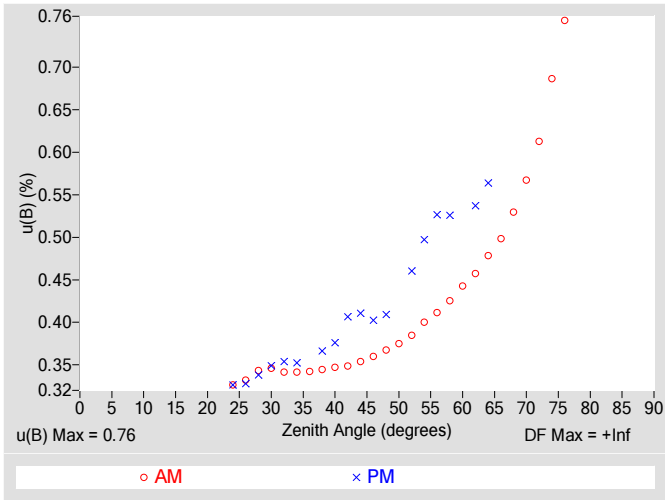


Figure 4. Residuals from Spline Interpolation

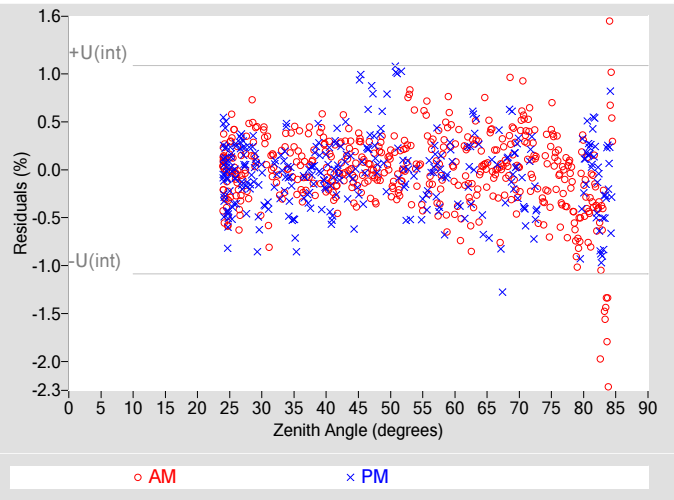


Table 3. Uncertainty using Spline Interpolation ‡

Type-B Standard Uncertainty, u(B) (%)	±0.76
Type-A Interpolating Function, u(int) (%)	±0.54
Combined Standard Uncertainty, u(c) (%)	±0.93
Effective degrees of freedom, DF(c)	5659
Coverage factor, k	1.96
Expanded Uncertainty, U95 (%)	±1.8
AM Valid zenith angle range	24° to 76°
PM Valid zenith angle range	24° to 64°

‡ An illustration for how to reduce the uncertainty in calculating the irradiance using a function rather than R@45°. Not accredited.

Table 4. Calibration Label Values

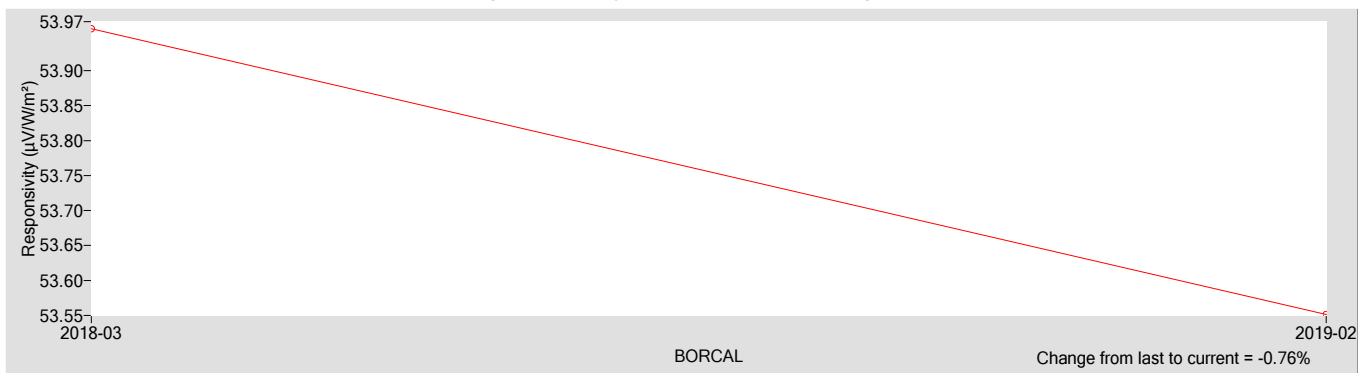
R @ 45° (μV/W/m²)	Rnet (μV/W/m²) †
53.551	2.5000

† Rnet determination date: Estimated

Table 5. Uncertainty using R @ 45°

Type-B Expanded Uncertainty, U(B) (%)	±1.0
Offset Uncertainty, U(off) (%)	+1.8 / -3.9
Expanded Uncertainty, U (%)	+2.8 / -5.0
Effective degrees of freedom, DF	+Inf
Coverage factor, k	1.96
Valid zenith angle range	30.0° to 60.0°

Figure 5. History of instrument at Zenith Angle = 45°



References:

- [1] Reda, I.; Hickey, J.; Long, C.; Myers, D.; Stoffel, T.; Wilcox, S.; Michalsky, J. J.; Dutton, E. G.; Nelson, D. (2005). "Using a Blackbody to Calculate Net Longwave Responsivity of Shortwave Solar Pyranometers to Correct for Their Thermal Offset Error During Outdoor Calibration Using the Component Sum Method." Journal of Atmospheric and Oceanic Technology. , 2005; pp. 1531-1540; NREL Report No. JA-560-36646. doi:10.1175/JTECH1782.1
- [2] Reda, I.; Myers, D.; Stoffel, T. (2008). "Uncertainty Estimate for the Outdoor Calibration of Solar Pyranometers: A Metrologist Perspective." Measure. (NCSLI Journal of Measurement Science). Vol. 3(4), December 2008; pp. 58-66; NREL Report No. JA-581-4137
- [3] Reda, I.; Andreas, A. (2004). "Solar Position Algorithm for Solar Radiation Applications." Solar Energy. Vol. 76(5), 2004; pp. 577-589; NREL Report No. JA-560-35518. doi:10.1016/j.solener.2003.12.003
- [4] Stoffel, T.; Reda, I. (2009). "NREL Pyrheliometer Comparisons: 22 September - 3 October 2008 (NPC-2008)." 54 pp.; NREL Report No. TP-550-45016.
- [5] Reda, I.; Stoffel, T.; Myers, D. (2003). "Method to Calibrate a Solar Pyranometer for Measuring Reference Diffuse Irradiance." Solar Energy. Vol. 74, 2003; pp. 103-112; NREL Report No. JA-560-35025. doi:10.1016/S0038-092X(03)00124-5
- [6] Reda, I. (1996). Calibration of a Solar Absolute Cavity Radiometer with Traceability to the World Radiometric Reference. 79 pp.; NREL Report No. TP-463-20619.
- [7] Reda, I.; Gröbner, J.; Stoffel, T.; Myers, D.; Forgan, B. (2008). Improvements in the Blackbody Calibration of Pyrgeometers. ARM 2008 Science Team Meeting (Poster).



# National Renewable Energy Laboratory

## Solar Radiation Research Laboratory

### Metrology Laboratory

### Calibration Certificate



<b>Test Instrument:</b>	Pyranometer	<b>Manufacturer:</b>	Kipp & Zonen
<b>Model:</b>	CMP22	<b>Serial Number:</b>	140043
<b>Calibration Date:</b>	5/3/2019	<b>Due Date:</b>	5/3/2020
<b>Customer:</b>	NREL-SRRL-BMS	<b>Environmental Conditions:</b>	see page 4
<b>Test Dates:</b>	5/3		

This certifies that the above product was calibrated in compliance with ISO/IEC 17025:2005. Measurement uncertainties at the time of calibration are consistent with the Guide to the Expression of Uncertainty in Measurement (GUM) using Reda et al., 2008. All nominal values are traceable to the International System (SI) Units of Measurement.

No statement of compliance with specifications is made or implied on this certificate. However, the estimated uncertainties are the uncertainties of the calibration process; users must add other uncertainties that are relevant to their measuring system, environmental and sky conditions, outdoor set-up, and site location.

The Type-B Standard Uncertainty of using the responsivity at each even zenith angle is reported, and the Expanded Uncertainty of the calibration is reported using two methods:

1. The Expanded Uncertainty of using the responsivity at zenith angle = 45°, within the zenith angle range from 30.0° to 60.0°
2. The Expanded Uncertainty of using Spline Interpolating Functions for the responsivity versus zenith angle.

This certificate applies only to the item identified above and shall not be reproduced other than in full, without specific written approval from the calibration facility. Certificate without signature is not valid.

**Table 1. Traceability**

Measurement Type	Instrument	Calibration Date	Calibration Due Date
Beam Irradiance †	Eppley Absolute Cavity Radiometer Model HF, S/N 29219	09/24/2018	09/24/2019
Diffuse Irradiance †	Hukseflux Pyranometer Model SR25, S/N 2541	04/19/2019	04/19/2020
Diffuse Irradiance †	Hukseflux Pyranometer Model SR25, S/N 2542	04/19/2019	04/19/2020
Data Acquisition	NREL Data Acquisition System Model RAP-DAQ, S/N 2005-998	02/14/2019	02/14/2021
Data Acquisition	NREL Data Acquisition System Model RAP-DAQ, S/N 2005-999	02/14/2019	02/14/2021
Infrared Irradiance ‡	Kipp & Zonen Pyrgeometer Model CG4, S/N FT002	04/16/2018	04/16/2022

† Through the World Radiometric Reference (WRR)

‡ Through the World Infrared Standard Group (WISG)

**Number of pages of certificate:** 4

**Calibration Procedure:** BORCAL-P00-Calibration and QA Procedure; available upon request.

**Setup:** Radiometers are calibrated outdoors, using the sun as the source. Pyranometers and pyrgeometers are installed for horizontal measurements, with their signal connectors oriented north, if their design permits.

The shading disk for the reference diffuse subtends a solid angle of 5°. Pyrheliometers are installed on solar trackers.

**Calibrated by:** RCC

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Ibrahim Reda, Technical Manager

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Date

For questions or comments, please contact the technical manager at:

ibrahim.reda@nrel.gov; 303-384-6385; 15013 Denver West Parkway, Golden, CO 80401, USA

# Calibration Results

## 140043 Kipp & Zonen CMP22

The responsivity ( $R$ ,  $\mu\text{V}/\text{W}/\text{m}^2$ ) of the test instrument during calibration is calculated using this Measurement Equation:

$$R = (V - R_{net} * W_{net}) / I \tag{1}$$

where,

- $V$  = radiometer output voltage (microvolts),
- $R_{net}$  = radiometer net infrared responsivity ( $\mu\text{V}/\text{W}/\text{m}^2$ ), see Table 4,
- $W_{net}$  = effective net infrared measured by pyrgeometer ( $\text{W}/\text{m}^2$ ),
- =  $W_{in} - W_{out} = W_{in} - \sigma * T_c^4$
- where,  $W_{in}$  = incoming infrared ( $\text{W}/\text{m}^2$ ),  $\sigma = 5.6704\text{e-}8 \text{ W}\cdot\text{m}^{-2}\cdot\text{K}^{-4}$ ,
- $T_c$  = case temperature of pyrgeometer (K).
- $I$  = reference irradiance ( $\text{W}/\text{m}^2$ ), beam (B) or global (G)
- where,  $G = B * \text{COS}(Z) + D$ ,
- $Z$  = zenith angle (degrees),
- $D$  = reference diffuse irradiance ( $\text{W}/\text{m}^2$ ).

Figure 1. Responsivity vs Zenith Angle

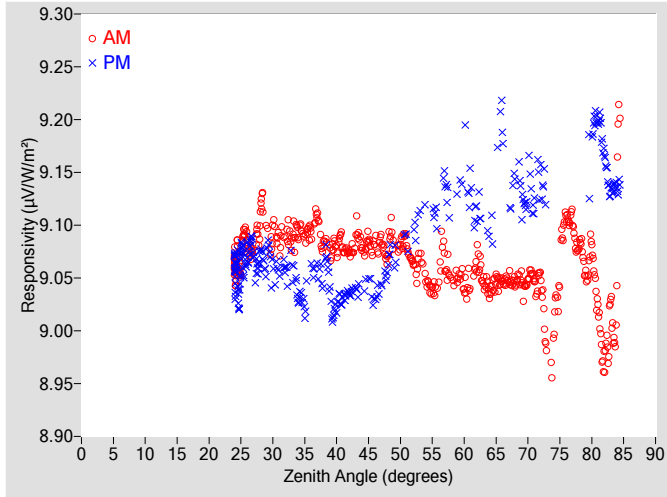


Figure 2. Responsivity vs Local Standard Time

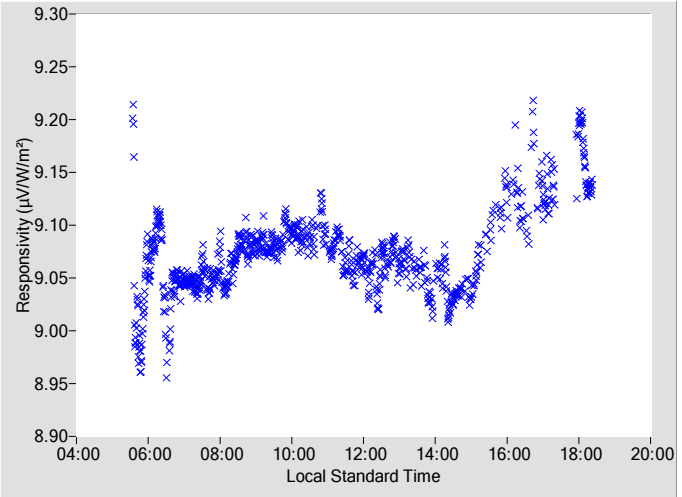


Table 2. Instrument Responsivity (R) and Calibration Type-B Standard Uncertainty, u(B)

Zenith Angle (deg.)	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle	Zenith Angle (deg.)	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle
0	N/A	N/A	N/A	N/A	N/A	N/A	46	9.0846	0.35	108.34	9.0283	0.38	251.79
2	N/A	N/A	N/A	N/A	N/A	N/A	48	9.0732	0.35	105.95	9.0594	0.39	254.21
4	N/A	N/A	N/A	N/A	N/A	N/A	50	9.0832	0.36	103.74	N/A	N/A	N/A
6	N/A	N/A	N/A	N/A	N/A	N/A	52	9.0650	0.37	101.75	9.0993	0.44	258.65
8	N/A	N/A	N/A	N/A	N/A	N/A	54	9.0474	0.38	99.63	9.1193	0.47	260.29
10	N/A	N/A	N/A	N/A	N/A	N/A	56	9.0505	0.39	97.78	N/A	N/A	N/A
12	N/A	N/A	N/A	N/A	N/A	N/A	58	9.0507	0.39	96.09	N/A	N/A	N/A
14	N/A	N/A	N/A	N/A	N/A	N/A	60	9.0433	0.41	94.20	9.1948	N/A	266.07
16	N/A	N/A	N/A	N/A	N/A	N/A	62	9.0651	0.42	92.45	9.1132	0.51	267.59
18	N/A	N/A	N/A	N/A	N/A	N/A	64	9.0365	0.44	90.79	9.0994	0.55	269.45
20	N/A	N/A	N/A	N/A	N/A	N/A	66	9.0464	0.46	89.10	9.1945	N/A	271.02
22	N/A	N/A	N/A	N/A	N/A	N/A	68	9.0462	0.48	87.49	9.1463	N/A	272.60
24	9.0606	0.32	174.60	9.0587	0.32	185.66	70	9.0487	0.52	85.85	9.1442	N/A	274.28
26	9.0846	0.32	153.77	9.0691	0.32	206.06	72	9.0466	0.57	84.27	9.1351	N/A	275.91
28	9.1059	0.33	144.08	9.0693	0.33	215.43	74	8.9907	0.63	82.63	N/A	N/A	N/A
30	9.0920	0.34	137.37	9.0557	0.34	222.58	76	9.1073	0.69	81.04	N/A	N/A	N/A
32	9.0912	0.33	131.78	9.0563	0.34	228.46	78	9.0799	N/A	79.43	N/A	N/A	N/A
34	9.0943	0.33	127.08	9.0310	0.34	233.16	80	9.0779	N/A	77.83	9.1888	N/A	282.52
36	9.0927	0.33	123.17	9.0613	0.35	237.42	82	8.9739	N/A	76.17	9.1635	N/A	284.05
38	9.0810	0.33	119.47	9.0546	0.35	240.73	84	9.1013	N/A	74.51	9.1362	N/A	285.72
40	9.0758	0.33	116.28	9.0231	0.36	243.88	86	N/A	N/A	N/A	N/A	N/A	N/A
42	9.0738	0.34	113.44	9.0350	0.40	246.90	88	N/A	N/A	N/A	N/A	N/A	N/A
44	9.0794	0.34	110.71	N/A	N/A	N/A	90	N/A	N/A	N/A	N/A	N/A	N/A

N/A - Not Available

Figure 3. Type-B Standard Uncertainty vs Zenith Angle

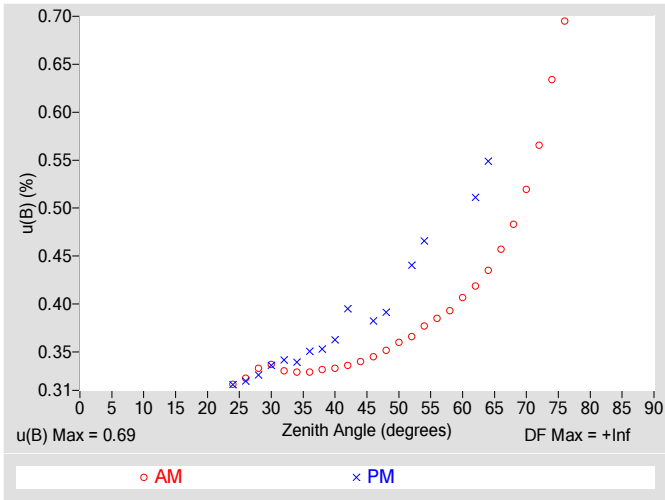


Figure 4. Residuals from Spline Interpolation

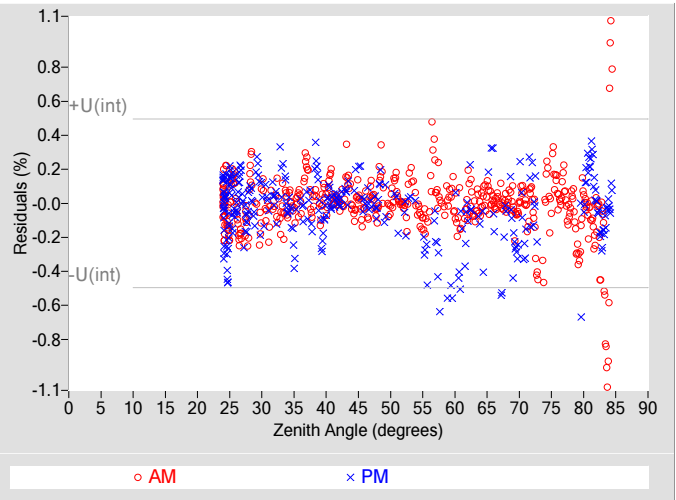


Table 3. Uncertainty using Spline Interpolation ‡

Type-B Standard Uncertainty, u(B) (%)	±0.69
Type-A Interpolating Function, u(int) (%)	±0.25
Combined Standard Uncertainty, u(c) (%)	±0.74
Effective degrees of freedom, DF(c)	53737
Coverage factor, k	1.96
Expanded Uncertainty, U95 (%)	±1.4
AM Valid zenith angle range	24° to 76°
PM Valid zenith angle range	24° to 64°

‡ An illustration for how to reduce the uncertainty in calculating the irradiance using a function rather than R@45°. Not accredited.

Table 4. Calibration Label Values

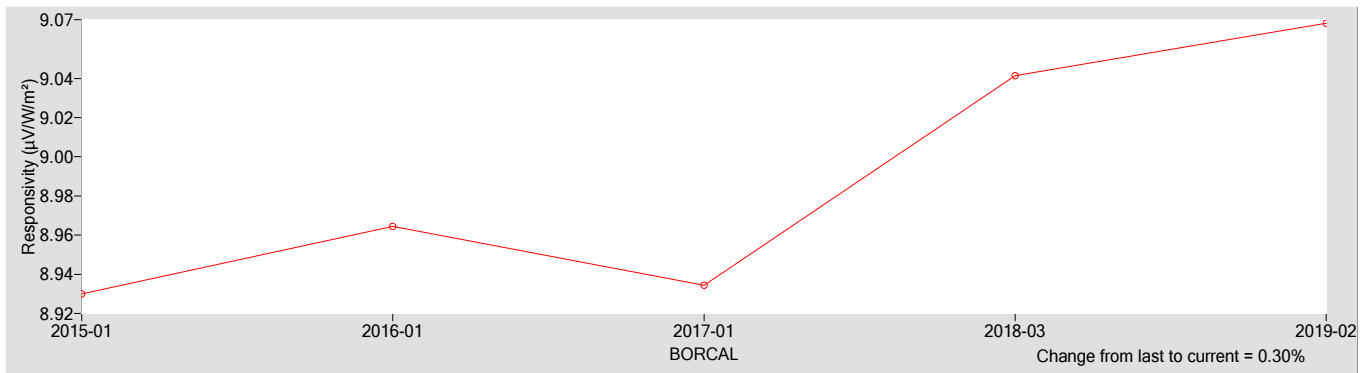
R @ 45° (μV/W/m²)	Rnet (μV/W/m²) †
9.0682	0.087000

† Rnet determination date: Estimated

Table 5. Uncertainty using R @ 45°

Type-B Expanded Uncertainty, U(B) (%)	±0.91
Offset Uncertainty, U(off) (%)	+1.4 / -0.50
Expanded Uncertainty, U (%)	+2.3 / -1.4
Effective degrees of freedom, DF	+Inf
Coverage factor, k	1.96
Valid zenith angle range	30.0° to 60.0°

Figure 5. History of instrument at Zenith Angle = 45°



References:

[1] Reda, I.; Hickey, J.; Long, C.; Myers, D.; Stoffel, T.; Wilcox, S.; Michalsky, J. J.; Dutton, E. G.; Nelson, D. (2005). "Using a Blackbody to Calculate Net Longwave Responsivity of Shortwave Solar Pyranometers to Correct for Their Thermal Offset Error During Outdoor Calibration Using the Component Sum Method." Journal of Atmospheric and Oceanic Technology. , 2005; pp. 1531-1540; NREL Report No. JA-560-36646. doi:10.1175/JTECH1782.1

[2] Reda, I.; Myers, D.; Stoffel, T. (2008). "Uncertainty Estimate for the Outdoor Calibration of Solar Pyranometers: A Metrologist Perspective." Measure. (NCSLI Journal of Measurement Science). Vol. 3(4), December 2008; pp. 58-66; NREL Report No. JA-581-4137

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[6] Reda, I. (1996). Calibration of a Solar Absolute Cavity Radiometer with Traceability to the World Radiometric Reference. 79 pp.; NREL Report No. TP-463-20619.

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# National Renewable Energy Laboratory

## Solar Radiation Research Laboratory

### Metrology Laboratory

### Calibration Certificate



<b>Test Instrument:</b>	Pyrheliometer	<b>Manufacturer:</b>	Kipp & Zonen
<b>Model:</b>	CHP1	<b>Serial Number:</b>	140108
<b>Calibration Date:</b>	5/3/2019	<b>Due Date:</b>	5/3/2020
<b>Customer:</b>	NREL-SRRL-BMS	<b>Environmental Conditions:</b>	see page 4
<b>Test Dates:</b>	5/3		

This certifies that the above product was calibrated in compliance with ISO/IEC 17025:2005. Measurement uncertainties at the time of calibration are consistent with the Guide to the Expression of Uncertainty in Measurement (GUM) using Reda et al., 2008. All nominal values are traceable to the International System (SI) Units of Measurement.

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Diffuse Irradiance †	Hukseflux Pyranometer Model SR25, S/N 2541	04/19/2019	04/19/2020
Diffuse Irradiance †	Hukseflux Pyranometer Model SR25, S/N 2542	04/19/2019	04/19/2020
Data Acquisition	NREL Data Acquisition System Model RAP-DAQ, S/N 2005-998	02/14/2019	02/14/2021
Data Acquisition	NREL Data Acquisition System Model RAP-DAQ, S/N 2005-999	02/14/2019	02/14/2021

† Through the World Radiometric Reference (WRR)

**Number of pages of certificate:** 4

**Calibration Procedure:** BORCAL-P00-Calibration and QA Procedure; available upon request.

**Setup:** Radiometers are calibrated outdoors, using the sun as the source. Pyranometers and pyrgeometers are installed for horizontal measurements, with their signal connectors oriented north, if their design permits.

The shading disk for the reference diffuse subtends a solid angle of 5°. Pyrheliometers are installed on solar trackers.

**Calibrated by:** RCC

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Ibrahim Reda, Technical Manager

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Date

For questions or comments, please contact the technical manager at:

ibrahim.reda@nrel.gov; 303-384-6385; 15013 Denver West Parkway, Golden, CO 80401, USA

# Calibration Results

## 140108 Kipp & Zonen CHP1

The responsivity ( $R$ ,  $\mu\text{V}/\text{W}/\text{m}^2$ ) of the test instrument during calibration is calculated using this Measurement Equation:

$$R = (V - R_{net} * W_{net}) / I \tag{1}$$

where,

- $V$  = radiometer output voltage (microvolts),
- $R_{net}$  = radiometer net infrared responsivity ( $\mu\text{V}/\text{W}/\text{m}^2$ ), see Table 4,
- $W_{net}$  = effective net infrared measured by pyrgeometer ( $\text{W}/\text{m}^2$ ),
- =  $W_{in} - W_{out} = W_{in} - \sigma * T_c^4$
- where,  $W_{in}$  = incoming infrared ( $\text{W}/\text{m}^2$ ),  $\sigma = 5.6704\text{e-}8 \text{ W}\cdot\text{m}^{-2}\cdot\text{K}^{-4}$ ,
- $T_c$  = case temperature of pyrgeometer (K).
- $I$  = reference irradiance ( $\text{W}/\text{m}^2$ ), beam (B) or global (G)
- where,  $G = B * \text{COS}(Z) + D$ ,
- $Z$  = zenith angle (degrees),
- $D$  = reference diffuse irradiance ( $\text{W}/\text{m}^2$ ).

Figure 1. Responsivity vs Zenith Angle

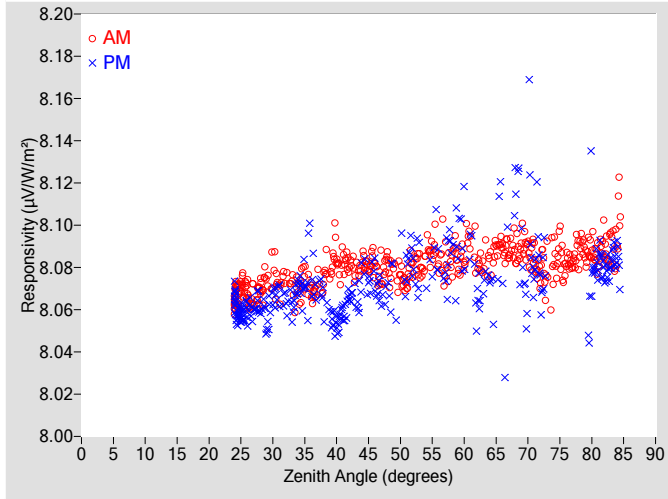


Figure 2. Responsivity vs Local Standard Time

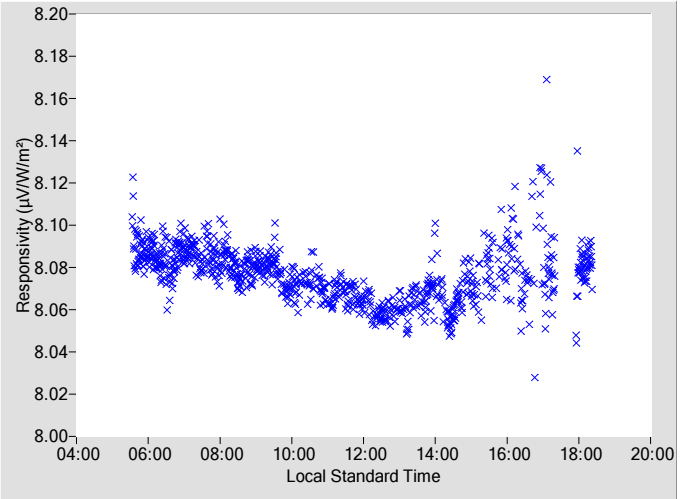


Table 2. Instrument Responsivity (R) and Calibration Type-B Standard Uncertainty, u(B)

Zenith Angle (deg.)	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle	Zenith Angle (deg.)	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle
0	N/A	N/A	N/A	N/A	N/A	N/A	46	8.0800	0.28	108.27	8.0744	0.28	251.93
2	N/A	N/A	N/A	N/A	N/A	N/A	48	8.0812	0.28	105.88	8.0701	0.29	254.21
4	N/A	N/A	N/A	N/A	N/A	N/A	50	8.0774	0.28	103.73	8.0962	0.30	256.55
6	N/A	N/A	N/A	N/A	N/A	N/A	52	8.0798	0.28	101.79	8.0821	0.29	258.37
8	N/A	N/A	N/A	N/A	N/A	N/A	54	8.0861	0.28	99.77	8.0702	0.30	260.54
10	N/A	N/A	N/A	N/A	N/A	N/A	56	8.0799	0.28	97.82	8.0822	0.30	262.18
12	N/A	N/A	N/A	N/A	N/A	N/A	58	8.0824	0.28	95.93	8.0901	0.30	264.14
14	N/A	N/A	N/A	N/A	N/A	N/A	60	8.0814	0.29	94.15	8.0955	N/A	265.88
16	N/A	N/A	N/A	N/A	N/A	N/A	62	8.0849	0.29	92.49	8.0649	0.30	267.72
18	N/A	N/A	N/A	N/A	N/A	N/A	64	8.0834	0.29	90.77	8.0743	0.30	269.35
20	N/A	N/A	N/A	N/A	N/A	N/A	66	8.0895	0.29	89.10	8.0724	N/A	271.06
22	N/A	N/A	N/A	N/A	N/A	N/A	68	8.0886	0.29	87.47	8.1155	N/A	272.67
24	8.0655	0.28	174.40	8.0639	0.28	185.29	70	8.0875	0.29	85.88	8.1004	N/A	274.32
26	8.0679	0.28	153.95	8.0595	0.28	205.72	72	8.0785	0.30	84.26	8.0697	N/A	275.94
28	8.0697	0.28	144.37	8.0612	0.28	215.69	74	8.0848	0.30	82.64	N/A	N/A	N/A
30	8.0786	0.28	137.22	8.0677	0.28	223.11	76	8.0820	0.30	81.04	N/A	N/A	N/A
32	8.0760	0.28	131.86	8.0639	0.28	228.47	78	8.0880	N/A	79.42	N/A	N/A	N/A
34	8.0698	0.28	126.98	8.0719	0.28	233.02	80	8.0887	N/A	77.77	8.0876	N/A	282.47
36	8.0690	0.28	122.98	8.0804	0.28	237.23	82	8.0900	N/A	76.16	8.0781	N/A	284.04
38	8.0734	0.28	119.44	8.0635	0.28	240.44	84	8.0990	N/A	74.45	8.0852	N/A	285.76
40	8.0874	0.28	116.30	8.0519	0.28	243.86	86	N/A	N/A	N/A	N/A	N/A	N/A
42	8.0809	0.28	113.46	8.0661	0.28	246.74	88	N/A	N/A	N/A	N/A	N/A	N/A
44	8.0835	0.28	110.66	8.0758	0.28	249.41	90	N/A	N/A	N/A	N/A	N/A	N/A

N/A - Not Available



Figure 3. Type-B Standard Uncertainty vs Zenith Angle

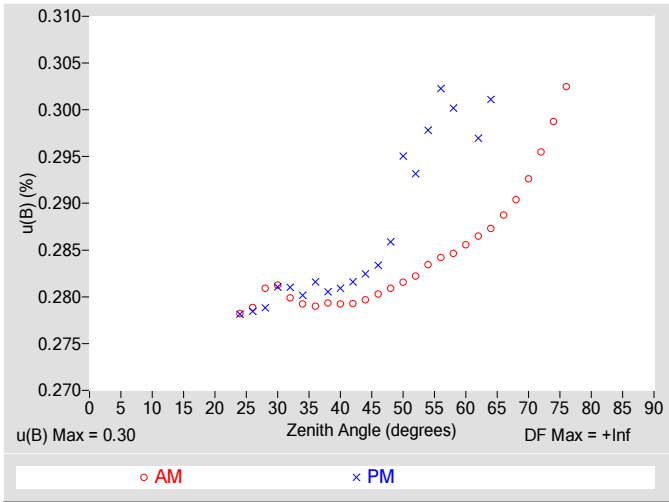


Figure 4. Residuals from Spline Interpolation

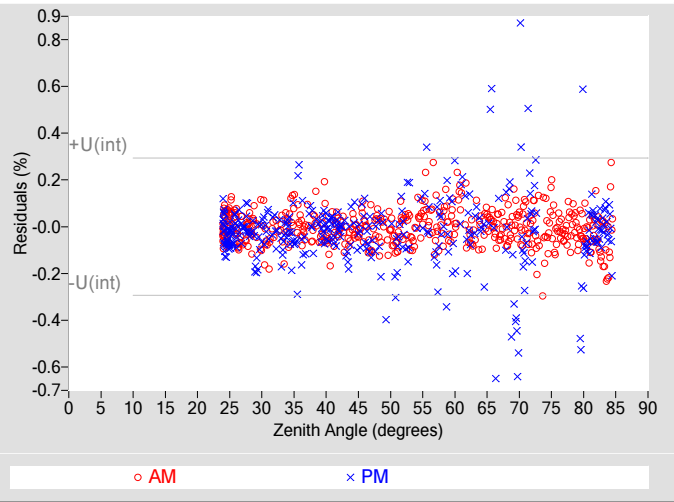


Table 3. Uncertainty using Spline Interpolation ‡

Type-B Standard Uncertainty, u(B) (%)	±0.30
Type-A Interpolating Function, u(int) (%)	±0.15
Combined Standard Uncertainty, u(c) (%)	±0.34
Effective degrees of freedom, DF(c)	19237
Coverage factor, k	1.96
Expanded Uncertainty, U95 (%)	±0.66
AM Valid zenith angle range	24° to 76°
PM Valid zenith angle range	24° to 64°

‡ An illustration for how to reduce the uncertainty in calculating the irradiance using a function rather than R@45°. Not accredited.

Table 4. Calibration Label Values

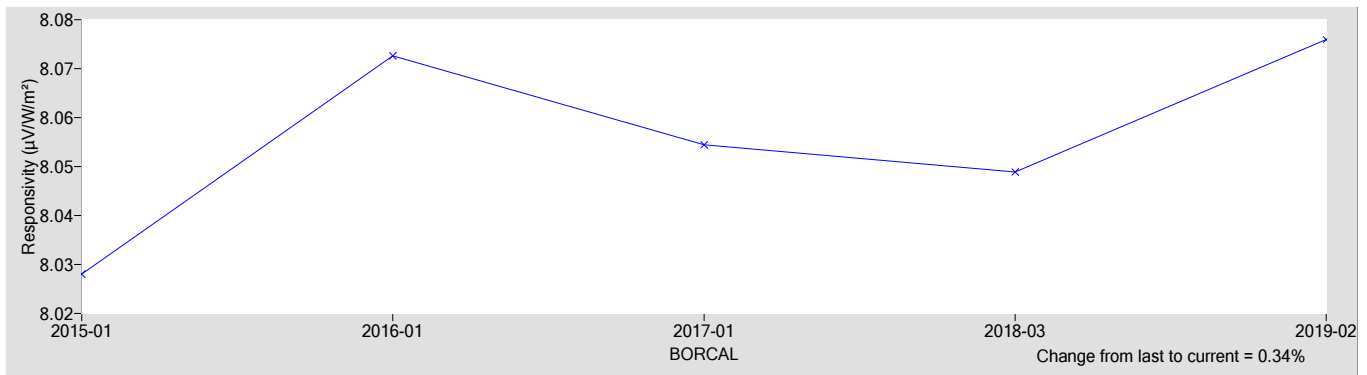
R @ 45° (μV/W/m²)	Rnet (μV/W/m²) †
8.0759	0

† Rnet determination date: N/A

Table 5. Uncertainty using R @ 45°

Type-B Expanded Uncertainty, U(B) (%)	±0.59
Offset Uncertainty, U(off) (%)	+0.25 / -0.30
Expanded Uncertainty, U (%)	+0.84 / -0.89
Effective degrees of freedom, DF	+Inf
Coverage factor, k	1.96
Valid zenith angle range	30.0° to 60.0°

Figure 5. History of instrument at Zenith Angle = 45°



References:

[1] Reda, I.; Hickey, J.; Long, C.; Myers, D.; Stoffel, T.; Wilcox, S.; Michalsky, J. J.; Dutton, E. G.; Nelson, D. (2005). "Using a Blackbody to Calculate Net Longwave Responsivity of Shortwave Solar Pyranometers to Correct for Their Thermal Offset Error During Outdoor Calibration Using the Component Sum Method." Journal of Atmospheric and Oceanic Technology. , 2005; pp. 1531-1540; NREL Report No. JA-560-36646. doi:10.1175/JTECH1782.1

[2] Reda, I.; Myers, D.; Stoffel, T. (2008). "Uncertainty Estimate for the Outdoor Calibration of Solar Pyranometers: A Metrologist Perspective." Measure. (NCSLI Journal of Measurement Science). Vol. 3(4), December 2008; pp. 58-66; NREL Report No. JA-581-4137

[3] Reda, I.; Andreas, A. (2004). "Solar Position Algorithm for Solar Radiation Applications." Solar Energy. Vol. 76(5), 2004; pp. 577-589; NREL Report No. JA-560-35518. doi:10.1016/j.solener.2003.12.003

[4] Stoffel, T.; Reda, I. (2009). "NREL Pyrheliometer Comparisons: 22 September - 3 October 2008 (NPC-2008)." 54 pp.; NREL Report No. TP-550-45016.

[5] Reda, I.; Stoffel, T.; Myers, D. (2003). "Method to Calibrate a Solar Pyranometer for Measuring Reference Diffuse Irradiance." Solar Energy. Vol. 74, 2003; pp. 103-112; NREL Report No. JA-560-35025. doi:10.1016/S0038-092X(03)00124-5

[6] Reda, I. (1996). Calibration of a Solar Absolute Cavity Radiometer with Traceability to the World Radiometric Reference. 79 pp.; NREL Report No. TP-463-20619.

[7] Reda, I.; Gröbner, J.; Stoffel, T.; Myers, D.; Forgan, B. (2008). Improvements in the Blackbody Calibration of Pyrgeometers. ARM 2008 Science Team Meeting (Poster).



# National Renewable Energy Laboratory

## Solar Radiation Research Laboratory

### Metrology Laboratory

### Calibration Certificate



<b>Test Instrument:</b>	Pyranometer	<b>Manufacturer:</b>	Kipp & Zonen
<b>Model:</b>	CMP11	<b>Serial Number:</b>	140712
<b>Calibration Date:</b>	5/3/2019	<b>Due Date:</b>	5/3/2020
<b>Customer:</b>	NREL-SRRL-BMS	<b>Environmental Conditions:</b>	see page 4
<b>Test Dates:</b>	5/3		

This certifies that the above product was calibrated in compliance with ISO/IEC 17025:2005. Measurement uncertainties at the time of calibration are consistent with the Guide to the Expression of Uncertainty in Measurement (GUM) using Reda et al., 2008. All nominal values are traceable to the International System (SI) Units of Measurement.

No statement of compliance with specifications is made or implied on this certificate. However, the estimated uncertainties are the uncertainties of the calibration process; users must add other uncertainties that are relevant to their measuring system, environmental and sky conditions, outdoor set-up, and site location.

The Type-B Standard Uncertainty of using the responsivity at each even zenith angle is reported, and the Expanded Uncertainty of the calibration is reported using two methods:

1. The Expanded Uncertainty of using the responsivity at zenith angle = 45°, within the zenith angle range from 30.0° to 60.0°
2. The Expanded Uncertainty of using Spline Interpolating Functions for the responsivity versus zenith angle.

This certificate applies only to the item identified above and shall not be reproduced other than in full, without specific written approval from the calibration facility. Certificate without signature is not valid.

**Table 1. Traceability**

Measurement Type	Instrument	Calibration Date	Calibration Due Date
Beam Irradiance †	Eppley Absolute Cavity Radiometer Model HF, S/N 29219	09/24/2018	09/24/2019
Diffuse Irradiance †	Hukseflux Pyranometer Model SR25, S/N 2541	04/19/2019	04/19/2020
Diffuse Irradiance †	Hukseflux Pyranometer Model SR25, S/N 2542	04/19/2019	04/19/2020
Data Acquisition	NREL Data Acquisition System Model RAP-DAQ, S/N 2005-998	02/14/2019	02/14/2021
Data Acquisition	NREL Data Acquisition System Model RAP-DAQ, S/N 2005-999	02/14/2019	02/14/2021
Infrared Irradiance ‡	Kipp & Zonen Pyrgeometer Model CG4, S/N FT002	04/16/2018	04/16/2022

† Through the World Radiometric Reference (WRR)

‡ Through the World Infrared Standard Group (WISG)

**Number of pages of certificate:** 4

**Calibration Procedure:** BORCAL-P00-Calibration and QA Procedure; available upon request.

**Setup:** Radiometers are calibrated outdoors, using the sun as the source. Pyranometers and pyrgeometers are installed for horizontal measurements, with their signal connectors oriented north, if their design permits.

The shading disk for the reference diffuse subtends a solid angle of 5°. Pyrheliometers are installed on solar trackers.

**Calibrated by:** RCC

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Ibrahim Reda, Technical Manager

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Date

For questions or comments, please contact the technical manager at:

ibrahim.reda@nrel.gov; 303-384-6385; 15013 Denver West Parkway, Golden, CO 80401, USA

# Calibration Results

## 140712 Kipp & Zonen CMP11

The responsivity ( $R$ ,  $\mu\text{V}/\text{W}/\text{m}^2$ ) of the test instrument during calibration is calculated using this Measurement Equation:

$$R = (V - R_{net} * W_{net}) / I \tag{1}$$

where,

- $V$  = radiometer output voltage (microvolts),
- $R_{net}$  = radiometer net infrared responsivity ( $\mu\text{V}/\text{W}/\text{m}^2$ ), see Table 4,
- $W_{net}$  = effective net infrared measured by pyrgeometer ( $\text{W}/\text{m}^2$ ),
- =  $W_{in} - W_{out} = W_{in} - \sigma * T_c^4$
- where,  $W_{in}$  = incoming infrared ( $\text{W}/\text{m}^2$ ),  $\sigma = 5.6704\text{e-}8 \text{ W}\cdot\text{m}^{-2}\cdot\text{K}^{-4}$ ,
- $T_c$  = case temperature of pyrgeometer (K).
- $I$  = reference irradiance ( $\text{W}/\text{m}^2$ ), beam (B) or global (G)
- where,  $G = B * \text{COS}(Z) + D$ ,
- $Z$  = zenith angle (degrees),
- $D$  = reference diffuse irradiance ( $\text{W}/\text{m}^2$ ).

Figure 1. Responsivity vs Zenith Angle

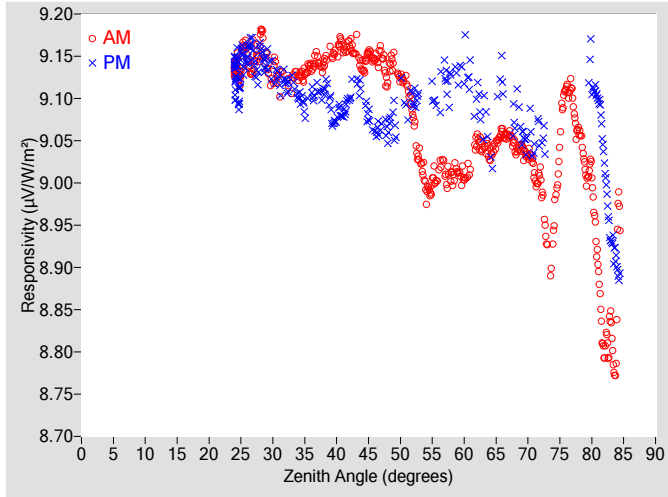


Figure 2. Responsivity vs Local Standard Time

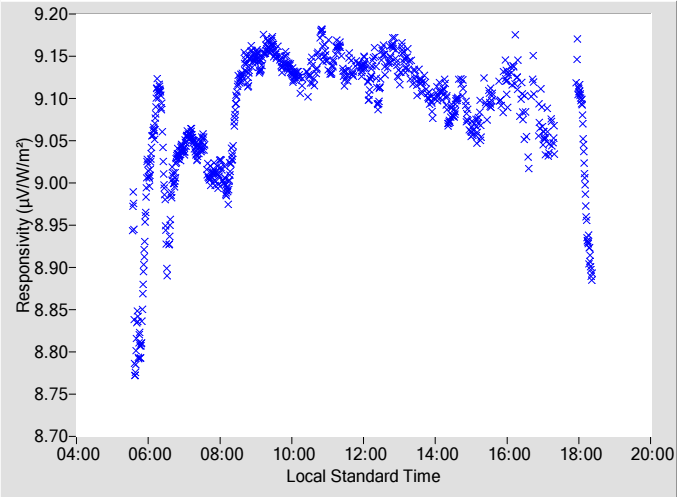


Table 2. Instrument Responsivity (R) and Calibration Type-B Standard Uncertainty, u(B)

Zenith Angle (deg.)	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle	Zenith Angle (deg.)	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle
0	N/A	N/A	N/A	N/A	N/A	N/A	46	9.1476	0.35	108.31	9.0580	0.39	252.02
2	N/A	N/A	N/A	N/A	N/A	N/A	48	9.1229	0.35	105.99	9.0610	0.40	254.20
4	N/A	N/A	N/A	N/A	N/A	N/A	50	9.1244	0.36	103.74	9.1242	0.44	256.51
6	N/A	N/A	N/A	N/A	N/A	N/A	52	9.0797	0.37	101.69	9.0995	0.44	258.49
8	N/A	N/A	N/A	N/A	N/A	N/A	54	8.9930	0.38	99.68	N/A	N/A	N/A
10	N/A	N/A	N/A	N/A	N/A	N/A	56	9.0149	0.39	97.78	9.0832	N/A	262.54
12	N/A	N/A	N/A	N/A	N/A	N/A	58	9.0061	0.40	95.94	9.1293	0.51	263.98
14	N/A	N/A	N/A	N/A	N/A	N/A	60	9.0080	0.41	94.23	9.1464	N/A	266.02
16	N/A	N/A	N/A	N/A	N/A	N/A	62	9.0491	0.42	92.45	9.1090	0.51	267.67
18	N/A	N/A	N/A	N/A	N/A	N/A	64	9.0343	0.44	90.78	9.0307	N/A	269.53
20	N/A	N/A	N/A	N/A	N/A	N/A	66	9.0595	0.46	89.14	9.1252	N/A	271.02
22	N/A	N/A	N/A	N/A	N/A	N/A	68	9.0422	0.49	87.48	9.0853	N/A	272.63
24	9.1351	0.32	175.08	9.1296	0.32	185.09	70	9.0334	0.53	85.84	9.0534	N/A	274.14
26	9.1515	0.32	154.05	9.1485	0.32	205.96	72	9.0025	0.57	84.26	9.0458	N/A	275.90
28	9.1678	0.34	144.11	9.1540	0.33	215.79	74	8.9502	0.64	82.61	N/A	N/A	N/A
30	9.1324	0.34	137.05	9.1284	0.34	222.72	76	9.1111	0.70	81.04	N/A	N/A	N/A
32	N/A	N/A	N/A	9.1182	0.34	228.55	78	9.0606	N/A	79.43	N/A	N/A	N/A
34	9.1263	0.33	126.67	9.1012	0.34	233.22	80	9.0099	N/A	77.82	9.1291	N/A	282.39
36	9.1368	0.33	122.99	9.1073	0.35	237.50	82	8.8054	N/A	76.17	9.0202	N/A	284.05
38	9.1392	0.33	119.50	9.1092	0.36	240.73	84	8.8845	N/A	74.50	8.8989	N/A	285.72
40	9.1569	0.34	116.16	9.0782	0.37	243.88	86	N/A	N/A	N/A	N/A	N/A	N/A
42	9.1656	0.34	113.29	9.0997	0.40	246.89	88	N/A	N/A	N/A	N/A	N/A	N/A
44	9.1374	0.34	110.67	9.1116	0.40	249.09	90	N/A	N/A	N/A	N/A	N/A	N/A

N/A - Not Available

Figure 3. Type-B Standard Uncertainty vs Zenith Angle

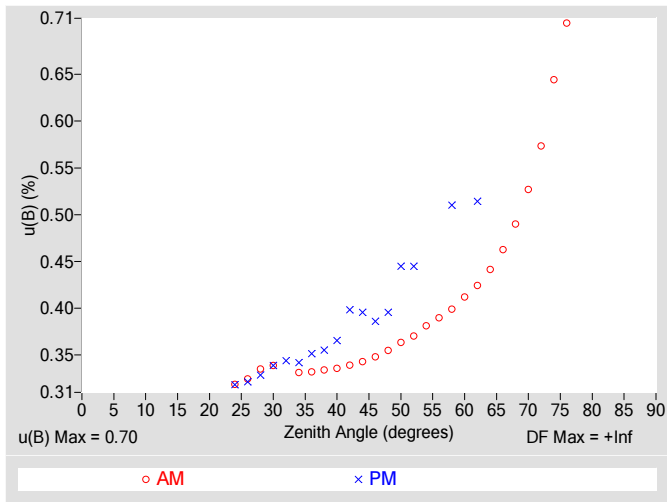


Figure 4. Residuals from Spline Interpolation

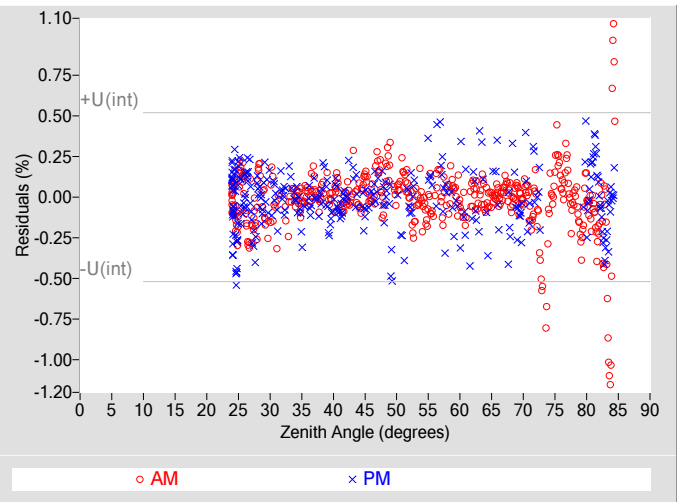


Table 3. Uncertainty using Spline Interpolation ‡

Type-B Standard Uncertainty, u(B) (%)	±0.70
Type-A Interpolating Function, u(int) (%)	±0.26
Combined Standard Uncertainty, u(c) (%)	±0.75
Effective degrees of freedom, DF(c)	46379
Coverage factor, k	1.96
Expanded Uncertainty, U95 (%)	±1.5
AM Valid zenith angle range	24° to 76°
PM Valid zenith angle range	24° to 62°

‡ An illustration for how to reduce the uncertainty in calculating the irradiance using a function rather than R@45°. Not accredited.

Table 4. Calibration Label Values

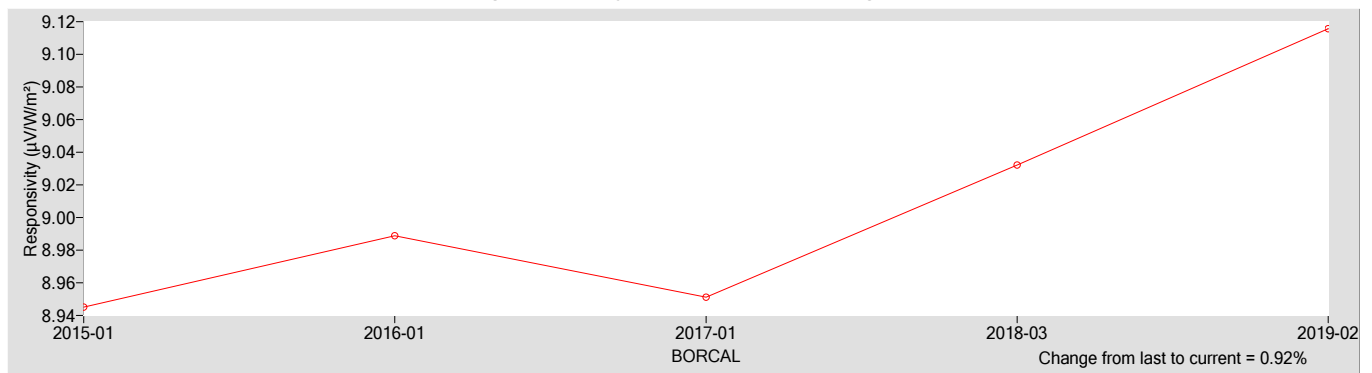
R @ 45° (μV/W/m²)	Rnet (μV/W/m²) †
9.1157	0.20500

† Rnet determination date: Estimated

Table 5. Uncertainty using R @ 45°

Type-B Expanded Uncertainty, U(B) (%)	±1.00
Offset Uncertainty, U(off) (%)	+0.55 / -1.3
Expanded Uncertainty, U (%)	+1.5 / -2.3
Effective degrees of freedom, DF	+Inf
Coverage factor, k	1.96
Valid zenith angle range	30.0° to 60.0°

Figure 5. History of instrument at Zenith Angle = 45°



References:

[1] Reda, I.; Hickey, J.; Long, C.; Myers, D.; Stoffel, T.; Wilcox, S.; Michalsky, J. J.; Dutton, E. G.; Nelson, D. (2005). "Using a Blackbody to Calculate Net Longwave Responsivity of Shortwave Solar Pyranometers to Correct for Their Thermal Offset Error During Outdoor Calibration Using the Component Sum Method." Journal of Atmospheric and Oceanic Technology. , 2005; pp. 1531-1540; NREL Report No. JA-560-36646. doi:10.1175/JTECH1782.1

[2] Reda, I.; Myers, D.; Stoffel, T. (2008). "Uncertainty Estimate for the Outdoor Calibration of Solar Pyranometers: A Metrologist Perspective." Measure. (NCSLI Journal of Measurement Science). Vol. 3(4), December 2008; pp. 58-66; NREL Report No. JA-581-4137

[3] Reda, I.; Andreas, A. (2004). "Solar Position Algorithm for Solar Radiation Applications." Solar Energy. Vol. 76(5), 2004; pp. 577-589; NREL Report No. JA-560-35518. doi:10.1016/j.solener.2003.12.003

[4] Stoffel, T.; Reda, I. (2009). "NREL Pyrheliometer Comparisons: 22 September - 3 October 2008 (NPC-2008)." 54 pp.; NREL Report No. TP-550-45016.

[5] Reda, I.; Stoffel, T.; Myers, D. (2003). "Method to Calibrate a Solar Pyranometer for Measuring Reference Diffuse Irradiance." Solar Energy. Vol. 74, 2003; pp. 103-112; NREL Report No. JA-560-35025. doi:10.1016/S0038-092X(03)00124-5

[6] Reda, I. (1996). Calibration of a Solar Absolute Cavity Radiometer with Traceability to the World Radiometric Reference. 79 pp.; NREL Report No. TP-463-20619.

[7] Reda, I.; Gröbner, J.; Stoffel, T.; Myers, D.; Forgan, B. (2008). Improvements in the Blackbody Calibration of Pyrgometers. ARM 2008 Science Team Meeting (Poster).



# National Renewable Energy Laboratory

## Solar Radiation Research Laboratory

### Metrology Laboratory

### Calibration Certificate



<b>Test Instrument:</b>	Silicon Pyranometer	<b>Manufacturer:</b>	Kipp & Zonen
<b>Model:</b>	SP-LITE2	<b>Serial Number:</b>	151027
<b>Calibration Date:</b>	5/3/2019	<b>Due Date:</b>	5/3/2020
<b>Customer:</b>	NREL-SRRL-BMS	<b>Environmental Conditions:</b>	see page 4
<b>Test Dates:</b>	5/3		

This certifies that the above product was calibrated in compliance with ISO/IEC 17025:2005. Measurement uncertainties at the time of calibration are consistent with the Guide to the Expression of Uncertainty in Measurement (GUM) using Reda et al., 2008. All nominal values are traceable to the International System (SI) Units of Measurement.

No statement of compliance with specifications is made or implied on this certificate. However, the estimated uncertainties are the uncertainties of the calibration process; users must add other uncertainties that are relevant to their measuring system, environmental and sky conditions, outdoor set-up, and site location.

The Type-B Standard Uncertainty of using the responsivity at each even zenith angle is reported, and the Expanded Uncertainty of the calibration is reported using two methods:

1. The Expanded Uncertainty of using the responsivity at zenith angle = 45°, within the zenith angle range from 30.0° to 60.0°
2. The Expanded Uncertainty of using Spline Interpolating Functions for the responsivity versus zenith angle.

This certificate applies only to the item identified above and shall not be reproduced other than in full, without specific written approval from the calibration facility. Certificate without signature is not valid.

**Table 1. Traceability**

Measurement Type	Instrument	Calibration Date	Calibration Due Date
Beam Irradiance †	Eppley Absolute Cavity Radiometer Model HF, S/N 29219	09/24/2018	09/24/2019
Diffuse Irradiance †	Hukseflux Pyranometer Model SR25, S/N 2541	04/19/2019	04/19/2020
Diffuse Irradiance †	Hukseflux Pyranometer Model SR25, S/N 2542	04/19/2019	04/19/2020
Data Acquisition	NREL Data Acquisition System Model RAP-DAQ, S/N 2005-998	02/14/2019	02/14/2021
Data Acquisition	NREL Data Acquisition System Model RAP-DAQ, S/N 2005-999	02/14/2019	02/14/2021

† Through the World Radiometric Reference (WRR)

**Number of pages of certificate:** 4

**Calibration Procedure:** BORCAL-P00-Calibration and QA Procedure; available upon request.

**Setup:** Radiometers are calibrated outdoors, using the sun as the source. Pyranometers and pyrgeometers are installed for horizontal measurements, with their signal connectors oriented north, if their design permits.

The shading disk for the reference diffuse subtends a solid angle of 5°. Pyrheliometers are installed on solar trackers.

**Calibrated by:** RCC

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Ibrahim Reda, Technical Manager

-----  
Date

For questions or comments, please contact the technical manager at:

ibrahim.reda@nrel.gov; 303-384-6385; 15013 Denver West Parkway, Golden, CO 80401, USA

# Calibration Results

## 151027 Kipp & Zonen SP-LITE2

The responsivity ( $R$ ,  $\mu\text{V}/\text{W}/\text{m}^2$ ) of the test instrument during calibration is calculated using this Measurement Equation:

$$R = (V - R_{net} * W_{net}) / I \tag{1}$$

where,

- $V$  = radiometer output voltage (microvolts),
  - $R_{net}$  = radiometer net infrared responsivity ( $\mu\text{V}/\text{W}/\text{m}^2$ ), see Table 4,
  - $W_{net}$  = effective net infrared measured by pyrgeometer ( $\text{W}/\text{m}^2$ ),
  - =  $W_{in} - W_{out} = W_{in} - \sigma * T_c^4$
  - where,  $W_{in}$  = incoming infrared ( $\text{W}/\text{m}^2$ ),  $\sigma = 5.6704\text{e-}8 \text{ W}\cdot\text{m}^{-2}\cdot\text{K}^{-4}$ ,
  - $T_c$  = case temperature of pyrgeometer (K).
- $I$  = reference irradiance ( $\text{W}/\text{m}^2$ ), beam (B) or global (G)
  - where,  $G = B * \text{COS}(Z) + D$ ,
  - $Z$  = zenith angle (degrees),
  - $D$  = reference diffuse irradiance ( $\text{W}/\text{m}^2$ ).

Figure 1. Responsivity vs Zenith Angle

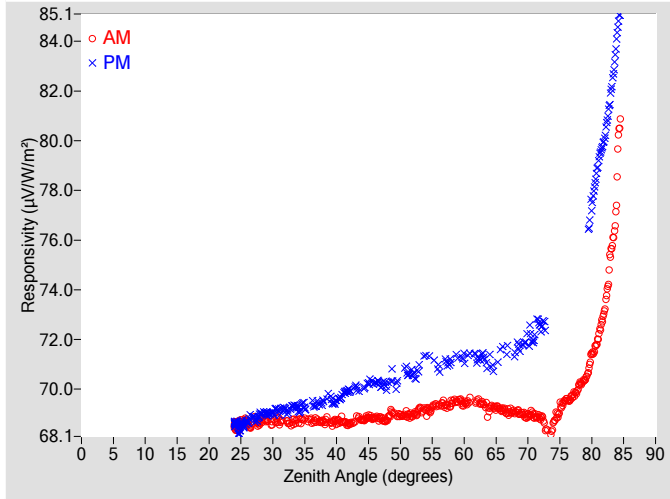


Figure 2. Responsivity vs Local Standard Time

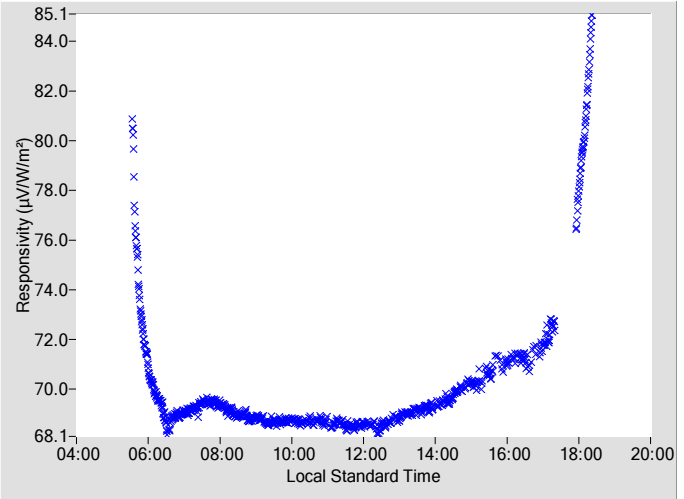
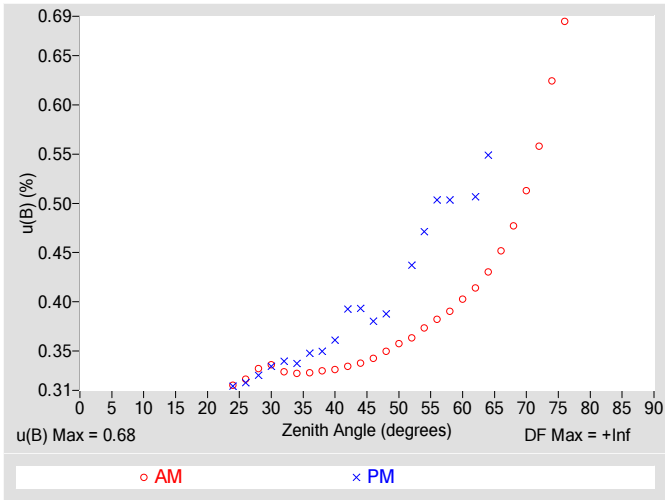


Table 2. Instrument Responsivity (R) and Calibration Type-B Standard Uncertainty,  $u(B)$

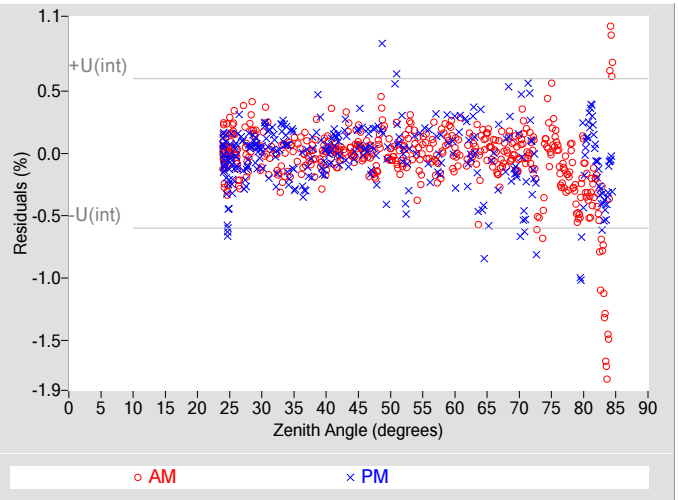
Zenith Angle (deg.)	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	AM $u(B)$ $\pm$ (%)	Azimuth Angle	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	PM $u(B)$ $\pm$ (%)	Azimuth Angle	Zenith Angle (deg.)	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	AM $u(B)$ $\pm$ (%)	Azimuth Angle	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	PM $u(B)$ $\pm$ (%)	Azimuth Angle
0	N/A	N/A	N/A	N/A	N/A	N/A	46	68.844	0.34	108.30	70.244	0.38	251.84
2	N/A	N/A	N/A	N/A	N/A	N/A	48	68.833	0.35	105.89	70.118	0.39	254.06
4	N/A	N/A	N/A	N/A	N/A	N/A	50	68.947	0.36	103.73	N/A	N/A	N/A
6	N/A	N/A	N/A	N/A	N/A	N/A	52	68.960	0.36	101.69	70.602	0.44	258.45
8	N/A	N/A	N/A	N/A	N/A	N/A	54	69.152	0.37	99.71	71.356	0.47	260.44
10	N/A	N/A	N/A	N/A	N/A	N/A	56	69.356	0.38	97.77	70.831	0.50	262.32
12	N/A	N/A	N/A	N/A	N/A	N/A	58	69.424	0.39	95.98	71.146	0.50	264.03
14	N/A	N/A	N/A	N/A	N/A	N/A	60	69.423	0.40	94.20	71.231	N/A	265.88
16	N/A	N/A	N/A	N/A	N/A	N/A	62	69.525	0.41	92.47	71.238	0.51	267.67
18	N/A	N/A	N/A	N/A	N/A	N/A	64	69.219	0.43	90.82	71.144	0.55	269.48
20	N/A	N/A	N/A	N/A	N/A	N/A	66	69.174	0.45	89.10	71.718	N/A	271.06
22	N/A	N/A	N/A	N/A	N/A	N/A	68	69.085	0.48	87.50	71.391	N/A	272.62
24	68.524	0.32	174.16	68.594	0.31	184.92	70	68.915	0.51	85.84	72.180	N/A	274.39
26	68.617	0.32	153.92	68.693	0.32	205.84	72	68.855	0.56	84.26	72.534	N/A	275.90
28	68.647	0.33	144.26	68.970	0.33	215.75	74	68.581	0.62	82.65	N/A	N/A	N/A
30	68.644	0.34	137.44	69.027	0.33	222.89	76	69.570	0.68	81.04	N/A	N/A	N/A
32	68.725	0.33	131.07	69.149	0.34	228.51	78	70.131	N/A	79.42	N/A	N/A	N/A
34	68.744	0.33	126.92	69.199	0.34	233.09	80	71.375	N/A	77.78	77.534	N/A	282.42
36	68.741	0.33	122.90	69.538	0.35	237.57	82	73.285	N/A	76.12	80.155	N/A	284.04
38	68.705	0.33	119.44	69.476	0.35	240.40	84	78.911	N/A	74.46	84.434	N/A	285.76
40	68.699	0.33	116.31	69.534	0.36	243.80	86	N/A	N/A	N/A	N/A	N/A	N/A
42	68.608	0.33	113.36	69.936	0.39	246.68	88	N/A	N/A	N/A	N/A	N/A	N/A
44	68.763	0.34	110.73	70.016	0.39	249.81	90	N/A	N/A	N/A	N/A	N/A	N/A

N/A - Not Available

**Figure 3. Type-B Standard Uncertainty vs Zenith Angle**



**Figure 4. Residuals from Spline Interpolation**



**Table 3. Uncertainty using Spline Interpolation ‡**

Type-B Standard Uncertainty, u(B) (%)	±0.68
Type-A Interpolating Function, u(int) (%)	±0.30
Combined Standard Uncertainty, u(c) (%)	±0.75
Effective degrees of freedom, DF(c)	25796
Coverage factor, k	1.96
Expanded Uncertainty, U95 (%)	±1.5
AM Valid zenith angle range	24° to 76°
PM Valid zenith angle range	24° to 64°

‡ An illustration for how to reduce the uncertainty in calculating the irradiance using a function rather than R@45°. Not accredited.

**Table 4. Calibration Label Values**

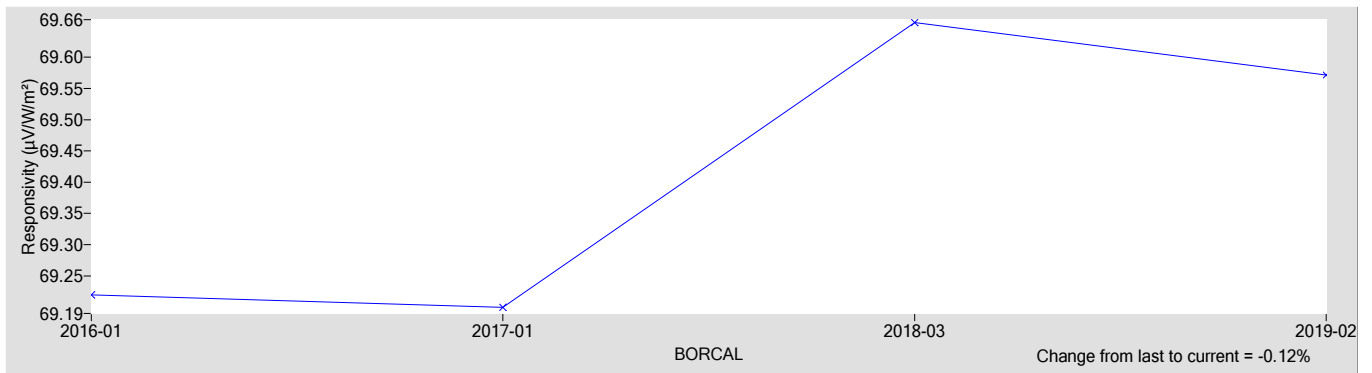
R @ 45° (μV/W/m²)	Rnet (μV/W/m²) †
69.571	0

† Rnet determination date: N/A

**Table 5. Uncertainty using R @ 45°**

Type-B Expanded Uncertainty, U(B) (%)	±0.99
Offset Uncertainty, U(off) (%)	+2.6 / -1.4
Expanded Uncertainty, U (%)	+3.6 / -2.4
Effective degrees of freedom, DF	+Inf
Coverage factor, k	1.96
Valid zenith angle range	30.0° to 60.0°

**Figure 5. History of instrument at Zenith Angle = 45°**



**References:**

[1] Reda, I.; Hickey, J.; Long, C.; Myers, D.; Stoffel, T.; Wilcox, S.; Michalsky, J. J.; Dutton, E. G.; Nelson, D. (2005). "Using a Blackbody to Calculate Net Longwave Responsivity of Shortwave Solar Pyranometers to Correct for Their Thermal Offset Error During Outdoor Calibration Using the Component Sum Method." Journal of Atmospheric and Oceanic Technology. , 2005; pp. 1531-1540; NREL Report No. JA-560-36646. doi:10.1175/JTECH1782.1

[2] Reda, I.; Myers, D.; Stoffel, T. (2008). "Uncertainty Estimate for the Outdoor Calibration of Solar Pyranometers: A Metrologist Perspective." Measure. (NCSLI Journal of Measurement Science). Vol. 3(4), December 2008; pp. 58-66; NREL Report No. JA-581-4137

[3] Reda, I.; Andreas, A. (2004). "Solar Position Algorithm for Solar Radiation Applications." Solar Energy. Vol. 76(5), 2004; pp. 577-589; NREL Report No. JA-560-35518. doi:10.1016/j.solener.2003.12.003

[4] Stoffel, T.; Reda, I. (2009). "NREL Pyrheliometer Comparisons: 22 September - 3 October 2008 (NPC-2008)." 54 pp.; NREL Report No. TP-550-45016.

[5] Reda, I.; Stoffel, T.; Myers, D. (2003). "Method to Calibrate a Solar Pyranometer for Measuring Reference Diffuse Irradiance." Solar Energy. Vol. 74, 2003; pp. 103-112; NREL Report No. JA-560-35025. doi:10.1016/S0038-092X(03)00124-5

[6] Reda, I. (1996). Calibration of a Solar Absolute Cavity Radiometer with Traceability to the World Radiometric Reference. 79 pp.; NREL Report No. TP-463-20619.

[7] Reda, I.; Gröbner, J.; Stoffel, T.; Myers, D.; Forgan, B. (2008). Improvements in the Blackbody Calibration of Pyrgeometers. ARM 2008 Science Team Meeting (Poster).





# National Renewable Energy Laboratory

## Solar Radiation Research Laboratory

### Metrology Laboratory

### Calibration Certificate



<b>Test Instrument:</b>	Pyranometer	<b>Manufacturer:</b>	Kipp & Zonen
<b>Model:</b>	CMP22	<b>Serial Number:</b>	170535
<b>Calibration Date:</b>	5/3/2019	<b>Due Date:</b>	5/3/2020
<b>Customer:</b>	NREL-SRRL-BMS	<b>Environmental Conditions:</b>	see page 4
<b>Test Dates:</b>	5/3		

This certifies that the above product was calibrated in compliance with ISO/IEC 17025:2005. Measurement uncertainties at the time of calibration are consistent with the Guide to the Expression of Uncertainty in Measurement (GUM) using Reda et al., 2008. All nominal values are traceable to the International System (SI) Units of Measurement.

No statement of compliance with specifications is made or implied on this certificate. However, the estimated uncertainties are the uncertainties of the calibration process; users must add other uncertainties that are relevant to their measuring system, environmental and sky conditions, outdoor set-up, and site location.

The Type-B Standard Uncertainty of using the responsivity at each even zenith angle is reported, and the Expanded Uncertainty of the calibration is reported using two methods:

1. The Expanded Uncertainty of using the responsivity at zenith angle = 45°, within the zenith angle range from 30.0° to 60.0°
2. The Expanded Uncertainty of using Spline Interpolating Functions for the responsivity versus zenith angle.

This certificate applies only to the item identified above and shall not be reproduced other than in full, without specific written approval from the calibration facility. Certificate without signature is not valid.

**Table 1. Traceability**

Measurement Type	Instrument	Calibration Date	Calibration Due Date
Beam Irradiance †	Eppley Absolute Cavity Radiometer Model HF, S/N 29219	09/24/2018	09/24/2019
Diffuse Irradiance †	Hukseflux Pyranometer Model SR25, S/N 2541	04/19/2019	04/19/2020
Diffuse Irradiance †	Hukseflux Pyranometer Model SR25, S/N 2542	04/19/2019	04/19/2020
Data Acquisition	NREL Data Acquisition System Model RAP-DAQ, S/N 2005-998	02/14/2019	02/14/2021
Data Acquisition	NREL Data Acquisition System Model RAP-DAQ, S/N 2005-999	02/14/2019	02/14/2021
Infrared Irradiance ‡	Kipp & Zonen Pyrgeometer Model CG4, S/N FT002	04/16/2018	04/16/2022

† Through the World Radiometric Reference (WRR)

‡ Through the World Infrared Standard Group (WISG)

**Number of pages of certificate:** 4

**Calibration Procedure:** BORCAL-P00-Calibration and QA Procedure; available upon request.

**Setup:** Radiometers are calibrated outdoors, using the sun as the source. Pyranometers and pyrgeometers are installed for horizontal measurements, with their signal connectors oriented north, if their design permits.

The shading disk for the reference diffuse subtends a solid angle of 5°. Pyrheliometers are installed on solar trackers.

**Calibrated by:** RCC

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Ibrahim Reda, Technical Manager

-----  
Date

For questions or comments, please contact the technical manager at:

ibrahim.reda@nrel.gov; 303-384-6385; 15013 Denver West Parkway, Golden, CO 80401, USA



# Calibration Results

## 170535 Kipp & Zonen CMP22

The responsivity ( $R$ ,  $\mu\text{V}/\text{W}/\text{m}^2$ ) of the test instrument during calibration is calculated using this Measurement Equation:

$$R = (V - R_{net} * W_{net}) / I \tag{1}$$

where,

- $V$  = radiometer output voltage (microvolts),
  - $R_{net}$  = radiometer net infrared responsivity ( $\mu\text{V}/\text{W}/\text{m}^2$ ), see Table 4,
  - $W_{net}$  = effective net infrared measured by pyrgeometer ( $\text{W}/\text{m}^2$ ),
  - =  $W_{in} - W_{out} = W_{in} - \sigma * T_c^4$
  - where,  $W_{in}$  = incoming infrared ( $\text{W}/\text{m}^2$ ),  $\sigma = 5.6704\text{e-}8 \text{ W}\cdot\text{m}^{-2}\cdot\text{K}^{-4}$ ,
  - $T_c$  = case temperature of pyrgeometer (K).
- $I$  = reference irradiance ( $\text{W}/\text{m}^2$ ), beam (B) or global (G)
  - where,  $G = B * \text{COS}(Z) + D$ ,
  - $Z$  = zenith angle (degrees),
  - $D$  = reference diffuse irradiance ( $\text{W}/\text{m}^2$ ).

Figure 1. Responsivity vs Zenith Angle

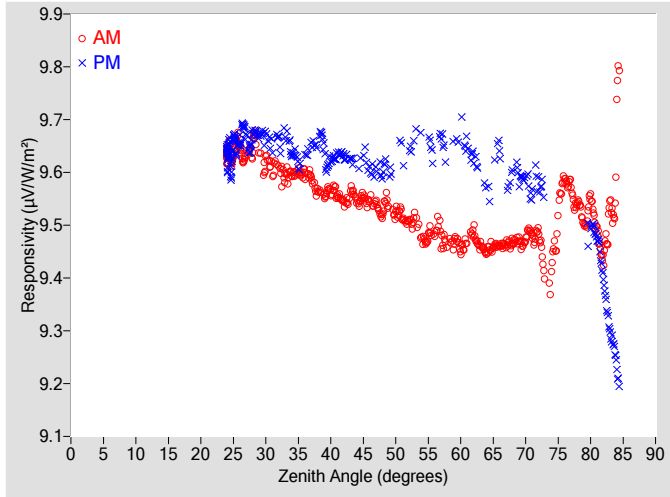


Figure 2. Responsivity vs Local Standard Time

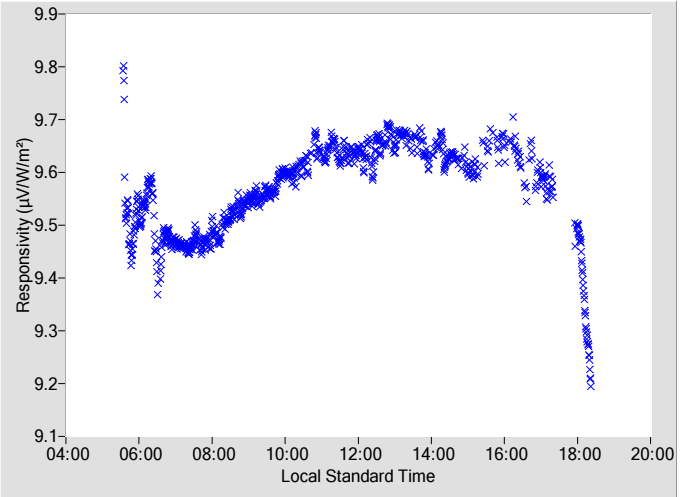


Table 2. Instrument Responsivity (R) and Calibration Type-B Standard Uncertainty, u(B)

Zenith Angle (deg.)	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle	Zenith Angle (deg.)	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle
0	N/A	N/A	N/A	N/A	N/A	N/A	46	9.5498	0.34	108.34	9.6044	0.38	251.79
2	N/A	N/A	N/A	N/A	N/A	N/A	48	9.5238	0.35	105.95	9.5999	0.39	254.21
4	N/A	N/A	N/A	N/A	N/A	N/A	50	9.5240	0.36	103.74	N/A	N/A	N/A
6	N/A	N/A	N/A	N/A	N/A	N/A	52	9.5070	0.37	101.75	9.6452	0.44	258.65
8	N/A	N/A	N/A	N/A	N/A	N/A	54	9.4740	0.38	99.63	9.6749	0.47	260.29
10	N/A	N/A	N/A	N/A	N/A	N/A	56	9.4841	0.38	97.78	N/A	N/A	N/A
12	N/A	N/A	N/A	N/A	N/A	N/A	58	9.4581	0.39	96.09	N/A	N/A	N/A
14	N/A	N/A	N/A	N/A	N/A	N/A	60	9.4569	0.41	94.20	9.7047	N/A	266.07
16	N/A	N/A	N/A	N/A	N/A	N/A	62	9.4840	0.42	92.45	9.6309	0.51	267.59
18	N/A	N/A	N/A	N/A	N/A	N/A	64	9.4493	0.43	90.79	9.5722	0.55	269.45
20	N/A	N/A	N/A	N/A	N/A	N/A	66	9.4621	0.46	89.10	9.6425	N/A	271.02
22	N/A	N/A	N/A	N/A	N/A	N/A	68	9.4676	0.48	87.49	9.6024	N/A	272.60
24	9.6339	0.32	174.60	9.6360	0.32	185.66	70	9.4747	0.52	85.85	9.5918	N/A	274.28
26	9.6467	0.32	153.77	9.6617	0.32	206.06	72	9.4817	0.56	84.27	9.5727	N/A	275.91
28	9.6526	0.33	144.08	9.6654	0.33	215.43	74	9.4148	0.63	82.63	N/A	N/A	N/A
30	9.6177	0.34	137.37	9.6671	0.34	222.58	76	9.5856	0.69	81.04	N/A	N/A	N/A
32	9.6115	0.33	131.78	9.6587	0.34	228.46	78	9.5413	N/A	79.43	N/A	N/A	N/A
34	9.5981	0.33	127.08	9.6339	0.34	233.16	80	9.5481	N/A	77.83	9.4978	N/A	282.52
36	9.5979	0.33	123.17	9.6336	0.35	237.42	82	9.4445	N/A	76.17	9.3914	N/A	284.05
38	9.5628	0.33	119.47	9.6576	0.35	240.73	84	9.6598	N/A	74.51	9.2330	N/A	285.72
40	9.5625	0.33	116.28	9.6233	0.36	243.88	86	N/A	N/A	N/A	N/A	N/A	N/A
42	9.5444	0.34	113.44	9.6276	0.40	246.90	88	N/A	N/A	N/A	N/A	N/A	N/A
44	9.5471	0.34	110.71	N/A	N/A	N/A	90	N/A	N/A	N/A	N/A	N/A	N/A

N/A - Not Available

Figure 3. Type-B Standard Uncertainty vs Zenith Angle

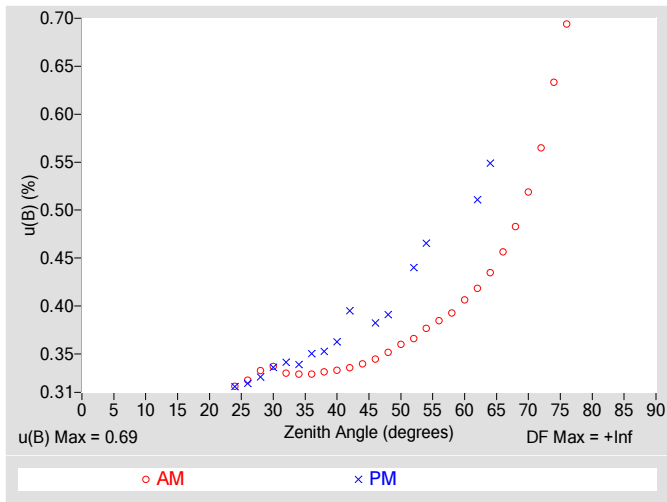


Figure 4. Residuals from Spline Interpolation

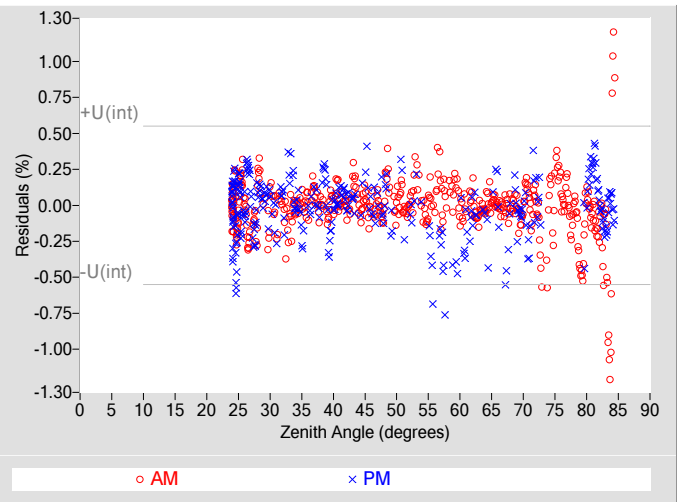


Table 3. Uncertainty using Spline Interpolation ‡

Type-B Standard Uncertainty, u(B) (%)	±0.69
Type-A Interpolating Function, u(int) (%)	±0.28
Combined Standard Uncertainty, u(c) (%)	±0.75
Effective degrees of freedom, DF(c)	36639
Coverage factor, k	1.96
Expanded Uncertainty, U95 (%)	±1.5
AM Valid zenith angle range	24° to 76°
PM Valid zenith angle range	24° to 64°

‡ An illustration for how to reduce the uncertainty in calculating the irradiance using a function rather than R@45°. Not accredited.

Table 4. Calibration Label Values

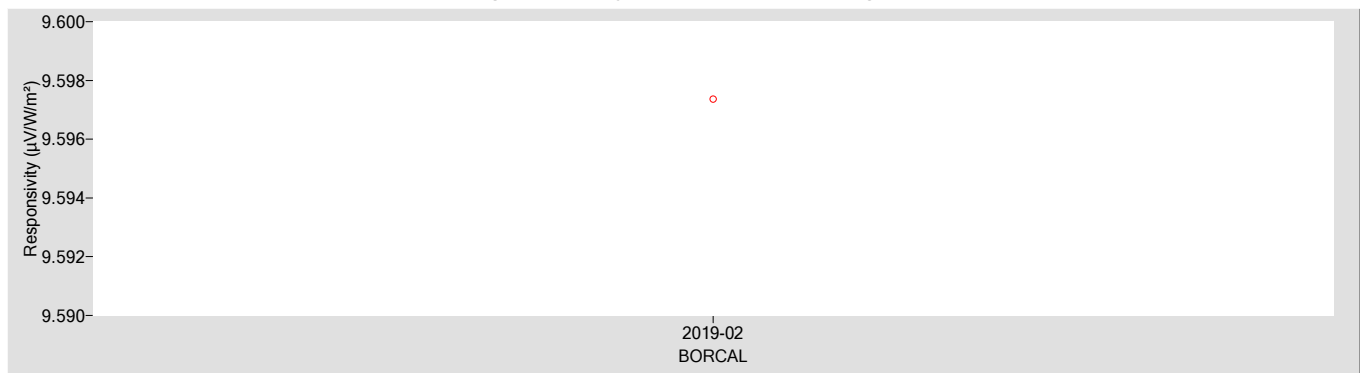
R @ 45° (μV/W/m²)	Rnet (μV/W/m²) †
9.5974	0.087000

† Rnet determination date: Estimated

Table 5. Uncertainty using R @ 45°

Type-B Expanded Uncertainty, U(B) (%)	±0.91
Offset Uncertainty, U(off) (%)	+1.1 / -1.5
Expanded Uncertainty, U (%)	+2.0 / -2.4
Effective degrees of freedom, DF	+Inf
Coverage factor, k	1.96
Valid zenith angle range	30.0° to 60.0°

Figure 5. History of instrument at Zenith Angle = 45°



References:

[1] Reda, I.; Hickey, J.; Long, C.; Myers, D.; Stoffel, T.; Wilcox, S.; Michalsky, J. J.; Dutton, E. G.; Nelson, D. (2005). "Using a Blackbody to Calculate Net Longwave Responsivity of Shortwave Solar Pyranometers to Correct for Their Thermal Offset Error During Outdoor Calibration Using the Component Sum Method." Journal of Atmospheric and Oceanic Technology. , 2005; pp. 1531-1540; NREL Report No. JA-560-36646. doi:10.1175/JTECH1782.1

[2] Reda, I.; Myers, D.; Stoffel, T. (2008). "Uncertainty Estimate for the Outdoor Calibration of Solar Pyranometers: A Metrologist Perspective." Measure. (NCSLI Journal of Measurement Science). Vol. 3(4), December 2008; pp. 58-66; NREL Report No. JA-581-4137

[3] Reda, I.; Andreas, A. (2004). "Solar Position Algorithm for Solar Radiation Applications." Solar Energy. Vol. 76(5), 2004; pp. 577-589; NREL Report No. JA-560-35518. doi:10.1016/j.solener.2003.12.003

[4] Stoffel, T.; Reda, I. (2009). "NREL Pyrheliometer Comparisons: 22 September - 3 October 2008 (NPC-2008)." 54 pp.; NREL Report No. TP-550-45016.

[5] Reda, I.; Stoffel, T.; Myers, D. (2003). "Method to Calibrate a Solar Pyranometer for Measuring Reference Diffuse Irradiance." Solar Energy. Vol. 74, 2003; pp. 103-112; NREL Report No. JA-560-35025. doi:10.1016/S0038-092X(03)00124-5

[6] Reda, I. (1996). Calibration of a Solar Absolute Cavity Radiometer with Traceability to the World Radiometric Reference. 79 pp.; NREL Report No. TP-463-20619.

[7] Reda, I.; Gröbner, J.; Stoffel, T.; Myers, D.; Forgan, B. (2008). Improvements in the Blackbody Calibration of Pyrgeometers. ARM 2008 Science Team Meeting (Poster).



# National Renewable Energy Laboratory

## Solar Radiation Research Laboratory

### Metrology Laboratory

### Calibration Certificate



<b>Test Instrument:</b>	Pyranometer	<b>Manufacturer:</b>	Hukseflux
<b>Model:</b>	SR25	<b>Serial Number:</b>	2529
<b>Calibration Date:</b>	5/3/2019	<b>Due Date:</b>	5/3/2020
<b>Customer:</b>	NREL-SRRL-BMS	<b>Environmental Conditions:</b>	see page 4
<b>Test Dates:</b>	5/3		

This certifies that the above product was calibrated in compliance with ISO/IEC 17025:2005. Measurement uncertainties at the time of calibration are consistent with the Guide to the Expression of Uncertainty in Measurement (GUM) using Reda et al., 2008. All nominal values are traceable to the International System (SI) Units of Measurement.

No statement of compliance with specifications is made or implied on this certificate. However, the estimated uncertainties are the uncertainties of the calibration process; users must add other uncertainties that are relevant to their measuring system, environmental and sky conditions, outdoor set-up, and site location.

The Type-B Standard Uncertainty of using the responsivity at each even zenith angle is reported, and the Expanded Uncertainty of the calibration is reported using two methods:

1. The Expanded Uncertainty of using the responsivity at zenith angle = 45°, within the zenith angle range from 30.0° to 60.0°
2. The Expanded Uncertainty of using Spline Interpolating Functions for the responsivity versus zenith angle.

This certificate applies only to the item identified above and shall not be reproduced other than in full, without specific written approval from the calibration facility. Certificate without signature is not valid.

**Table 1. Traceability**

Measurement Type	Instrument	Calibration Date	Calibration Due Date
Beam Irradiance †	Eppley Absolute Cavity Radiometer Model HF, S/N 29219	09/24/2018	09/24/2019
Diffuse Irradiance †	Hukseflux Pyranometer Model SR25, S/N 2541	04/19/2019	04/19/2020
Diffuse Irradiance †	Hukseflux Pyranometer Model SR25, S/N 2542	04/19/2019	04/19/2020
Data Acquisition	NREL Data Acquisition System Model RAP-DAQ, S/N 2005-998	02/14/2019	02/14/2021
Data Acquisition	NREL Data Acquisition System Model RAP-DAQ, S/N 2005-999	02/14/2019	02/14/2021
Infrared Irradiance ‡	Kipp & Zonen Pyrgeometer Model CG4, S/N FT002	04/16/2018	04/16/2022

† Through the World Radiometric Reference (WRR)

‡ Through the World Infrared Standard Group (WISG)

**Number of pages of certificate:** 4

**Calibration Procedure:** BORCAL-P00-Calibration and QA Procedure; available upon request.

**Setup:** Radiometers are calibrated outdoors, using the sun as the source. Pyranometers and pyrgeometers are installed for horizontal measurements, with their signal connectors oriented north, if their design permits.

The shading disk for the reference diffuse subtends a solid angle of 5°. Pyrheliometers are installed on solar trackers.

**Calibrated by:** RCC

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Ibrahim Reda, Technical Manager

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Date

For questions or comments, please contact the technical manager at:

ibrahim.reda@nrel.gov; 303-384-6385; 15013 Denver West Parkway, Golden, CO 80401, USA

# Calibration Results

## 2529 Hukseflux SR25

The responsivity ( $R$ ,  $\mu\text{V}/\text{W}/\text{m}^2$ ) of the test instrument during calibration is calculated using this Measurement Equation:

$$R = (V - R_{net} * W_{net}) / I \quad [1]$$

where,

- $V$  = radiometer output voltage (microvolts),
- $R_{net}$  = radiometer net infrared responsivity ( $\mu\text{V}/\text{W}/\text{m}^2$ ), see Table 4,
- $W_{net}$  = effective net infrared measured by pyrgeometer ( $\text{W}/\text{m}^2$ ),
- =  $W_{in} - W_{out} = W_{in} - \sigma * T_c^4$
- where,  $W_{in}$  = incoming infrared ( $\text{W}/\text{m}^2$ ),  $\sigma = 5.6704\text{e-}8 \text{ W}\cdot\text{m}^{-2}\cdot\text{K}^{-4}$ ,
- $T_c$  = case temperature of pyrgeometer (K).
- $I$  = reference irradiance ( $\text{W}/\text{m}^2$ ), beam (B) or global (G)
- where,  $G = B * \text{COS}(Z) + D$ ,
- $Z$  = zenith angle (degrees),
- $D$  = reference diffuse irradiance ( $\text{W}/\text{m}^2$ ).

Figure 1. Responsivity vs Zenith Angle

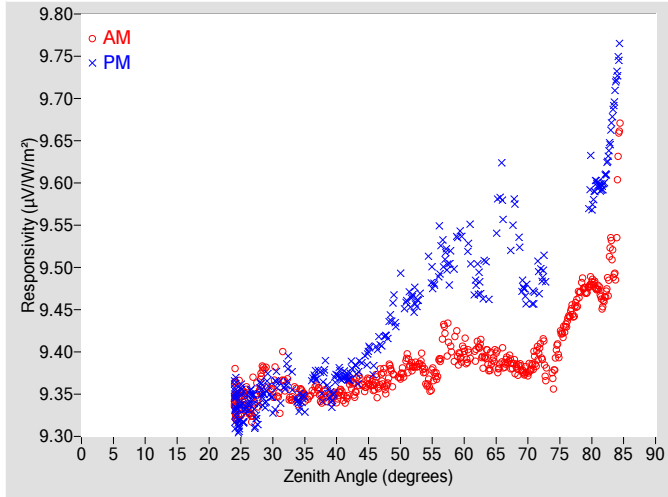


Figure 2. Responsivity vs Local Standard Time

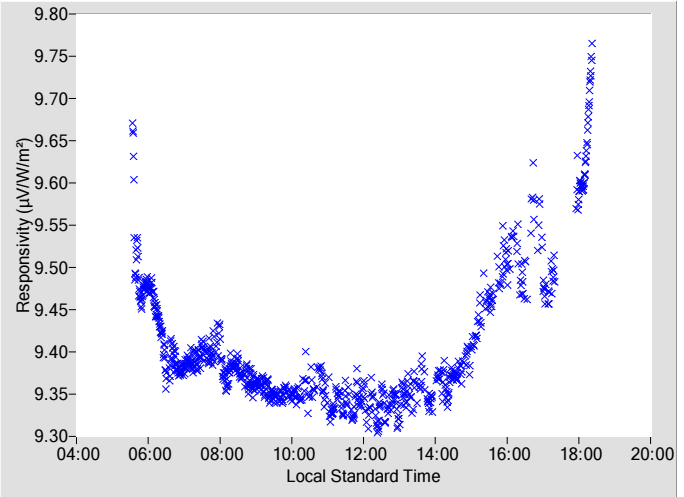


Table 2. Instrument Responsivity (R) and Calibration Type-B Standard Uncertainty, u(B)

Zenith Angle (deg.)	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle	Zenith Angle (deg.)	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle
0	N/A	N/A	N/A	N/A	N/A	N/A	46	9.3629	0.34	108.24	9.3951	0.38	251.90
2	N/A	N/A	N/A	N/A	N/A	N/A	48	9.3647	0.35	105.94	9.4237	0.39	254.20
4	N/A	N/A	N/A	N/A	N/A	N/A	50	9.3717	0.36	103.68	9.4934	0.43	256.39
6	N/A	N/A	N/A	N/A	N/A	N/A	52	9.3825	0.37	101.72	9.4641	0.44	258.42
8	N/A	N/A	N/A	N/A	N/A	N/A	54	9.3679	0.38	99.68	N/A	N/A	N/A
10	N/A	N/A	N/A	N/A	N/A	N/A	56	9.3819	0.38	97.81	9.5103	0.51	262.44
12	N/A	N/A	N/A	N/A	N/A	N/A	58	9.4035	0.39	96.04	9.5120	0.50	263.98
14	N/A	N/A	N/A	N/A	N/A	N/A	60	9.4027	0.41	94.17	N/A	N/A	N/A
16	N/A	N/A	N/A	N/A	N/A	N/A	62	9.4026	0.42	92.49	9.4840	0.51	267.68
18	N/A	N/A	N/A	N/A	N/A	N/A	64	9.3843	0.43	90.78	9.4623	0.55	269.25
20	N/A	N/A	N/A	N/A	N/A	N/A	66	9.3904	0.46	89.05	9.5868	N/A	271.01
22	N/A	N/A	N/A	N/A	N/A	N/A	68	9.3839	0.48	87.48	9.5780	N/A	272.59
24	9.3379	0.32	174.14	9.3432	0.32	185.41	70	9.3772	0.52	85.82	9.4798	N/A	274.13
26	9.3403	0.32	153.65	9.3364	0.32	205.79	72	9.3993	0.56	84.27	9.4849	N/A	275.96
28	9.3624	0.33	144.15	9.3546	0.33	216.06	74	9.3715	0.63	82.65	N/A	N/A	N/A
30	9.3562	0.34	137.21	9.3401	0.34	222.49	76	9.4319	0.69	81.04	N/A	N/A	N/A
32	9.3601	0.33	132.01	9.3649	0.34	228.56	78	9.4661	N/A	79.42	N/A	N/A	N/A
34	9.3440	0.33	126.86	9.3399	0.34	233.18	80	9.4828	N/A	77.82	9.5787	N/A	282.42
36	9.3498	0.33	123.10	9.3677	0.35	237.49	82	9.4627	N/A	76.16	9.6035	N/A	284.04
38	9.3497	0.33	119.38	9.3699	0.35	240.67	84	9.5829	N/A	74.48	9.7326	N/A	285.71
40	9.3465	0.33	116.25	9.3705	0.36	243.81	86	N/A	N/A	N/A	N/A	N/A	N/A
42	9.3625	0.34	113.36	9.3731	0.39	246.78	88	N/A	N/A	N/A	N/A	N/A	N/A
44	9.3609	0.34	110.65	9.3871	0.39	249.35	90	N/A	N/A	N/A	N/A	N/A	N/A

N/A - Not Available

Figure 3. Type-B Standard Uncertainty vs Zenith Angle

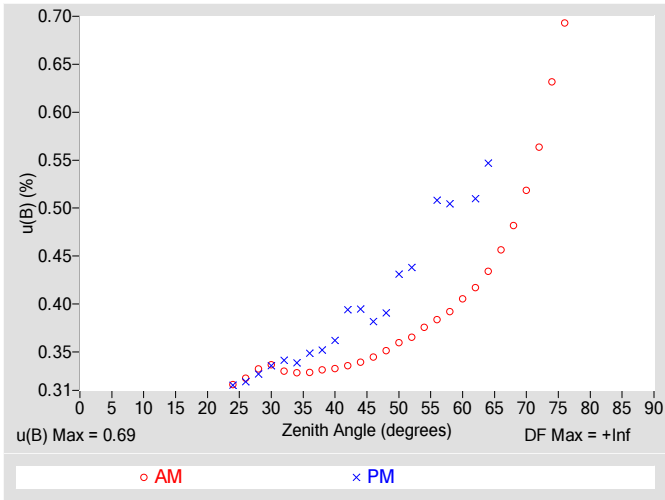


Figure 4. Residuals from Spline Interpolation

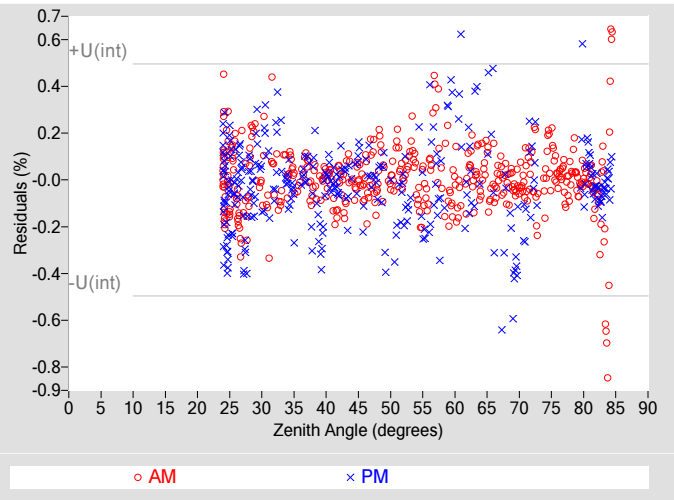


Table 3. Uncertainty using Spline Interpolation ‡

Type-B Standard Uncertainty, $u(B)$ (%)	$\pm 0.69$
Type-A Interpolating Function, $u(int)$ (%)	$\pm 0.25$
Combined Standard Uncertainty, $u(c)$ (%)	$\pm 0.74$
Effective degrees of freedom, $DF(c)$	50382
Coverage factor, $k$	1.96
Expanded Uncertainty, $U95$ (%)	$\pm 1.4$
AM Valid zenith angle range	24° to 76°
PM Valid zenith angle range	24° to 64°

‡ An illustration for how to reduce the uncertainty in calculating the irradiance using a function rather than  $R@45^\circ$ . Not accredited.

Table 4. Calibration Label Values

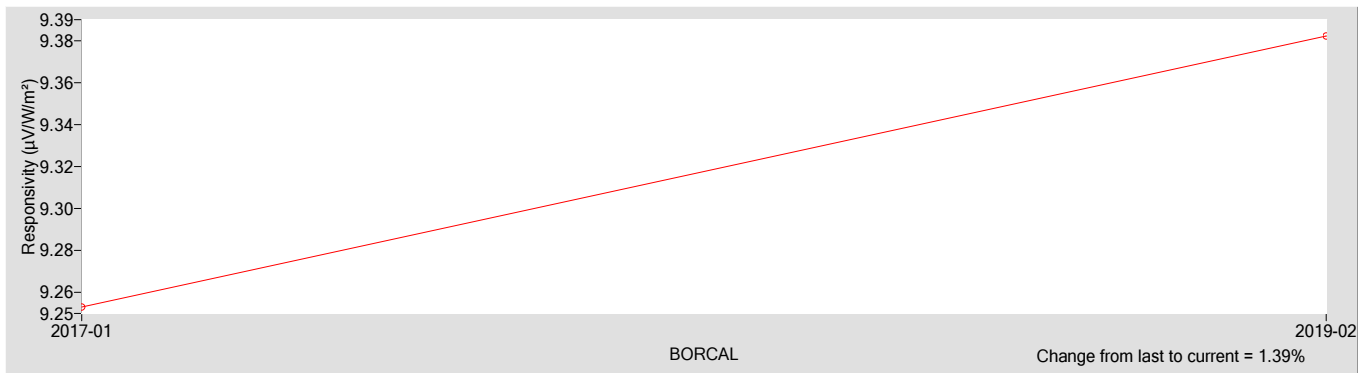
$R @ 45^\circ$ ( $\mu V/W/m^2$ )	$R_{net}$ ( $\mu V/W/m^2$ ) †
9.3822	0.043000

†  $R_{net}$  determination date: Estimated

Table 5. Uncertainty using  $R @ 45^\circ$

Type-B Expanded Uncertainty, $U(B)$ (%)	$\pm 1.00$
Offset Uncertainty, $U(off)$ (%)	+1.4 / -0.45
Expanded Uncertainty, $U$ (%)	+2.4 / -1.4
Effective degrees of freedom, $DF$	+Inf
Coverage factor, $k$	1.96
Valid zenith angle range	30.0° to 60.0°

Figure 5. History of instrument at Zenith Angle = 45°



References:

[1] Reda, I.; Hickey, J.; Long, C.; Myers, D.; Stoffel, T.; Wilcox, S.; Michalsky, J. J.; Dutton, E. G.; Nelson, D. (2005). "Using a Blackbody to Calculate Net Longwave Responsivity of Shortwave Solar Pyranometers to Correct for Their Thermal Offset Error During Outdoor Calibration Using the Component Sum Method." Journal of Atmospheric and Oceanic Technology. , 2005; pp. 1531-1540; NREL Report No. JA-560-36646. doi:10.1175/JTECH1782.1

[2] Reda, I.; Myers, D.; Stoffel, T. (2008). "Uncertainty Estimate for the Outdoor Calibration of Solar Pyranometers: A Metrologist Perspective." Measure. (NCSLI Journal of Measurement Science). Vol. 3(4), December 2008; pp. 58-66; NREL Report No. JA-581-4137

[3] Reda, I.; Andreas, A. (2004). "Solar Position Algorithm for Solar Radiation Applications." Solar Energy. Vol. 76(5), 2004; pp. 577-589; NREL Report No. JA-560-35518. doi:10.1016/j.solener.2003.12.003

[4] Stoffel, T.; Reda, I. (2009). "NREL Pyrheliometer Comparisons: 22 September - 3 October 2008 (NPC-2008)." 54 pp.; NREL Report No. TP-550-45016.

[5] Reda, I.; Stoffel, T.; Myers, D. (2003). "Method to Calibrate a Solar Pyranometer for Measuring Reference Diffuse Irradiance." Solar Energy. Vol. 74, 2003; pp. 103-112; NREL Report No. JA-560-35025. doi:10.1016/S0038-092X(03)00124-5

[6] Reda, I. (1996). Calibration of a Solar Absolute Cavity Radiometer with Traceability to the World Radiometric Reference. 79 pp.; NREL Report No. TP-463-20619.

[7] Reda, I.; Gröbner, J.; Stoffel, T.; Myers, D.; Forgan, B. (2008). Improvements in the Blackbody Calibration of Pyrgeometers. ARM 2008 Science Team Meeting (Poster).



# National Renewable Energy Laboratory

## Solar Radiation Research Laboratory

### Metrology Laboratory

### Calibration Certificate



<b>Test Instrument:</b>	Pyranometer	<b>Manufacturer:</b>	Hukseflux
<b>Model:</b>	SR25	<b>Serial Number:</b>	2543
<b>Calibration Date:</b>	5/3/2019	<b>Due Date:</b>	5/3/2020
<b>Customer:</b>	NREL-SRRL-BMS	<b>Environmental Conditions:</b>	see page 4
<b>Test Dates:</b>	5/3		

This certifies that the above product was calibrated in compliance with ISO/IEC 17025:2005. Measurement uncertainties at the time of calibration are consistent with the Guide to the Expression of Uncertainty in Measurement (GUM) using Reda et al., 2008. All nominal values are traceable to the International System (SI) Units of Measurement.

No statement of compliance with specifications is made or implied on this certificate. However, the estimated uncertainties are the uncertainties of the calibration process; users must add other uncertainties that are relevant to their measuring system, environmental and sky conditions, outdoor set-up, and site location.

The Type-B Standard Uncertainty of using the responsivity at each even zenith angle is reported, and the Expanded Uncertainty of the calibration is reported using two methods:

1. The Expanded Uncertainty of using the responsivity at zenith angle = 45°, within the zenith angle range from 30.0° to 60.0°
2. The Expanded Uncertainty of using Spline Interpolating Functions for the responsivity versus zenith angle.

This certificate applies only to the item identified above and shall not be reproduced other than in full, without specific written approval from the calibration facility. Certificate without signature is not valid.

**Table 1. Traceability**

Measurement Type	Instrument	Calibration Date	Calibration Due Date
Beam Irradiance †	Eppley Absolute Cavity Radiometer Model HF, S/N 29219	09/24/2018	09/24/2019
Diffuse Irradiance †	Hukseflux Pyranometer Model SR25, S/N 2541	04/19/2019	04/19/2020
Diffuse Irradiance †	Hukseflux Pyranometer Model SR25, S/N 2542	04/19/2019	04/19/2020
Data Acquisition	NREL Data Acquisition System Model RAP-DAQ, S/N 2005-998	02/14/2019	02/14/2021
Data Acquisition	NREL Data Acquisition System Model RAP-DAQ, S/N 2005-999	02/14/2019	02/14/2021
Infrared Irradiance ‡	Kipp & Zonen Pyrgeometer Model CG4, S/N FT002	04/16/2018	04/16/2022

† Through the World Radiometric Reference (WRR)

‡ Through the World Infrared Standard Group (WISG)

**Number of pages of certificate:** 4

**Calibration Procedure:** BORCAL-P00-Calibration and QA Procedure; available upon request.

**Setup:** Radiometers are calibrated outdoors, using the sun as the source. Pyranometers and pyrgeometers are installed for horizontal measurements, with their signal connectors oriented north, if their design permits.

The shading disk for the reference diffuse subtends a solid angle of 5°. Pyrheliometers are installed on solar trackers.

**Calibrated by:** RCC

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Ibrahim Reda, Technical Manager

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Date

For questions or comments, please contact the technical manager at:

ibrahim.reda@nrel.gov; 303-384-6385; 15013 Denver West Parkway, Golden, CO 80401, USA

# Calibration Results

## 2543 Hukseflux SR25

The responsivity ( $R$ ,  $\mu\text{V}/\text{W}/\text{m}^2$ ) of the test instrument during calibration is calculated using this Measurement Equation:

$$R = (V - R_{net} * W_{net}) / I \tag{1}$$

where,

- $V$  = radiometer output voltage (microvolts),
  - $R_{net}$  = radiometer net infrared responsivity ( $\mu\text{V}/\text{W}/\text{m}^2$ ), see Table 4,
  - $W_{net}$  = effective net infrared measured by pyrgeometer ( $\text{W}/\text{m}^2$ ),
  - =  $W_{in} - W_{out} = W_{in} - \sigma * T_c^4$
  - where,  $W_{in}$  = incoming infrared ( $\text{W}/\text{m}^2$ ),  $\sigma = 5.6704\text{e-}8 \text{ W}\cdot\text{m}^{-2}\cdot\text{K}^{-4}$ ,
  - $T_c$  = case temperature of pyrgeometer (K).
- $I$  = reference irradiance ( $\text{W}/\text{m}^2$ ), beam (B) or global (G)
  - where,  $G = B * \text{COS}(Z) + D$ ,
  - $Z$  = zenith angle (degrees),
  - $D$  = reference diffuse irradiance ( $\text{W}/\text{m}^2$ ).

Figure 1. Responsivity vs Zenith Angle

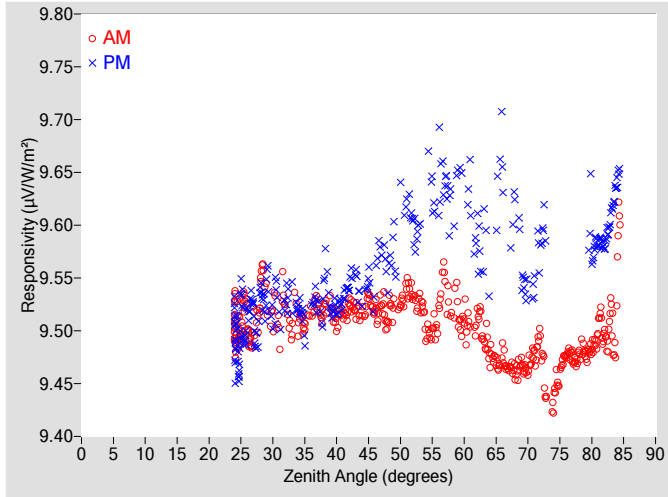


Figure 2. Responsivity vs Local Standard Time

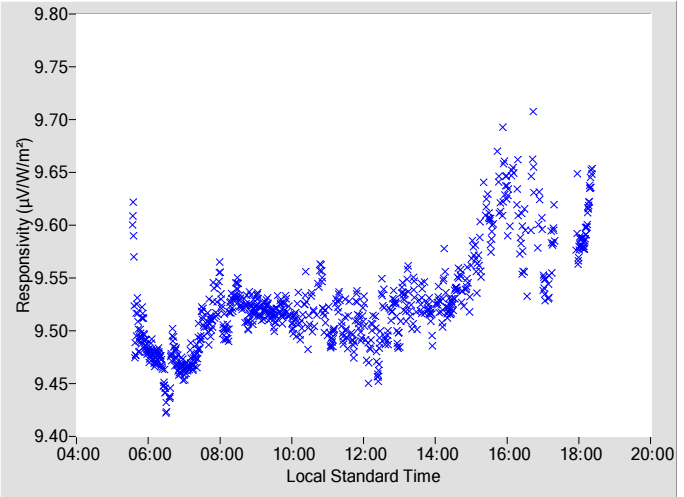


Table 2. Instrument Responsivity (R) and Calibration Type-B Standard Uncertainty, u(B)

Zenith Angle (deg.)	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle	Zenith Angle (deg.)	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle
0	N/A	N/A	N/A	N/A	N/A	N/A	46	9.5203	0.34	108.24	9.5470	0.38	251.90
2	N/A	N/A	N/A	N/A	N/A	N/A	48	9.5103	0.35	105.94	9.5520	0.39	254.20
4	N/A	N/A	N/A	N/A	N/A	N/A	50	9.5253	0.36	103.68	9.6405	0.43	256.39
6	N/A	N/A	N/A	N/A	N/A	N/A	52	9.5350	0.37	101.72	9.6019	0.44	258.42
8	N/A	N/A	N/A	N/A	N/A	N/A	54	9.5016	0.38	99.68	N/A	N/A	N/A
10	N/A	N/A	N/A	N/A	N/A	N/A	56	9.5156	0.38	97.81	9.6413	0.51	262.44
12	N/A	N/A	N/A	N/A	N/A	N/A	58	9.5156	0.39	96.04	9.6312	0.50	263.98
14	N/A	N/A	N/A	N/A	N/A	N/A	60	9.5098	0.41	94.17	N/A	N/A	N/A
16	N/A	N/A	N/A	N/A	N/A	N/A	62	9.5087	0.42	92.49	9.5840	0.51	267.68
18	N/A	N/A	N/A	N/A	N/A	N/A	64	9.4775	0.43	90.78	9.5327	0.55	269.25
20	N/A	N/A	N/A	N/A	N/A	N/A	66	9.4785	0.46	89.05	9.6645	N/A	271.01
22	N/A	N/A	N/A	N/A	N/A	N/A	68	9.4621	0.48	87.48	9.6278	N/A	272.59
24	9.5036	0.32	174.17	9.4980	0.32	185.41	70	9.4648	0.52	85.82	9.5487	N/A	274.13
26	9.5062	0.32	153.65	9.5074	0.32	205.79	72	9.4875	0.56	84.27	9.5791	N/A	275.96
28	9.5356	0.33	144.15	9.5331	0.33	216.06	74	9.4329	0.63	82.65	N/A	N/A	N/A
30	9.5182	0.34	137.21	9.5133	0.34	222.49	76	9.4766	0.69	81.04	N/A	N/A	N/A
32	9.5250	0.33	132.01	9.5268	0.34	228.56	78	9.4762	N/A	79.42	N/A	N/A	N/A
34	9.5078	0.33	126.86	9.5210	0.34	233.18	80	9.4831	N/A	77.82	9.5727	N/A	282.42
36	9.5171	0.33	123.10	9.5259	0.35	237.49	82	9.4941	N/A	76.16	9.5812	N/A	284.04
38	9.5214	0.33	119.38	9.5418	0.35	240.67	84	9.5560	N/A	74.48	9.6420	N/A	285.71
40	9.5085	0.33	116.25	9.5208	0.36	243.81	86	N/A	N/A	N/A	N/A	N/A	N/A
42	9.5254	0.34	113.36	9.5455	0.39	246.78	88	N/A	N/A	N/A	N/A	N/A	N/A
44	9.5184	0.34	110.65	9.5232	0.39	249.35	90	N/A	N/A	N/A	N/A	N/A	N/A

N/A - Not Available



Figure 3. Type-B Standard Uncertainty vs Zenith Angle

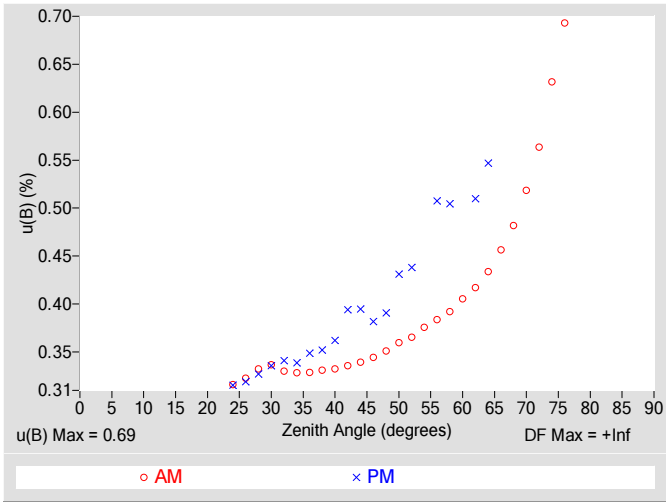


Figure 4. Residuals from Spline Interpolation

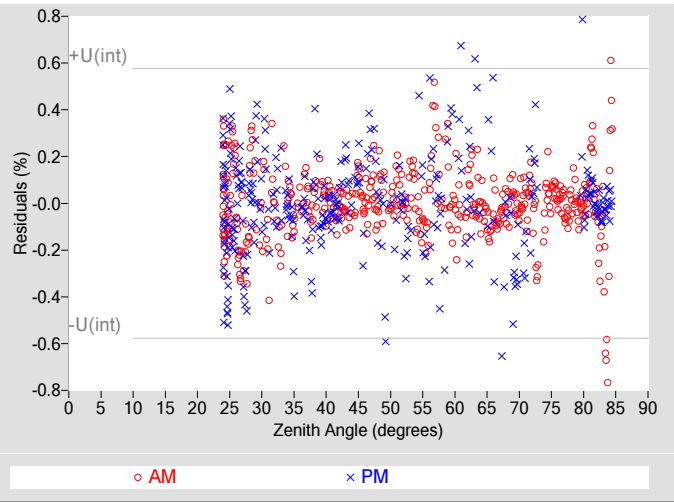


Table 3. Uncertainty using Spline Interpolation ‡

Type-B Standard Uncertainty, $u(B)$ (%)	$\pm 0.69$
Type-A Interpolating Function, $u(int)$ (%)	$\pm 0.29$
Combined Standard Uncertainty, $u(c)$ (%)	$\pm 0.75$
Effective degrees of freedom, $DF(c)$	29791
Coverage factor, $k$	1.96
Expanded Uncertainty, $U95$ (%)	$\pm 1.5$
AM Valid zenith angle range	24° to 76°
PM Valid zenith angle range	24° to 64°

‡ An illustration for how to reduce the uncertainty in calculating the irradiance using a function rather than  $R@45^\circ$ . Not accredited.

Table 4. Calibration Label Values

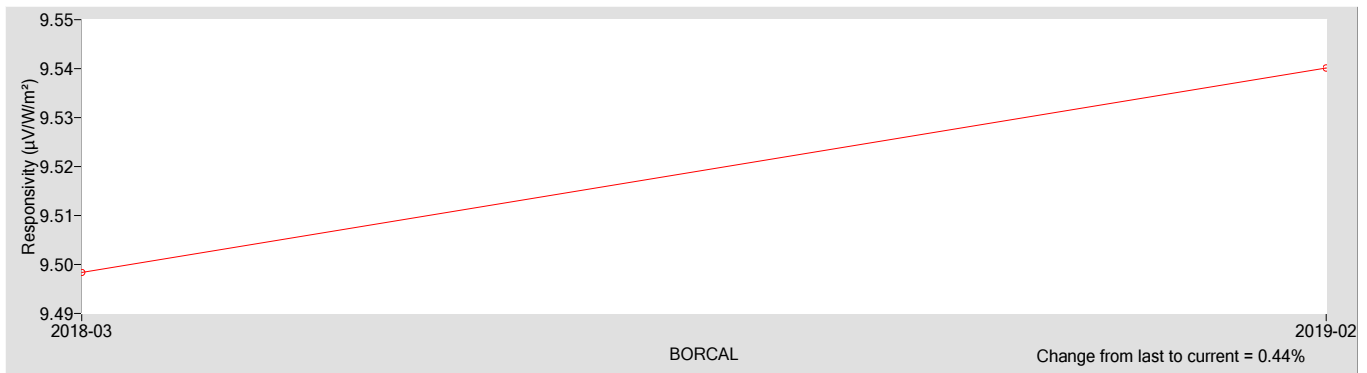
$R @ 45^\circ$ ( $\mu V/W/m^2$ )	$R_{net}$ ( $\mu V/W/m^2$ ) †
9.5401	0.043000

†  $R_{net}$  determination date: Estimated

Table 5. Uncertainty using  $R @ 45^\circ$

Type-B Expanded Uncertainty, $U(B)$ (%)	$\pm 0.99$
Offset Uncertainty, $U(off)$ (%)	+1.1 / -0.40
Expanded Uncertainty, $U$ (%)	+2.1 / -1.4
Effective degrees of freedom, $DF$	+Inf
Coverage factor, $k$	1.96
Valid zenith angle range	30.0° to 60.0°

Figure 5. History of instrument at Zenith Angle = 45°



References:

[1] Reda, I.; Hickey, J.; Long, C.; Myers, D.; Stoffel, T.; Wilcox, S.; Michalsky, J. J.; Dutton, E. G.; Nelson, D. (2005). "Using a Blackbody to Calculate Net Longwave Responsivity of Shortwave Solar Pyranometers to Correct for Their Thermal Offset Error During Outdoor Calibration Using the Component Sum Method." Journal of Atmospheric and Oceanic Technology. , 2005; pp. 1531-1540; NREL Report No. JA-560-36646. doi:10.1175/JTECH1782.1

[2] Reda, I.; Myers, D.; Stoffel, T. (2008). "Uncertainty Estimate for the Outdoor Calibration of Solar Pyranometers: A Metrologist Perspective." Measure. (NCSLI Journal of Measurement Science). Vol. 3(4), December 2008; pp. 58-66; NREL Report No. JA-581-4137

[3] Reda, I.; Andreas, A. (2004). "Solar Position Algorithm for Solar Radiation Applications." Solar Energy. Vol. 76(5), 2004; pp. 577-589; NREL Report No. JA-560-35518. doi:10.1016/j.solener.2003.12.003

[4] Stoffel, T.; Reda, I. (2009). "NREL Pyrheliometer Comparisons: 22 September - 3 October 2008 (NPC-2008)." 54 pp.; NREL Report No. TP-550-45016.

[5] Reda, I.; Stoffel, T.; Myers, D. (2003). "Method to Calibrate a Solar Pyranometer for Measuring Reference Diffuse Irradiance." Solar Energy. Vol. 74, 2003; pp. 103-112; NREL Report No. JA-560-35025. doi:10.1016/S0038-092X(03)00124-5

[6] Reda, I. (1996). Calibration of a Solar Absolute Cavity Radiometer with Traceability to the World Radiometric Reference. 79 pp.; NREL Report No. TP-463-20619.

[7] Reda, I.; Gröbner, J.; Stoffel, T.; Myers, D.; Forgan, B. (2008). Improvements in the Blackbody Calibration of Pyrgeometers. ARM 2008 Science Team Meeting (Poster).





# National Renewable Energy Laboratory

## Solar Radiation Research Laboratory

### Metrology Laboratory

### Calibration Certificate



<b>Test Instrument:</b>	Precision Spectral Pyranometer (Ventilated)	<b>Manufacturer:</b>	Eppley
<b>Model:</b>	PSP	<b>Serial Number:</b>	28402F3
<b>Calibration Date:</b>	5/3/2019	<b>Due Date:</b>	5/3/2020
<b>Customer:</b>	NREL-SRRL-BMS	<b>Environmental Conditions:</b>	see page 4
<b>Test Dates:</b>	5/3		

This certifies that the above product was calibrated in compliance with ISO/IEC 17025:2005. Measurement uncertainties at the time of calibration are consistent with the Guide to the Expression of Uncertainty in Measurement (GUM) using Reda et al., 2008. All nominal values are traceable to the International System (SI) Units of Measurement.

No statement of compliance with specifications is made or implied on this certificate. However, the estimated uncertainties are the uncertainties of the calibration process; users must add other uncertainties that are relevant to their measuring system, environmental and sky conditions, outdoor set-up, and site location.

The Type-B Standard Uncertainty of using the responsivity at each even zenith angle is reported, and the Expanded Uncertainty of the calibration is reported using two methods:

1. The Expanded Uncertainty of using the responsivity at zenith angle = 45°, within the zenith angle range from 30.0° to 60.0°
2. The Expanded Uncertainty of using Spline Interpolating Functions for the responsivity versus zenith angle.

This certificate applies only to the item identified above and shall not be reproduced other than in full, without specific written approval from the calibration facility. Certificate without signature is not valid.

**Table 1. Traceability**

Measurement Type	Instrument	Calibration Date	Calibration Due Date
Beam Irradiance †	Eppley Absolute Cavity Radiometer Model HF, S/N 29219	09/24/2018	09/24/2019
Diffuse Irradiance †	Hukseflux Pyranometer Model SR25, S/N 2541	04/19/2019	04/19/2020
Diffuse Irradiance †	Hukseflux Pyranometer Model SR25, S/N 2542	04/19/2019	04/19/2020
Data Acquisition	NREL Data Acquisition System Model RAP-DAQ, S/N 2005-998	02/14/2019	02/14/2021
Data Acquisition	NREL Data Acquisition System Model RAP-DAQ, S/N 2005-999	02/14/2019	02/14/2021
Infrared Irradiance ‡	Eppley Downwelling Pyrgeometer (Ventilated) Model PIR-V, S/N 37757F3	04/02/2019	04/02/2023

† Through the World Radiometric Reference (WRR)

‡ Through the World Infrared Standard Group (WISG)

**Number of pages of certificate:** 4

**Calibration Procedure:** BORCAL-P00-Calibration and QA Procedure; available upon request.

**Setup:** Radiometers are calibrated outdoors, using the sun as the source. Pyranometers and pyrgeometers are installed for horizontal measurements, with their signal connectors oriented north, if their design permits.

The shading disk for the reference diffuse subtends a solid angle of 5°. Pyrheliometers are installed on solar trackers.

**Calibrated by:** RCC

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Ibrahim Reda, Technical Manager

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Date

For questions or comments, please contact the technical manager at:

ibrahim.reda@nrel.gov; 303-384-6385; 15013 Denver West Parkway, Golden, CO 80401, USA

# Calibration Results

## 28402F3 Eppley PSP

The responsivity ( $R$ ,  $\mu\text{V}/\text{W}/\text{m}^2$ ) of the test instrument during calibration is calculated using this Measurement Equation:

$$R = (V - R_{net} * W_{net}) / I \tag{1}$$

where,

- $V$  = radiometer output voltage (microvolts),
  - $R_{net}$  = radiometer net infrared responsivity ( $\mu\text{V}/\text{W}/\text{m}^2$ ), see Table 4,
  - $W_{net}$  = effective net infrared measured by pyrgeometer ( $\text{W}/\text{m}^2$ ),
  - =  $W_{in} - W_{out} = W_{in} - \sigma * T_c^4$
  - where,  $W_{in}$  = incoming infrared ( $\text{W}/\text{m}^2$ ),  $\sigma = 5.6704\text{e-}8 \text{ W}\cdot\text{m}^{-2}\cdot\text{K}^{-4}$ ,
  - $T_c$  = case temperature of pyrgeometer (K).
- $I$  = reference irradiance ( $\text{W}/\text{m}^2$ ), beam (B) or global (G)
  - where,  $G = B * \text{COS}(Z) + D$ ,
  - $Z$  = zenith angle (degrees),
  - $D$  = reference diffuse irradiance ( $\text{W}/\text{m}^2$ ).

Figure 1. Responsivity vs Zenith Angle

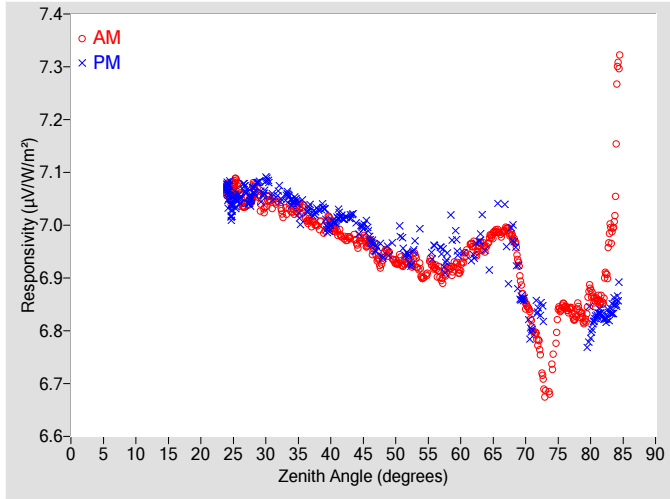


Figure 2. Responsivity vs Local Standard Time

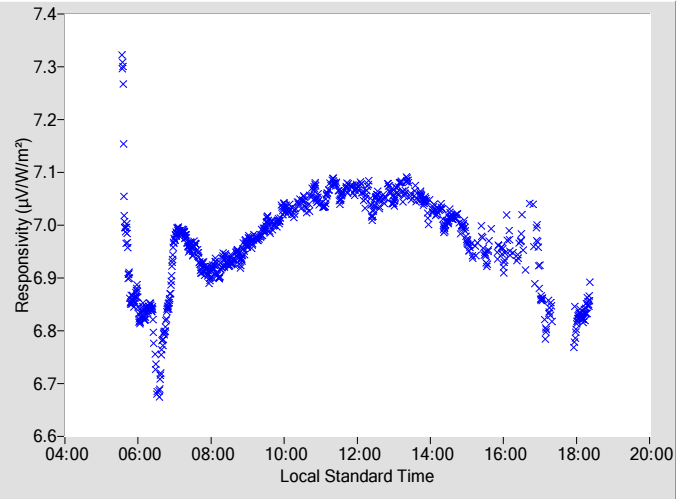


Table 2. Instrument Responsivity (R) and Calibration Type-B Standard Uncertainty, u(B)

Zenith Angle (deg.)	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle	Zenith Angle (deg.)	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle
0	N/A	N/A	N/A	N/A	N/A	N/A	46	6.9681	0.36	108.27	6.9749	0.40	251.97
2	N/A	N/A	N/A	N/A	N/A	N/A	48	6.9387	0.37	105.85	6.9397	0.41	254.11
4	N/A	N/A	N/A	N/A	N/A	N/A	50	6.9303	0.38	103.76	N/A	N/A	N/A
6	N/A	N/A	N/A	N/A	N/A	N/A	52	6.9365	0.38	101.71	6.9387	0.46	258.46
8	N/A	N/A	N/A	N/A	N/A	N/A	54	6.9041	0.40	99.70	6.9932	0.49	260.15
10	N/A	N/A	N/A	N/A	N/A	N/A	56	6.9202	0.41	97.80	6.9618	0.53	262.26
12	N/A	N/A	N/A	N/A	N/A	N/A	58	6.9169	0.42	95.99	6.9369	0.53	264.00
14	N/A	N/A	N/A	N/A	N/A	N/A	60	6.9190	0.43	94.22	N/A	N/A	N/A
16	N/A	N/A	N/A	N/A	N/A	N/A	62	6.9621	0.45	92.49	6.9410	0.53	267.70
18	N/A	N/A	N/A	N/A	N/A	N/A	64	6.9598	0.47	90.76	6.9529	0.56	269.13
20	N/A	N/A	N/A	N/A	N/A	N/A	66	6.9850	0.49	89.12	7.0412	N/A	270.81
22	N/A	N/A	N/A	N/A	N/A	N/A	68	6.9783	0.52	87.50	6.9836	N/A	272.67
24	7.0698	0.33	174.48	7.0638	0.32	185.80	70	6.8503	0.56	85.86	6.8620	N/A	274.11
26	7.0624	0.33	153.87	7.0499	0.33	205.88	72	6.7731	0.61	84.24	6.8353	N/A	275.88
28	7.0632	0.34	144.21	7.0612	0.34	215.89	74	6.7249	0.69	82.62	N/A	N/A	N/A
30	7.0350	0.35	137.27	7.0791	0.35	222.70	76	6.8473	0.76	81.01	N/A	N/A	N/A
32	7.0441	0.34	132.06	7.0600	0.35	228.48	78	6.8389	N/A	79.45	N/A	N/A	N/A
34	7.0300	0.34	127.04	7.0443	0.35	233.22	80	6.8759	N/A	77.80	6.8081	N/A	282.42
36	7.0199	0.34	122.82	N/A	N/A	N/A	82	6.8719	N/A	76.14	6.8244	N/A	284.03
38	6.9979	0.34	119.53	7.0307	0.36	240.67	84	7.1837	N/A	74.48	6.8540	N/A	285.69
40	7.0059	0.35	116.31	6.9996	0.37	243.83	86	N/A	N/A	N/A	N/A	N/A	N/A
42	6.9764	0.35	113.18	7.0126	0.40	246.74	88	N/A	N/A	N/A	N/A	N/A	N/A
44	6.9656	0.35	110.72	7.0044	0.41	249.31	90	N/A	N/A	N/A	N/A	N/A	N/A

N/A - Not Available

Figure 3. Type-B Standard Uncertainty vs Zenith Angle

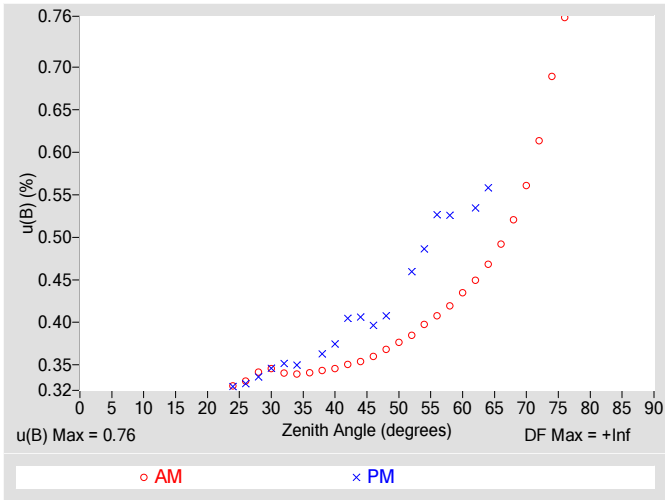


Figure 4. Residuals from Spline Interpolation

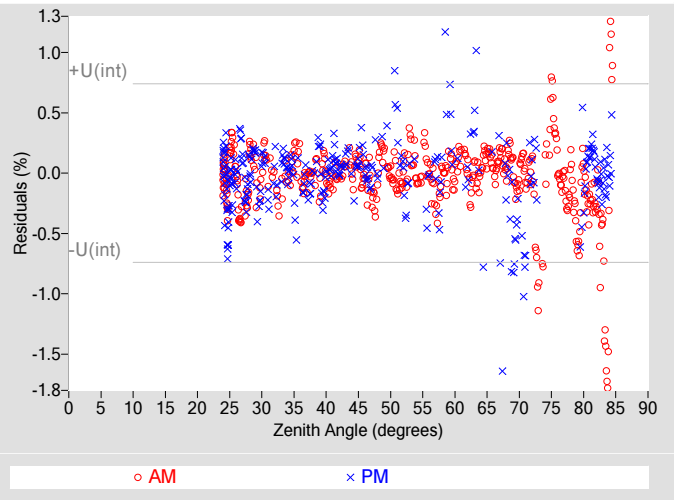


Table 3. Uncertainty using Spline Interpolation ‡

Type-B Standard Uncertainty, $u(B)$ (%)	$\pm 0.76$
Type-A Interpolating Function, $u(int)$ (%)	$\pm 0.37$
Combined Standard Uncertainty, $u(c)$ (%)	$\pm 0.84$
Effective degrees of freedom, $DF(c)$	17905
Coverage factor, $k$	1.96
Expanded Uncertainty, $U95$ (%)	$\pm 1.7$
AM Valid zenith angle range	24° to 76°
PM Valid zenith angle range	24° to 64°

‡ An illustration for how to reduce the uncertainty in calculating the irradiance using a function rather than  $R@45^\circ$ . Not accredited.

Table 4. Calibration Label Values

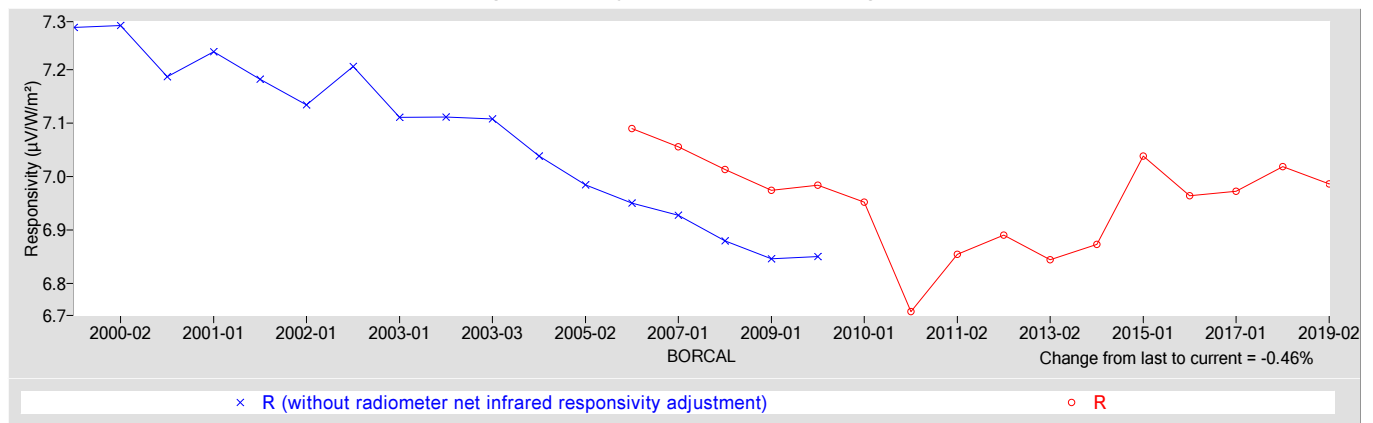
$R @ 45^\circ$ ( $\mu V/W/m^2$ )	$R_{net}$ ( $\mu V/W/m^2$ ) †
6.9865	0.64000

†  $R_{net}$  determination date: 02/28/2006

Table 5. Uncertainty using  $R @ 45^\circ$

Type-B Expanded Uncertainty, $U(B)$ (%)	$\pm 1.0$
Offset Uncertainty, $U(off)$ (%)	+1.3 / -1.2
Expanded Uncertainty, $U$ (%)	+2.4 / -2.2
Effective degrees of freedom, $DF$	+Inf
Coverage factor, $k$	1.96
Valid zenith angle range	30.0° to 60.0°

Figure 5. History of instrument at Zenith Angle = 45°



References:

[1] Reda, I.; Hickey, J.; Long, C.; Myers, D.; Stoffel, T.; Wilcox, S.; Michalsky, J. J.; Dutton, E. G.; Nelson, D. (2005). "Using a Blackbody to Calculate Net Longwave Responsivity of Shortwave Solar Pyranometers to Correct for Their Thermal Offset Error During Outdoor Calibration Using the Component Sum Method." Journal of Atmospheric and Oceanic Technology. , 2005; pp. 1531-1540; NREL Report No. JA-560-36646. doi:10.1175/JTECH1782.1

[2] Reda, I.; Myers, D.; Stoffel, T. (2008). "Uncertainty Estimate for the Outdoor Calibration of Solar Pyranometers: A Metrologist Perspective." Measure. (NCSLI Journal of Measurement Science). Vol. 3(4), December 2008; pp. 58-66; NREL Report No. JA-581-4137

[3] Reda, I.; Andreas, A. (2004). "Solar Position Algorithm for Solar Radiation Applications." Solar Energy. Vol. 76(5), 2004; pp. 577-589; NREL Report No. JA-560-35518. doi:10.1016/j.solener.2003.12.003

[4] Stoffel, T.; Reda, I. (2009). "NREL Pyrheliometer Comparisons: 22 September - 3 October 2008 (NPC-2008)." 54 pp.; NREL Report No. TP-550-45016.

[5] Reda, I.; Stoffel, T.; Myers, D. (2003). "Method to Calibrate a Solar Pyranometer for Measuring Reference Diffuse Irradiance." Solar Energy. Vol. 74, 2003; pp. 103-112; NREL Report No. JA-560-35025. doi:10.1016/S0038-092X(03)00124-5

[6] Reda, I. (1996). Calibration of a Solar Absolute Cavity Radiometer with Traceability to the World Radiometric Reference. 79 pp.; NREL Report No. TP-463-20619.

[7] Reda, I.; Gröbner, J.; Stoffel, T.; Myers, D.; Forgan, B. (2008). Improvements in the Blackbody Calibration of Pyrgeometers. ARM 2008 Science Team Meeting (Poster).



# National Renewable Energy Laboratory

## Solar Radiation Research Laboratory

### Metrology Laboratory

### Calibration Certificate



<b>Test Instrument:</b>	Normal Incidence Pyrheliometer	<b>Manufacturer:</b>	Eppley
<b>Model:</b>	NIP	<b>Serial Number:</b>	31137E6
<b>Calibration Date:</b>	5/3/2019	<b>Due Date:</b>	5/3/2020
<b>Customer:</b>	NREL-SRRL-BMS	<b>Environmental Conditions:</b>	see page 4
<b>Test Dates:</b>	5/3		

This certifies that the above product was calibrated in compliance with ISO/IEC 17025:2005. Measurement uncertainties at the time of calibration are consistent with the Guide to the Expression of Uncertainty in Measurement (GUM) using Reda et al., 2008. All nominal values are traceable to the International System (SI) Units of Measurement.

No statement of compliance with specifications is made or implied on this certificate. However, the estimated uncertainties are the uncertainties of the calibration process; users must add other uncertainties that are relevant to their measuring system, environmental and sky conditions, outdoor set-up, and site location.

The Type-B Standard Uncertainty of using the responsivity at each even zenith angle is reported, and the Expanded Uncertainty of the calibration is reported using two methods:

1. The Expanded Uncertainty of using the responsivity at zenith angle = 45°, within the zenith angle range from 30.0° to 60.0°
2. The Expanded Uncertainty of using Spline Interpolating Functions for the responsivity versus zenith angle.

This certificate applies only to the item identified above and shall not be reproduced other than in full, without specific written approval from the calibration facility. Certificate without signature is not valid.

**Table 1. Traceability**

Measurement Type	Instrument	Calibration Date	Calibration Due Date
Beam Irradiance †	Eppley Absolute Cavity Radiometer Model HF, S/N 29219	09/24/2018	09/24/2019
Diffuse Irradiance †	Hukseflux Pyranometer Model SR25, S/N 2541	04/19/2019	04/19/2020
Diffuse Irradiance †	Hukseflux Pyranometer Model SR25, S/N 2542	04/19/2019	04/19/2020
Data Acquisition	NREL Data Acquisition System Model RAP-DAQ, S/N 2005-998	02/14/2019	02/14/2021
Data Acquisition	NREL Data Acquisition System Model RAP-DAQ, S/N 2005-999	02/14/2019	02/14/2021

† Through the World Radiometric Reference (WRR)

**Number of pages of certificate:** 4

**Calibration Procedure:** BORCAL-P00-Calibration and QA Procedure; available upon request.

**Setup:** Radiometers are calibrated outdoors, using the sun as the source. Pyranometers and pyrgeometers are installed for horizontal measurements, with their signal connectors oriented north, if their design permits.

The shading disk for the reference diffuse subtends a solid angle of 5°. Pyrheliometers are installed on solar trackers.

**Calibrated by:** RCC

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Ibrahim Reda, Technical Manager

-----  
Date

For questions or comments, please contact the technical manager at:

ibrahim.reda@nrel.gov; 303-384-6385; 15013 Denver West Parkway, Golden, CO 80401, USA

# Calibration Results

## 31137E6 Eppley NIP

The responsivity ( $R$ ,  $\mu\text{V}/\text{W}/\text{m}^2$ ) of the test instrument during calibration is calculated using this Measurement Equation:

$$R = (V - R_{net} * W_{net}) / I \tag{1}$$

where,

- $V$  = radiometer output voltage (microvolts),
- $R_{net}$  = radiometer net infrared responsivity ( $\mu\text{V}/\text{W}/\text{m}^2$ ), see Table 4,
- $W_{net}$  = effective net infrared measured by pyrgeometer ( $\text{W}/\text{m}^2$ ),
- =  $W_{in} - W_{out} = W_{in} - \sigma * T_c^4$
- where,  $W_{in}$  = incoming infrared ( $\text{W}/\text{m}^2$ ),  $\sigma = 5.6704\text{e-}8 \text{ W}\cdot\text{m}^{-2}\cdot\text{K}^{-4}$ ,
- $T_c$  = case temperature of pyrgeometer (K).
- $I$  = reference irradiance ( $\text{W}/\text{m}^2$ ), beam (B) or global (G)
- where,  $G = B * \text{COS}(Z) + D$ ,
- $Z$  = zenith angle (degrees),
- $D$  = reference diffuse irradiance ( $\text{W}/\text{m}^2$ ).

Figure 1. Responsivity vs Zenith Angle

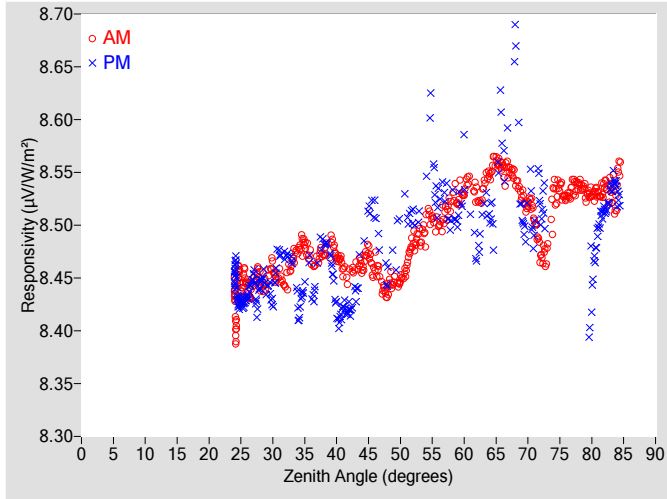


Figure 2. Responsivity vs Local Standard Time

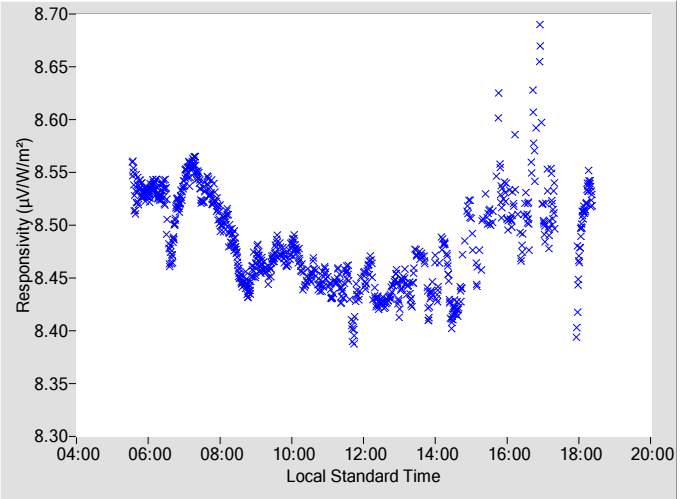


Table 2. Instrument Responsivity (R) and Calibration Type-B Standard Uncertainty, u(B)

Zenith Angle (deg.)	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle	Zenith Angle (deg.)	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle
0	N/A	N/A	N/A	N/A	N/A	N/A	46	8.4638	0.28	108.27	8.5125	0.28	251.87
2	N/A	N/A	N/A	N/A	N/A	N/A	48	8.4369	0.28	105.93	8.4527	0.29	254.07
4	N/A	N/A	N/A	N/A	N/A	N/A	50	8.4481	0.28	103.72	8.5060	0.29	256.21
6	N/A	N/A	N/A	N/A	N/A	N/A	52	8.4839	0.28	101.68	8.5077	0.29	258.42
8	N/A	N/A	N/A	N/A	N/A	N/A	54	8.4936	0.28	99.82	8.5463	0.30	260.53
10	N/A	N/A	N/A	N/A	N/A	N/A	56	8.4998	0.28	97.72	8.5208	0.30	262.27
12	N/A	N/A	N/A	N/A	N/A	N/A	58	8.5223	0.28	95.96	8.5110	0.30	264.13
14	N/A	N/A	N/A	N/A	N/A	N/A	60	8.5299	0.29	94.24	8.5598	N/A	265.96
16	N/A	N/A	N/A	N/A	N/A	N/A	62	8.5286	0.29	92.49	8.4718	0.30	267.68
18	N/A	N/A	N/A	N/A	N/A	N/A	64	8.5479	0.29	90.77	8.5097	0.30	269.42
20	N/A	N/A	N/A	N/A	N/A	N/A	66	8.5533	0.29	89.13	8.5850	N/A	271.02
22	N/A	N/A	N/A	N/A	N/A	N/A	68	8.5441	0.29	87.52	8.6715	N/A	272.66
24	8.4190	0.28	173.36	8.4543	0.28	185.64	70	8.5185	0.29	85.88	8.5209	N/A	274.17
26	8.4441	0.28	154.55	8.4330	0.28	206.04	72	8.4722	0.30	84.25	8.5129	N/A	275.93
28	8.4461	0.28	144.51	8.4450	0.28	216.05	74	8.5248	0.30	82.64	N/A	N/A	N/A
30	8.4595	0.28	137.14	8.4309	0.28	222.92	76	8.5269	0.30	81.03	N/A	N/A	N/A
32	8.4445	0.28	131.70	8.4719	0.28	228.51	78	8.5382	N/A	79.42	N/A	N/A	N/A
34	8.4776	0.28	126.84	8.4221	0.28	233.07	80	8.5297	N/A	77.77	8.4513	N/A	282.46
36	8.4698	0.28	123.06	8.4509	0.28	237.04	82	8.5373	N/A	76.16	8.5141	N/A	284.03
38	8.4730	0.28	119.34	8.4837	0.28	240.75	84	8.5408	N/A	74.45	8.5302	N/A	285.75
40	8.4704	0.28	116.29	8.4214	0.28	243.82	86	N/A	N/A	N/A	N/A	N/A	N/A
42	8.4512	0.28	113.55	8.4196	0.28	246.74	88	N/A	N/A	N/A	N/A	N/A	N/A
44	8.4601	0.28	110.71	8.4851	0.28	249.79	90	N/A	N/A	N/A	N/A	N/A	N/A

N/A - Not Available

Figure 3. Type-B Standard Uncertainty vs Zenith Angle

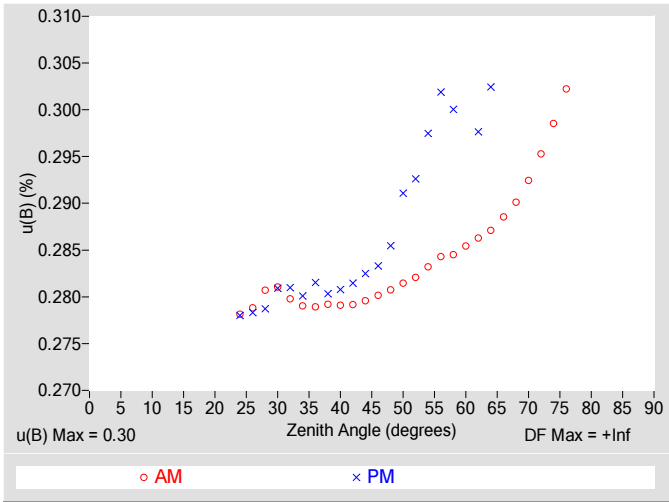


Figure 4. Residuals from Spline Interpolation

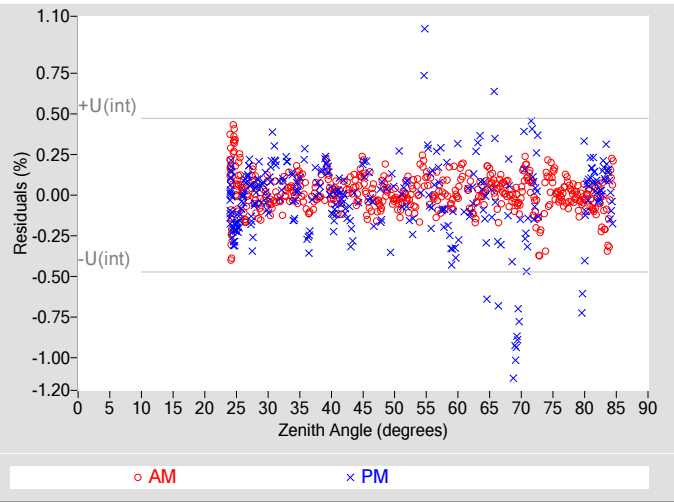


Table 3. Uncertainty using Spline Interpolation ‡

Type-B Standard Uncertainty, $u(B)$ (%)	$\pm 0.30$
Type-A Interpolating Function, $u(int)$ (%)	$\pm 0.24$
Combined Standard Uncertainty, $u(c)$ (%)	$\pm 0.38$
Effective degrees of freedom, $DF(c)$	4667
Coverage factor, $k$	1.96
Expanded Uncertainty, $U95$ (%)	$\pm 0.75$
AM Valid zenith angle range	24° to 76°
PM Valid zenith angle range	24° to 64°

‡ An illustration for how to reduce the uncertainty in calculating the irradiance using a function rather than  $R@45^\circ$ . Not accredited.

Table 4. Calibration Label Values

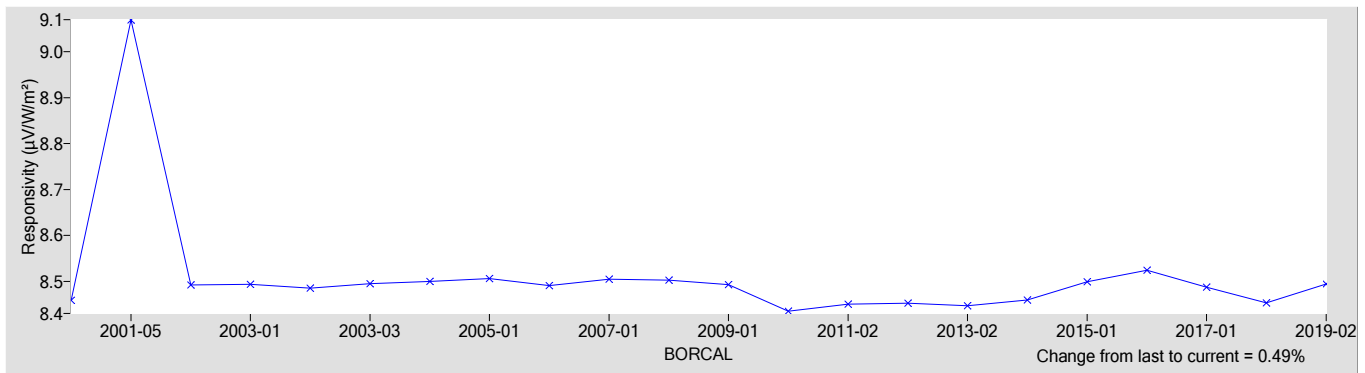
$R @ 45^\circ$ ( $\mu V/W/m^2$ )	$R_{net}$ ( $\mu V/W/m^2$ ) †
8.4944	0

†  $R_{net}$  determination date: N/A

Table 5. Uncertainty using  $R @ 45^\circ$

Type-B Expanded Uncertainty, $U(B)$ (%)	$\pm 0.59$
Offset Uncertainty, $U(off)$ (%)	+0.77 / -0.88
Expanded Uncertainty, $U$ (%)	+1.4 / -1.5
Effective degrees of freedom, $DF$	+Inf
Coverage factor, $k$	1.96
Valid zenith angle range	30.0° to 60.0°

Figure 5. History of instrument at Zenith Angle = 45°



References:

[1] Reda, I.; Hickey, J.; Long, C.; Myers, D.; Stoffel, T.; Wilcox, S.; Michalsky, J. J.; Dutton, E. G.; Nelson, D. (2005). "Using a Blackbody to Calculate Net Longwave Responsivity of Shortwave Solar Pyranometers to Correct for Their Thermal Offset Error During Outdoor Calibration Using the Component Sum Method." Journal of Atmospheric and Oceanic Technology. , 2005; pp. 1531-1540; NREL Report No. JA-560-36646. doi:10.1175/JTECH1782.1

[2] Reda, I.; Myers, D.; Stoffel, T. (2008). "Uncertainty Estimate for the Outdoor Calibration of Solar Pyranometers: A Metrologist Perspective." Measure. (NCSLI Journal of Measurement Science). Vol. 3(4), December 2008; pp. 58-66; NREL Report No. JA-581-4137

[3] Reda, I.; Andreas, A. (2004). "Solar Position Algorithm for Solar Radiation Applications." Solar Energy. Vol. 76(5), 2004; pp. 577-589; NREL Report No. JA-560-35518. doi:10.1016/j.solener.2003.12.003

[4] Stoffel, T.; Reda, I. (2009). "NREL Pyrheliometer Comparisons: 22 September - 3 October 2008 (NPC-2008)." 54 pp.; NREL Report No. TP-550-45016.

[5] Reda, I.; Stoffel, T.; Myers, D. (2003). "Method to Calibrate a Solar Pyranometer for Measuring Reference Diffuse Irradiance." Solar Energy. Vol. 74, 2003; pp. 103-112; NREL Report No. JA-560-35025. doi:10.1016/S0038-092X(03)00124-5

[6] Reda, I. (1996). Calibration of a Solar Absolute Cavity Radiometer with Traceability to the World Radiometric Reference. 79 pp.; NREL Report No. TP-463-20619.

[7] Reda, I.; Gröbner, J.; Stoffel, T.; Myers, D.; Forgan, B. (2008). Improvements in the Blackbody Calibration of Pyrgeometers. ARM 2008 Science Team Meeting (Poster).



# National Renewable Energy Laboratory

## Solar Radiation Research Laboratory

### Metrology Laboratory

### Calibration Certificate



<b>Test Instrument:</b>	Black and White Pyranometer	<b>Manufacturer:</b>	Eppley
<b>Model:</b>	8-48	<b>Serial Number:</b>	32331
<b>Calibration Date:</b>	5/3/2019	<b>Due Date:</b>	5/3/2020
<b>Customer:</b>	NREL-SRRL-BMS	<b>Environmental Conditions:</b>	see page 4
<b>Test Dates:</b>	5/3		

This certifies that the above product was calibrated in compliance with ISO/IEC 17025:2005. Measurement uncertainties at the time of calibration are consistent with the Guide to the Expression of Uncertainty in Measurement (GUM) using Reda et al., 2008. All nominal values are traceable to the International System (SI) Units of Measurement.

No statement of compliance with specifications is made or implied on this certificate. However, the estimated uncertainties are the uncertainties of the calibration process; users must add other uncertainties that are relevant to their measuring system, environmental and sky conditions, outdoor set-up, and site location.

The Type-B Standard Uncertainty of using the responsivity at each even zenith angle is reported, and the Expanded Uncertainty of the calibration is reported using two methods:

1. The Expanded Uncertainty of using the responsivity at zenith angle = 45°, within the zenith angle range from 30.0° to 60.0°
2. The Expanded Uncertainty of using Spline Interpolating Functions for the responsivity versus zenith angle.

This certificate applies only to the item identified above and shall not be reproduced other than in full, without specific written approval from the calibration facility. Certificate without signature is not valid.

**Table 1. Traceability**

Measurement Type	Instrument	Calibration Date	Calibration Due Date
Beam Irradiance †	Eppley Absolute Cavity Radiometer Model HF, S/N 29219	09/24/2018	09/24/2019
Diffuse Irradiance †	Hukseflux Pyranometer Model SR25, S/N 2541	04/19/2019	04/19/2020
Diffuse Irradiance †	Hukseflux Pyranometer Model SR25, S/N 2542	04/19/2019	04/19/2020
Data Acquisition	NREL Data Acquisition System Model RAP-DAQ, S/N 2005-998	02/14/2019	02/14/2021
Data Acquisition	NREL Data Acquisition System Model RAP-DAQ, S/N 2005-999	02/14/2019	02/14/2021

† Through the World Radiometric Reference (WRR)

**Number of pages of certificate:** 4

**Calibration Procedure:** BORCAL-P00-Calibration and QA Procedure; available upon request.

**Setup:** Radiometers are calibrated outdoors, using the sun as the source. Pyranometers and pyrgeometers are installed for horizontal measurements, with their signal connectors oriented north, if their design permits.

The shading disk for the reference diffuse subtends a solid angle of 5°. Pyrheliometers are installed on solar trackers.

**Calibrated by:** RCC

-----  
Ibrahim Reda, Technical Manager

-----  
Date

For questions or comments, please contact the technical manager at:

ibrahim.reda@nrel.gov; 303-384-6385; 15013 Denver West Parkway, Golden, CO 80401, USA

# Calibration Results

32331 Eppley 8-48

The responsivity ( $R$ ,  $\mu\text{V}/\text{W}/\text{m}^2$ ) of the test instrument during calibration is calculated using this Measurement Equation:

$$R = (V - R_{net} * W_{net}) / I \tag{1}$$

where,

- $V$  = radiometer output voltage (microvolts),
  - $R_{net}$  = radiometer net infrared responsivity ( $\mu\text{V}/\text{W}/\text{m}^2$ ), see Table 4,
  - $W_{net}$  = effective net infrared measured by pyrgeometer ( $\text{W}/\text{m}^2$ ),
  - =  $W_{in} - W_{out} = W_{in} - \sigma * T_c^4$
  - where,  $W_{in}$  = incoming infrared ( $\text{W}/\text{m}^2$ ),  $\sigma = 5.6704\text{e-}8 \text{ W}\cdot\text{m}^{-2}\cdot\text{K}^{-4}$ ,
  - $T_c$  = case temperature of pyrgeometer (K).
- $I$  = reference irradiance ( $\text{W}/\text{m}^2$ ), beam (B) or global (G)  
 where,  $G = B * \text{COS}(Z) + D$ ,  
 $Z$  = zenith angle (degrees),  
 $D$  = reference diffuse irradiance ( $\text{W}/\text{m}^2$ ).

Figure 1. Responsivity vs Zenith Angle

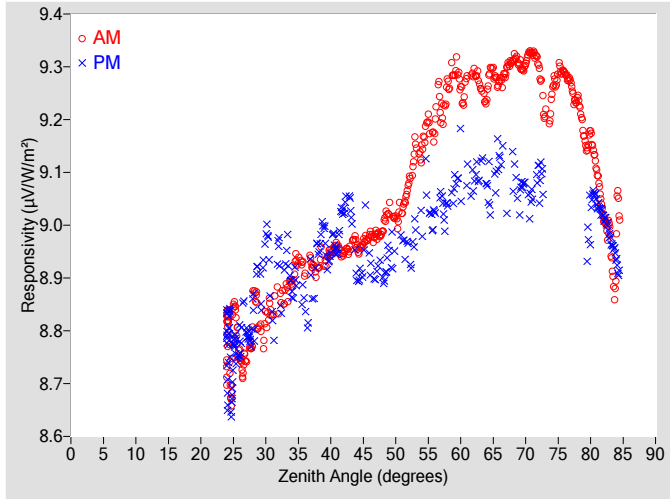


Figure 2. Responsivity vs Local Standard Time

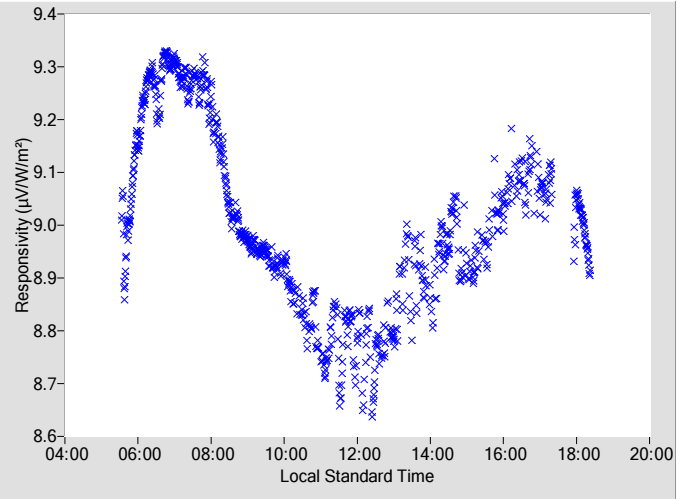


Table 2. Instrument Responsivity (R) and Calibration Type-B Standard Uncertainty, u(B)

Zenith Angle (deg.)	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle	Zenith Angle (deg.)	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle
0	N/A	N/A	N/A	N/A	N/A	N/A	46	8.9793	0.34	108.27	8.9270	0.38	251.95
2	N/A	N/A	N/A	N/A	N/A	N/A	48	8.9916	0.35	105.93	8.8950	0.39	254.36
4	N/A	N/A	N/A	N/A	N/A	N/A	50	9.0098	0.36	103.73	8.9512	0.42	256.20
6	N/A	N/A	N/A	N/A	N/A	N/A	52	9.0803	0.37	101.68	8.9532	0.44	258.42
8	N/A	N/A	N/A	N/A	N/A	N/A	54	9.1409	0.38	99.71	9.0031	0.47	260.42
10	N/A	N/A	N/A	N/A	N/A	N/A	56	9.1865	0.38	97.81	9.0175	0.50	262.22
12	N/A	N/A	N/A	N/A	N/A	N/A	58	9.2594	0.39	95.97	9.0399	0.50	264.06
14	N/A	N/A	N/A	N/A	N/A	N/A	60	9.2576	0.41	94.18	9.1140	N/A	265.95
16	N/A	N/A	N/A	N/A	N/A	N/A	62	9.2872	0.42	92.46	9.0846	0.51	267.65
18	N/A	N/A	N/A	N/A	N/A	N/A	64	9.2445	0.43	90.77	9.0688	0.55	269.42
20	N/A	N/A	N/A	N/A	N/A	N/A	66	9.2722	0.45	89.15	9.1202	N/A	271.03
22	N/A	N/A	N/A	N/A	N/A	N/A	68	9.3123	0.48	87.47	9.1064	N/A	272.78
24	8.7995	0.32	174.09	8.7644	0.32	185.36	70	9.3050	0.52	85.88	9.0807	N/A	274.12
26	8.7505	0.32	153.68	8.7737	0.32	206.06	72	9.3003	0.56	84.25	9.0867	N/A	275.93
28	8.8102	0.33	144.46	8.8179	0.33	215.87	74	9.2369	0.63	82.64	N/A	N/A	N/A
30	8.8143	0.34	137.29	8.9824	0.34	223.09	76	9.2885	0.69	81.03	N/A	N/A	N/A
32	8.8619	0.33	131.64	8.9339	0.34	228.49	78	9.2355	N/A	79.41	N/A	N/A	N/A
34	8.8916	0.33	126.95	8.8824	0.34	233.00	80	9.1710	N/A	77.81	9.0321	N/A	282.45
36	8.9064	0.33	122.96	8.8492	0.35	237.12	82	9.0151	N/A	76.15	9.0170	N/A	284.08
38	8.9162	0.33	119.43	8.9563	0.35	240.70	84	8.9883	N/A	74.45	8.9256	N/A	285.75
40	8.9491	0.33	116.29	8.9506	0.36	243.78	86	N/A	N/A	N/A	N/A	N/A	N/A
42	8.9474	0.34	113.48	9.0287	0.39	246.74	88	N/A	N/A	N/A	N/A	N/A	N/A
44	8.9625	0.34	110.71	8.8990	0.40	249.49	90	N/A	N/A	N/A	N/A	N/A	N/A

N/A - Not Available



Figure 3. Type-B Standard Uncertainty vs Zenith Angle

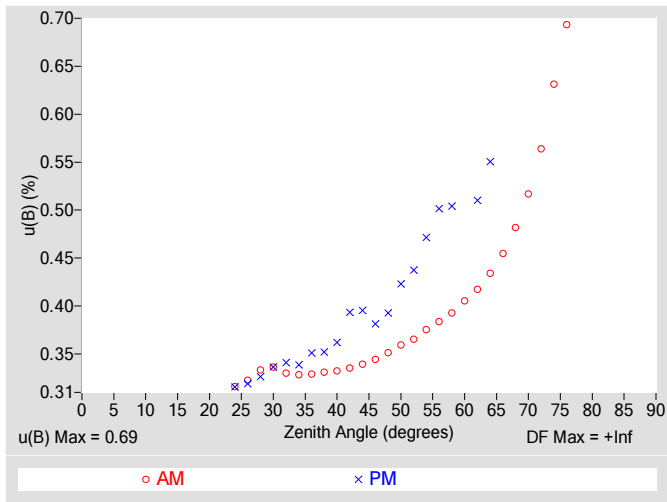


Figure 4. Residuals from Spline Interpolation

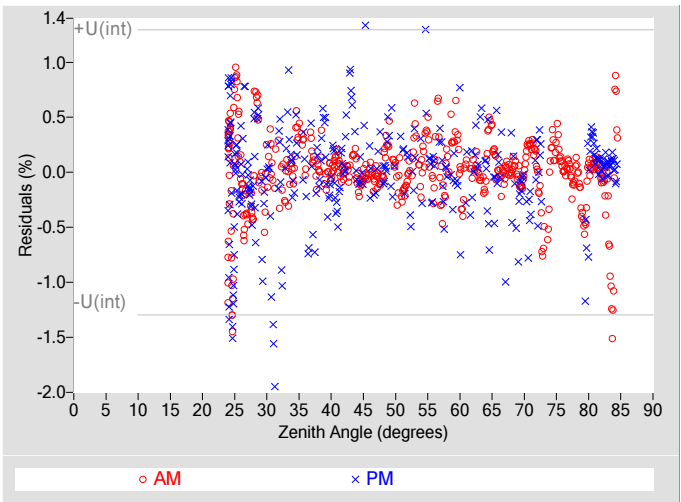


Table 3. Uncertainty using Spline Interpolation ‡

Type-B Standard Uncertainty, $u(B)$ (%)	$\pm 0.69$
Type-A Interpolating Function, $u(int)$ (%)	$\pm 0.65$
Combined Standard Uncertainty, $u(c)$ (%)	$\pm 0.95$
Effective degrees of freedom, $DF(c)$	3140
Coverage factor, $k$	1.96
Expanded Uncertainty, $U95$ (%)	$\pm 1.9$
AM Valid zenith angle range	24° to 76°
PM Valid zenith angle range	24° to 64°

‡ An illustration for how to reduce the uncertainty in calculating the irradiance using a function rather than  $R@45^\circ$ . Not accredited.

Table 4. Calibration Label Values

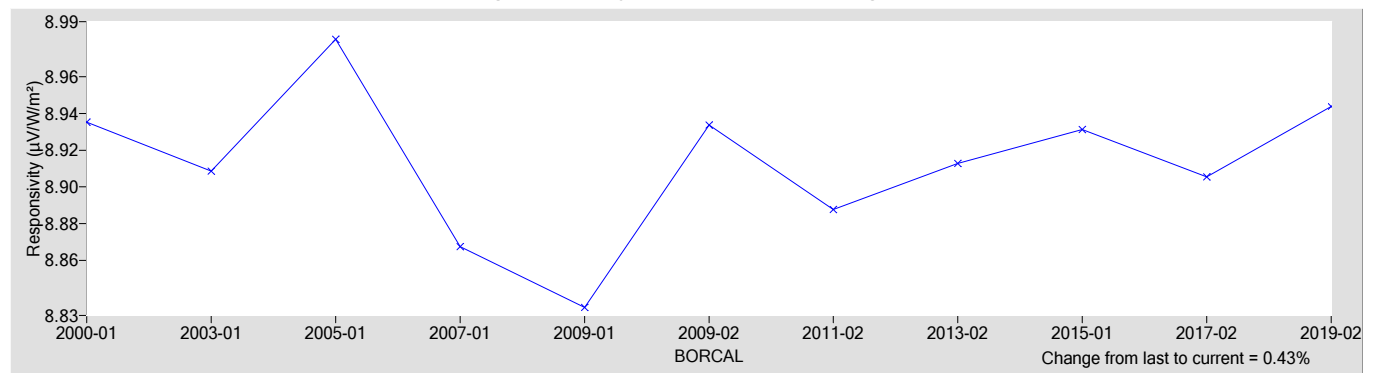
$R @ 45^\circ$ ( $\mu V/W/m^2$ )	$R_{net}$ ( $\mu V/W/m^2$ ) †
8.9438	0

†  $R_{net}$  determination date: N/A

Table 5. Uncertainty using  $R @ 45^\circ$

Type-B Expanded Uncertainty, $U(B)$ (%)	$\pm 0.99$
Offset Uncertainty, $U(off)$ (%)	+3.5 / -1.4
Expanded Uncertainty, $U$ (%)	+4.5 / -2.4
Effective degrees of freedom, $DF$	+Inf
Coverage factor, $k$	1.96
Valid zenith angle range	30.0° to 60.0°

Figure 5. History of instrument at Zenith Angle = 45°



## References:

- [1] Reda, I.; Hickey, J.; Long, C.; Myers, D.; Stoffel, T.; Wilcox, S.; Michalsky, J. J.; Dutton, E. G.; Nelson, D. (2005). "Using a Blackbody to Calculate Net Longwave Responsivity of Shortwave Solar Pyranometers to Correct for Their Thermal Offset Error During Outdoor Calibration Using the Component Sum Method." *Journal of Atmospheric and Oceanic Technology*, 2005; pp. 1531-1540; NREL Report No. JA-560-36646. doi:10.1175/JTECH1782.1
- [2] Reda, I.; Myers, D.; Stoffel, T. (2008). "Uncertainty Estimate for the Outdoor Calibration of Solar Pyranometers: A Metrologist Perspective." *Measure*. (NCSLI Journal of Measurement Science). Vol. 3(4), December 2008; pp. 58-66; NREL Report No. JA-581-4137
- [3] Reda, I.; Andreas, A. (2004). "Solar Position Algorithm for Solar Radiation Applications." *Solar Energy*. Vol. 76(5), 2004; pp. 577-589; NREL Report No. JA-560-35518. doi:10.1016/j.solener.2003.12.003
- [4] Stoffel, T.; Reda, I. (2009). "NREL Pyrheliometer Comparisons: 22 September - 3 October 2008 (NPC-2008)." 54 pp.; NREL Report No. TP-550-45016.
- [5] Reda, I.; Stoffel, T.; Myers, D. (2003). "Method to Calibrate a Solar Pyranometer for Measuring Reference Diffuse Irradiance." *Solar Energy*. Vol. 74, 2003; pp. 103-112; NREL Report No. JA-560-35025. doi:10.1016/S0038-092X(03)00124-5
- [6] Reda, I. (1996). *Calibration of a Solar Absolute Cavity Radiometer with Traceability to the World Radiometric Reference*. 79 pp.; NREL Report No. TP-463-20619.
- [7] Reda, I.; Gröbner, J.; Stoffel, T.; Myers, D.; Forgan, B. (2008). Improvements in the Blackbody Calibration of Pyrgeometers. ARM 2008 Science Team Meeting (Poster).



# National Renewable Energy Laboratory

## Solar Radiation Research Laboratory

### Metrology Laboratory

### Calibration Certificate



<b>Test Instrument:</b>	Black and White Pyranometer	<b>Manufacturer:</b>	Eppley
<b>Model:</b>	8-48	<b>Serial Number:</b>	34718
<b>Calibration Date:</b>	5/3/2019	<b>Due Date:</b>	5/3/2020
<b>Customer:</b>	NREL-SRRL-BMS	<b>Environmental Conditions:</b>	see page 4
<b>Test Dates:</b>	5/3		

This certifies that the above product was calibrated in compliance with ISO/IEC 17025:2005. Measurement uncertainties at the time of calibration are consistent with the Guide to the Expression of Uncertainty in Measurement (GUM) using Reda et al., 2008. All nominal values are traceable to the International System (SI) Units of Measurement.

No statement of compliance with specifications is made or implied on this certificate. However, the estimated uncertainties are the uncertainties of the calibration process; users must add other uncertainties that are relevant to their measuring system, environmental and sky conditions, outdoor set-up, and site location.

The Type-B Standard Uncertainty of using the responsivity at each even zenith angle is reported, and the Expanded Uncertainty of the calibration is reported using two methods:

1. The Expanded Uncertainty of using the responsivity at zenith angle = 45°, within the zenith angle range from 30.0° to 60.0°
2. The Expanded Uncertainty of using Spline Interpolating Functions for the responsivity versus zenith angle.

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**Table 1. Traceability**

Measurement Type	Instrument	Calibration Date	Calibration Due Date
Beam Irradiance †	Eppley Absolute Cavity Radiometer Model HF, S/N 29219	09/24/2018	09/24/2019
Diffuse Irradiance †	Hukseflux Pyranometer Model SR25, S/N 2541	04/19/2019	04/19/2020
Diffuse Irradiance †	Hukseflux Pyranometer Model SR25, S/N 2542	04/19/2019	04/19/2020
Data Acquisition	NREL Data Acquisition System Model RAP-DAQ, S/N 2005-998	02/14/2019	02/14/2021
Data Acquisition	NREL Data Acquisition System Model RAP-DAQ, S/N 2005-999	02/14/2019	02/14/2021

† Through the World Radiometric Reference (WRR)

**Number of pages of certificate:** 4

**Calibration Procedure:** BORCAL-P00-Calibration and QA Procedure; available upon request.

**Setup:** Radiometers are calibrated outdoors, using the sun as the source. Pyranometers and pyrgeometers are installed for horizontal measurements, with their signal connectors oriented north, if their design permits.

The shading disk for the reference diffuse subtends a solid angle of 5°. Pyrheliometers are installed on solar trackers.

**Calibrated by:** RCC

-----  
Ibrahim Reda, Technical Manager

-----  
Date

For questions or comments, please contact the technical manager at:

ibrahim.reda@nrel.gov; 303-384-6385; 15013 Denver West Parkway, Golden, CO 80401, USA

# Calibration Results

## 34718 Eppley 8-48

The responsivity ( $R$ ,  $\mu\text{V}/\text{W}/\text{m}^2$ ) of the test instrument during calibration is calculated using this Measurement Equation:

$$R = (V - R_{net} * W_{net}) / I \tag{1}$$

where,

- $V$  = radiometer output voltage (microvolts),
  - $R_{net}$  = radiometer net infrared responsivity ( $\mu\text{V}/\text{W}/\text{m}^2$ ), see Table 4,
  - $W_{net}$  = effective net infrared measured by pyrgeometer ( $\text{W}/\text{m}^2$ ),
  - =  $W_{in} - W_{out} = W_{in} - \sigma * T_c^4$
  - where,  $W_{in}$  = incoming infrared ( $\text{W}/\text{m}^2$ ),  $\sigma = 5.6704\text{e-}8 \text{ W}\cdot\text{m}^{-2}\cdot\text{K}^{-4}$ ,
  - $T_c$  = case temperature of pyrgeometer (K).
- $I$  = reference irradiance ( $\text{W}/\text{m}^2$ ), beam (B) or global (G)
  - where,  $G = B * \text{COS}(Z) + D$ ,
  - $Z$  = zenith angle (degrees),
  - $D$  = reference diffuse irradiance ( $\text{W}/\text{m}^2$ ).

Figure 1. Responsivity vs Zenith Angle

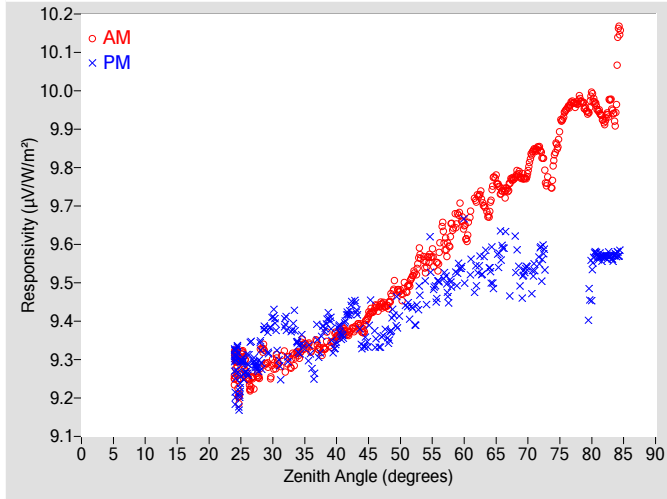


Figure 2. Responsivity vs Local Standard Time

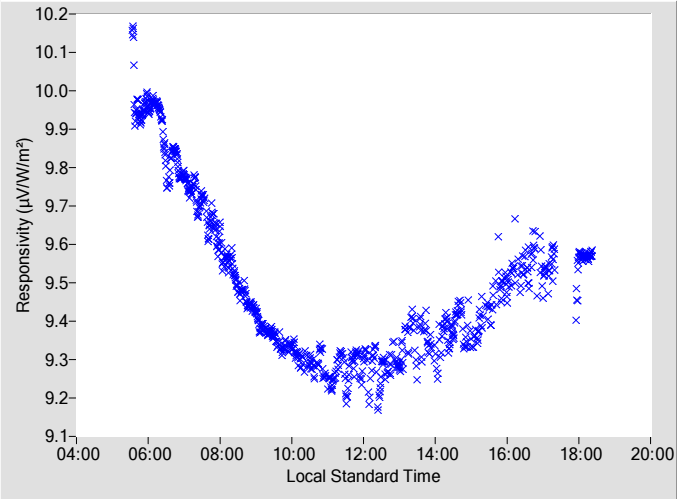
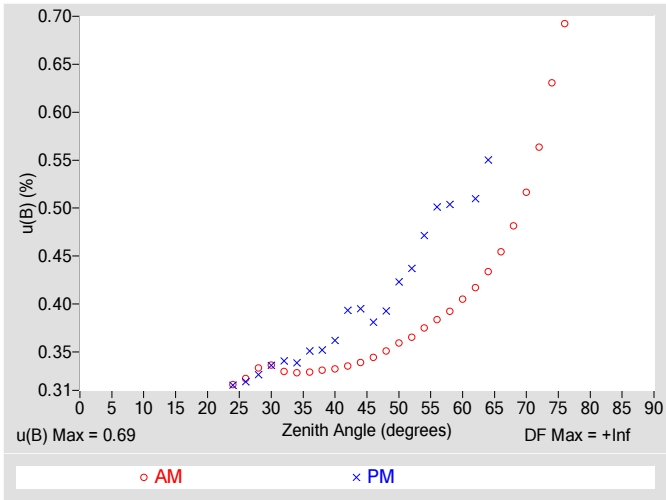


Table 2. Instrument Responsivity (R) and Calibration Type-B Standard Uncertainty, u(B)

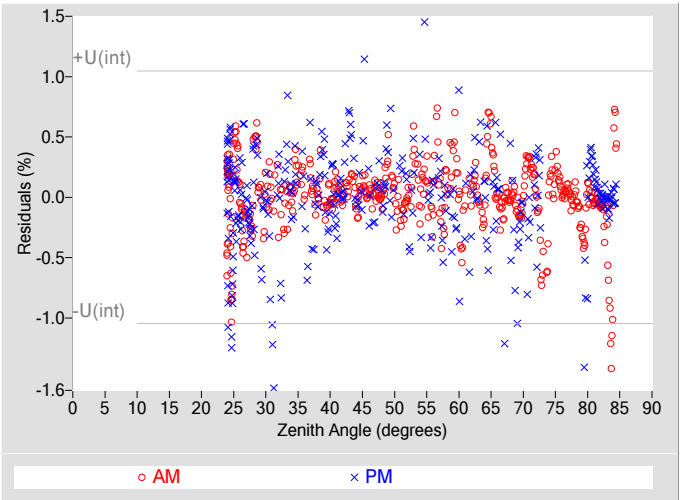
Zenith Angle (deg.)	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle	Zenith Angle (deg.)	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle
0	N/A	N/A	N/A	N/A	N/A	N/A	46	9.4326	0.34	108.27	9.3536	0.38	251.95
2	N/A	N/A	N/A	N/A	N/A	N/A	48	9.4403	0.35	105.93	9.3499	0.39	254.36
4	N/A	N/A	N/A	N/A	N/A	N/A	50	9.4718	0.36	103.73	9.4132	0.42	256.20
6	N/A	N/A	N/A	N/A	N/A	N/A	52	9.5215	0.37	101.68	9.4209	0.44	258.42
8	N/A	N/A	N/A	N/A	N/A	N/A	54	9.5476	0.38	99.71	9.4743	0.47	260.42
10	N/A	N/A	N/A	N/A	N/A	N/A	56	9.5633	0.38	97.81	9.4931	0.50	262.22
12	N/A	N/A	N/A	N/A	N/A	N/A	58	9.6337	0.39	95.97	9.4995	0.50	264.06
14	N/A	N/A	N/A	N/A	N/A	N/A	60	9.6424	0.41	94.18	9.5827	N/A	265.95
16	N/A	N/A	N/A	N/A	N/A	N/A	62	9.7195	0.42	92.46	9.5211	0.51	267.65
18	N/A	N/A	N/A	N/A	N/A	N/A	64	9.6916	0.43	90.77	9.5267	0.55	269.42
20	N/A	N/A	N/A	N/A	N/A	N/A	66	9.7391	0.45	89.15	9.5845	N/A	271.03
22	N/A	N/A	N/A	N/A	N/A	N/A	68	9.7769	0.48	87.47	9.5780	N/A	272.78
24	9.2933	0.32	174.09	9.2825	0.32	185.36	70	9.7900	0.52	85.88	9.5424	N/A	274.12
26	9.2542	0.32	153.68	9.2828	0.32	206.06	72	9.8416	0.56	84.25	9.5599	N/A	275.93
28	9.2823	0.33	144.46	9.3076	0.33	215.87	74	9.8012	0.63	82.64	N/A	N/A	N/A
30	9.2814	0.34	137.29	9.4147	0.34	223.09	76	9.9510	0.69	81.03	N/A	N/A	N/A
32	9.2989	0.33	131.64	9.3798	0.34	228.49	78	9.9743	N/A	79.41	N/A	N/A	N/A
34	9.3136	0.33	126.95	9.3344	0.34	233.00	80	9.9841	N/A	77.81	9.5328	N/A	282.45
36	9.3208	0.33	122.96	9.2959	0.35	237.12	82	9.9204	N/A	76.15	9.5691	N/A	284.08
38	9.3249	0.33	119.43	9.3823	0.35	240.70	84	10.074	N/A	74.45	9.5739	N/A	285.75
40	9.3643	0.33	116.29	9.3492	0.36	243.78	86	N/A	N/A	N/A	N/A	N/A	N/A
42	9.3692	0.34	113.48	9.4239	0.39	246.74	88	N/A	N/A	N/A	N/A	N/A	N/A
44	9.3784	0.34	110.71	9.3348	0.40	249.49	90	N/A	N/A	N/A	N/A	N/A	N/A

N/A - Not Available

**Figure 3. Type-B Standard Uncertainty vs Zenith Angle**



**Figure 4. Residuals from Spline Interpolation**



**Table 3. Uncertainty using Spline Interpolation ‡**

Type-B Standard Uncertainty, $u(B)$ (%)	$\pm 0.69$
Type-A Interpolating Function, $u(int)$ (%)	$\pm 0.52$
Combined Standard Uncertainty, $u(c)$ (%)	$\pm 0.87$
Effective degrees of freedom, $DF(c)$	5166
Coverage factor, $k$	1.96
Expanded Uncertainty, $U95$ (%)	$\pm 1.7$
AM Valid zenith angle range	24° to 76°
PM Valid zenith angle range	24° to 64°

‡ An illustration for how to reduce the uncertainty in calculating the irradiance using a function rather than  $R@45^\circ$ . Not accredited.

**Table 4. Calibration Label Values**

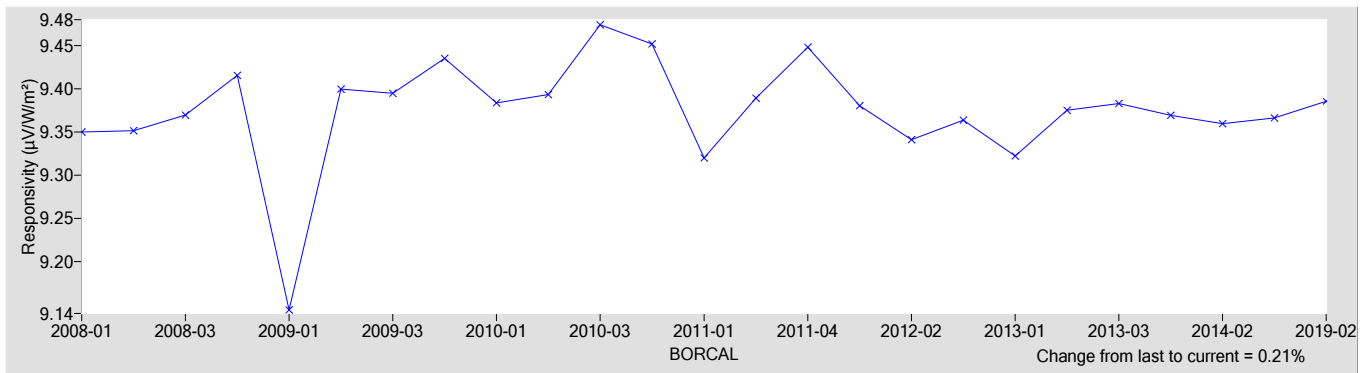
$R @ 45^\circ$ ( $\mu V/W/m^2$ )	$R_{net}$ ( $\mu V/W/m^2$ ) †
9.3855	0

†  $R_{net}$  determination date: N/A

**Table 5. Uncertainty using  $R @ 45^\circ$**

Type-B Expanded Uncertainty, $U(B)$ (%)	$\pm 0.99$
Offset Uncertainty, $U(off)$ (%)	+2.7 / -1.1
Expanded Uncertainty, $U$ (%)	+3.7 / -2.1
Effective degrees of freedom, $DF$	+Inf
Coverage factor, $k$	1.96
Valid zenith angle range	30.0° to 60.0°

**Figure 5. History of instrument at Zenith Angle = 45°**



**References:**

[1] Reda, I.; Hickey, J.; Long, C.; Myers, D.; Stoffel, T.; Wilcox, S.; Michalsky, J. J.; Dutton, E. G.; Nelson, D. (2005). "Using a Blackbody to Calculate Net Longwave Responsivity of Shortwave Solar Pyranometers to Correct for Their Thermal Offset Error During Outdoor Calibration Using the Component Sum Method." Journal of Atmospheric and Oceanic Technology. , 2005; pp. 1531-1540; NREL Report No. JA-560-36646. doi:10.1175/JTECH1782.1

[2] Reda, I.; Myers, D.; Stoffel, T. (2008). "Uncertainty Estimate for the Outdoor Calibration of Solar Pyranometers: A Metrologist Perspective." Measure. (NCSLI Journal of Measurement Science). Vol. 3(4), December 2008; pp. 58-66; NREL Report No. JA-581-4137

[3] Reda, I.; Andreas, A. (2004). "Solar Position Algorithm for Solar Radiation Applications." Solar Energy. Vol. 76(5), 2004; pp. 577-589; NREL Report No. JA-560-35518. doi:10.1016/j.solener.2003.12.003

[4] Stoffel, T.; Reda, I. (2009). "NREL Pyrheliometer Comparisons: 22 September - 3 October 2008 (NPC-2008)." 54 pp.; NREL Report No. TP-550-45016.

[5] Reda, I.; Stoffel, T.; Myers, D. (2003). "Method to Calibrate a Solar Pyranometer for Measuring Reference Diffuse Irradiance." Solar Energy. Vol. 74, 2003; pp. 103-112; NREL Report No. JA-560-35025. doi:10.1016/S0038-092X(03)00124-5

[6] Reda, I. (1996). Calibration of a Solar Absolute Cavity Radiometer with Traceability to the World Radiometric Reference. 79 pp.; NREL Report No. TP-463-20619.

[7] Reda, I.; Gröbner, J.; Stoffel, T.; Myers, D.; Forgan, B. (2008). Improvements in the Blackbody Calibration of Pyrgometers. ARM 2008 Science Team Meeting (Poster).



# National Renewable Energy Laboratory

## Solar Radiation Research Laboratory

### Metrology Laboratory

### Calibration Certificate



<b>Test Instrument:</b>	GPP Pyranometer	<b>Manufacturer:</b>	Eppley
<b>Model:</b>	GPP	<b>Serial Number:</b>	37831F3
<b>Calibration Date:</b>	5/3/2019	<b>Due Date:</b>	5/3/2020
<b>Customer:</b>	NREL-SRRL-BMS	<b>Environmental Conditions:</b>	see page 4
<b>Test Dates:</b>	5/3		

This certifies that the above product was calibrated in compliance with ISO/IEC 17025:2005. Measurement uncertainties at the time of calibration are consistent with the Guide to the Expression of Uncertainty in Measurement (GUM) using Reda et al., 2008. All nominal values are traceable to the International System (SI) Units of Measurement.

No statement of compliance with specifications is made or implied on this certificate. However, the estimated uncertainties are the uncertainties of the calibration process; users must add other uncertainties that are relevant to their measuring system, environmental and sky conditions, outdoor set-up, and site location.

The Type-B Standard Uncertainty of using the responsivity at each even zenith angle is reported, and the Expanded Uncertainty of the calibration is reported using two methods:

1. The Expanded Uncertainty of using the responsivity at zenith angle = 45°, within the zenith angle range from 30.0° to 60.0°
2. The Expanded Uncertainty of using Spline Interpolating Functions for the responsivity versus zenith angle.

This certificate applies only to the item identified above and shall not be reproduced other than in full, without specific written approval from the calibration facility. Certificate without signature is not valid.

**Table 1. Traceability**

Measurement Type	Instrument	Calibration Date	Calibration Due Date
Beam Irradiance †	Eppley Absolute Cavity Radiometer Model HF, S/N 29219	09/24/2018	09/24/2019
Diffuse Irradiance †	Hukseflux Pyranometer Model SR25, S/N 2541	04/19/2019	04/19/2020
Diffuse Irradiance †	Hukseflux Pyranometer Model SR25, S/N 2542	04/19/2019	04/19/2020
Data Acquisition	NREL Data Acquisition System Model RAP-DAQ, S/N 2005-998	02/14/2019	02/14/2021
Data Acquisition	NREL Data Acquisition System Model RAP-DAQ, S/N 2005-999	02/14/2019	02/14/2021
Infrared Irradiance ‡	Kipp & Zonen Pyrgeometer Model CG4, S/N FT002	04/16/2018	04/16/2022

† Through the World Radiometric Reference (WRR)

‡ Through the World Infrared Standard Group (WISG)

**Number of pages of certificate:** 4

**Calibration Procedure:** BORCAL-P00-Calibration and QA Procedure; available upon request.

**Setup:** Radiometers are calibrated outdoors, using the sun as the source. Pyranometers and pyrgeometers are installed for horizontal measurements, with their signal connectors oriented north, if their design permits.

The shading disk for the reference diffuse subtends a solid angle of 5°. Pyrheliometers are installed on solar trackers.

**Calibrated by:** RCC

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Ibrahim Reda, Technical Manager

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Date

For questions or comments, please contact the technical manager at:

ibrahim.reda@nrel.gov; 303-384-6385; 15013 Denver West Parkway, Golden, CO 80401, USA

# Calibration Results

## 37831F3 Eppley GPP

The responsivity ( $R$ ,  $\mu\text{V}/\text{W}/\text{m}^2$ ) of the test instrument during calibration is calculated using this Measurement Equation:

$$R = (V - R_{net} * W_{net}) / I \tag{1}$$

where,

- $V$  = radiometer output voltage (microvolts),
  - $R_{net}$  = radiometer net infrared responsivity ( $\mu\text{V}/\text{W}/\text{m}^2$ ), see Table 4,
  - $W_{net}$  = effective net infrared measured by pyrgeometer ( $\text{W}/\text{m}^2$ ),
  - =  $W_{in} - W_{out} = W_{in} - \sigma * T_c^4$
  - where,  $W_{in}$  = incoming infrared ( $\text{W}/\text{m}^2$ ),  $\sigma = 5.6704\text{e-}8 \text{ W}\cdot\text{m}^{-2}\cdot\text{K}^{-4}$ ,
  - $T_c$  = case temperature of pyrgeometer (K).
- $I$  = reference irradiance ( $\text{W}/\text{m}^2$ ), beam (B) or global (G)
  - where,  $G = B * \text{COS}(Z) + D$ ,
  - $Z$  = zenith angle (degrees),
  - $D$  = reference diffuse irradiance ( $\text{W}/\text{m}^2$ ).

Figure 1. Responsivity vs Zenith Angle

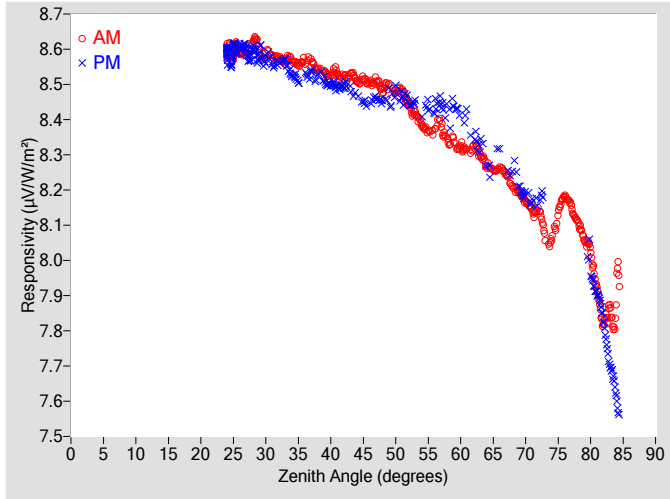


Figure 2. Responsivity vs Local Standard Time

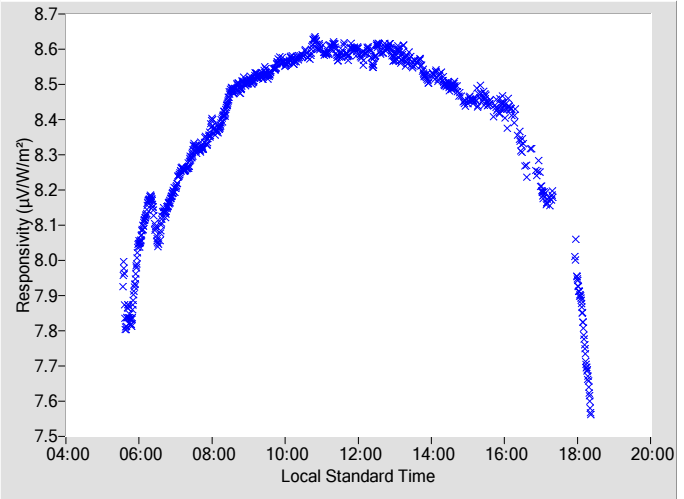


Table 2. Instrument Responsivity (R) and Calibration Type-B Standard Uncertainty, u(B)

Zenith Angle (deg.)	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	AM u(B) $\pm$ (%)	Azimuth Angle	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	PM u(B) $\pm$ (%)	Azimuth Angle	Zenith Angle (deg.)	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	AM u(B) $\pm$ (%)	Azimuth Angle	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	PM u(B) $\pm$ (%)	Azimuth Angle
0	N/A	N/A	N/A	N/A	N/A	N/A	46	8.5061	0.35	108.20	8.4457	0.38	252.15
2	N/A	N/A	N/A	N/A	N/A	N/A	48	8.4841	0.35	105.94	8.4501	0.39	254.02
4	N/A	N/A	N/A	N/A	N/A	N/A	50	8.4827	0.36	103.79	8.4783	0.44	256.35
6	N/A	N/A	N/A	N/A	N/A	N/A	52	8.4431	0.37	101.68	8.4526	0.44	258.34
8	N/A	N/A	N/A	N/A	N/A	N/A	54	8.3868	0.38	99.72	8.4080	0.48	260.49
10	N/A	N/A	N/A	N/A	N/A	N/A	56	8.3682	0.39	97.84	8.4314	0.51	262.38
12	N/A	N/A	N/A	N/A	N/A	N/A	58	8.3364	0.40	95.88	8.4367	0.52	264.22
14	N/A	N/A	N/A	N/A	N/A	N/A	60	8.3223	0.41	94.19	8.4117	N/A	265.77
16	N/A	N/A	N/A	N/A	N/A	N/A	62	8.3202	0.42	92.58	8.3440	0.51	267.86
18	N/A	N/A	N/A	N/A	N/A	N/A	64	8.2705	0.44	90.78	8.2684	0.55	269.25
20	N/A	N/A	N/A	N/A	N/A	N/A	66	8.2619	0.46	89.16	8.3176	N/A	271.01
22	N/A	N/A	N/A	N/A	N/A	N/A	68	8.2089	0.49	87.48	8.2683	N/A	272.76
24	8.5926	0.32	174.08	8.5894	0.32	185.42	70	8.1672	0.52	85.84	8.1895	N/A	274.17
26	8.5980	0.32	154.09	8.6010	0.32	205.50	72	8.1420	0.57	84.24	8.1637	N/A	275.94
28	8.6152	0.33	144.18	8.6004	0.33	216.34	74	8.0593	0.64	82.69	N/A	N/A	N/A
30	8.5849	0.34	137.49	8.5709	0.34	222.41	76	8.1791	0.70	81.03	N/A	N/A	N/A
32	8.5762	0.33	131.85	8.5610	0.34	228.26	78	8.1100	N/A	79.42	N/A	N/A	N/A
34	8.5693	0.33	127.01	8.5264	0.34	233.02	80	8.0249	N/A	77.81	7.9834	N/A	282.39
36	8.5642	0.33	123.02	8.5322	0.35	237.49	82	7.8252	N/A	76.16	7.8242	N/A	284.04
38	8.5437	0.33	119.57	8.5279	0.35	240.71	84	7.9084	N/A	74.50	7.6043	N/A	285.71
40	8.5223	0.33	116.30	8.4991	0.36	243.81	86	N/A	N/A	N/A	N/A	N/A	N/A
42	8.5266	0.34	113.28	8.4968	0.40	246.88	88	N/A	N/A	N/A	N/A	N/A	N/A
44	8.5099	0.34	110.72	8.4714	0.40	249.40	90	N/A	N/A	N/A	N/A	N/A	N/A

N/A - Not Available

Figure 3. Type-B Standard Uncertainty vs Zenith Angle

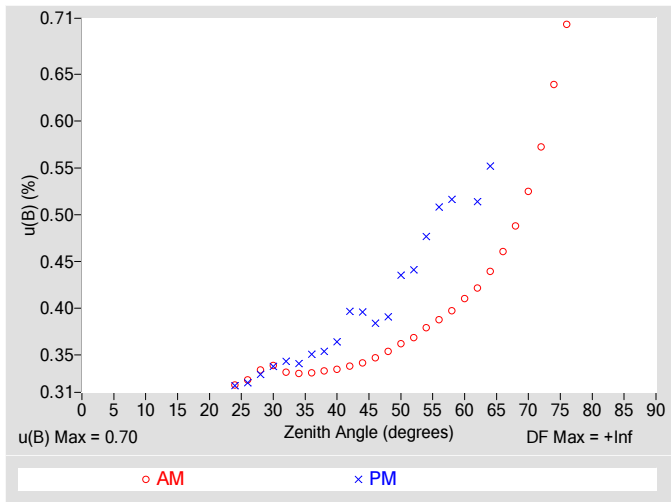


Figure 4. Residuals from Spline Interpolation

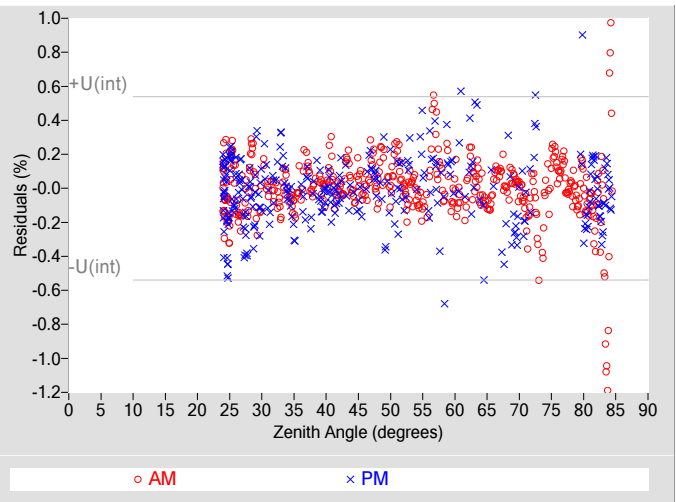


Table 3. Uncertainty using Spline Interpolation ‡

Type-B Standard Uncertainty, $u(B)$ (%)	$\pm 0.70$
Type-A Interpolating Function, $u(int)$ (%)	$\pm 0.27$
Combined Standard Uncertainty, $u(c)$ (%)	$\pm 0.75$
Effective degrees of freedom, $DF(c)$	40251
Coverage factor, $k$	1.96
Expanded Uncertainty, $U95$ (%)	$\pm 1.5$
AM Valid zenith angle range	24° to 76°
PM Valid zenith angle range	24° to 64°

‡ An illustration for how to reduce the uncertainty in calculating the irradiance using a function rather than  $R@45^\circ$ . Not accredited.

Table 4. Calibration Label Values

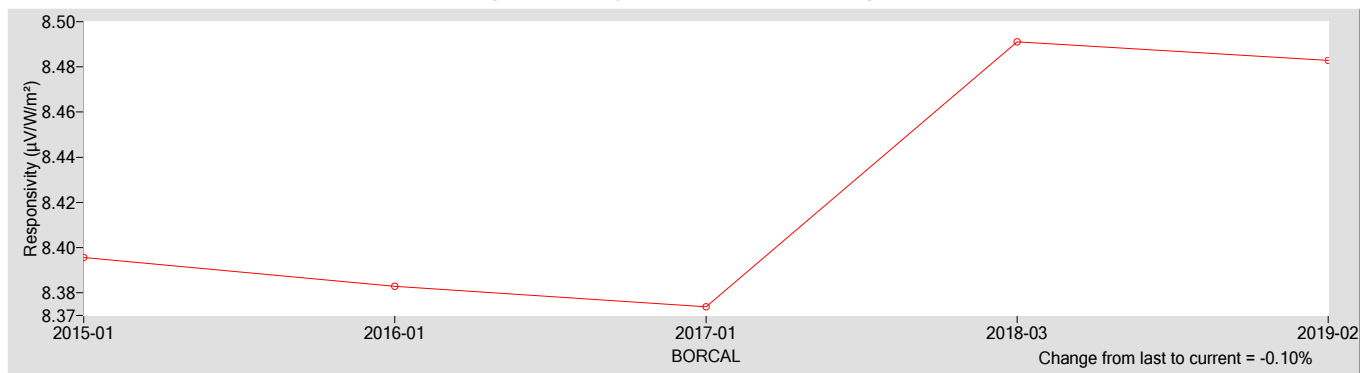
$R @ 45^\circ$ ( $\mu V/W/m^2$ )	$R_{net}$ ( $\mu V/W/m^2$ ) †
8.4828	0.15000

†  $R_{net}$  determination date: Estimated

Table 5. Uncertainty using  $R @ 45^\circ$

Type-B Expanded Uncertainty, $U(B)$ (%)	$\pm 1.0$
Offset Uncertainty, $U(off)$ (%)	+1.2 / -1.9
Expanded Uncertainty, $U$ (%)	+2.2 / -2.9
Effective degrees of freedom, $DF$	+Inf
Coverage factor, $k$	1.96
Valid zenith angle range	30.0° to 60.0°

Figure 5. History of instrument at Zenith Angle = 45°



## References:

- [1] Reda, I.; Hickey, J.; Long, C.; Myers, D.; Stoffel, T.; Wilcox, S.; Michalsky, J. J.; Dutton, E. G.; Nelson, D. (2005). "Using a Blackbody to Calculate Net Longwave Responsivity of Shortwave Solar Pyranometers to Correct for Their Thermal Offset Error During Outdoor Calibration Using the Component Sum Method." *Journal of Atmospheric and Oceanic Technology*, 2005; pp. 1531-1540; NREL Report No. JA-560-36646. doi:10.1175/JTECH1782.1
- [2] Reda, I.; Myers, D.; Stoffel, T. (2008). "Uncertainty Estimate for the Outdoor Calibration of Solar Pyranometers: A Metrologist Perspective." *Measure*. (NCSLI Journal of Measurement Science). Vol. 3(4), December 2008; pp. 58-66; NREL Report No. JA-581-4137
- [3] Reda, I.; Andreas, A. (2004). "Solar Position Algorithm for Solar Radiation Applications." *Solar Energy*. Vol. 76(5), 2004; pp. 577-589; NREL Report No. JA-560-35518. doi:10.1016/j.solener.2003.12.003
- [4] Stoffel, T.; Reda, I. (2009). "NREL Pyrheliometer Comparisons: 22 September - 3 October 2008 (NPC-2008)." 54 pp.; NREL Report No. TP-550-45016.
- [5] Reda, I.; Stoffel, T.; Myers, D. (2003). "Method to Calibrate a Solar Pyranometer for Measuring Reference Diffuse Irradiance." *Solar Energy*. Vol. 74, 2003; pp. 103-112; NREL Report No. JA-560-35025. doi:10.1016/S0038-092X(03)00124-5
- [6] Reda, I. (1996). *Calibration of a Solar Absolute Cavity Radiometer with Traceability to the World Radiometric Reference*. 79 pp.; NREL Report No. TP-463-20619.
- [7] Reda, I.; Gröbner, J.; Stoffel, T.; Myers, D.; Forgan, B. (2008). Improvements in the Blackbody Calibration of Pyrheliometers. ARM 2008 Science Team Meeting (Poster).





# National Renewable Energy Laboratory

## Solar Radiation Research Laboratory

### Metrology Laboratory

### Calibration Certificate



<b>Test Instrument:</b>	Standard Precision Pyranometer (Ventilated)	<b>Manufacturer:</b>	Eppley
<b>Model:</b>	SPP	<b>Serial Number:</b>	37839F3
<b>Calibration Date:</b>	5/3/2019	<b>Due Date:</b>	5/3/2020
<b>Customer:</b>	NREL-SRRL-BMS	<b>Environmental Conditions:</b>	see page 4
<b>Test Dates:</b>	5/3		

This certifies that the above product was calibrated in compliance with ISO/IEC 17025:2005. Measurement uncertainties at the time of calibration are consistent with the Guide to the Expression of Uncertainty in Measurement (GUM) using Reda et al., 2008. All nominal values are traceable to the International System (SI) Units of Measurement.

No statement of compliance with specifications is made or implied on this certificate. However, the estimated uncertainties are the uncertainties of the calibration process; users must add other uncertainties that are relevant to their measuring system, environmental and sky conditions, outdoor set-up, and site location.

The Type-B Standard Uncertainty of using the responsivity at each even zenith angle is reported, and the Expanded Uncertainty of the calibration is reported using two methods:

1. The Expanded Uncertainty of using the responsivity at zenith angle = 45°, within the zenith angle range from 30.0° to 60.0°
2. The Expanded Uncertainty of using Spline Interpolating Functions for the responsivity versus zenith angle.

This certificate applies only to the item identified above and shall not be reproduced other than in full, without specific written approval from the calibration facility. Certificate without signature is not valid.

**Table 1. Traceability**

Measurement Type	Instrument	Calibration Date	Calibration Due Date
Beam Irradiance †	Eppley Absolute Cavity Radiometer Model HF, S/N 29219	09/24/2018	09/24/2019
Diffuse Irradiance †	Hukseflux Pyranometer Model SR25, S/N 2541	04/19/2019	04/19/2020
Diffuse Irradiance †	Hukseflux Pyranometer Model SR25, S/N 2542	04/19/2019	04/19/2020
Data Acquisition	NREL Data Acquisition System Model RAP-DAQ, S/N 2005-998	02/14/2019	02/14/2021
Data Acquisition	NREL Data Acquisition System Model RAP-DAQ, S/N 2005-999	02/14/2019	02/14/2021
Infrared Irradiance ‡	Eppley Downwelling Pyrgeometer (Ventilated) Model PIR-V, S/N 37757F3	04/02/2019	04/02/2023

† Through the World Radiometric Reference (WRR)

‡ Through the World Infrared Standard Group (WISG)

**Number of pages of certificate:** 4

**Calibration Procedure:** BORCAL-P00-Calibration and QA Procedure; available upon request.

**Setup:** Radiometers are calibrated outdoors, using the sun as the source. Pyranometers and pyrgeometers are installed for horizontal measurements, with their signal connectors oriented north, if their design permits.

The shading disk for the reference diffuse subtends a solid angle of 5°. Pyrheliometers are installed on solar trackers.

**Calibrated by:** RCC

-----  
Ibrahim Reda, Technical Manager

-----  
Date

For questions or comments, please contact the technical manager at:

ibrahim.reda@nrel.gov; 303-384-6385; 15013 Denver West Parkway, Golden, CO 80401, USA



# Calibration Results

## 37839F3 Eppley SPP

The responsivity ( $R$ ,  $\mu\text{V}/\text{W}/\text{m}^2$ ) of the test instrument during calibration is calculated using this Measurement Equation:

$$R = (V - R_{net} * W_{net}) / I \tag{1}$$

where,

- $V$  = radiometer output voltage (microvolts),
  - $R_{net}$  = radiometer net infrared responsivity ( $\mu\text{V}/\text{W}/\text{m}^2$ ), see Table 4,
  - $W_{net}$  = effective net infrared measured by pyrgeometer ( $\text{W}/\text{m}^2$ ),
  - =  $W_{in} - W_{out} = W_{in} - \sigma * T_c^4$
  - where,  $W_{in}$  = incoming infrared ( $\text{W}/\text{m}^2$ ),  $\sigma = 5.6704\text{e-}8 \text{ W}\cdot\text{m}^{-2}\cdot\text{K}^{-4}$ ,
  - $T_c$  = case temperature of pyrgeometer (K).
- $I$  = reference irradiance ( $\text{W}/\text{m}^2$ ), beam (B) or global (G)
  - where,  $G = B * \text{COS}(Z) + D$ ,
  - $Z$  = zenith angle (degrees),
  - $D$  = reference diffuse irradiance ( $\text{W}/\text{m}^2$ ).

Figure 1. Responsivity vs Zenith Angle

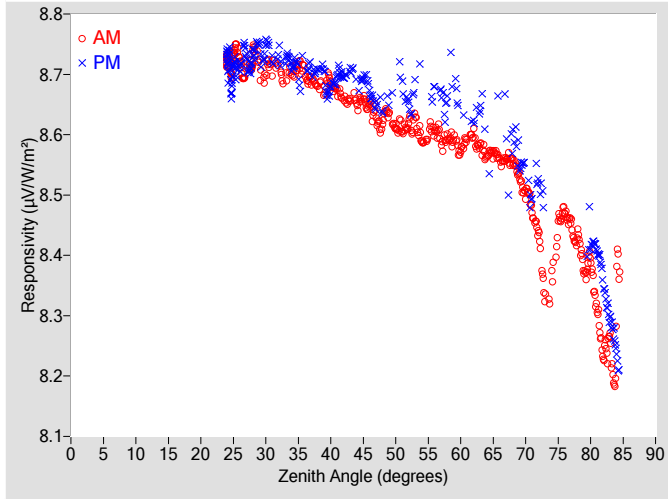


Figure 2. Responsivity vs Local Standard Time

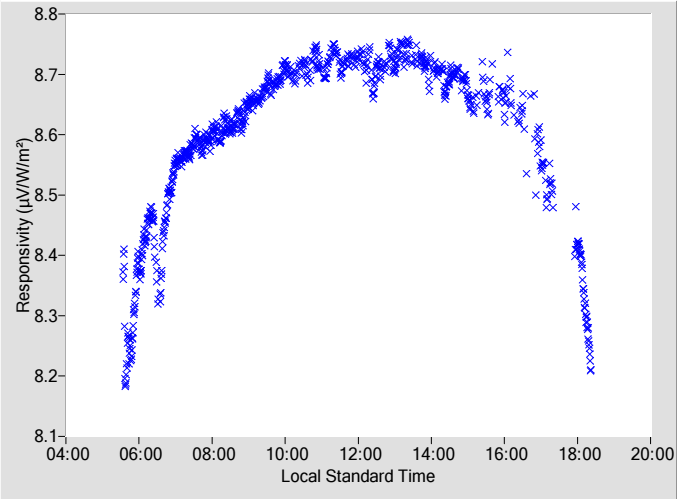


Table 2. Instrument Responsivity (R) and Calibration Type-B Standard Uncertainty, u(B)

Zenith Angle (deg.)	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle	Zenith Angle (deg.)	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle
0	N/A	N/A	N/A	N/A	N/A	N/A	46	8.6512	0.35	108.27	8.6686	0.39	251.97
2	N/A	N/A	N/A	N/A	N/A	N/A	48	8.6247	0.36	105.85	8.6372	0.40	254.11
4	N/A	N/A	N/A	N/A	N/A	N/A	50	8.6128	0.37	103.76	N/A	N/A	N/A
6	N/A	N/A	N/A	N/A	N/A	N/A	52	8.6189	0.38	101.71	8.6513	0.45	258.46
8	N/A	N/A	N/A	N/A	N/A	N/A	54	8.5911	0.39	99.70	8.7174	0.48	260.15
10	N/A	N/A	N/A	N/A	N/A	N/A	56	8.6069	0.40	97.80	8.6797	0.52	262.26
12	N/A	N/A	N/A	N/A	N/A	N/A	58	8.5940	0.41	95.99	8.6563	0.52	264.00
14	N/A	N/A	N/A	N/A	N/A	N/A	60	8.5742	0.42	94.22	N/A	N/A	N/A
16	N/A	N/A	N/A	N/A	N/A	N/A	62	8.5985	0.43	92.49	8.6213	0.52	267.70
18	N/A	N/A	N/A	N/A	N/A	N/A	64	8.5628	0.45	90.76	8.6091	0.54	269.13
20	N/A	N/A	N/A	N/A	N/A	N/A	66	8.5585	0.48	89.12	8.6645	N/A	270.81
22	N/A	N/A	N/A	N/A	N/A	N/A	68	8.5566	0.50	87.50	8.5915	N/A	272.67
24	8.7243	0.32	174.48	8.7218	0.32	185.80	70	8.5059	0.54	85.86	8.5542	N/A	274.11
26	8.7235	0.33	153.87	8.7135	0.32	205.88	72	8.4320	0.59	84.24	8.5162	N/A	275.88
28	8.7295	0.34	144.21	8.7293	0.33	215.89	74	8.3598	0.66	82.62	N/A	N/A	N/A
30	8.7001	0.34	137.27	8.7453	0.34	222.70	76	8.4728	0.73	81.01	N/A	N/A	N/A
32	8.7148	0.34	132.06	8.7300	0.35	228.48	78	8.4283	N/A	79.45	N/A	N/A	N/A
34	8.7037	0.33	127.04	8.7132	0.34	233.22	80	8.3895	N/A	77.80	8.4315	N/A	282.42
36	8.7002	0.34	122.82	N/A	N/A	N/A	82	8.2401	N/A	76.14	8.3529	N/A	284.03
38	8.6799	0.34	119.53	8.7084	0.36	240.67	84	8.3092	N/A	74.48	8.2376	N/A	285.69
40	8.6879	0.34	116.31	8.6776	0.37	243.83	86	N/A	N/A	N/A	N/A	N/A	N/A
42	8.6601	0.34	113.18	8.6958	0.40	246.74	88	N/A	N/A	N/A	N/A	N/A	N/A
44	8.6511	0.35	110.72	8.6918	0.40	249.31	90	N/A	N/A	N/A	N/A	N/A	N/A

N/A - Not Available

Figure 3. Type-B Standard Uncertainty vs Zenith Angle

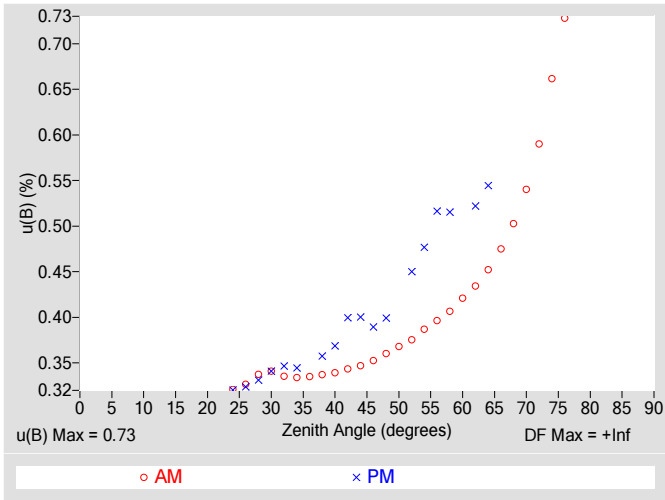


Figure 4. Residuals from Spline Interpolation

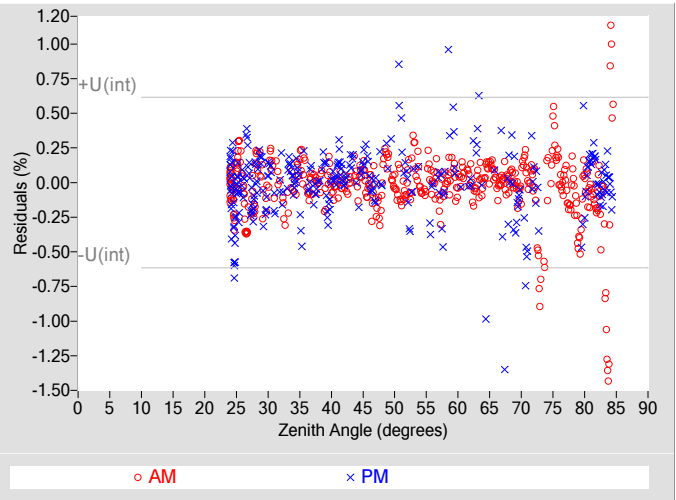


Table 3. Uncertainty using Spline Interpolation ‡

Type-B Standard Uncertainty, u(B) (%)	±0.73
Type-A Interpolating Function, u(int) (%)	±0.31
Combined Standard Uncertainty, u(c) (%)	±0.79
Effective degrees of freedom, DF(c)	28688
Coverage factor, k	1.96
Expanded Uncertainty, U95 (%)	±1.5
AM Valid zenith angle range	24° to 76°
PM Valid zenith angle range	24° to 64°

‡ An illustration for how to reduce the uncertainty in calculating the irradiance using a function rather than R@45°. Not accredited.

Table 4. Calibration Label Values

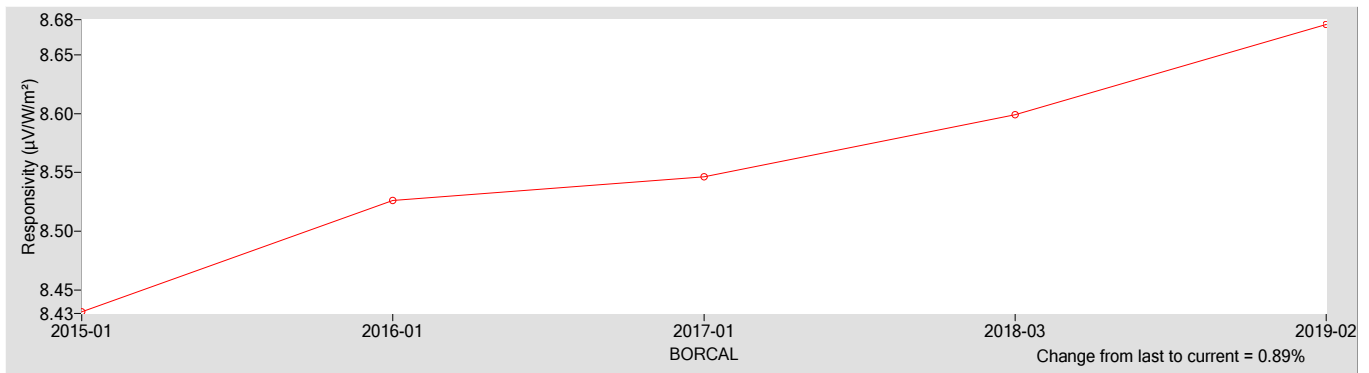
R @ 45° (μV/W/m²)	Rnet (μV/W/m²) †
8.6758	0.30000

† Rnet determination date: Estimated

Table 5. Uncertainty using R @ 45°

Type-B Expanded Uncertainty, U(B) (%)	±1.0
Offset Uncertainty, U(off) (%)	+0.80 / -1.2
Expanded Uncertainty, U (%)	+1.8 / -2.2
Effective degrees of freedom, DF	+Inf
Coverage factor, k	1.96
Valid zenith angle range	30.0° to 60.0°

Figure 5. History of instrument at Zenith Angle = 45°



References:

[1] Reda, I.; Hickey, J.; Long, C.; Myers, D.; Stoffel, T.; Wilcox, S.; Michalsky, J. J.; Dutton, E. G.; Nelson, D. (2005). "Using a Blackbody to Calculate Net Longwave Responsivity of Shortwave Solar Pyranometers to Correct for Their Thermal Offset Error During Outdoor Calibration Using the Component Sum Method." Journal of Atmospheric and Oceanic Technology. , 2005; pp. 1531-1540; NREL Report No. JA-560-36646. doi:10.1175/JTECH1782.1

[2] Reda, I.; Myers, D.; Stoffel, T. (2008). "Uncertainty Estimate for the Outdoor Calibration of Solar Pyranometers: A Metrologist Perspective." Measure. (NCSLI Journal of Measurement Science). Vol. 3(4), December 2008; pp. 58-66; NREL Report No. JA-581-4137

[3] Reda, I.; Andreas, A. (2004). "Solar Position Algorithm for Solar Radiation Applications." Solar Energy. Vol. 76(5), 2004; pp. 577-589; NREL Report No. JA-560-35518. doi:10.1016/j.solener.2003.12.003

[4] Stoffel, T.; Reda, I. (2009). "NREL Pyrheliometer Comparisons: 22 September - 3 October 2008 (NPC-2008)." 54 pp.; NREL Report No. TP-550-45016.

[5] Reda, I.; Stoffel, T.; Myers, D. (2003). "Method to Calibrate a Solar Pyranometer for Measuring Reference Diffuse Irradiance." Solar Energy. Vol. 74, 2003; pp. 103-112; NREL Report No. JA-560-35025. doi:10.1016/S0038-092X(03)00124-5

[6] Reda, I. (1996). Calibration of a Solar Absolute Cavity Radiometer with Traceability to the World Radiometric Reference. 79 pp.; NREL Report No. TP-463-20619.

[7] Reda, I.; Gröbner, J.; Stoffel, T.; Myers, D.; Forgan, B. (2008). Improvements in the Blackbody Calibration of Pyrgeometers. ARM 2008 Science Team Meeting (Poster).



# National Renewable Energy Laboratory

## Solar Radiation Research Laboratory

### Metrology Laboratory

### Calibration Certificate



<b>Test Instrument:</b>	Short Normal Incidence Pyrheliometer	<b>Manufacturer:</b>	Eppley
<b>Model:</b>	sNIP	<b>Serial Number:</b>	37882E6
<b>Calibration Date:</b>	5/3/2019	<b>Due Date:</b>	5/3/2020
<b>Customer:</b>	NREL-SRRL-BMS	<b>Environmental Conditions:</b>	see page 4
<b>Test Dates:</b>	5/3		

This certifies that the above product was calibrated in compliance with ISO/IEC 17025:2005. Measurement uncertainties at the time of calibration are consistent with the Guide to the Expression of Uncertainty in Measurement (GUM) using Reda et al., 2008. All nominal values are traceable to the International System (SI) Units of Measurement.

No statement of compliance with specifications is made or implied on this certificate. However, the estimated uncertainties are the uncertainties of the calibration process; users must add other uncertainties that are relevant to their measuring system, environmental and sky conditions, outdoor set-up, and site location.

The Type-B Standard Uncertainty of using the responsivity at each even zenith angle is reported, and the Expanded Uncertainty of the calibration is reported using two methods:

1. The Expanded Uncertainty of using the responsivity at zenith angle = 45°, within the zenith angle range from 30.0° to 60.0°
2. The Expanded Uncertainty of using Spline Interpolating Functions for the responsivity versus zenith angle.

This certificate applies only to the item identified above and shall not be reproduced other than in full, without specific written approval from the calibration facility. Certificate without signature is not valid.

**Table 1. Traceability**

Measurement Type	Instrument	Calibration Date	Calibration Due Date
Beam Irradiance †	Eppley Absolute Cavity Radiometer Model HF, S/N 29219	09/24/2018	09/24/2019
Diffuse Irradiance †	Hukseflux Pyranometer Model SR25, S/N 2541	04/19/2019	04/19/2020
Diffuse Irradiance †	Hukseflux Pyranometer Model SR25, S/N 2542	04/19/2019	04/19/2020
Data Acquisition	NREL Data Acquisition System Model RAP-DAQ, S/N 2005-998	02/14/2019	02/14/2021
Data Acquisition	NREL Data Acquisition System Model RAP-DAQ, S/N 2005-999	02/14/2019	02/14/2021

† Through the World Radiometric Reference (WRR)

**Number of pages of certificate:** 4

**Calibration Procedure:** BORCAL-P00-Calibration and QA Procedure; available upon request.

**Setup:** Radiometers are calibrated outdoors, using the sun as the source. Pyranometers and pyrgeometers are installed for horizontal measurements, with their signal connectors oriented north, if their design permits.

The shading disk for the reference diffuse subtends a solid angle of 5°. Pyrheliometers are installed on solar trackers.

**Calibrated by:** RCC

-----  
Ibrahim Reda, Technical Manager

-----  
Date

For questions or comments, please contact the technical manager at:

ibrahim.reda@nrel.gov; 303-384-6385; 15013 Denver West Parkway, Golden, CO 80401, USA

# Calibration Results

## 37882E6 Eppley sNIP

The responsivity ( $R$ ,  $\mu\text{V}/\text{W}/\text{m}^2$ ) of the test instrument during calibration is calculated using this Measurement Equation:

$$R = (V - R_{net} * W_{net}) / I \tag{1}$$

where,

- $V$  = radiometer output voltage (microvolts),
- $R_{net}$  = radiometer net infrared responsivity ( $\mu\text{V}/\text{W}/\text{m}^2$ ), see Table 4,
- $W_{net}$  = effective net infrared measured by pyrgeometer ( $\text{W}/\text{m}^2$ ),
- =  $W_{in} - W_{out} = W_{in} - \sigma * T_c^4$
- where,  $W_{in}$  = incoming infrared ( $\text{W}/\text{m}^2$ ),  $\sigma = 5.6704\text{e-}8 \text{ W}\cdot\text{m}^{-2}\cdot\text{K}^{-4}$ ,
- $T_c$  = case temperature of pyrgeometer (K).
- $I$  = reference irradiance ( $\text{W}/\text{m}^2$ ), beam (B) or global (G)
- where,  $G = B * \text{COS}(Z) + D$ ,
- $Z$  = zenith angle (degrees),
- $D$  = reference diffuse irradiance ( $\text{W}/\text{m}^2$ ).

Figure 1. Responsivity vs Zenith Angle

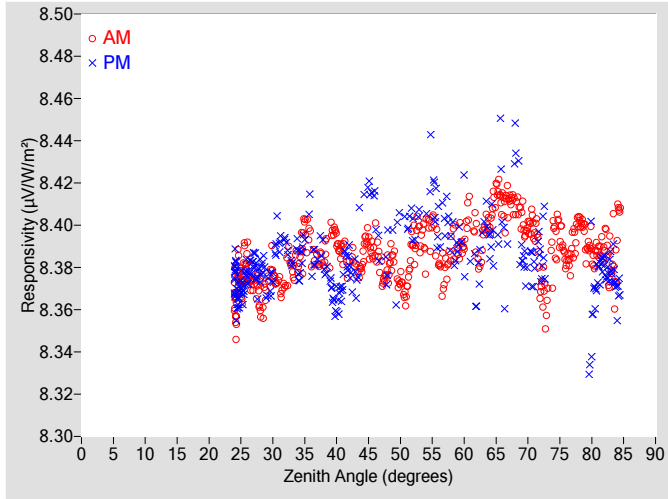


Figure 2. Responsivity vs Local Standard Time

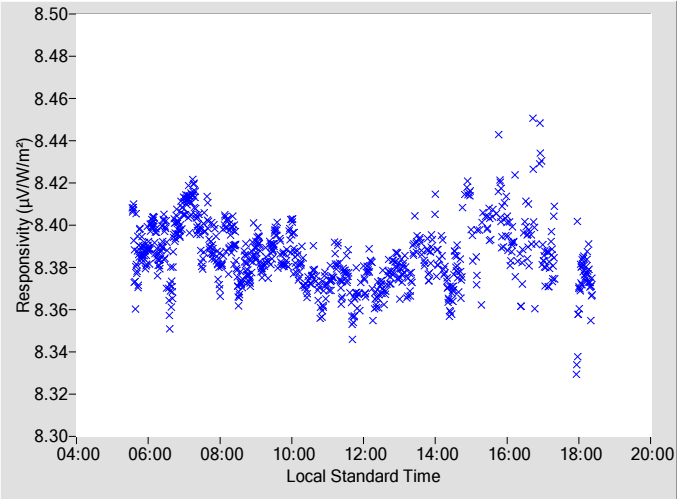


Table 2. Instrument Responsivity (R) and Calibration Type-B Standard Uncertainty, u(B)

Zenith Angle (deg.)	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle	Zenith Angle (deg.)	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle
0	N/A	N/A	N/A	N/A	N/A	N/A	46	8.3920	0.28	108.27	8.4093	0.28	251.87
2	N/A	N/A	N/A	N/A	N/A	N/A	48	8.3779	0.28	105.93	8.3827	0.29	254.07
4	N/A	N/A	N/A	N/A	N/A	N/A	50	8.3736	0.28	103.72	8.4059	0.29	256.21
6	N/A	N/A	N/A	N/A	N/A	N/A	52	8.3919	0.28	101.68	8.3993	0.29	258.42
8	N/A	N/A	N/A	N/A	N/A	N/A	54	8.3895	0.28	99.82	8.4055	0.30	260.53
10	N/A	N/A	N/A	N/A	N/A	N/A	56	8.3814	0.28	97.72	8.3956	0.30	262.27
12	N/A	N/A	N/A	N/A	N/A	N/A	58	8.3920	0.28	95.96	8.3948	0.30	264.13
14	N/A	N/A	N/A	N/A	N/A	N/A	60	8.3903	0.29	94.24	8.3997	N/A	265.96
16	N/A	N/A	N/A	N/A	N/A	N/A	62	8.3914	0.29	92.49	8.3685	0.30	267.68
18	N/A	N/A	N/A	N/A	N/A	N/A	64	8.3998	0.29	90.77	8.3912	0.30	269.42
20	N/A	N/A	N/A	N/A	N/A	N/A	66	8.4097	0.29	89.13	8.4090	N/A	271.02
22	N/A	N/A	N/A	N/A	N/A	N/A	68	8.4085	0.29	87.52	8.4372	N/A	272.66
24	8.3627	0.28	173.36	8.3772	0.28	185.35	70	8.3988	0.29	85.88	8.3799	N/A	274.17
26	8.3825	0.28	154.55	8.3769	0.28	206.04	72	8.3717	0.30	84.25	8.3807	N/A	275.93
28	8.3636	0.28	144.51	8.3789	0.28	216.05	74	8.3911	0.30	82.64	N/A	N/A	N/A
30	8.3793	0.28	137.14	8.3786	0.28	222.92	76	8.3828	0.30	81.03	N/A	N/A	N/A
32	8.3740	0.28	131.70	8.3918	0.28	228.51	78	8.4020	N/A	79.42	N/A	N/A	N/A
34	8.3812	0.28	126.84	8.3817	0.28	233.07	80	8.3852	N/A	77.74	8.3651	N/A	282.46
36	8.3888	0.28	123.06	8.3953	0.28	237.04	82	8.3917	N/A	76.16	8.3802	N/A	284.03
38	8.3849	0.28	119.34	8.3829	0.28	240.75	84	8.3966	N/A	74.45	8.3686	N/A	285.75
40	8.3939	0.28	116.29	8.3622	0.28	243.82	86	N/A	N/A	N/A	N/A	N/A	N/A
42	8.3790	0.28	113.55	8.3813	0.28	246.74	88	N/A	N/A	N/A	N/A	N/A	N/A
44	8.3816	0.28	110.71	8.4146	0.28	249.79	90	N/A	N/A	N/A	N/A	N/A	N/A

N/A - Not Available

Figure 3. Type-B Standard Uncertainty vs Zenith Angle

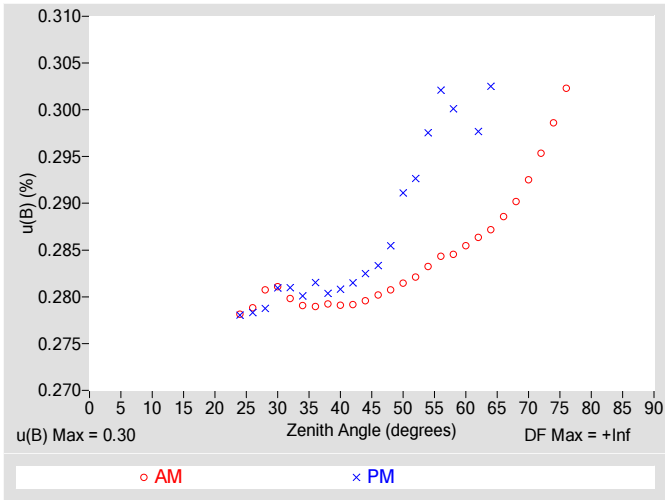


Figure 4. Residuals from Spline Interpolation

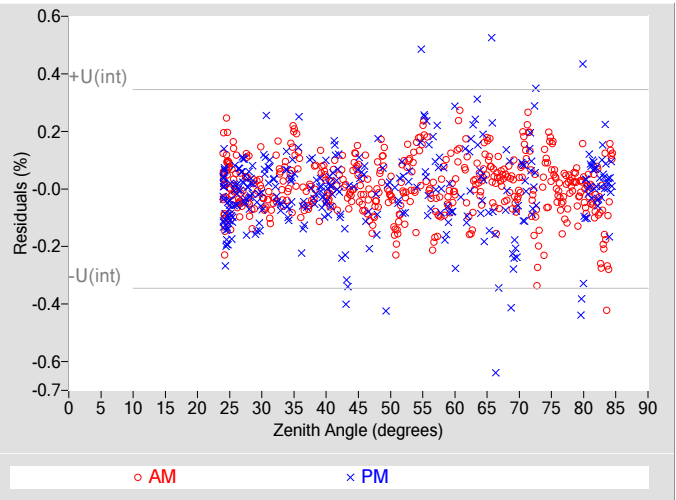


Table 3. Uncertainty using Spline Interpolation ‡

Type-B Standard Uncertainty, $u(B)$ (%)	$\pm 0.30$
Type-A Interpolating Function, $u(int)$ (%)	$\pm 0.17$
Combined Standard Uncertainty, $u(c)$ (%)	$\pm 0.35$
Effective degrees of freedom, $DF(c)$	11080
Coverage factor, $k$	1.96
Expanded Uncertainty, $U95$ (%)	$\pm 0.68$
AM Valid zenith angle range	24° to 76°
PM Valid zenith angle range	24° to 64°

‡ An illustration for how to reduce the uncertainty in calculating the irradiance using a function rather than  $R@45^\circ$ . Not accredited.

Table 4. Calibration Label Values

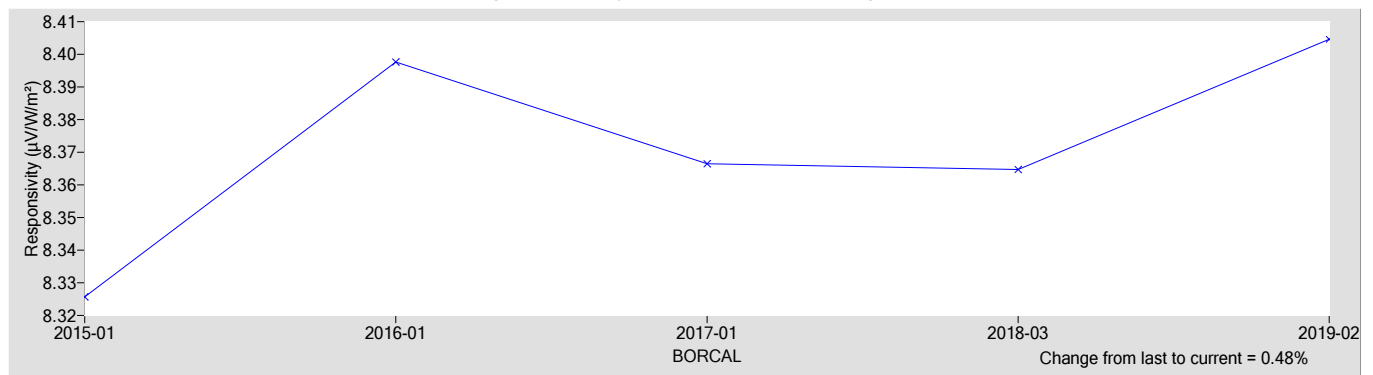
$R @ 45^\circ$ ( $\mu V/W/m^2$ )	$R_{net}$ ( $\mu V/W/m^2$ ) †
8.4047	0

†  $R_{net}$  determination date: N/A

Table 5. Uncertainty using  $R @ 45^\circ$

Type-B Expanded Uncertainty, $U(B)$ (%)	$\pm 0.59$
Offset Uncertainty, $U(off)$ (%)	+0.12 / -0.51
Expanded Uncertainty, $U$ (%)	+0.71 / -1.1
Effective degrees of freedom, $DF$	+Inf
Coverage factor, $k$	1.96
Valid zenith angle range	30.0° to 60.0°

Figure 5. History of instrument at Zenith Angle = 45°



References:

[1] Reda, I.; Hickey, J.; Long, C.; Myers, D.; Stoffel, T.; Wilcox, S.; Michalsky, J. J.; Dutton, E. G.; Nelson, D. (2005). "Using a Blackbody to Calculate Net Longwave Responsivity of Shortwave Solar Pyranometers to Correct for Their Thermal Offset Error During Outdoor Calibration Using the Component Sum Method." Journal of Atmospheric and Oceanic Technology. , 2005; pp. 1531-1540; NREL Report No. JA-560-36646. doi:10.1175/JTECH1782.1

[2] Reda, I.; Myers, D.; Stoffel, T. (2008). "Uncertainty Estimate for the Outdoor Calibration of Solar Pyranometers: A Metrologist Perspective." Measure. (NCSLI Journal of Measurement Science). Vol. 3(4), December 2008; pp. 58-66; NREL Report No. JA-581-4137

[3] Reda, I.; Andreas, A. (2004). "Solar Position Algorithm for Solar Radiation Applications." Solar Energy. Vol. 76(5), 2004; pp. 577-589; NREL Report No. JA-560-35518. doi:10.1016/j.solener.2003.12.003

[4] Stoffel, T.; Reda, I. (2009). "NREL Pyrheliometer Comparisons: 22 September - 3 October 2008 (NPC-2008)." 54 pp.; NREL Report No. TP-550-45016.

[5] Reda, I.; Stoffel, T.; Myers, D. (2003). "Method to Calibrate a Solar Pyranometer for Measuring Reference Diffuse Irradiance." Solar Energy. Vol. 74, 2003; pp. 103-112; NREL Report No. JA-560-35025. doi:10.1016/S0038-092X(03)00124-5

[6] Reda, I. (1996). Calibration of a Solar Absolute Cavity Radiometer with Traceability to the World Radiometric Reference. 79 pp.; NREL Report No. TP-463-20619.

[7] Reda, I.; Gröbner, J.; Stoffel, T.; Myers, D.; Forgan, B. (2008). Improvements in the Blackbody Calibration of Pyrgeometers. ARM 2008 Science Team Meeting (Poster).



# National Renewable Energy Laboratory

## Solar Radiation Research Laboratory

### Metrology Laboratory

### Calibration Certificate



<b>Test Instrument:</b>	Si pyranometer	<b>Manufacturer:</b>	Apogee
<b>Model:</b>	SP-110	<b>Serial Number:</b>	40337
<b>Calibration Date:</b>	5/3/2019	<b>Due Date:</b>	5/3/2020
<b>Customer:</b>	NREL-SRRL-BMS	<b>Environmental Conditions:</b>	see page 4
<b>Test Dates:</b>	5/3		

This certifies that the above product was calibrated in compliance with ISO/IEC 17025:2005. Measurement uncertainties at the time of calibration are consistent with the Guide to the Expression of Uncertainty in Measurement (GUM) using Reda et al., 2008. All nominal values are traceable to the International System (SI) Units of Measurement.

No statement of compliance with specifications is made or implied on this certificate. However, the estimated uncertainties are the uncertainties of the calibration process; users must add other uncertainties that are relevant to their measuring system, environmental and sky conditions, outdoor set-up, and site location.

The Type-B Standard Uncertainty of using the responsivity at each even zenith angle is reported, and the Expanded Uncertainty of the calibration is reported using two methods:

1. The Expanded Uncertainty of using the responsivity at zenith angle = 45°, within the zenith angle range from 30.0° to 60.0°
2. The Expanded Uncertainty of using Spline Interpolating Functions for the responsivity versus zenith angle.

This certificate applies only to the item identified above and shall not be reproduced other than in full, without specific written approval from the calibration facility. Certificate without signature is not valid.

**Table 1. Traceability**

Measurement Type	Instrument	Calibration Date	Calibration Due Date
Beam Irradiance †	Eppley Absolute Cavity Radiometer Model HF, S/N 29219	09/24/2018	09/24/2019
Diffuse Irradiance †	Hukseflux Pyranometer Model SR25, S/N 2541	04/19/2019	04/19/2020
Diffuse Irradiance †	Hukseflux Pyranometer Model SR25, S/N 2542	04/19/2019	04/19/2020
Data Acquisition	NREL Data Acquisition System Model RAP-DAQ, S/N 2005-998	02/14/2019	02/14/2021
Data Acquisition	NREL Data Acquisition System Model RAP-DAQ, S/N 2005-999	02/14/2019	02/14/2021

† Through the World Radiometric Reference (WRR)

**Number of pages of certificate:** 4

**Calibration Procedure:** BORCAL-P00-Calibration and QA Procedure; available upon request.

**Setup:** Radiometers are calibrated outdoors, using the sun as the source. Pyranometers and pyrgeometers are installed for horizontal measurements, with their signal connectors oriented north, if their design permits.

The shading disk for the reference diffuse subtends a solid angle of 5°. Pyrheliometers are installed on solar trackers.

**Calibrated by:** RCC

-----  
Ibrahim Reda, Technical Manager

-----  
Date

For questions or comments, please contact the technical manager at:

ibrahim.reda@nrel.gov; 303-384-6385; 15013 Denver West Parkway, Golden, CO 80401, USA

# Calibration Results

## 40337 Apogee SP-110

The responsivity ( $R$ ,  $\mu\text{V}/\text{W}/\text{m}^2$ ) of the test instrument during calibration is calculated using this Measurement Equation:

$$R = (V - R_{net} * W_{net}) / I \tag{1}$$

where,

- $V$  = radiometer output voltage (microvolts),
  - $R_{net}$  = radiometer net infrared responsivity ( $\mu\text{V}/\text{W}/\text{m}^2$ ), see Table 4,
  - $W_{net}$  = effective net infrared measured by pyrgeometer ( $\text{W}/\text{m}^2$ ),
  - =  $W_{in} - W_{out} = W_{in} - \sigma * T_c^4$
  - where,  $W_{in}$  = incoming infrared ( $\text{W}/\text{m}^2$ ),  $\sigma = 5.6704\text{e-}8 \text{ W}\cdot\text{m}^{-2}\cdot\text{K}^{-4}$ ,
  - $T_c$  = case temperature of pyrgeometer (K).
- $I$  = reference irradiance ( $\text{W}/\text{m}^2$ ), beam (B) or global (G)
  - where,  $G = B * \text{COS}(Z) + D$ ,
  - $Z$  = zenith angle (degrees),
  - $D$  = reference diffuse irradiance ( $\text{W}/\text{m}^2$ ).

Figure 1. Responsivity vs Zenith Angle

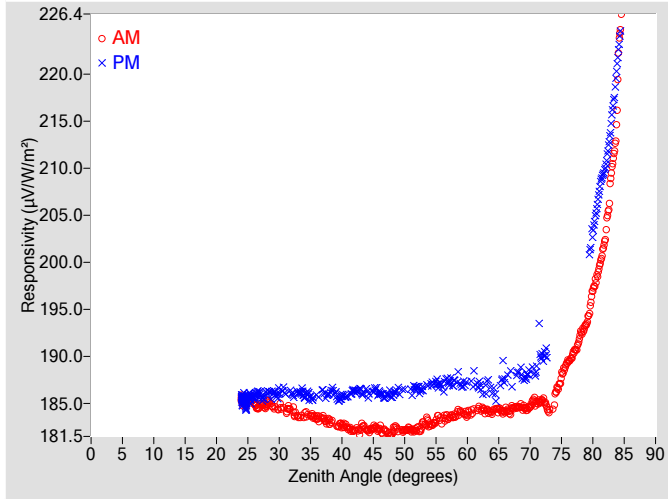


Figure 2. Responsivity vs Local Standard Time

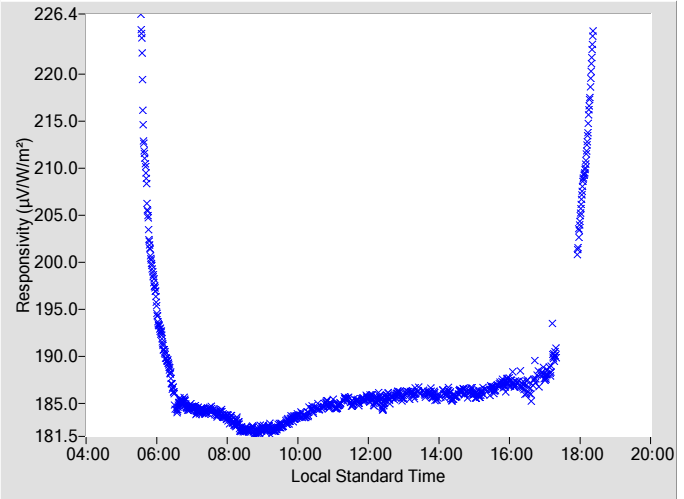


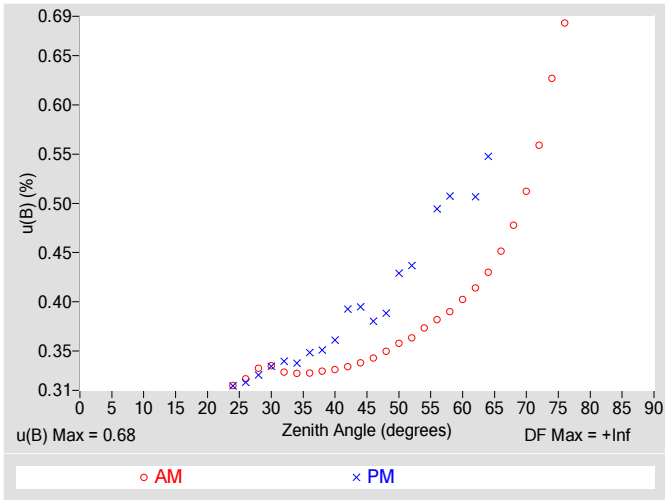
Table 2. Instrument Responsivity (R) and Calibration Type-B Standard Uncertainty, u(B)

Zenith Angle (deg.)	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle	Zenith Angle (deg.)	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle
0	N/A	N/A	N/A	N/A	N/A	N/A	46	182.30	0.34	108.33	186.05	0.38	251.87
2	N/A	N/A	N/A	N/A	N/A	N/A	48	181.88	0.35	105.92	185.76	0.39	254.14
4	N/A	N/A	N/A	N/A	N/A	N/A	50	182.14	0.36	103.70	186.50	0.43	256.42
6	N/A	N/A	N/A	N/A	N/A	N/A	52	182.28	0.36	101.72	186.71	0.44	258.45
8	N/A	N/A	N/A	N/A	N/A	N/A	54	182.77	0.37	99.70	186.97	N/A	260.67
10	N/A	N/A	N/A	N/A	N/A	N/A	56	183.15	0.38	97.75	186.66	0.49	262.33
12	N/A	N/A	N/A	N/A	N/A	N/A	58	183.64	0.39	96.01	187.25	0.51	264.15
14	N/A	N/A	N/A	N/A	N/A	N/A	60	183.93	0.40	94.22	187.27	N/A	265.80
16	N/A	N/A	N/A	N/A	N/A	N/A	62	184.42	0.41	92.47	186.86	0.51	267.65
18	N/A	N/A	N/A	N/A	N/A	N/A	64	184.12	0.43	90.81	186.35	0.55	269.46
20	N/A	N/A	N/A	N/A	N/A	N/A	66	184.24	0.45	89.12	187.42	N/A	270.99
22	N/A	N/A	N/A	N/A	N/A	N/A	68	184.60	0.48	87.46	188.19	N/A	272.68
24	185.37	0.31	174.67	185.45	0.31	185.88	70	184.68	0.51	85.86	188.31	N/A	274.11
26	184.91	0.32	153.48	185.74	0.32	206.15	72	185.33	0.56	84.24	189.91	N/A	275.92
28	184.82	0.33	144.53	186.21	0.33	215.95	74	186.00	0.63	82.58	N/A	N/A	N/A
30	184.57	0.34	137.22	186.05	0.33	222.49	76	189.37	0.68	81.06	N/A	N/A	N/A
32	184.37	0.33	131.48	186.01	0.34	228.66	78	192.20	N/A	79.40	N/A	N/A	N/A
34	183.87	0.33	126.81	185.85	0.34	233.04	80	197.00	N/A	77.80	203.60	N/A	282.44
36	183.47	0.33	122.94	185.80	0.35	237.37	82	202.70	N/A	76.19	210.37	N/A	284.07
38	183.09	0.33	119.53	186.10	0.35	240.65	84	219.27	N/A	74.48	222.18	N/A	285.74
40	182.69	0.33	116.27	185.72	0.36	243.76	86	N/A	N/A	N/A	N/A	N/A	N/A
42	182.11	0.33	113.46	186.34	0.39	246.71	88	N/A	N/A	N/A	N/A	N/A	N/A
44	182.15	0.34	110.57	186.12	0.39	249.54	90	N/A	N/A	N/A	N/A	N/A	N/A

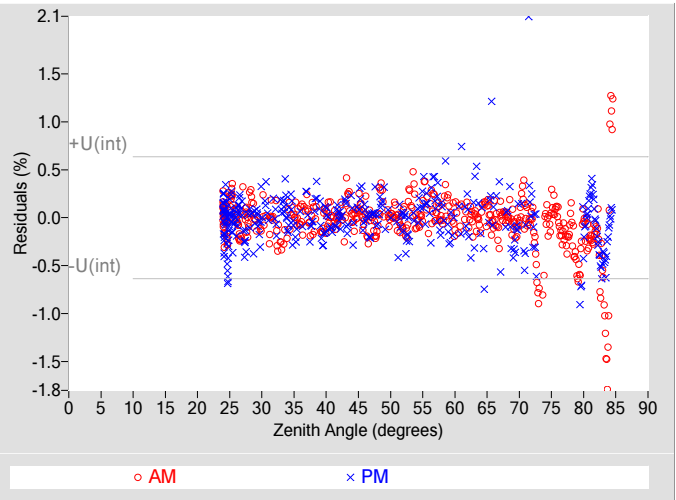
N/A - Not Available



**Figure 3. Type-B Standard Uncertainty vs Zenith Angle**



**Figure 4. Residuals from Spline Interpolation**



**Table 3. Uncertainty using Spline Interpolation ‡**

Type-B Standard Uncertainty, u(B) (%)	±0.68
Type-A Interpolating Function, u(int) (%)	±0.32
Combined Standard Uncertainty, u(c) (%)	±0.75
Effective degrees of freedom, DF(c)	22782
Coverage factor, k	1.96
Expanded Uncertainty, U95 (%)	±1.5
AM Valid zenith angle range	24° to 76°
PM Valid zenith angle range	24° to 64°

‡ An illustration for how to reduce the uncertainty in calculating the irradiance using a function rather than R@45°. Not accredited.

**Table 4. Calibration Label Values**

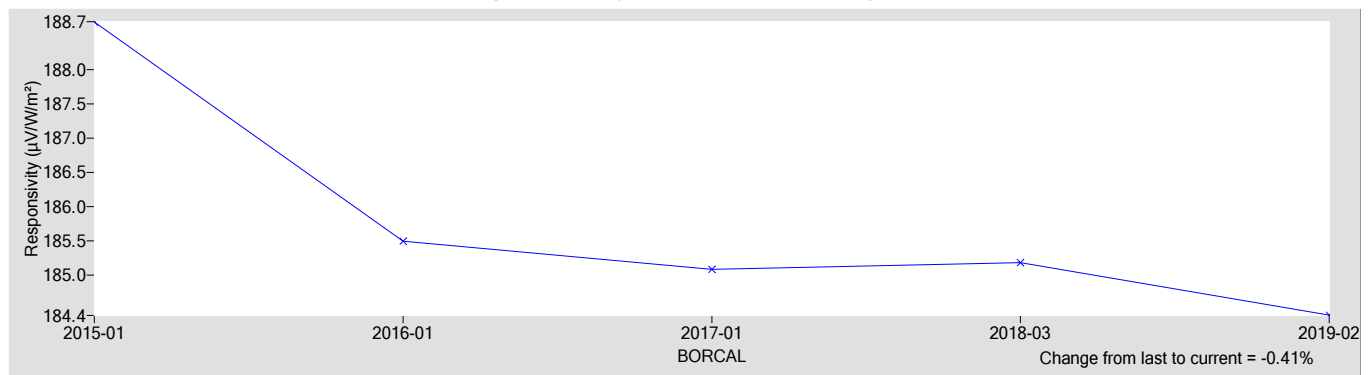
R @ 45° (μV/W/m²)	Rnet (μV/W/m²) †
184.41	0

† Rnet determination date: N/A

**Table 5. Uncertainty using R @ 45°**

Type-B Expanded Uncertainty, U(B) (%)	±0.99
Offset Uncertainty, U(off) (%)	+1.6 / -1.4
Expanded Uncertainty, U (%)	+2.5 / -2.4
Effective degrees of freedom, DF	+Inf
Coverage factor, k	1.96
Valid zenith angle range	30.0° to 60.0°

**Figure 5. History of instrument at Zenith Angle = 45°**



**References:**

[1] Reda, I.; Hickey, J.; Long, C.; Myers, D.; Stoffel, T.; Wilcox, S.; Michalsky, J. J.; Dutton, E. G.; Nelson, D. (2005). "Using a Blackbody to Calculate Net Longwave Responsivity of Shortwave Solar Pyranometers to Correct for Their Thermal Offset Error During Outdoor Calibration Using the Component Sum Method." Journal of Atmospheric and Oceanic Technology. , 2005; pp. 1531-1540; NREL Report No. JA-560-36646. doi:10.1175/JTECH1782.1

[2] Reda, I.; Myers, D.; Stoffel, T. (2008). "Uncertainty Estimate for the Outdoor Calibration of Solar Pyranometers: A Metrologist Perspective." Measure. (NCSLI Journal of Measurement Science). Vol. 3(4), December 2008; pp. 58-66; NREL Report No. JA-581-4137

[3] Reda, I.; Andreas, A. (2004). "Solar Position Algorithm for Solar Radiation Applications." Solar Energy. Vol. 76(5), 2004; pp. 577-589; NREL Report No. JA-560-35518. doi:10.1016/j.solener.2003.12.003

[4] Stoffel, T.; Reda, I. (2009). "NREL Pyrheliometer Comparisons: 22 September - 3 October 2008 (NPC-2008)." 54 pp.; NREL Report No. TP-550-45016.

[5] Reda, I.; Stoffel, T.; Myers, D. (2003). "Method to Calibrate a Solar Pyranometer for Measuring Reference Diffuse Irradiance." Solar Energy. Vol. 74, 2003; pp. 103-112; NREL Report No. JA-560-35025. doi:10.1016/S0038-092X(03)00124-5

[6] Reda, I. (1996). Calibration of a Solar Absolute Cavity Radiometer with Traceability to the World Radiometric Reference. 79 pp.; NREL Report No. TP-463-20619.

[7] Reda, I.; Gröbner, J.; Stoffel, T.; Myers, D.; Forgan, B. (2008). Improvements in the Blackbody Calibration of Pyrgeometers. ARM 2008 Science Team Meeting (Poster).





# Calibration Results

## 9206 Hukseflux DR02

The responsivity ( $R$ ,  $\mu\text{V}/\text{W}/\text{m}^2$ ) of the test instrument during calibration is calculated using this Measurement Equation:

$$R = (V - R_{net} * W_{net}) / I \tag{1}$$

where,

- $V$  = radiometer output voltage (microvolts),
  - $R_{net}$  = radiometer net infrared responsivity ( $\mu\text{V}/\text{W}/\text{m}^2$ ), see Table 4,
  - $W_{net}$  = effective net infrared measured by pyrgeometer ( $\text{W}/\text{m}^2$ ),
  - =  $W_{in} - W_{out} = W_{in} - \sigma * T_c^4$
  - where,  $W_{in}$  = incoming infrared ( $\text{W}/\text{m}^2$ ),  $\sigma = 5.6704\text{e-}8 \text{ W}\cdot\text{m}^{-2}\cdot\text{K}^{-4}$ ,
  - $T_c$  = case temperature of pyrgeometer (K).
- $I$  = reference irradiance ( $\text{W}/\text{m}^2$ ), beam (B) or global (G)
  - where,  $G = B * \text{COS}(Z) + D$ ,
  - $Z$  = zenith angle (degrees),
  - $D$  = reference diffuse irradiance ( $\text{W}/\text{m}^2$ ).

Figure 1. Responsivity vs Zenith Angle

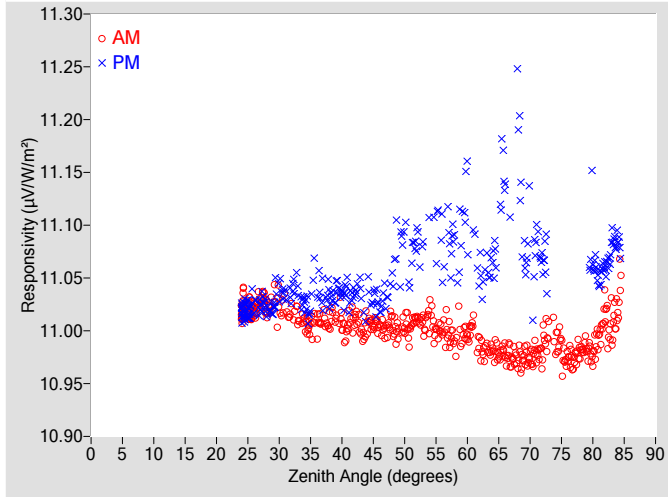


Figure 2. Responsivity vs Local Standard Time

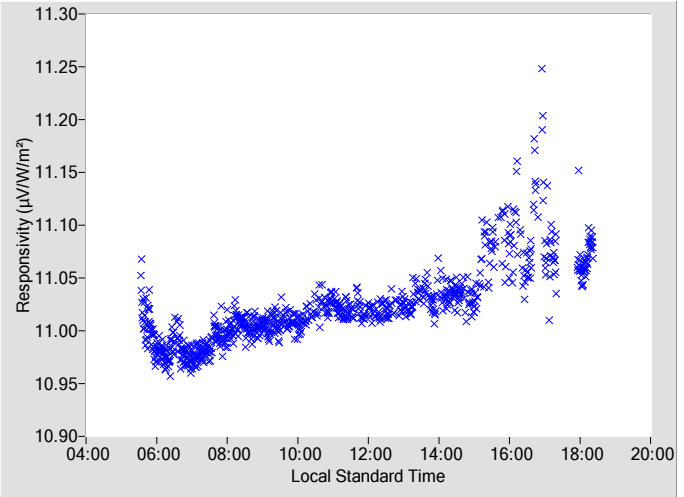


Table 2. Instrument Responsivity (R) and Calibration Type-B Standard Uncertainty, u(B)

Zenith Angle (deg.)	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	AM u(B) $\pm$ (%)	Azimuth Angle	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	PM u(B) $\pm$ (%)	Azimuth Angle	Zenith Angle (deg.)	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	AM u(B) $\pm$ (%)	Azimuth Angle	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	PM u(B) $\pm$ (%)	Azimuth Angle
0	N/A	N/A	N/A	N/A	N/A	N/A	46	11.004	0.28	108.23	11.021	0.28	251.95
2	N/A	N/A	N/A	N/A	N/A	N/A	48	11.008	0.28	105.94	11.047	0.29	254.17
4	N/A	N/A	N/A	N/A	N/A	N/A	50	11.006	0.28	103.72	11.098	0.29	256.38
6	N/A	N/A	N/A	N/A	N/A	N/A	52	11.011	0.28	101.74	11.088	0.29	258.37
8	N/A	N/A	N/A	N/A	N/A	N/A	54	11.015	0.28	99.75	11.107	0.30	260.33
10	N/A	N/A	N/A	N/A	N/A	N/A	56	11.003	0.28	97.79	11.076	0.30	262.35
12	N/A	N/A	N/A	N/A	N/A	N/A	58	10.987	0.28	95.93	11.088	0.30	264.02
14	N/A	N/A	N/A	N/A	N/A	N/A	60	10.993	0.28	94.19	11.128	N/A	265.88
16	N/A	N/A	N/A	N/A	N/A	N/A	62	10.987	0.29	92.49	11.056	0.30	267.69
18	N/A	N/A	N/A	N/A	N/A	N/A	64	10.983	0.29	90.82	11.065	0.30	269.40
20	N/A	N/A	N/A	N/A	N/A	N/A	66	10.977	0.29	89.13	11.138	N/A	270.96
22	N/A	N/A	N/A	N/A	N/A	N/A	68	10.974	0.29	87.47	11.219	N/A	272.71
24	11.021	0.28	174.05	11.019	0.28	185.09	70	10.975	0.29	85.88	11.137	N/A	274.17
26	11.019	0.28	153.79	11.021	0.28	205.89	72	10.984	0.29	84.25	11.065	N/A	275.94
28	11.021	0.28	144.32	11.021	0.28	215.48	74	10.992	0.30	82.63	N/A	N/A	N/A
30	11.023	0.28	137.63	11.041	0.28	222.90	76	10.974	0.30	81.03	N/A	N/A	N/A
32	11.017	0.28	131.72	11.038	0.28	228.46	78	10.980	N/A	79.42	N/A	N/A	N/A
34	11.009	0.28	127.00	11.027	0.28	233.01	80	10.978	N/A	77.77	11.061	N/A	282.51
36	11.005	0.28	122.71	11.032	0.28	237.39	82	11.022	N/A	76.16	11.060	N/A	284.04
38	11.007	0.28	119.46	11.034	0.28	240.63	84	11.027	N/A	74.45	11.085	N/A	285.75
40	11.011	0.28	116.29	11.035	0.28	243.82	86	N/A	N/A	N/A	N/A	N/A	N/A
42	11.009	0.28	113.40	11.036	0.28	246.75	88	N/A	N/A	N/A	N/A	N/A	N/A
44	11.005	0.28	110.78	11.032	0.28	249.53	90	N/A	N/A	N/A	N/A	N/A	N/A

N/A - Not Available

Figure 3. Type-B Standard Uncertainty vs Zenith Angle

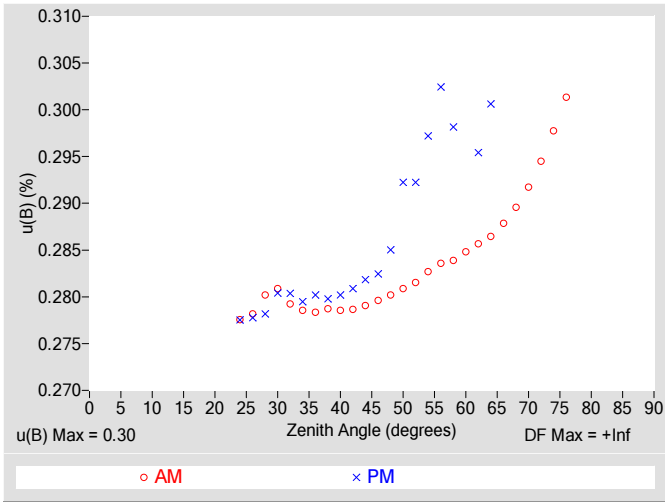


Figure 4. Residuals from Spline Interpolation

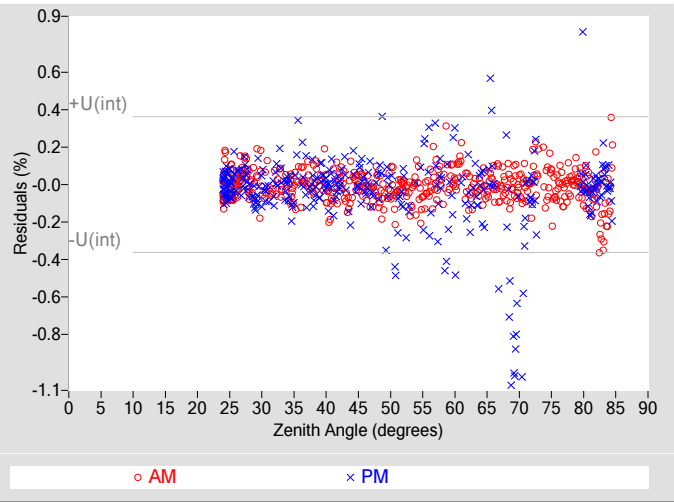


Table 3. Uncertainty using Spline Interpolation ‡

Type-B Standard Uncertainty, u(B) (%)	±0.30
Type-A Interpolating Function, u(int) (%)	±0.18
Combined Standard Uncertainty, u(c) (%)	±0.35
Effective degrees of freedom, DF(c)	9777
Coverage factor, k	1.96
Expanded Uncertainty, U95 (%)	±0.69
AM Valid zenith angle range	24° to 76°
PM Valid zenith angle range	24° to 64°

‡ An illustration for how to reduce the uncertainty in calculating the irradiance using a function rather than R@45°. Not accredited.

Table 4. Calibration Label Values

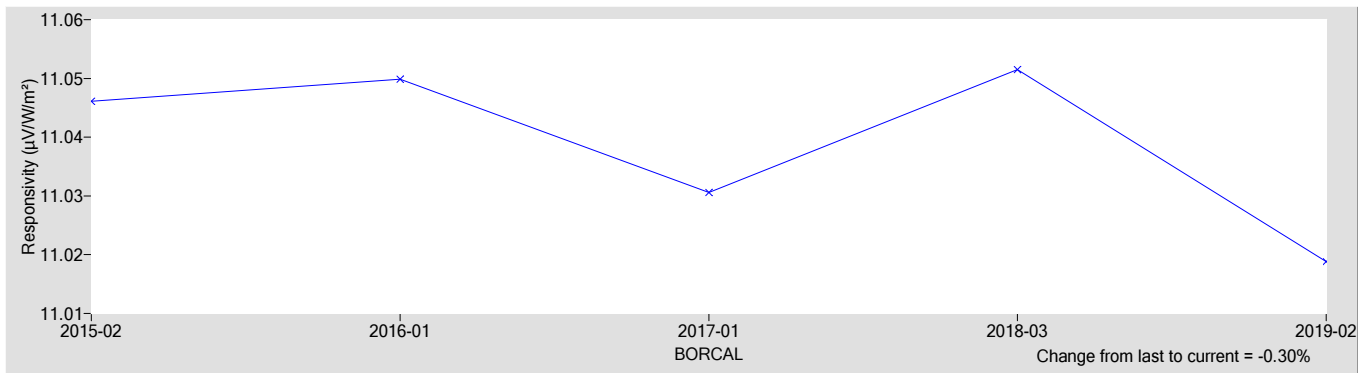
R @ 45° (μV/W/m²)	Rnet (μV/W/m²) †
11.019	0

† Rnet determination date: N/A

Table 5. Uncertainty using R @ 45°

Type-B Expanded Uncertainty, U(B) (%)	±0.59
Offset Uncertainty, U(off) (%)	+0.99 / -0.29
Expanded Uncertainty, U (%)	+1.6 / -0.88
Effective degrees of freedom, DF	+Inf
Coverage factor, k	1.96
Valid zenith angle range	30.0° to 60.0°

Figure 5. History of instrument at Zenith Angle = 45°



References:

[1] Reda, I.; Hickey, J.; Long, C.; Myers, D.; Stoffel, T.; Wilcox, S.; Michalsky, J. J.; Dutton, E. G.; Nelson, D. (2005). "Using a Blackbody to Calculate Net Longwave Responsivity of Shortwave Solar Pyranometers to Correct for Their Thermal Offset Error During Outdoor Calibration Using the Component Sum Method." Journal of Atmospheric and Oceanic Technology. , 2005; pp. 1531-1540; NREL Report No. JA-560-36646. doi:10.1175/JTECH1782.1

[2] Reda, I.; Myers, D.; Stoffel, T. (2008). "Uncertainty Estimate for the Outdoor Calibration of Solar Pyranometers: A Metrologist Perspective." Measure. (NCSLI Journal of Measurement Science). Vol. 3(4), December 2008; pp. 58-66; NREL Report No. JA-581-4137

[3] Reda, I.; Andreas, A. (2004). "Solar Position Algorithm for Solar Radiation Applications." Solar Energy. Vol. 76(5), 2004; pp. 577-589; NREL Report No. JA-560-35518. doi:10.1016/j.solener.2003.12.003

[4] Stoffel, T.; Reda, I. (2009). "NREL Pyrheliometer Comparisons: 22 September - 3 October 2008 (NPC-2008)." 54 pp.; NREL Report No. TP-550-45016.

[5] Reda, I.; Stoffel, T.; Myers, D. (2003). "Method to Calibrate a Solar Pyranometer for Measuring Reference Diffuse Irradiance." Solar Energy. Vol. 74, 2003; pp. 103-112; NREL Report No. JA-560-35025. doi:10.1016/S0038-092X(03)00124-5

[6] Reda, I. (1996). Calibration of a Solar Absolute Cavity Radiometer with Traceability to the World Radiometric Reference. 79 pp.; NREL Report No. TP-463-20619.

[7] Reda, I.; Gröbner, J.; Stoffel, T.; Myers, D.; Forgan, B. (2008). Improvements in the Blackbody Calibration of Pyrgometers. ARM 2008 Science Team Meeting (Poster).



# National Renewable Energy Laboratory

## Solar Radiation Research Laboratory

### Metrology Laboratory

### Calibration Certificate



<b>Test Instrument:</b>	Sunshine Pyranometer - Global Output	<b>Manufacturer:</b>	Delta-T
<b>Model:</b>	SPN1	<b>Serial Number:</b>	A360
<b>Calibration Date:</b>	5/3/2019	<b>Due Date:</b>	5/3/2020
<b>Customer:</b>	NREL-SRRL-BMS	<b>Environmental Conditions:</b>	see page 4
<b>Test Dates:</b>	5/3		

This certifies that the above product was calibrated in compliance with ISO/IEC 17025:2005. Measurement uncertainties at the time of calibration are consistent with the Guide to the Expression of Uncertainty in Measurement (GUM) using Reda et al., 2008. All nominal values are traceable to the International System (SI) Units of Measurement.

No statement of compliance with specifications is made or implied on this certificate. However, the estimated uncertainties are the uncertainties of the calibration process; users must add other uncertainties that are relevant to their measuring system, environmental and sky conditions, outdoor set-up, and site location.

The Type-B Standard Uncertainty of using the responsivity at each even zenith angle is reported, and the Expanded Uncertainty of the calibration is reported using two methods:

1. The Expanded Uncertainty of using the responsivity at zenith angle = 45°, within the zenith angle range from 30.0° to 60.0°
2. The Expanded Uncertainty of using Spline Interpolating Functions for the responsivity versus zenith angle.

This certificate applies only to the item identified above and shall not be reproduced other than in full, without specific written approval from the calibration facility. Certificate without signature is not valid.

**Table 1. Traceability**

Measurement Type	Instrument	Calibration Date	Calibration Due Date
Beam Irradiance †	Eppley Absolute Cavity Radiometer Model HF, S/N 29219	09/24/2018	09/24/2019
Diffuse Irradiance †	Hukseflux Pyranometer Model SR25, S/N 2541	04/19/2019	04/19/2020
Diffuse Irradiance †	Hukseflux Pyranometer Model SR25, S/N 2542	04/19/2019	04/19/2020
Data Acquisition	NREL Data Acquisition System Model RAP-DAQ, S/N 2005-998	02/14/2019	02/14/2021
Data Acquisition	NREL Data Acquisition System Model RAP-DAQ, S/N 2005-999	02/14/2019	02/14/2021

† Through the World Radiometric Reference (WRR)

**Number of pages of certificate:** 4

**Calibration Procedure:** BORCAL-P00-Calibration and QA Procedure; available upon request.

**Setup:** Radiometers are calibrated outdoors, using the sun as the source. Pyranometers and pyrgeometers are installed for horizontal measurements, with their signal connectors oriented north, if their design permits.

The shading disk for the reference diffuse subtends a solid angle of 5°. Pyrheliometers are installed on solar trackers.

**Calibrated by:** RCC

-----  
Ibrahim Reda, Technical Manager

-----  
Date

For questions or comments, please contact the technical manager at:

ibrahim.reda@nrel.gov; 303-384-6385; 15013 Denver West Parkway, Golden, CO 80401, USA

# Calibration Results

## A360 Delta-T SPN1

The responsivity ( $R$ ,  $\mu\text{V}/\text{W}/\text{m}^2$ ) of the test instrument during calibration is calculated using this Measurement Equation:

$$R = (V - R_{net} * W_{net}) / I \quad [1]$$

where,

- $V$  = radiometer output voltage (microvolts),
- $R_{net}$  = radiometer net infrared responsivity ( $\mu\text{V}/\text{W}/\text{m}^2$ ), see Table 4,
- $W_{net}$  = effective net infrared measured by pyrgeometer ( $\text{W}/\text{m}^2$ ),
- $= W_{in} - W_{out} = W_{in} - \sigma * T_c^4$
- where,  $W_{in}$  = incoming infrared ( $\text{W}/\text{m}^2$ ),  $\sigma = 5.6704\text{e-}8 \text{ W}\cdot\text{m}^{-2}\cdot\text{K}^{-4}$ ,
- $T_c$  = case temperature of pyrgeometer (K).
- $I$  = reference irradiance ( $\text{W}/\text{m}^2$ ), beam (B) or global (G)
- where,  $G = B * \text{COS}(Z) + D$ ,
- $Z$  = zenith angle (degrees),
- $D$  = reference diffuse irradiance ( $\text{W}/\text{m}^2$ ).

Figure 1. Responsivity vs Zenith Angle

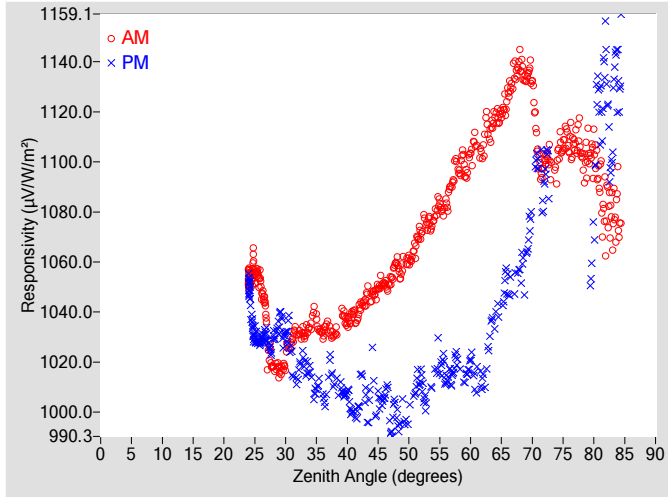


Figure 2. Responsivity vs Local Standard Time

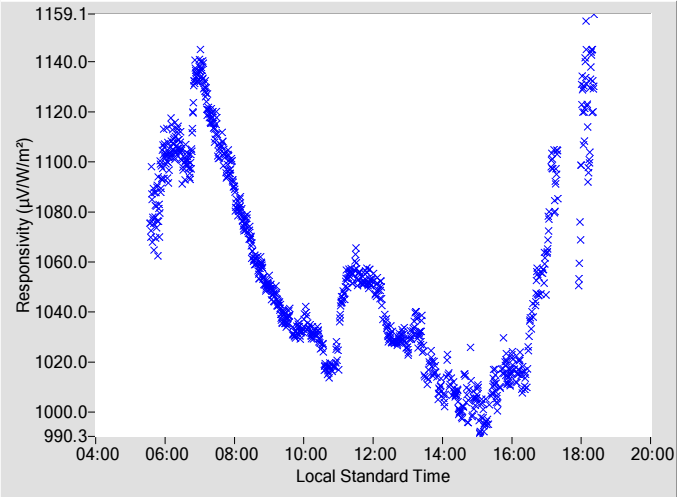
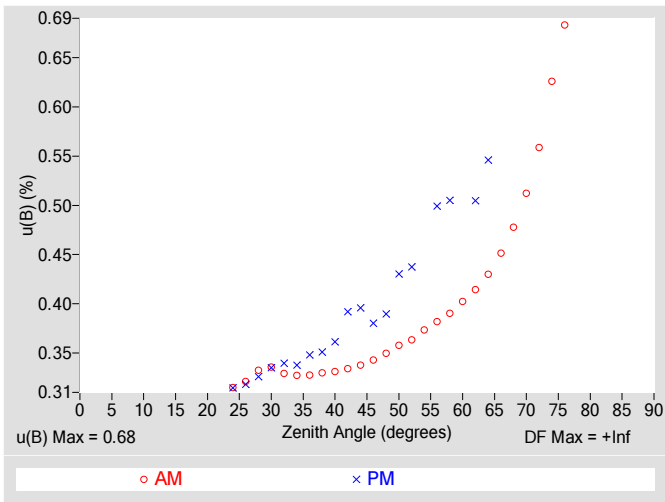


Table 2. Instrument Responsivity (R) and Calibration Type-B Standard Uncertainty, u(B)

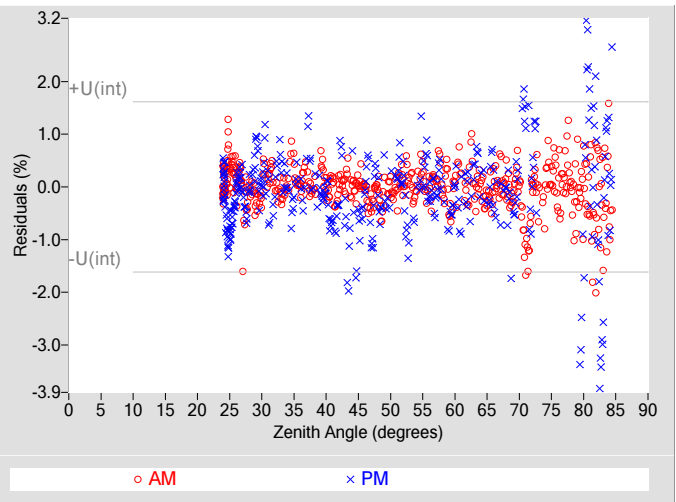
Zenith Angle (deg.)	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle	Zenith Angle (deg.)	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle
0	N/A	N/A	N/A	N/A	N/A	N/A	46	1051.4	0.34	108.28	1006.4	0.38	251.91
2	N/A	N/A	N/A	N/A	N/A	N/A	48	1059.9	0.35	105.92	999.28	0.39	254.23
4	N/A	N/A	N/A	N/A	N/A	N/A	50	1060.6	0.36	103.71	999.08	0.43	256.36
6	N/A	N/A	N/A	N/A	N/A	N/A	52	1071.3	0.36	101.69	1012.5	0.44	258.46
8	N/A	N/A	N/A	N/A	N/A	N/A	54	1077.3	0.37	99.67	1017.1	N/A	260.63
10	N/A	N/A	N/A	N/A	N/A	N/A	56	1083.1	0.38	97.78	1013.6	0.50	262.31
12	N/A	N/A	N/A	N/A	N/A	N/A	58	1096.9	0.39	95.94	1020.0	0.50	264.01
14	N/A	N/A	N/A	N/A	N/A	N/A	60	1102.5	0.40	94.22	1020.7	N/A	265.90
16	N/A	N/A	N/A	N/A	N/A	N/A	62	1105.1	0.41	92.44	1012.0	0.50	267.56
18	N/A	N/A	N/A	N/A	N/A	N/A	64	1117.7	0.43	90.81	1036.8	0.55	269.37
20	N/A	N/A	N/A	N/A	N/A	N/A	66	1125.6	0.45	89.12	1051.7	N/A	270.99
22	N/A	N/A	N/A	N/A	N/A	N/A	68	1139.2	0.48	87.46	1057.3	N/A	272.74
24	1052.8	0.31	174.66	1049.6	0.31	186.01	70	1131.8	0.51	85.87	1078.6	N/A	274.11
26	1050.5	0.32	153.98	1028.7	0.32	205.98	72	1100.1	0.56	84.24	1091.2	N/A	275.92
28	1017.8	0.33	144.51	1030.2	0.33	216.16	74	1099.9	0.63	82.60	N/A	N/A	N/A
30	1020.8	0.34	137.42	1030.2	0.33	223.01	76	1108.7	0.68	81.06	N/A	N/A	N/A
32	1031.4	0.33	131.55	1015.0	0.34	228.41	78	1102.3	N/A	79.40	N/A	N/A	N/A
34	1034.0	0.33	127.10	1016.0	0.34	233.00	80	1104.4	N/A	77.80	1085.5	N/A	282.47
36	1031.3	0.33	122.97	1005.5	0.35	237.43	82	1082.7	N/A	76.15	1135.2	N/A	284.07
38	1031.4	0.33	119.44	1011.6	0.35	240.63	84	1080.6	N/A	74.48	1129.4	N/A	285.74
40	1036.2	0.33	116.27	1008.0	0.36	243.83	86	N/A	N/A	N/A	N/A	N/A	N/A
42	1040.9	0.33	113.40	1005.5	0.39	246.62	88	N/A	N/A	N/A	N/A	N/A	N/A
44	1046.6	0.34	110.70	1019.2	0.40	249.65	90	N/A	N/A	N/A	N/A	N/A	N/A

N/A - Not Available

**Figure 3. Type-B Standard Uncertainty vs Zenith Angle**



**Figure 4. Residuals from Spline Interpolation**



**Table 3. Uncertainty using Spline Interpolation ‡**

Type-B Standard Uncertainty, $u(B)$ (%)	$\pm 0.68$
Type-A Interpolating Function, $u(int)$ (%)	$\pm 0.81$
Combined Standard Uncertainty, $u(c)$ (%)	$\pm 1.1$
Effective degrees of freedom, $DF(c)$	2203
Coverage factor, $k$	1.96
Expanded Uncertainty, $U95$ (%)	$\pm 2.1$
AM Valid zenith angle range	24° to 76°
PM Valid zenith angle range	24° to 64°

‡ An illustration for how to reduce the uncertainty in calculating the irradiance using a function rather than  $R@45^\circ$ . Not accredited.

**Table 4. Calibration Label Values**

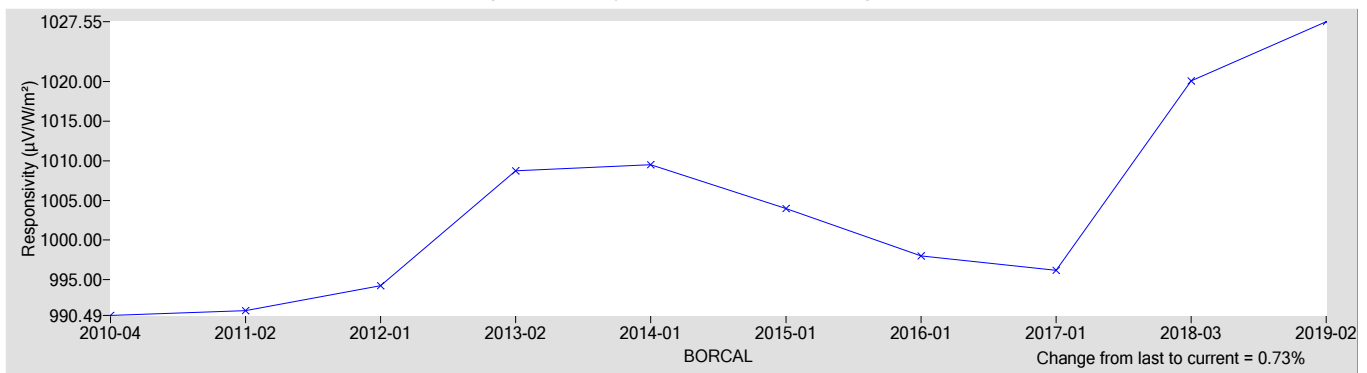
$R @ 45^\circ$ ( $\mu V/W/m^2$ )	$R_{net}$ ( $\mu V/W/m^2$ ) †
1027.5	0

†  $R_{net}$  determination date: N/A

**Table 5. Uncertainty using  $R @ 45^\circ$**

Type-B Expanded Uncertainty, $U(B)$ (%)	$\pm 0.99$
Offset Uncertainty, $U(off)$ (%)	+7.3 / -2.8
Expanded Uncertainty, $U$ (%)	+8.3 / -3.8
Effective degrees of freedom, $DF$	+Inf
Coverage factor, $k$	1.96
Valid zenith angle range	30.0° to 60.0°

**Figure 5. History of instrument at Zenith Angle = 45°**



**References:**

[1] Reda, I.; Hickey, J.; Long, C.; Myers, D.; Stoffel, T.; Wilcox, S.; Michalsky, J. J.; Dutton, E. G.; Nelson, D. (2005). "Using a Blackbody to Calculate Net Longwave Responsivity of Shortwave Solar Pyranometers to Correct for Their Thermal Offset Error During Outdoor Calibration Using the Component Sum Method." Journal of Atmospheric and Oceanic Technology. , 2005; pp. 1531-1540; NREL Report No. JA-560-36646. doi:10.1175/JTECH1782.1

[2] Reda, I.; Myers, D.; Stoffel, T. (2008). "Uncertainty Estimate for the Outdoor Calibration of Solar Pyranometers: A Metrologist Perspective." Measure. (NCSLI Journal of Measurement Science). Vol. 3(4), December 2008; pp. 58-66; NREL Report No. JA-581-4137

[3] Reda, I.; Andreas, A. (2004). "Solar Position Algorithm for Solar Radiation Applications." Solar Energy. Vol. 76(5), 2004; pp. 577-589; NREL Report No. JA-560-35518. doi:10.1016/j.solener.2003.12.003

[4] Stoffel, T.; Reda, I. (2009). "NREL Pyrheliometer Comparisons: 22 September - 3 October 2008 (NPC-2008)." 54 pp.; NREL Report No. TP-550-45016.

[5] Reda, I.; Stoffel, T.; Myers, D. (2003). "Method to Calibrate a Solar Pyranometer for Measuring Reference Diffuse Irradiance." Solar Energy. Vol. 74, 2003; pp. 103-112; NREL Report No. JA-560-35025. doi:10.1016/S0038-092X(03)00124-5

[6] Reda, I. (1996). Calibration of a Solar Absolute Cavity Radiometer with Traceability to the World Radiometric Reference. 79 pp.; NREL Report No. TP-463-20619.

[7] Reda, I.; Gröbner, J.; Stoffel, T.; Myers, D.; Forgan, B. (2008). Improvements in the Blackbody Calibration of Pyrgeometers. ARM 2008 Science Team Meeting (Poster).



# National Renewable Energy Laboratory

## Solar Radiation Research Laboratory

### Metrology Laboratory

### Calibration Certificate



<b>Test Instrument:</b>	Pyranometer	<b>Manufacturer:</b>	EKO
<b>Model:</b>	MS-802	<b>Serial Number:</b>	F14077R
<b>Calibration Date:</b>	5/3/2019	<b>Due Date:</b>	5/3/2020
<b>Customer:</b>	NREL-SRRL-BMS	<b>Environmental Conditions:</b>	see page 4
<b>Test Dates:</b>	5/3		

This certifies that the above product was calibrated in compliance with ISO/IEC 17025:2005. Measurement uncertainties at the time of calibration are consistent with the Guide to the Expression of Uncertainty in Measurement (GUM) using Reda et al., 2008. All nominal values are traceable to the International System (SI) Units of Measurement.

No statement of compliance with specifications is made or implied on this certificate. However, the estimated uncertainties are the uncertainties of the calibration process; users must add other uncertainties that are relevant to their measuring system, environmental and sky conditions, outdoor set-up, and site location.

The Type-B Standard Uncertainty of using the responsivity at each even zenith angle is reported, and the Expanded Uncertainty of the calibration is reported using two methods:

1. The Expanded Uncertainty of using the responsivity at zenith angle = 45°, within the zenith angle range from 30.0° to 60.0°
2. The Expanded Uncertainty of using Spline Interpolating Functions for the responsivity versus zenith angle.

This certificate applies only to the item identified above and shall not be reproduced other than in full, without specific written approval from the calibration facility. Certificate without signature is not valid.

**Table 1. Traceability**

Measurement Type	Instrument	Calibration Date	Calibration Due Date
Beam Irradiance †	Eppley Absolute Cavity Radiometer Model HF, S/N 29219	09/24/2018	09/24/2019
Diffuse Irradiance †	Hukseflux Pyranometer Model SR25, S/N 2541	04/19/2019	04/19/2020
Diffuse Irradiance †	Hukseflux Pyranometer Model SR25, S/N 2542	04/19/2019	04/19/2020
Data Acquisition	NREL Data Acquisition System Model RAP-DAQ, S/N 2005-998	02/14/2019	02/14/2021
Data Acquisition	NREL Data Acquisition System Model RAP-DAQ, S/N 2005-999	02/14/2019	02/14/2021
Infrared Irradiance ‡	Kipp & Zonen Pyrgeometer Model CG4, S/N FT002	04/16/2018	04/16/2022

† Through the World Radiometric Reference (WRR)

‡ Through the World Infrared Standard Group (WISG)

**Number of pages of certificate:** 4

**Calibration Procedure:** BORCAL-P00-Calibration and QA Procedure; available upon request.

**Setup:** Radiometers are calibrated outdoors, using the sun as the source. Pyranometers and pyrgeometers are installed for horizontal measurements, with their signal connectors oriented north, if their design permits.

The shading disk for the reference diffuse subtends a solid angle of 5°. Pyrheliometers are installed on solar trackers.

**Calibrated by:** RCC

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Ibrahim Reda, Technical Manager

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Date

For questions or comments, please contact the technical manager at:

ibrahim.reda@nrel.gov; 303-384-6385; 15013 Denver West Parkway, Golden, CO 80401, USA



# Calibration Results

## F14077R EKO MS-802

The responsivity ( $R$ ,  $\mu\text{V}/\text{W}/\text{m}^2$ ) of the test instrument during calibration is calculated using this Measurement Equation:

$$R = (V - R_{net} * W_{net}) / I \tag{1}$$

where,

- $V$  = radiometer output voltage (microvolts),
  - $R_{net}$  = radiometer net infrared responsivity ( $\mu\text{V}/\text{W}/\text{m}^2$ ), see Table 4,
  - $W_{net}$  = effective net infrared measured by pyrgeometer ( $\text{W}/\text{m}^2$ ),
  - =  $W_{in} - W_{out} = W_{in} - \sigma * T_c^4$
  - where,  $W_{in}$  = incoming infrared ( $\text{W}/\text{m}^2$ ),  $\sigma = 5.6704\text{e-}8 \text{ W}\cdot\text{m}^{-2}\cdot\text{K}^{-4}$ ,
  - $T_c$  = case temperature of pyrgeometer (K).
- $I$  = reference irradiance ( $\text{W}/\text{m}^2$ ), beam (B) or global (G)
  - where,  $G = B * \text{COS}(Z) + D$ ,
  - $Z$  = zenith angle (degrees),
  - $D$  = reference diffuse irradiance ( $\text{W}/\text{m}^2$ ).

Figure 1. Responsivity vs Zenith Angle

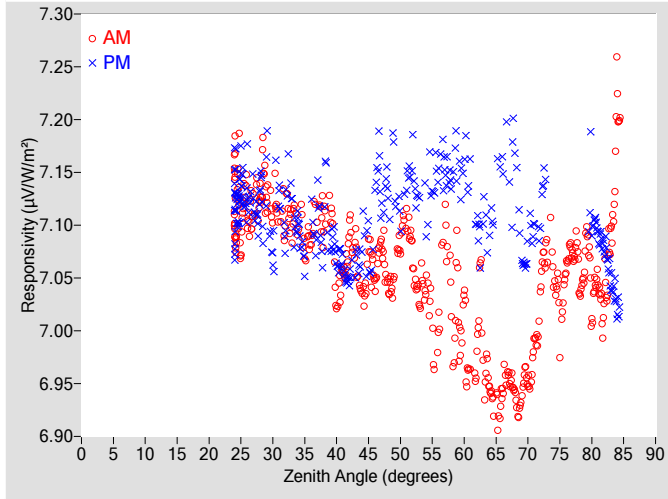


Figure 2. Responsivity vs Local Standard Time

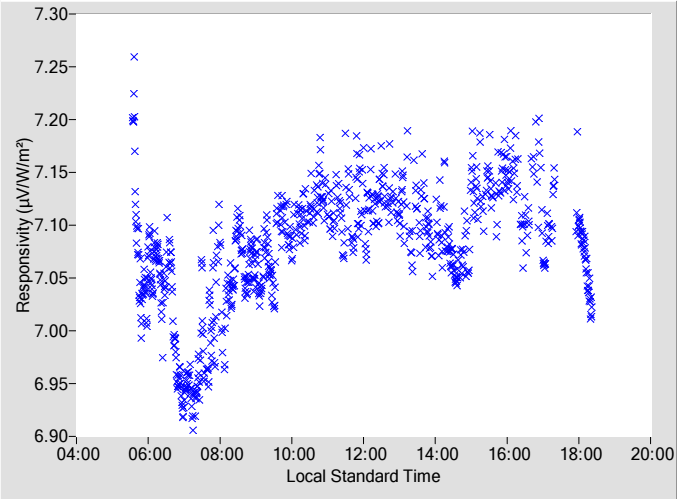


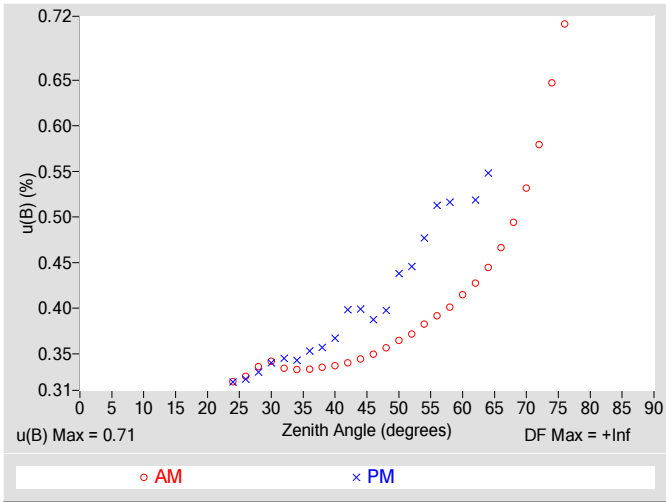
Table 2. Instrument Responsivity (R) and Calibration Type-B Standard Uncertainty, u(B)

Zenith Angle (deg.)	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle	Zenith Angle (deg.)	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle
0	N/A	N/A	N/A	N/A	N/A	N/A	46	7.0479	0.35	108.23	7.1368	0.39	252.01
2	N/A	N/A	N/A	N/A	N/A	N/A	48	7.0437	0.36	105.90	7.1329	0.40	254.21
4	N/A	N/A	N/A	N/A	N/A	N/A	50	7.0817	0.36	103.81	7.1116	0.44	256.30
6	N/A	N/A	N/A	N/A	N/A	N/A	52	7.0663	0.37	101.74	7.1598	0.45	258.41
8	N/A	N/A	N/A	N/A	N/A	N/A	54	7.0385	0.38	99.77	7.1098	0.48	260.49
10	N/A	N/A	N/A	N/A	N/A	N/A	56	6.9993	0.39	97.82	7.1474	0.51	262.28
12	N/A	N/A	N/A	N/A	N/A	N/A	58	7.0243	0.40	96.00	7.1450	0.52	264.12
14	N/A	N/A	N/A	N/A	N/A	N/A	60	7.0154	0.42	94.14	7.1655	N/A	265.99
16	N/A	N/A	N/A	N/A	N/A	N/A	62	6.9775	0.43	92.48	7.0989	0.52	267.67
18	N/A	N/A	N/A	N/A	N/A	N/A	64	6.9460	0.44	90.77	7.1033	0.55	269.47
20	N/A	N/A	N/A	N/A	N/A	N/A	66	6.9439	0.47	89.14	7.1566	N/A	271.05
22	N/A	N/A	N/A	N/A	N/A	N/A	68	6.9381	0.49	87.47	7.1747	N/A	272.65
24	7.1167	0.32	174.69	7.1208	0.32	185.37	70	6.9503	0.53	85.83	7.0741	N/A	274.17
26	7.1170	0.33	154.01	7.1202	0.32	205.85	72	7.0418	0.58	84.23	7.1120	N/A	275.96
28	7.1254	0.34	144.19	7.1382	0.33	216.00	74	7.0559	0.65	82.66	N/A	N/A	N/A
30	7.1084	0.34	137.76	7.0723	0.34	222.88	76	7.0588	0.71	81.03	N/A	N/A	N/A
32	7.1069	0.33	131.72	7.1036	0.34	228.39	78	7.0492	N/A	79.42	N/A	N/A	N/A
34	7.0934	0.33	127.12	7.0975	0.34	233.16	80	7.0297	N/A	77.81	7.1000	N/A	282.42
36	7.0844	0.33	123.00	7.1136	0.35	237.48	82	7.0294	N/A	76.16	7.0802	N/A	284.03
38	7.1055	0.34	119.40	7.1126	0.36	240.78	84	7.2087	N/A	74.50	7.0216	N/A	285.71
40	7.0274	0.34	116.33	7.0631	0.37	243.95	86	N/A	N/A	N/A	N/A	N/A	N/A
42	7.0907	0.34	113.35	7.0498	0.40	246.74	88	N/A	N/A	N/A	N/A	N/A	N/A
44	7.0346	0.34	110.61	7.0827	0.40	249.34	90	N/A	N/A	N/A	N/A	N/A	N/A

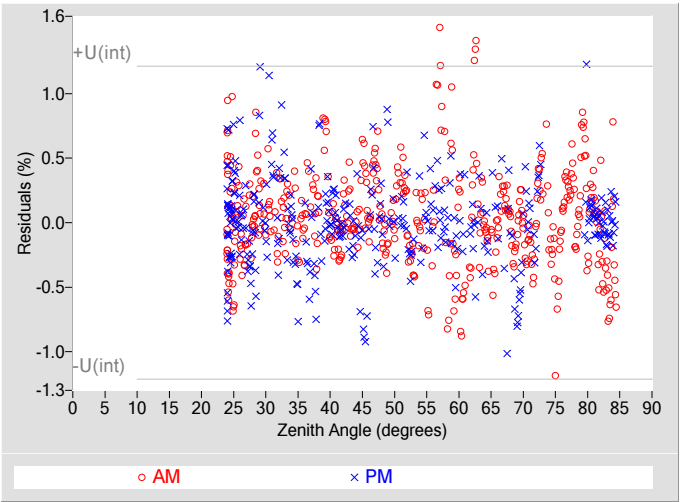
N/A - Not Available



**Figure 3. Type-B Standard Uncertainty vs Zenith Angle**



**Figure 4. Residuals from Spline Interpolation**



**Table 3. Uncertainty using Spline Interpolation ‡**

Type-B Standard Uncertainty, $u(B)$ (%)	$\pm 0.71$
Type-A Interpolating Function, $u(int)$ (%)	$\pm 0.61$
Combined Standard Uncertainty, $u(c)$ (%)	$\pm 0.93$
Effective degrees of freedom, $DF(c)$	3805
Coverage factor, $k$	1.96
Expanded Uncertainty, $U95$ (%)	$\pm 1.8$
AM Valid zenith angle range	24° to 76°
PM Valid zenith angle range	24° to 64°

‡ An illustration for how to reduce the uncertainty in calculating the irradiance using a function rather than  $R@45^\circ$ . Not accredited.

**Table 4. Calibration Label Values**

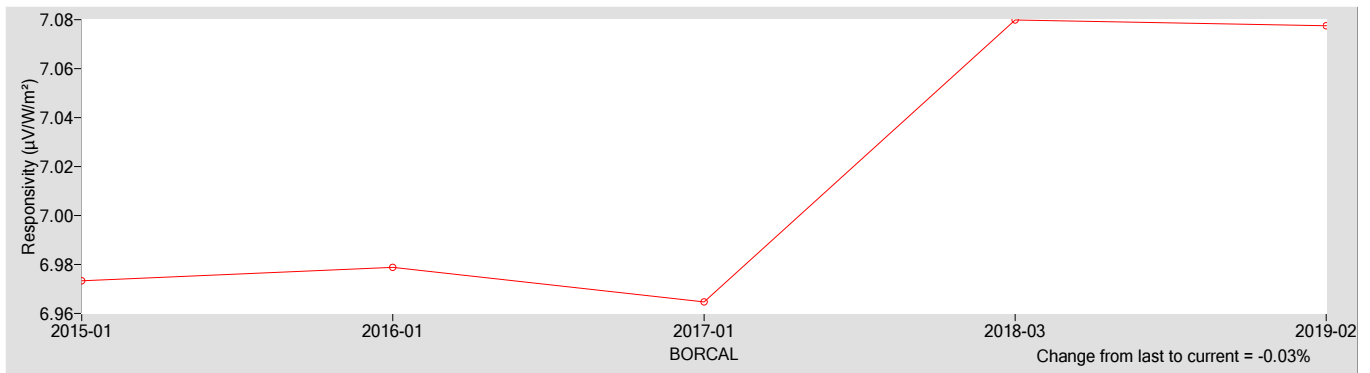
$R @ 45^\circ$ ( $\mu V/W/m^2$ )	$R_{net}$ ( $\mu V/W/m^2$ ) †
7.0776	0.18000

†  $R_{net}$  determination date: Estimated

**Table 5. Uncertainty using  $R @ 45^\circ$**

Type-B Expanded Uncertainty, $U(B)$ (%)	$\pm 1.0$
Offset Uncertainty, $U(off)$ (%)	+1.2 / -1.1
Expanded Uncertainty, $U$ (%)	+2.3 / -2.1
Effective degrees of freedom, $DF$	+Inf
Coverage factor, $k$	1.96
Valid zenith angle range	30.0° to 60.0°

**Figure 5. History of instrument at Zenith Angle = 45°**



**References:**

[1] Reda, I.; Hickey, J.; Long, C.; Myers, D.; Stoffel, T.; Wilcox, S.; Michalsky, J. J.; Dutton, E. G.; Nelson, D. (2005). "Using a Blackbody to Calculate Net Longwave Responsivity of Shortwave Solar Pyranometers to Correct for Their Thermal Offset Error During Outdoor Calibration Using the Component Sum Method." Journal of Atmospheric and Oceanic Technology. , 2005; pp. 1531-1540; NREL Report No. JA-560-36646. doi:10.1175/JTECH1782.1

[2] Reda, I.; Myers, D.; Stoffel, T. (2008). "Uncertainty Estimate for the Outdoor Calibration of Solar Pyranometers: A Metrologist Perspective." Measure. (NCSLI Journal of Measurement Science). Vol. 3(4), December 2008; pp. 58-66; NREL Report No. JA-581-4137

[3] Reda, I.; Andreas, A. (2004). "Solar Position Algorithm for Solar Radiation Applications." Solar Energy. Vol. 76(5), 2004; pp. 577-589; NREL Report No. JA-560-35518. doi:10.1016/j.solener.2003.12.003

[4] Stoffel, T.; Reda, I. (2009). "NREL Pyrheliometer Comparisons: 22 September - 3 October 2008 (NPC-2008)." 54 pp.; NREL Report No. TP-550-45016.

[5] Reda, I.; Stoffel, T.; Myers, D. (2003). "Method to Calibrate a Solar Pyranometer for Measuring Reference Diffuse Irradiance." Solar Energy. Vol. 74, 2003; pp. 103-112; NREL Report No. JA-560-35025. doi:10.1016/S0038-092X(03)00124-5

[6] Reda, I. (1996). Calibration of a Solar Absolute Cavity Radiometer with Traceability to the World Radiometric Reference. 79 pp.; NREL Report No. TP-463-20619.

[7] Reda, I.; Gröbner, J.; Stoffel, T.; Myers, D.; Forgan, B. (2008). Improvements in the Blackbody Calibration of Pyrgeometers. ARM 2008 Science Team Meeting (Poster).



# National Renewable Energy Laboratory

## Solar Radiation Research Laboratory

### Metrology Laboratory

### Calibration Certificate



<b>Test Instrument:</b>	Revised Silicon Pyranometer	<b>Manufacturer:</b>	Licor
<b>Model:</b>	LI200R	<b>Serial Number:</b>	PY100360
<b>Calibration Date:</b>	5/3/2019	<b>Due Date:</b>	5/3/2020
<b>Customer:</b>	NREL-SRRL-BMS	<b>Environmental Conditions:</b>	see page 4
<b>Test Dates:</b>	5/3		

This certifies that the above product was calibrated in compliance with ISO/IEC 17025:2005. Measurement uncertainties at the time of calibration are consistent with the Guide to the Expression of Uncertainty in Measurement (GUM) using Reda et al., 2008. All nominal values are traceable to the International System (SI) Units of Measurement.

No statement of compliance with specifications is made or implied on this certificate. However, the estimated uncertainties are the uncertainties of the calibration process; users must add other uncertainties that are relevant to their measuring system, environmental and sky conditions, outdoor set-up, and site location.

The Type-B Standard Uncertainty of using the responsivity at each even zenith angle is reported, and the Expanded Uncertainty of the calibration is reported using two methods:

1. The Expanded Uncertainty of using the responsivity at zenith angle = 45°, within the zenith angle range from 30.0° to 60.0°
2. The Expanded Uncertainty of using Spline Interpolating Functions for the responsivity versus zenith angle.

This certificate applies only to the item identified above and shall not be reproduced other than in full, without specific written approval from the calibration facility. Certificate without signature is not valid.

**Table 1. Traceability**

Measurement Type	Instrument	Calibration Date	Calibration Due Date
Beam Irradiance †	Eppley Absolute Cavity Radiometer Model HF, S/N 29219	09/24/2018	09/24/2019
Diffuse Irradiance †	Hukseflux Pyranometer Model SR25, S/N 2541	04/19/2019	04/19/2020
Diffuse Irradiance †	Hukseflux Pyranometer Model SR25, S/N 2542	04/19/2019	04/19/2020
Data Acquisition	NREL Data Acquisition System Model RAP-DAQ, S/N 2005-998	02/14/2019	02/14/2021
Data Acquisition	NREL Data Acquisition System Model RAP-DAQ, S/N 2005-999	02/14/2019	02/14/2021

† Through the World Radiometric Reference (WRR)

**Number of pages of certificate:** 4

**Calibration Procedure:** BORCAL-P00-Calibration and QA Procedure; available upon request.

**Setup:** Radiometers are calibrated outdoors, using the sun as the source. Pyranometers and pyrgeometers are installed for horizontal measurements, with their signal connectors oriented north, if their design permits.

The shading disk for the reference diffuse subtends a solid angle of 5°. Pyrheliometers are installed on solar trackers.

**Calibrated by:** RCC

-----  
Ibrahim Reda, Technical Manager

-----  
Date

For questions or comments, please contact the technical manager at:

ibrahim.reda@nrel.gov; 303-384-6385; 15013 Denver West Parkway, Golden, CO 80401, USA

# Calibration Results

PY100360 Licor LI200R

The responsivity ( $R$ ,  $\mu\text{V}/\text{W}/\text{m}^2$ ) of the test instrument during calibration is calculated using this Measurement Equation:

$$R = (V - R_{net} * W_{net}) / I \quad [1]$$

where,

- $V$  = radiometer output voltage (microvolts),
- $R_{net}$  = radiometer net infrared responsivity ( $\mu\text{V}/\text{W}/\text{m}^2$ ), see Table 4,
- $W_{net}$  = effective net infrared measured by pyrgeometer ( $\text{W}/\text{m}^2$ ),
- =  $W_{in} - W_{out} = W_{in} - \sigma * T_c^4$
- where,  $W_{in}$  = incoming infrared ( $\text{W}/\text{m}^2$ ),  $\sigma = 5.6704\text{e-}8 \text{ W}\cdot\text{m}^{-2}\cdot\text{K}^{-4}$ ,
- $T_c$  = case temperature of pyrgeometer (K).
- $I$  = reference irradiance ( $\text{W}/\text{m}^2$ ), beam (B) or global (G)
- where,  $G = B * \text{COS}(Z) + D$ ,
- $Z$  = zenith angle (degrees),
- $D$  = reference diffuse irradiance ( $\text{W}/\text{m}^2$ ).

Figure 1. Responsivity vs Zenith Angle

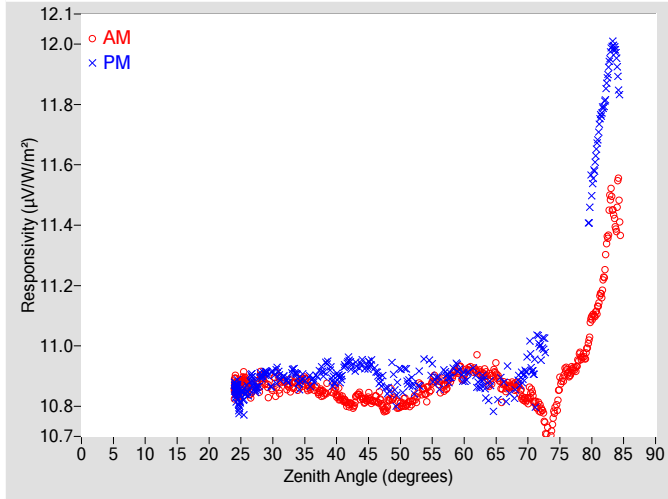


Figure 2. Responsivity vs Local Standard Time

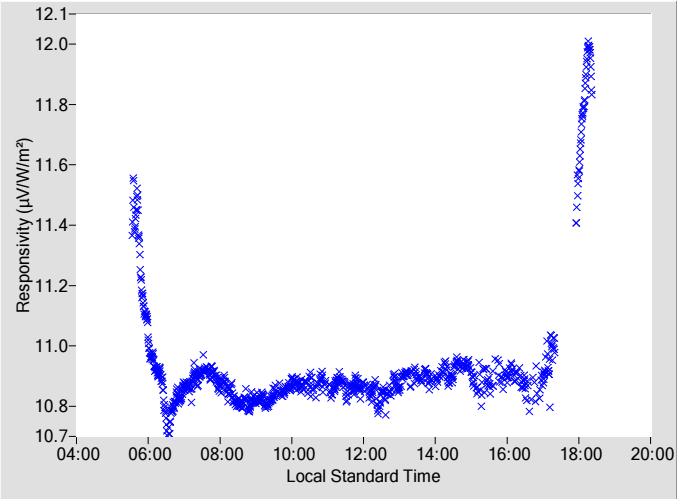


Table 2. Instrument Responsivity (R) and Calibration Type-B Standard Uncertainty, u(B)

Zenith Angle (deg.)	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	AM u(B) $\pm$ (%)	Azimuth Angle	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	PM u(B) $\pm$ (%)	Azimuth Angle	Zenith Angle (deg.)	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	AM u(B) $\pm$ (%)	Azimuth Angle	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	PM u(B) $\pm$ (%)	Azimuth Angle
0	N/A	N/A	N/A	N/A	N/A	N/A	46	10.823	0.34	108.12	10.920	0.38	251.96
2	N/A	N/A	N/A	N/A	N/A	N/A	48	10.806	0.35	105.89	10.854	0.39	254.20
4	N/A	N/A	N/A	N/A	N/A	N/A	50	10.802	0.36	103.74	10.923	0.43	256.34
6	N/A	N/A	N/A	N/A	N/A	N/A	52	10.818	0.36	101.72	10.869	0.44	258.41
8	N/A	N/A	N/A	N/A	N/A	N/A	54	10.843	0.37	99.73	N/A	N/A	N/A
10	N/A	N/A	N/A	N/A	N/A	N/A	56	10.866	0.38	97.70	10.878	0.50	262.32
12	N/A	N/A	N/A	N/A	N/A	N/A	58	10.894	0.39	95.94	10.911	0.51	264.15
14	N/A	N/A	N/A	N/A	N/A	N/A	60	10.897	0.40	94.25	10.892	N/A	265.89
16	N/A	N/A	N/A	N/A	N/A	N/A	62	10.929	0.42	92.52	10.881	0.51	267.66
18	N/A	N/A	N/A	N/A	N/A	N/A	64	10.887	0.43	90.78	10.857	0.54	269.36
20	N/A	N/A	N/A	N/A	N/A	N/A	66	10.859	0.45	89.10	10.887	N/A	271.02
22	N/A	N/A	N/A	N/A	N/A	N/A	68	10.865	0.48	87.48	10.840	N/A	272.64
24	10.865	0.32	174.34	10.852	0.32	186.43	70	10.829	0.52	85.85	10.990	N/A	274.36
26	10.869	0.32	154.44	10.849	0.32	206.07	72	10.790	0.56	84.26	10.991	N/A	275.87
28	10.886	0.33	143.99	10.893	0.33	215.87	74	10.762	0.63	82.65	N/A	N/A	N/A
30	10.875	0.34	137.05	10.900	0.34	222.72	76	10.920	0.69	81.04	N/A	N/A	N/A
32	10.873	0.33	131.60	10.892	0.34	228.69	78	10.959	N/A	79.43	N/A	N/A	N/A
34	10.874	0.33	127.01	10.885	0.34	233.09	80	11.093	N/A	77.78	11.539	N/A	282.43
36	10.865	0.33	123.07	10.886	0.35	237.15	82	11.261	N/A	76.12	11.812	N/A	284.04
38	10.844	0.33	119.48	10.918	0.35	240.68	84	11.468	N/A	74.46	11.918	N/A	285.72
40	10.844	0.33	116.31	10.896	0.36	243.85	86	N/A	N/A	N/A	N/A	N/A	N/A
42	10.808	0.34	113.32	10.947	0.39	246.74	88	N/A	N/A	N/A	N/A	N/A	N/A
44	10.825	0.34	110.71	10.945	0.39	249.29	90	N/A	N/A	N/A	N/A	N/A	N/A

N/A - Not Available

Figure 3. Type-B Standard Uncertainty vs Zenith Angle

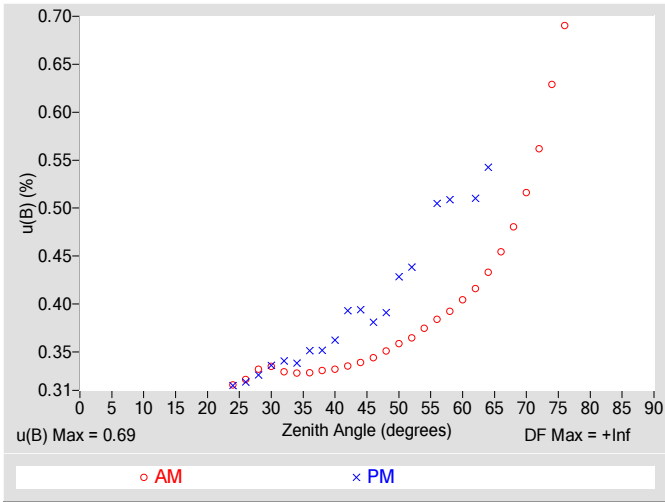


Figure 4. Residuals from Spline Interpolation

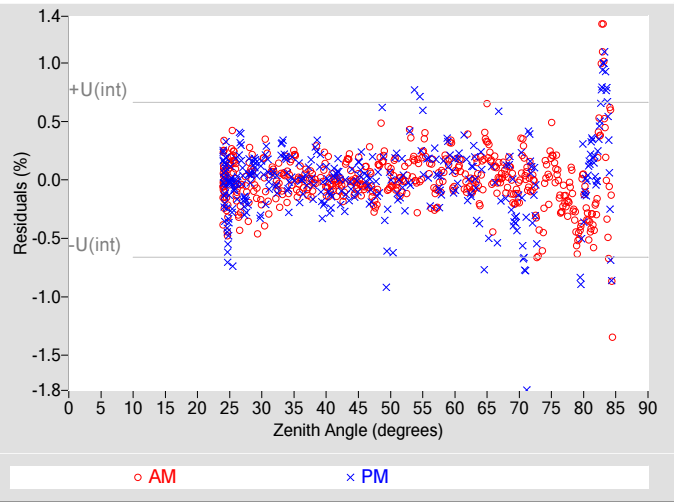


Table 3. Uncertainty using Spline Interpolation ‡

Type-B Standard Uncertainty, u(B) (%)	±0.69
Type-A Interpolating Function, u(int) (%)	±0.33
Combined Standard Uncertainty, u(c) (%)	±0.77
Effective degrees of freedom, DF(c)	19950
Coverage factor, k	1.96
Expanded Uncertainty, U95 (%)	±1.5
AM Valid zenith angle range	24° to 76°
PM Valid zenith angle range	24° to 64°

‡ An illustration for how to reduce the uncertainty in calculating the irradiance using a function rather than R@45°. Not accredited.

Table 4. Calibration Label Values

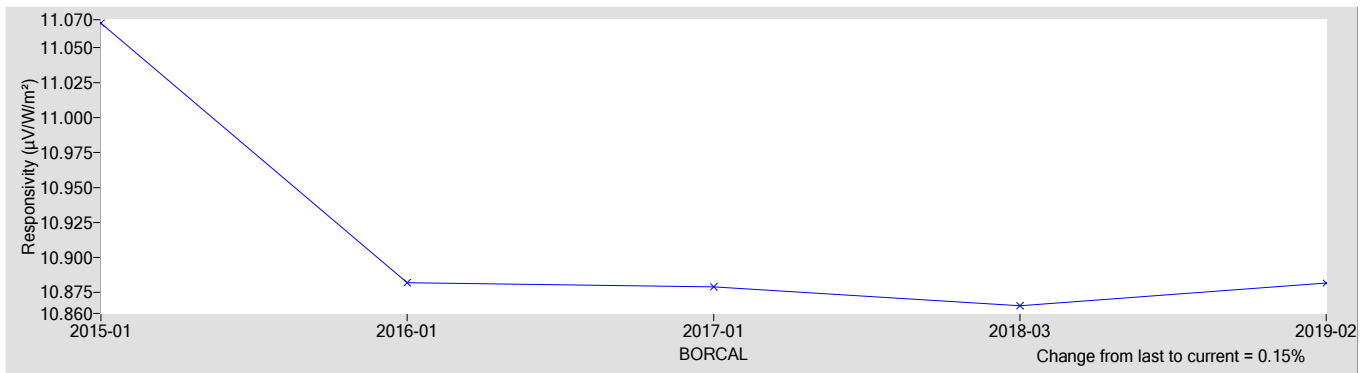
R @ 45° (μV/W/m²)	Rnet (μV/W/m²) †
10.882	0

† Rnet determination date: N/A

Table 5. Uncertainty using R @ 45°

Type-B Expanded Uncertainty, U(B) (%)	±1.00
Offset Uncertainty, U(off) (%)	+0.60 / -0.73
Expanded Uncertainty, U (%)	+1.6 / -1.7
Effective degrees of freedom, DF	+Inf
Coverage factor, k	1.96
Valid zenith angle range	30.0° to 60.0°

Figure 5. History of instrument at Zenith Angle = 45°



References:

[1] Reda, I.; Hickey, J.; Long, C.; Myers, D.; Stoffel, T.; Wilcox, S.; Michalsky, J. J.; Dutton, E. G.; Nelson, D. (2005). "Using a Blackbody to Calculate Net Longwave Responsivity of Shortwave Solar Pyranometers to Correct for Their Thermal Offset Error During Outdoor Calibration Using the Component Sum Method." Journal of Atmospheric and Oceanic Technology. , 2005; pp. 1531-1540; NREL Report No. JA-560-36646. doi:10.1175/JTECH1782.1

[2] Reda, I.; Myers, D.; Stoffel, T. (2008). "Uncertainty Estimate for the Outdoor Calibration of Solar Pyranometers: A Metrologist Perspective." Measure. (NCSLI Journal of Measurement Science). Vol. 3(4), December 2008; pp. 58-66; NREL Report No. JA-581-4137

[3] Reda, I.; Andreas, A. (2004). "Solar Position Algorithm for Solar Radiation Applications." Solar Energy. Vol. 76(5), 2004; pp. 577-589; NREL Report No. JA-560-35518. doi:10.1016/j.solener.2003.12.003

[4] Stoffel, T.; Reda, I. (2009). "NREL Pyrheliometer Comparisons: 22 September - 3 October 2008 (NPC-2008)." 54 pp.; NREL Report No. TP-550-45016.

[5] Reda, I.; Stoffel, T.; Myers, D. (2003). "Method to Calibrate a Solar Pyranometer for Measuring Reference Diffuse Irradiance." Solar Energy. Vol. 74, 2003; pp. 103-112; NREL Report No. JA-560-35025. doi:10.1016/S0038-092X(03)00124-5

[6] Reda, I. (1996). Calibration of a Solar Absolute Cavity Radiometer with Traceability to the World Radiometric Reference. 79 pp.; NREL Report No. TP-463-20619.

[7] Reda, I.; Gröbner, J.; Stoffel, T.; Myers, D.; Forgan, B. (2008). Improvements in the Blackbody Calibration of Pyrgometers. ARM 2008 Science Team Meeting (Poster).



# National Renewable Energy Laboratory

## Solar Radiation Research Laboratory

### Metrology Laboratory

### Calibration Certificate



<b>Test Instrument:</b>	Revised Silicon Pyranometer	<b>Manufacturer:</b>	Licor
<b>Model:</b>	LI200R	<b>Serial Number:</b>	PY102022
<b>Calibration Date:</b>	5/3/2019	<b>Due Date:</b>	5/3/2020
<b>Customer:</b>	NREL-SRRL-BMS	<b>Environmental Conditions:</b>	see page 4
<b>Test Dates:</b>	5/3		

This certifies that the above product was calibrated in compliance with ISO/IEC 17025:2005. Measurement uncertainties at the time of calibration are consistent with the Guide to the Expression of Uncertainty in Measurement (GUM) using Reda et al., 2008. All nominal values are traceable to the International System (SI) Units of Measurement.

No statement of compliance with specifications is made or implied on this certificate. However, the estimated uncertainties are the uncertainties of the calibration process; users must add other uncertainties that are relevant to their measuring system, environmental and sky conditions, outdoor set-up, and site location.

The Type-B Standard Uncertainty of using the responsivity at each even zenith angle is reported, and the Expanded Uncertainty of the calibration is reported using two methods:

1. The Expanded Uncertainty of using the responsivity at zenith angle = 45°, within the zenith angle range from 30.0° to 60.0°
2. The Expanded Uncertainty of using Spline Interpolating Functions for the responsivity versus zenith angle.

This certificate applies only to the item identified above and shall not be reproduced other than in full, without specific written approval from the calibration facility. Certificate without signature is not valid.

**Table 1. Traceability**

Measurement Type	Instrument	Calibration Date	Calibration Due Date
Beam Irradiance †	Eppley Absolute Cavity Radiometer Model HF, S/N 29219	09/24/2018	09/24/2019
Diffuse Irradiance †	Hukseflux Pyranometer Model SR25, S/N 2541	04/19/2019	04/19/2020
Diffuse Irradiance †	Hukseflux Pyranometer Model SR25, S/N 2542	04/19/2019	04/19/2020
Data Acquisition	NREL Data Acquisition System Model RAP-DAQ, S/N 2005-998	02/14/2019	02/14/2021
Data Acquisition	NREL Data Acquisition System Model RAP-DAQ, S/N 2005-999	02/14/2019	02/14/2021

† Through the World Radiometric Reference (WRR)

**Number of pages of certificate:** 4

**Calibration Procedure:** BORCAL-P00-Calibration and QA Procedure; available upon request.

**Setup:** Radiometers are calibrated outdoors, using the sun as the source. Pyranometers and pyrgeometers are installed for horizontal measurements, with their signal connectors oriented north, if their design permits.  
The shading disk for the reference diffuse subtends a solid angle of 5°. Pyrheliometers are installed on solar trackers.

**Calibrated by:** RCC

-----  
Ibrahim Reda, Technical Manager

-----  
Date

For questions or comments, please contact the technical manager at:  
ibrahim.reda@nrel.gov; 303-384-6385; 15013 Denver West Parkway, Golden, CO 80401, USA

# Calibration Results

## PY102022 Licor LI200R

The responsivity ( $R$ ,  $\mu\text{V}/\text{W}/\text{m}^2$ ) of the test instrument during calibration is calculated using this Measurement Equation:

$$R = (V - R_{net} * W_{net}) / I \quad [1]$$

where,

- $V$  = radiometer output voltage (microvolts),
- $R_{net}$  = radiometer net infrared responsivity ( $\mu\text{V}/\text{W}/\text{m}^2$ ), see Table 4,
- $W_{net}$  = effective net infrared measured by pyrgeometer ( $\text{W}/\text{m}^2$ ),
- =  $W_{in} - W_{out} = W_{in} - \sigma * T_c^4$
- where,  $W_{in}$  = incoming infrared ( $\text{W}/\text{m}^2$ ),  $\sigma = 5.6704\text{e-}8 \text{ W}\cdot\text{m}^{-2}\cdot\text{K}^{-4}$ ,
- $T_c$  = case temperature of pyrgeometer (K).
- $I$  = reference irradiance ( $\text{W}/\text{m}^2$ ), beam (B) or global (G)
- where,  $G = B * \text{COS}(Z) + D$ ,
- $Z$  = zenith angle (degrees),
- $D$  = reference diffuse irradiance ( $\text{W}/\text{m}^2$ ).

Figure 1. Responsivity vs Zenith Angle

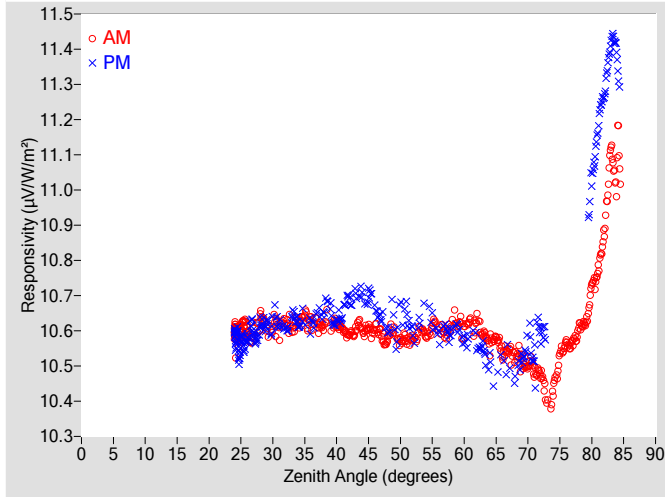


Figure 2. Responsivity vs Local Standard Time

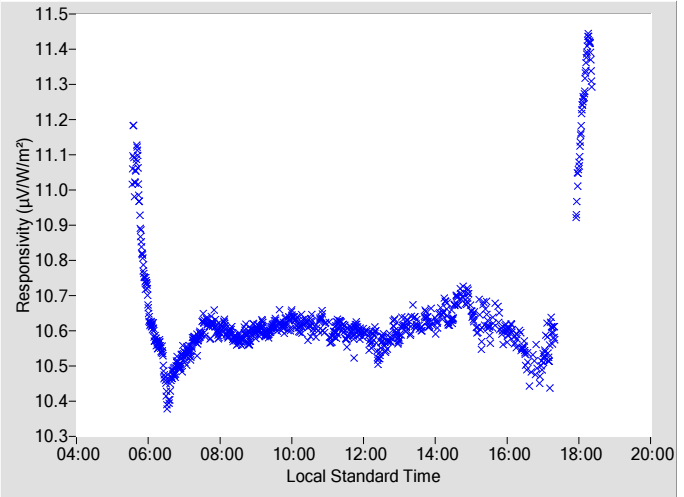
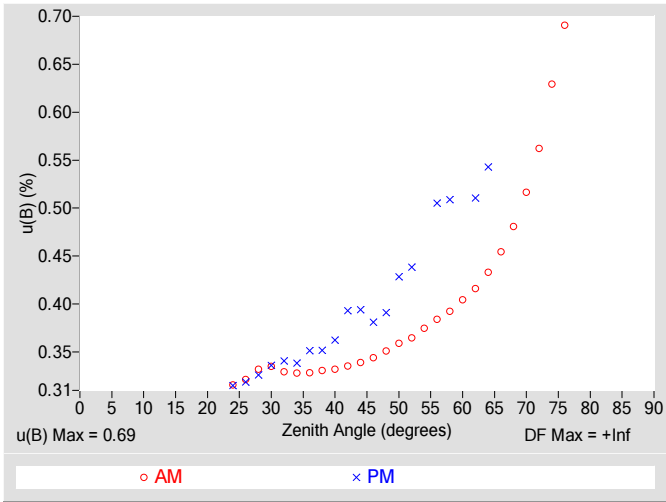


Table 2. Instrument Responsivity (R) and Calibration Type-B Standard Uncertainty, u(B)

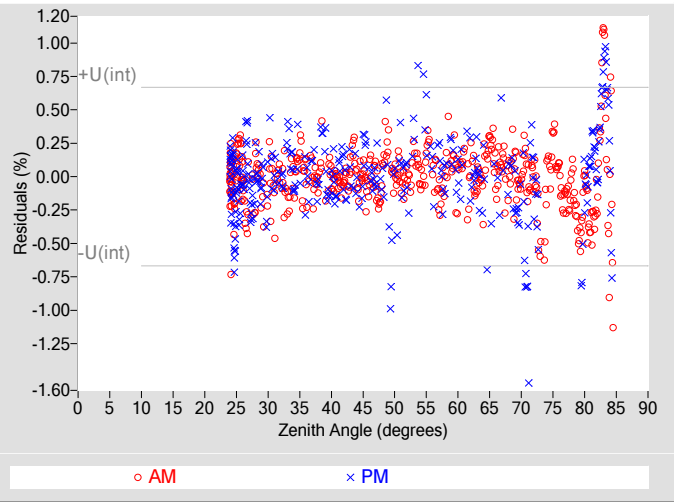
Zenith Angle (deg.)	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle	Zenith Angle (deg.)	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle
0	N/A	N/A	N/A	N/A	N/A	N/A	46	10.607	0.34	108.12	10.665	0.38	251.96
2	N/A	N/A	N/A	N/A	N/A	N/A	48	10.577	0.35	105.89	10.602	0.39	254.20
4	N/A	N/A	N/A	N/A	N/A	N/A	50	10.571	0.36	103.74	10.678	0.43	256.34
6	N/A	N/A	N/A	N/A	N/A	N/A	52	10.579	0.36	101.72	10.594	0.44	258.41
8	N/A	N/A	N/A	N/A	N/A	N/A	54	10.589	0.37	99.73	N/A	N/A	N/A
10	N/A	N/A	N/A	N/A	N/A	N/A	56	10.602	0.38	97.70	10.583	0.51	262.32
12	N/A	N/A	N/A	N/A	N/A	N/A	58	10.613	0.39	95.94	10.600	0.51	264.15
14	N/A	N/A	N/A	N/A	N/A	N/A	60	10.605	0.40	94.25	10.571	N/A	265.89
16	N/A	N/A	N/A	N/A	N/A	N/A	62	10.623	0.42	92.52	10.563	0.51	267.66
18	N/A	N/A	N/A	N/A	N/A	N/A	64	10.567	0.43	90.78	10.513	0.54	269.36
20	N/A	N/A	N/A	N/A	N/A	N/A	66	10.536	0.45	89.10	10.523	N/A	271.02
22	N/A	N/A	N/A	N/A	N/A	N/A	68	10.529	0.48	87.48	10.461	N/A	272.64
24	10.600	0.32	174.45	10.582	0.32	186.43	70	10.500	0.52	85.85	10.605	N/A	274.36
26	10.599	0.32	154.44	10.576	0.32	206.07	72	10.476	0.56	84.26	10.595	N/A	275.87
28	10.630	0.33	143.99	10.613	0.33	215.87	74	10.435	0.63	82.65	N/A	N/A	N/A
30	10.618	0.34	137.05	10.630	0.34	222.72	76	10.564	0.69	81.04	N/A	N/A	N/A
32	10.626	0.33	131.60	10.606	0.34	228.69	78	10.606	N/A	79.43	N/A	N/A	N/A
34	10.625	0.33	127.01	10.622	0.34	233.09	80	10.728	N/A	77.78	11.041	N/A	282.43
36	10.626	0.33	123.07	10.621	0.35	237.15	82	10.899	N/A	76.12	11.279	N/A	284.04
38	10.613	0.33	119.48	10.657	0.35	240.68	84	11.093	N/A	74.46	11.365	N/A	285.72
40	10.621	0.33	116.31	10.626	0.36	243.85	86	N/A	N/A	N/A	N/A	N/A	N/A
42	10.591	0.34	113.32	10.688	0.39	246.74	88	N/A	N/A	N/A	N/A	N/A	N/A
44	10.602	0.34	110.71	10.710	0.39	249.29	90	N/A	N/A	N/A	N/A	N/A	N/A

N/A - Not Available

**Figure 3. Type-B Standard Uncertainty vs Zenith Angle**



**Figure 4. Residuals from Spline Interpolation**



**Table 3. Uncertainty using Spline Interpolation ‡**

Type-B Standard Uncertainty, u(B) (%)	±0.69
Type-A Interpolating Function, u(int) (%)	±0.33
Combined Standard Uncertainty, u(c) (%)	±0.77
Effective degrees of freedom, DF(c)	19316
Coverage factor, k	1.96
Expanded Uncertainty, U95 (%)	±1.5
AM Valid zenith angle range	24° to 76°
PM Valid zenith angle range	24° to 64°

‡ An illustration for how to reduce the uncertainty in calculating the irradiance using a function rather than R@45°. Not accredited.

**Table 4. Calibration Label Values**

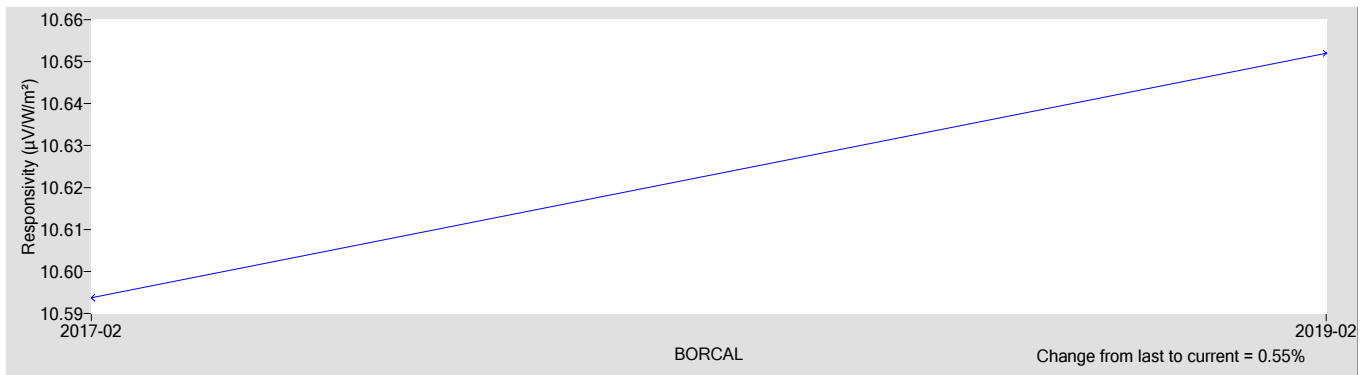
R @ 45° (μV/W/m²)	Rnet (μV/W/m²) †
10.652	0

† Rnet determination date: N/A

**Table 5. Uncertainty using R @ 45°**

Type-B Expanded Uncertainty, U(B) (%)	±1.00
Offset Uncertainty, U(off) (%)	+0.55 / -0.76
Expanded Uncertainty, U (%)	+1.5 / -1.8
Effective degrees of freedom, DF	+Inf
Coverage factor, k	1.96
Valid zenith angle range	30.0° to 60.0°

**Figure 5. History of instrument at Zenith Angle = 45°**



**References:**

[1] Reda, I.; Hickey, J.; Long, C.; Myers, D.; Stoffel, T.; Wilcox, S.; Michalsky, J. J.; Dutton, E. G.; Nelson, D. (2005). "Using a Blackbody to Calculate Net Longwave Responsivity of Shortwave Solar Pyranometers to Correct for Their Thermal Offset Error During Outdoor Calibration Using the Component Sum Method." Journal of Atmospheric and Oceanic Technology. , 2005; pp. 1531-1540; NREL Report No. JA-560-36646. doi:10.1175/JTECH1782.1

[2] Reda, I.; Myers, D.; Stoffel, T. (2008). "Uncertainty Estimate for the Outdoor Calibration of Solar Pyranometers: A Metrologist Perspective." Measure. (NCSLI Journal of Measurement Science). Vol. 3(4), December 2008; pp. 58-66; NREL Report No. JA-581-4137

[3] Reda, I.; Andreas, A. (2004). "Solar Position Algorithm for Solar Radiation Applications." Solar Energy. Vol. 76(5), 2004; pp. 577-589; NREL Report No. JA-560-35518. doi:10.1016/j.solener.2003.12.003

[4] Stoffel, T.; Reda, I. (2009). "NREL Pyrheliometer Comparisons: 22 September - 3 October 2008 (NPC-2008)." 54 pp.; NREL Report No. TP-550-45016.

[5] Reda, I.; Stoffel, T.; Myers, D. (2003). "Method to Calibrate a Solar Pyranometer for Measuring Reference Diffuse Irradiance." Solar Energy. Vol. 74, 2003; pp. 103-112; NREL Report No. JA-560-35025. doi:10.1016/S0038-092X(03)00124-5

[6] Reda, I. (1996). Calibration of a Solar Absolute Cavity Radiometer with Traceability to the World Radiometric Reference. 79 pp.; NREL Report No. TP-463-20619.

[7] Reda, I.; Gröbner, J.; Stoffel, T.; Myers, D.; Forgan, B. (2008). Improvements in the Blackbody Calibration of Pyrgometers. ARM 2008 Science Team Meeting (Poster).



# National Renewable Energy Laboratory

## Solar Radiation Research Laboratory

### Metrology Laboratory

### Calibration Certificate



<b>Test Instrument:</b>	Silicon Pyranometer	<b>Manufacturer:</b>	Licor
<b>Model:</b>	LI200	<b>Serial Number:</b>	PY28257
<b>Calibration Date:</b>	5/3/2019	<b>Due Date:</b>	5/3/2020
<b>Customer:</b>	NREL-SRRL-BMS	<b>Environmental Conditions:</b>	see page 4
<b>Test Dates:</b>	5/3		

This certifies that the above product was calibrated in compliance with ISO/IEC 17025:2005. Measurement uncertainties at the time of calibration are consistent with the Guide to the Expression of Uncertainty in Measurement (GUM) using Reda et al., 2008. All nominal values are traceable to the International System (SI) Units of Measurement.

No statement of compliance with specifications is made or implied on this certificate. However, the estimated uncertainties are the uncertainties of the calibration process; users must add other uncertainties that are relevant to their measuring system, environmental and sky conditions, outdoor set-up, and site location.

The Type-B Standard Uncertainty of using the responsivity at each even zenith angle is reported, and the Expanded Uncertainty of the calibration is reported using two methods:

1. The Expanded Uncertainty of using the responsivity at zenith angle = 45°, within the zenith angle range from 30.0° to 60.0°
2. The Expanded Uncertainty of using Spline Interpolating Functions for the responsivity versus zenith angle.

This certificate applies only to the item identified above and shall not be reproduced other than in full, without specific written approval from the calibration facility. Certificate without signature is not valid.

**Table 1. Traceability**

Measurement Type	Instrument	Calibration Date	Calibration Due Date
Beam Irradiance †	Eppley Absolute Cavity Radiometer Model HF, S/N 29219	09/24/2018	09/24/2019
Diffuse Irradiance †	Hukseflux Pyranometer Model SR25, S/N 2541	04/19/2019	04/19/2020
Diffuse Irradiance †	Hukseflux Pyranometer Model SR25, S/N 2542	04/19/2019	04/19/2020
Data Acquisition	NREL Data Acquisition System Model RAP-DAQ, S/N 2005-998	02/14/2019	02/14/2021
Data Acquisition	NREL Data Acquisition System Model RAP-DAQ, S/N 2005-999	02/14/2019	02/14/2021

† Through the World Radiometric Reference (WRR)

**Number of pages of certificate:** 4

**Calibration Procedure:** BORCAL-P00-Calibration and QA Procedure; available upon request.

**Setup:** Radiometers are calibrated outdoors, using the sun as the source. Pyranometers and pyrgeometers are installed for horizontal measurements, with their signal connectors oriented north, if their design permits.

The shading disk for the reference diffuse subtends a solid angle of 5°. Pyrheliometers are installed on solar trackers.

**Calibrated by:** RCC

-----  
Ibrahim Reda, Technical Manager

-----  
Date

For questions or comments, please contact the technical manager at:

ibrahim.reda@nrel.gov; 303-384-6385; 15013 Denver West Parkway, Golden, CO 80401, USA



# Calibration Results

## PY28257 Licor LI200

The responsivity ( $R$ ,  $\mu\text{V}/\text{W}/\text{m}^2$ ) of the test instrument during calibration is calculated using this Measurement Equation:

$$R = (V - R_{net} * W_{net}) / I \quad [1]$$

where,

- $V$  = radiometer output voltage (microvolts),
  - $R_{net}$  = radiometer net infrared responsivity ( $\mu\text{V}/\text{W}/\text{m}^2$ ), see Table 4,
  - $W_{net}$  = effective net infrared measured by pyrgeometer ( $\text{W}/\text{m}^2$ ),
  - =  $W_{in} - W_{out} = W_{in} - \sigma * T_c^4$
  - where,  $W_{in}$  = incoming infrared ( $\text{W}/\text{m}^2$ ),  $\sigma = 5.6704\text{e-}8 \text{ W}\cdot\text{m}^{-2}\cdot\text{K}^{-4}$ ,
  - $T_c$  = case temperature of pyrgeometer (K).
- $I$  = reference irradiance ( $\text{W}/\text{m}^2$ ), beam (B) or global (G)  
 where,  $G = B * \text{COS}(Z) + D$ ,  
 $Z$  = zenith angle (degrees),  
 $D$  = reference diffuse irradiance ( $\text{W}/\text{m}^2$ ).

Figure 1. Responsivity vs Zenith Angle

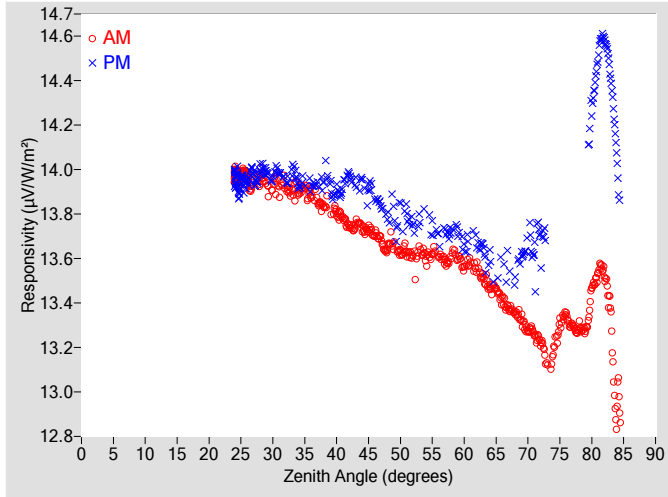


Figure 2. Responsivity vs Local Standard Time

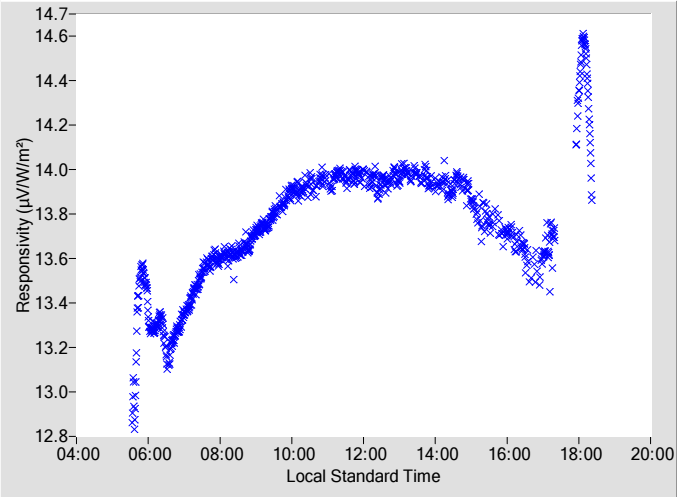


Table 2. Instrument Responsivity (R) and Calibration Type-B Standard Uncertainty, u(B)

Zenith Angle (deg.)	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle	Zenith Angle (deg.)	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle
0	N/A	N/A	N/A	N/A	N/A	N/A	46	13.709	0.34	108.12	13.862	0.38	251.96
2	N/A	N/A	N/A	N/A	N/A	N/A	48	13.650	0.35	105.89	13.786	0.39	254.20
4	N/A	N/A	N/A	N/A	N/A	N/A	50	13.626	0.36	103.74	13.851	0.43	256.34
6	N/A	N/A	N/A	N/A	N/A	N/A	52	13.616	0.36	101.72	13.751	0.44	258.41
8	N/A	N/A	N/A	N/A	N/A	N/A	54	13.606	0.37	99.73	N/A	N/A	N/A
10	N/A	N/A	N/A	N/A	N/A	N/A	56	13.611	0.38	97.70	13.693	0.50	262.32
12	N/A	N/A	N/A	N/A	N/A	N/A	58	13.618	0.39	95.94	13.729	0.51	264.15
14	N/A	N/A	N/A	N/A	N/A	N/A	60	13.559	0.40	94.25	13.645	N/A	265.89
16	N/A	N/A	N/A	N/A	N/A	N/A	62	13.558	0.42	92.52	13.675	0.51	267.66
18	N/A	N/A	N/A	N/A	N/A	N/A	64	13.469	0.43	90.78	13.598	0.54	269.36
20	N/A	N/A	N/A	N/A	N/A	N/A	66	13.414	0.45	89.10	13.591	N/A	271.02
22	N/A	N/A	N/A	N/A	N/A	N/A	68	13.355	0.48	87.48	13.499	N/A	272.64
24	13.974	0.32	174.34	13.961	0.31	186.43	70	13.279	0.52	85.85	13.727	N/A	274.36
26	13.969	0.32	154.44	13.947	0.32	206.07	72	13.226	0.56	84.26	13.680	N/A	275.87
28	13.963	0.33	143.99	13.995	0.33	215.87	74	13.184	0.63	82.65	N/A	N/A	N/A
30	13.935	0.33	137.05	13.964	0.34	222.72	76	13.346	0.69	81.04	N/A	N/A	N/A
32	13.928	0.33	131.60	13.955	0.34	228.69	78	13.286	N/A	79.43	N/A	N/A	N/A
34	13.904	0.33	127.01	13.936	0.34	233.09	80	13.461	N/A	77.78	14.293	N/A	282.43
36	13.889	0.33	123.07	13.930	0.35	237.15	82	13.524	N/A	76.12	14.581	N/A	284.04
38	13.837	0.33	119.48	13.958	0.35	240.68	84	12.955	N/A	74.46	14.015	N/A	285.72
40	13.808	0.33	116.31	13.911	0.36	243.85	86	N/A	N/A	N/A	N/A	N/A	N/A
42	13.748	0.34	113.32	13.974	0.39	246.74	88	N/A	N/A	N/A	N/A	N/A	N/A
44	13.741	0.34	110.71	13.958	0.39	249.29	90	N/A	N/A	N/A	N/A	N/A	N/A

N/A - Not Available

Figure 3. Type-B Standard Uncertainty vs Zenith Angle

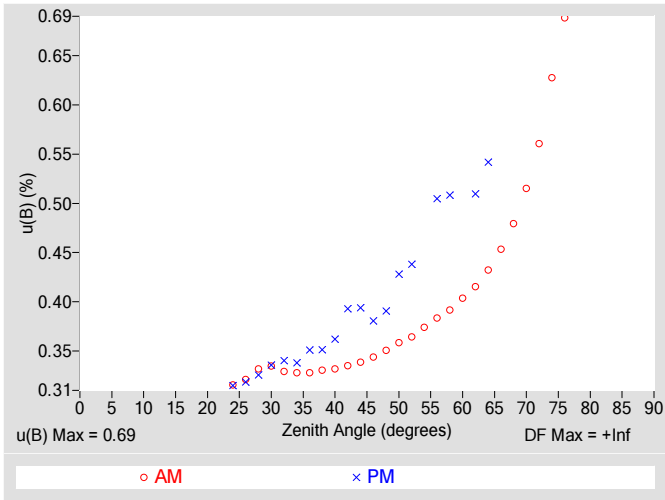


Figure 4. Residuals from Spline Interpolation

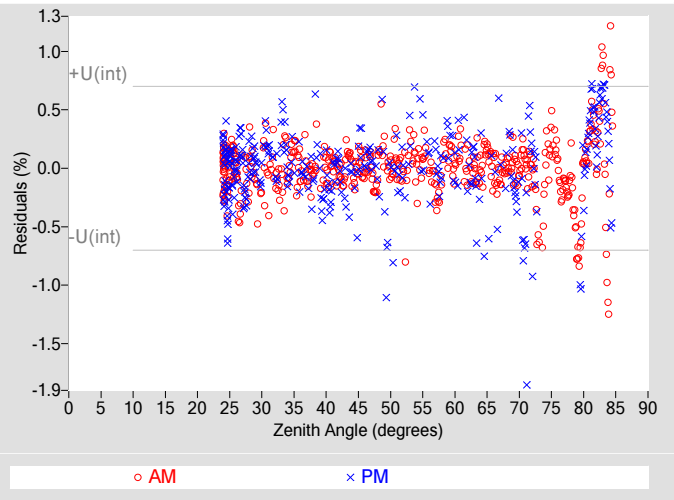


Table 3. Uncertainty using Spline Interpolation ‡

Type-B Standard Uncertainty, $u(B)$ (%)	$\pm 0.69$
Type-A Interpolating Function, $u(int)$ (%)	$\pm 0.35$
Combined Standard Uncertainty, $u(c)$ (%)	$\pm 0.77$
Effective degrees of freedom, $DF(c)$	16502
Coverage factor, $k$	1.96
Expanded Uncertainty, $U95$ (%)	$\pm 1.5$
AM Valid zenith angle range	24° to 76°
PM Valid zenith angle range	24° to 64°

‡ An illustration for how to reduce the uncertainty in calculating the irradiance using a function rather than  $R@45^\circ$ . Not accredited.

Table 4. Calibration Label Values

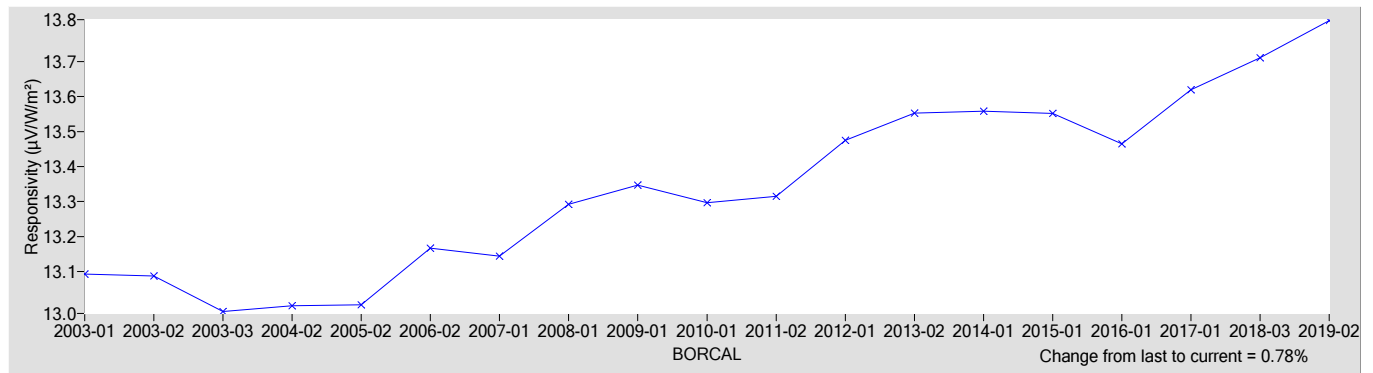
$R @ 45^\circ$ ( $\mu V/W/m^2$ )	$R_{net}$ ( $\mu V/W/m^2$ ) †
13.817	0

†  $R_{net}$  determination date: N/A

Table 5. Uncertainty using  $R @ 45^\circ$

Type-B Expanded Uncertainty, $U(B)$ (%)	$\pm 1.00$
Offset Uncertainty, $U(off)$ (%)	+1.1 / -1.9
Expanded Uncertainty, $U$ (%)	+2.1 / -2.9
Effective degrees of freedom, $DF$	+Inf
Coverage factor, $k$	1.96
Valid zenith angle range	30.0° to 60.0°

Figure 5. History of instrument at Zenith Angle = 45°



References:

[1] Reda, I.; Hickey, J.; Long, C.; Myers, D.; Stoffel, T.; Wilcox, S.; Michalsky, J. J.; Dutton, E. G.; Nelson, D. (2005). "Using a Blackbody to Calculate Net Longwave Responsivity of Shortwave Solar Pyranometers to Correct for Their Thermal Offset Error During Outdoor Calibration Using the Component Sum Method." Journal of Atmospheric and Oceanic Technology. , 2005; pp. 1531-1540; NREL Report No. JA-560-36646. doi:10.1175/JTECH1782.1

[2] Reda, I.; Myers, D.; Stoffel, T. (2008). "Uncertainty Estimate for the Outdoor Calibration of Solar Pyranometers: A Metrologist Perspective." Measure. (NCSLI Journal of Measurement Science). Vol. 3(4), December 2008; pp. 58-66; NREL Report No. JA-581-4137

[3] Reda, I.; Andreas, A. (2004). "Solar Position Algorithm for Solar Radiation Applications." Solar Energy. Vol. 76(5), 2004; pp. 577-589; NREL Report No. JA-560-35518. doi:10.1016/j.solener.2003.12.003

[4] Stoffel, T.; Reda, I. (2009). "NREL Pyrheliometer Comparisons: 22 September - 3 October 2008 (NPC-2008)." 54 pp.; NREL Report No. TP-550-45016.

[5] Reda, I.; Stoffel, T.; Myers, D. (2003). "Method to Calibrate a Solar Pyranometer for Measuring Reference Diffuse Irradiance." Solar Energy. Vol. 74, 2003; pp. 103-112; NREL Report No. JA-560-35025. doi:10.1016/S0038-092X(03)00124-5

[6] Reda, I. (1996). Calibration of a Solar Absolute Cavity Radiometer with Traceability to the World Radiometric Reference. 79 pp.; NREL Report No. TP-463-20619.

[7] Reda, I.; Gröbner, J.; Stoffel, T.; Myers, D.; Forgan, B. (2008). Improvements in the Blackbody Calibration of Pyrgeometers. ARM 2008 Science Team Meeting (Poster).



# National Renewable Energy Laboratory

## Solar Radiation Research Laboratory

### Metrology Laboratory

### Calibration Certificate



<b>Test Instrument:</b>	Semiconductor Pyrheliometer	<b>Manufacturer:</b>	Licor
<b>Model:</b>	LI201SB	<b>Serial Number:</b>	PYHR101
<b>Calibration Date:</b>	5/3/2019	<b>Due Date:</b>	5/3/2020
<b>Customer:</b>	NREL-SRRL-BMS	<b>Environmental Conditions:</b>	see page 4
<b>Test Dates:</b>	5/3		

This certifies that the above product was calibrated in compliance with ISO/IEC 17025:2005. Measurement uncertainties at the time of calibration are consistent with the Guide to the Expression of Uncertainty in Measurement (GUM) using Reda et al., 2008. All nominal values are traceable to the International System (SI) Units of Measurement.

No statement of compliance with specifications is made or implied on this certificate. However, the estimated uncertainties are the uncertainties of the calibration process; users must add other uncertainties that are relevant to their measuring system, environmental and sky conditions, outdoor set-up, and site location.

The Type-B Standard Uncertainty of using the responsivity at each even zenith angle is reported, and the Expanded Uncertainty of the calibration is reported using two methods:

1. The Expanded Uncertainty of using the responsivity at zenith angle = 45°, within the zenith angle range from 30.0° to 60.0°
2. The Expanded Uncertainty of using Spline Interpolating Functions for the responsivity versus zenith angle.

This certificate applies only to the item identified above and shall not be reproduced other than in full, without specific written approval from the calibration facility. Certificate without signature is not valid.

**Table 1. Traceability**

Measurement Type	Instrument	Calibration Date	Calibration Due Date
Beam Irradiance †	Eppley Absolute Cavity Radiometer Model HF, S/N 29219	09/24/2018	09/24/2019
Diffuse Irradiance †	Hukseflux Pyranometer Model SR25, S/N 2541	04/19/2019	04/19/2020
Diffuse Irradiance †	Hukseflux Pyranometer Model SR25, S/N 2542	04/19/2019	04/19/2020
Data Acquisition	NREL Data Acquisition System Model RAP-DAQ, S/N 2005-998	02/14/2019	02/14/2021
Data Acquisition	NREL Data Acquisition System Model RAP-DAQ, S/N 2005-999	02/14/2019	02/14/2021

† Through the World Radiometric Reference (WRR)

**Number of pages of certificate:** 4

**Calibration Procedure:** BORCAL-P00-Calibration and QA Procedure; available upon request.

**Setup:** Radiometers are calibrated outdoors, using the sun as the source. Pyranometers and pyrgeometers are installed for horizontal measurements, with their signal connectors oriented north, if their design permits.

The shading disk for the reference diffuse subtends a solid angle of 5°. Pyrheliometers are installed on solar trackers.

**Calibrated by:** RCC

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Ibrahim Reda, Technical Manager

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Date

For questions or comments, please contact the technical manager at:

ibrahim.reda@nrel.gov; 303-384-6385; 15013 Denver West Parkway, Golden, CO 80401, USA

# Calibration Results

## PYHR101 Licor LI201SB

The responsivity ( $R$ ,  $\mu\text{V}/\text{W}/\text{m}^2$ ) of the test instrument during calibration is calculated using this Measurement Equation:

$$R = (V - R_{net} * W_{net}) / I \tag{1}$$

where,

- $V$  = radiometer output voltage (microvolts),
  - $R_{net}$  = radiometer net infrared responsivity ( $\mu\text{V}/\text{W}/\text{m}^2$ ), see Table 4,
  - $W_{net}$  = effective net infrared measured by pyrgeometer ( $\text{W}/\text{m}^2$ ),
  - =  $W_{in} - W_{out} = W_{in} - \sigma * T_c^4$
  - where,  $W_{in}$  = incoming infrared ( $\text{W}/\text{m}^2$ ),  $\sigma = 5.6704\text{e-}8 \text{ W}\cdot\text{m}^{-2}\cdot\text{K}^{-4}$ ,
  - $T_c$  = case temperature of pyrgeometer (K).
- $I$  = reference irradiance ( $\text{W}/\text{m}^2$ ), beam (B) or global (G)
  - where,  $G = B * \text{COS}(Z) + D$ ,
  - $Z$  = zenith angle (degrees),
  - $D$  = reference diffuse irradiance ( $\text{W}/\text{m}^2$ ).

Figure 1. Responsivity vs Zenith Angle

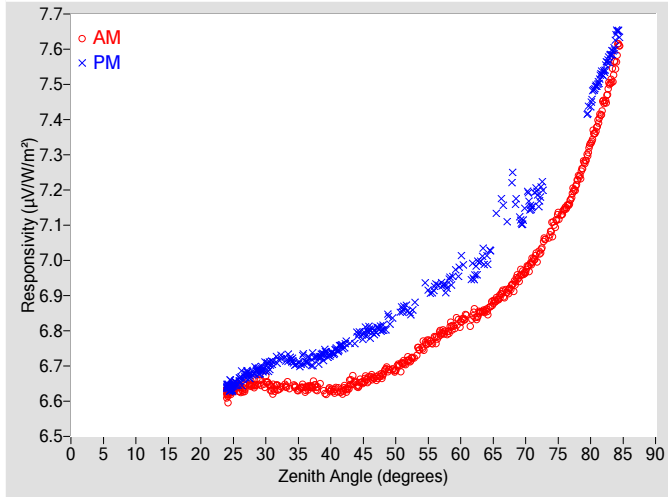


Figure 2. Responsivity vs Local Standard Time

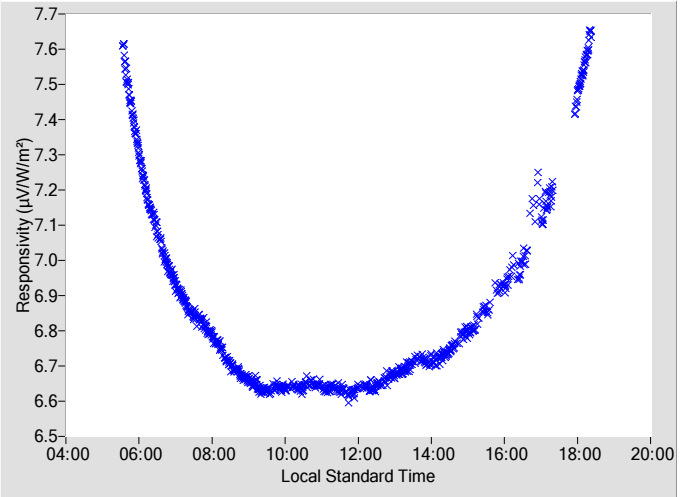


Table 2. Instrument Responsivity (R) and Calibration Type-B Standard Uncertainty, u(B)

Zenith Angle (deg.)	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle	Zenith Angle (deg.)	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle
0	N/A	N/A	N/A	N/A	N/A	N/A	46	6.6678	0.28	108.22	6.7992	0.28	251.84
2	N/A	N/A	N/A	N/A	N/A	N/A	48	6.6754	0.28	105.93	6.8047	0.29	254.18
4	N/A	N/A	N/A	N/A	N/A	N/A	50	6.6891	0.28	103.77	N/A	N/A	N/A
6	N/A	N/A	N/A	N/A	N/A	N/A	52	6.7169	0.28	101.64	6.8509	0.29	258.54
8	N/A	N/A	N/A	N/A	N/A	N/A	54	6.7545	0.28	99.68	N/A	N/A	N/A
10	N/A	N/A	N/A	N/A	N/A	N/A	56	6.7779	0.29	97.68	6.9249	0.30	262.32
12	N/A	N/A	N/A	N/A	N/A	N/A	58	6.7946	0.29	95.89	6.9328	0.30	264.15
14	N/A	N/A	N/A	N/A	N/A	N/A	60	6.8237	0.29	94.15	6.9976	N/A	265.88
16	N/A	N/A	N/A	N/A	N/A	N/A	62	6.8456	0.29	92.47	6.9616	0.30	267.68
18	N/A	N/A	N/A	N/A	N/A	N/A	64	6.8549	0.29	90.74	7.0013	0.30	269.44
20	N/A	N/A	N/A	N/A	N/A	N/A	66	6.8967	0.29	89.11	7.1758	N/A	271.25
22	N/A	N/A	N/A	N/A	N/A	N/A	68	6.9274	0.29	87.48	7.2353	N/A	272.64
24	6.6249	0.28	174.79	6.6421	0.28	186.06	70	6.9708	0.29	85.85	7.1723	N/A	274.36
26	6.6365	0.28	154.41	6.6673	0.28	206.22	72	7.0150	0.30	84.18	7.1767	N/A	275.91
28	6.6443	0.28	144.25	6.6789	0.28	215.94	74	7.0869	0.30	82.65	N/A	N/A	N/A
30	6.6545	0.28	136.96	6.7034	0.28	223.17	76	7.1455	0.30	81.04	N/A	N/A	N/A
32	6.6390	0.28	131.78	6.7192	0.28	228.46	78	7.2268	N/A	79.43	N/A	N/A	N/A
34	N/A	N/A	N/A	6.7164	0.28	233.10	80	7.3320	N/A	77.78	7.4478	N/A	282.47
36	6.6340	0.28	122.90	6.7154	0.28	237.16	82	7.4466	N/A	76.12	7.5332	N/A	284.05
38	6.6355	0.28	119.66	6.7206	0.28	240.93	84	7.5808	N/A	74.46	7.6449	N/A	285.72
40	6.6331	0.28	116.39	6.7351	0.28	243.96	86	N/A	N/A	N/A	N/A	N/A	N/A
42	6.6331	0.28	113.30	6.7562	0.28	246.76	88	N/A	N/A	N/A	N/A	N/A	N/A
44	6.6471	0.28	110.72	6.7905	0.28	249.59	90	N/A	N/A	N/A	N/A	N/A	N/A

N/A - Not Available

Figure 3. Type-B Standard Uncertainty vs Zenith Angle

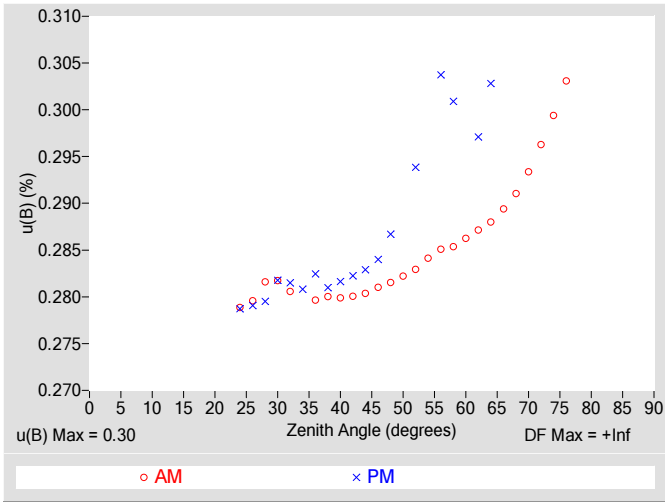


Figure 4. Residuals from Spline Interpolation

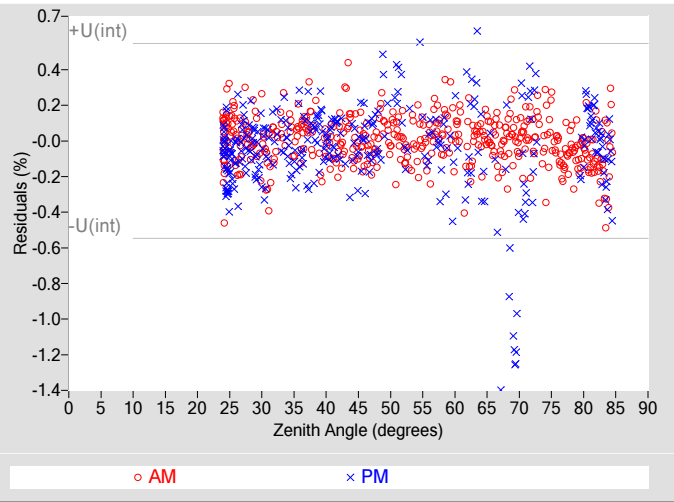


Table 3. Uncertainty using Spline Interpolation ‡

Type-B Standard Uncertainty, u(B) (%)	±0.30
Type-A Interpolating Function, u(int) (%)	±0.27
Combined Standard Uncertainty, u(c) (%)	±0.41
Effective degrees of freedom, DF(c)	3348
Coverage factor, k	1.96
Expanded Uncertainty, U95 (%)	±0.80
AM Valid zenith angle range	24° to 76°
PM Valid zenith angle range	24° to 64°

‡ An illustration for how to reduce the uncertainty in calculating the irradiance using a function rather than R@45°. Not accredited.

Table 4. Calibration Label Values

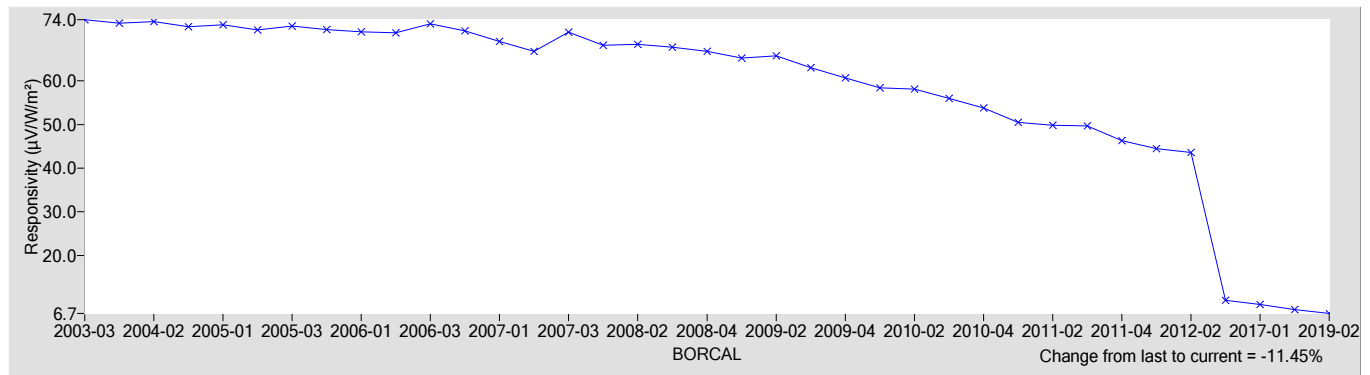
R @ 45° (μV/W/m²)	Rnet (μV/W/m²) †
6.7215	0

† Rnet determination date: N/A

Table 5. Uncertainty using R @ 45°

Type-B Expanded Uncertainty, U(B) (%)	±0.60
Offset Uncertainty, U(off) (%)	+4.1 / -1.3
Expanded Uncertainty, U (%)	+4.7 / -1.9
Effective degrees of freedom, DF	+Inf
Coverage factor, k	1.96
Valid zenith angle range	30.0° to 60.0°

Figure 5. History of instrument at Zenith Angle = 45°



References:

[1] Reda, I.; Hickey, J.; Long, C.; Myers, D.; Stoffel, T.; Wilcox, S.; Michalsky, J. J.; Dutton, E. G.; Nelson, D. (2005). "Using a Blackbody to Calculate Net Longwave Responsivity of Shortwave Solar Pyranometers to Correct for Their Thermal Offset Error During Outdoor Calibration Using the Component Sum Method." Journal of Atmospheric and Oceanic Technology. , 2005; pp. 1531-1540; NREL Report No. JA-560-36646. doi:10.1175/JTECH1782.1

[2] Reda, I.; Myers, D.; Stoffel, T. (2008). "Uncertainty Estimate for the Outdoor Calibration of Solar Pyranometers: A Metrologist Perspective." Measure. (NCSLI Journal of Measurement Science). Vol. 3(4), December 2008; pp. 58-66; NREL Report No. JA-581-4137

[3] Reda, I.; Andreas, A. (2004). "Solar Position Algorithm for Solar Radiation Applications." Solar Energy. Vol. 76(5), 2004; pp. 577-589; NREL Report No. JA-560-35518. doi:10.1016/j.solener.2003.12.003

[4] Stoffel, T.; Reda, I. (2009). "NREL Pyrheliometer Comparisons: 22 September - 3 October 2008 (NPC-2008)." 54 pp.; NREL Report No. TP-550-45016.

[5] Reda, I.; Stoffel, T.; Myers, D. (2003). "Method to Calibrate a Solar Pyranometer for Measuring Reference Diffuse Irradiance." Solar Energy. Vol. 74, 2003; pp. 103-112; NREL Report No. JA-560-35025. doi:10.1016/S0038-092X(03)00124-5

[6] Reda, I. (1996). Calibration of a Solar Absolute Cavity Radiometer with Traceability to the World Radiometric Reference. 79 pp.; NREL Report No. TP-463-20619.

[7] Reda, I.; Gröbner, J.; Stoffel, T.; Myers, D.; Forgan, B. (2008). Improvements in the Blackbody Calibration of Pyrgeometers. ARM 2008 Science Team Meeting (Poster).



# National Renewable Energy Laboratory

## Solar Radiation Research Laboratory

### Metrology Laboratory

### Calibration Certificate



<b>Test Instrument:</b>	Pyranometer	<b>Manufacturer:</b>	EKO
<b>Model:</b>	MS-602	<b>Serial Number:</b>	S13071483
<b>Calibration Date:</b>	5/3/2019	<b>Due Date:</b>	5/3/2020
<b>Customer:</b>	NREL-SRRL-BMS	<b>Environmental Conditions:</b>	see page 4
<b>Test Dates:</b>	5/3		

This certifies that the above product was calibrated in compliance with ISO/IEC 17025:2005. Measurement uncertainties at the time of calibration are consistent with the Guide to the Expression of Uncertainty in Measurement (GUM) using Reda et al., 2008. All nominal values are traceable to the International System (SI) Units of Measurement.

No statement of compliance with specifications is made or implied on this certificate. However, the estimated uncertainties are the uncertainties of the calibration process; users must add other uncertainties that are relevant to their measuring system, environmental and sky conditions, outdoor set-up, and site location.

The Type-B Standard Uncertainty of using the responsivity at each even zenith angle is reported, and the Expanded Uncertainty of the calibration is reported using two methods:

1. The Expanded Uncertainty of using the responsivity at zenith angle = 45°, within the zenith angle range from 30.0° to 60.0°
2. The Expanded Uncertainty of using Spline Interpolating Functions for the responsivity versus zenith angle.

This certificate applies only to the item identified above and shall not be reproduced other than in full, without specific written approval from the calibration facility. Certificate without signature is not valid.

**Table 1. Traceability**

Measurement Type	Instrument	Calibration Date	Calibration Due Date
Beam Irradiance †	Eppley Absolute Cavity Radiometer Model HF, S/N 29219	09/24/2018	09/24/2019
Diffuse Irradiance †	Hukseflux Pyranometer Model SR25, S/N 2541	04/19/2019	04/19/2020
Diffuse Irradiance †	Hukseflux Pyranometer Model SR25, S/N 2542	04/19/2019	04/19/2020
Data Acquisition	NREL Data Acquisition System Model RAP-DAQ, S/N 2005-998	02/14/2019	02/14/2021
Data Acquisition	NREL Data Acquisition System Model RAP-DAQ, S/N 2005-999	02/14/2019	02/14/2021
Infrared Irradiance ‡	Kipp & Zonen Pyrgeometer Model CG4, S/N FT002	04/16/2018	04/16/2022

† Through the World Radiometric Reference (WRR)

‡ Through the World Infrared Standard Group (WISG)

**Number of pages of certificate:** 4

**Calibration Procedure:** BORCAL-P00-Calibration and QA Procedure; available upon request.

**Setup:** Radiometers are calibrated outdoors, using the sun as the source. Pyranometers and pyrgeometers are installed for horizontal measurements, with their signal connectors oriented north, if their design permits.

The shading disk for the reference diffuse subtends a solid angle of 5°. Pyrheliometers are installed on solar trackers.

**Calibrated by:** RCC

-----  
Ibrahim Reda, Technical Manager

-----  
Date

For questions or comments, please contact the technical manager at:

ibrahim.reda@nrel.gov; 303-384-6385; 15013 Denver West Parkway, Golden, CO 80401, USA

# Calibration Results

## S13071483 EKO MS-602

The responsivity ( $R$ ,  $\mu\text{V}/\text{W}/\text{m}^2$ ) of the test instrument during calibration is calculated using this Measurement Equation:

$$R = (V - R_{net} * W_{net}) / I \tag{1}$$

where,

- $V$  = radiometer output voltage (microvolts),
  - $R_{net}$  = radiometer net infrared responsivity ( $\mu\text{V}/\text{W}/\text{m}^2$ ), see Table 4,
  - $W_{net}$  = effective net infrared measured by pyrgeometer ( $\text{W}/\text{m}^2$ ),
  - =  $W_{in} - W_{out} = W_{in} - \sigma * T_c^4$
  - where,  $W_{in}$  = incoming infrared ( $\text{W}/\text{m}^2$ ),  $\sigma = 5.6704\text{e-}8 \text{ W}\cdot\text{m}^{-2}\cdot\text{K}^{-4}$ ,
  - $T_c$  = case temperature of pyrgeometer (K).
- $I$  = reference irradiance ( $\text{W}/\text{m}^2$ ), beam (B) or global (G)
  - where,  $G = B * \text{COS}(Z) + D$ ,
  - $Z$  = zenith angle (degrees),
  - $D$  = reference diffuse irradiance ( $\text{W}/\text{m}^2$ ).

Figure 1. Responsivity vs Zenith Angle

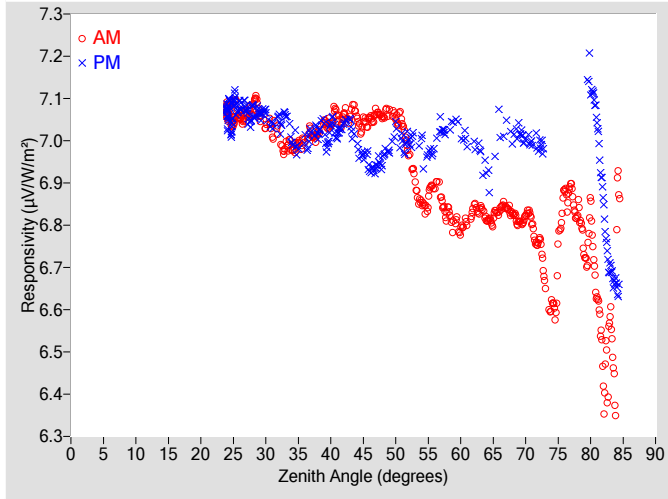


Figure 2. Responsivity vs Local Standard Time

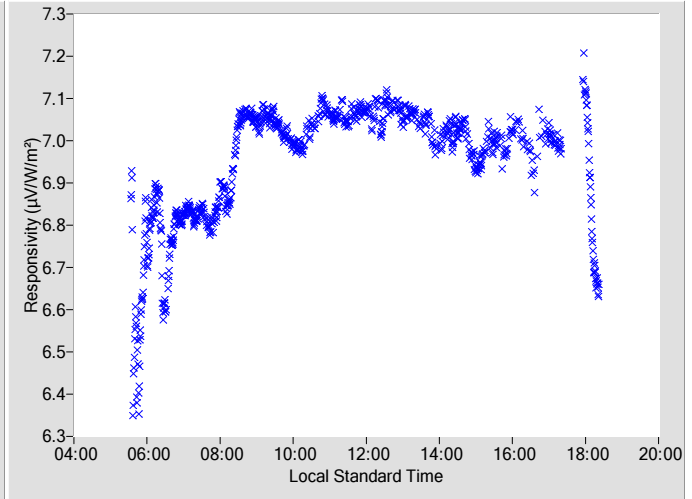


Table 2. Instrument Responsivity (R) and Calibration Type-B Standard Uncertainty, u(B)

Zenith Angle (deg.)	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle	Zenith Angle (deg.)	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle
0	N/A	N/A	N/A	N/A	N/A	N/A	46	7.0542	0.36	108.22	6.9324	0.40	251.93
2	N/A	N/A	N/A	N/A	N/A	N/A	48	7.0564	0.36	105.93	6.9544	0.41	254.23
4	N/A	N/A	N/A	N/A	N/A	N/A	50	7.0547	0.37	103.72	7.0275	0.45	256.33
6	N/A	N/A	N/A	N/A	N/A	N/A	52	6.9745	0.38	101.76	7.0043	0.46	258.41
8	N/A	N/A	N/A	N/A	N/A	N/A	54	6.8533	0.40	99.71	6.9839	0.49	260.51
10	N/A	N/A	N/A	N/A	N/A	N/A	56	6.8918	0.41	97.76	6.9810	0.52	262.22
12	N/A	N/A	N/A	N/A	N/A	N/A	58	6.8311	0.42	95.97	N/A	N/A	N/A
14	N/A	N/A	N/A	N/A	N/A	N/A	60	6.7897	0.43	94.14	7.0045	N/A	266.05
16	N/A	N/A	N/A	N/A	N/A	N/A	62	6.8426	0.44	92.47	6.9889	0.53	267.80
18	N/A	N/A	N/A	N/A	N/A	N/A	64	6.8135	0.46	90.77	6.9353	0.56	269.36
20	N/A	N/A	N/A	N/A	N/A	N/A	66	6.8342	0.48	89.12	7.0410	N/A	271.00
22	N/A	N/A	N/A	N/A	N/A	N/A	68	6.8275	0.51	87.47	7.0096	N/A	272.65
24	7.0683	0.33	174.38	7.0660	0.33	184.81	70	6.8212	0.55	85.87	6.9991	N/A	274.16
26	7.0590	0.33	153.78	7.0812	0.33	205.83	72	6.7611	0.60	84.25	6.9854	N/A	275.95
28	7.0735	0.34	144.35	7.0686	0.34	215.84	74	6.6091	0.68	82.63	N/A	N/A	N/A
30	7.0323	0.35	137.27	7.0700	0.35	222.45	76	6.8783	0.74	81.02	N/A	N/A	N/A
32	7.0249	0.34	132.18	7.0475	0.35	228.58	78	6.8324	N/A	79.41	N/A	N/A	N/A
34	6.9777	0.34	126.98	6.9975	0.35	233.06	80	6.8179	N/A	77.81	7.1379	N/A	282.38
36	6.9997	0.34	123.22	7.0042	0.36	237.20	82	6.4402	N/A	76.15	6.8528	N/A	284.03
38	7.0189	0.34	119.39	7.0191	0.36	240.74	84	6.6707	N/A	74.48	6.6532	N/A	285.70
40	7.0422	0.34	116.16	7.0410	0.37	243.92	86	N/A	N/A	N/A	N/A	N/A	N/A
42	7.0626	0.35	113.33	7.0440	0.41	246.92	88	N/A	N/A	N/A	N/A	N/A	N/A
44	7.0524	0.35	110.61	6.9858	0.41	249.65	90	N/A	N/A	N/A	N/A	N/A	N/A

N/A - Not Available

Figure 3. Type-B Standard Uncertainty vs Zenith Angle

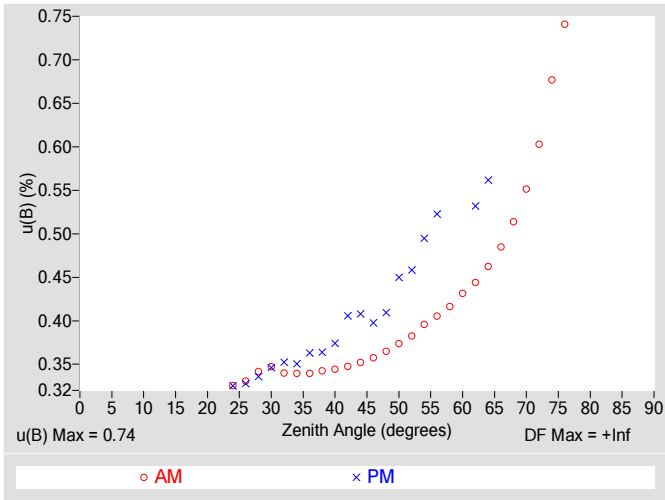


Figure 4. Residuals from Spline Interpolation

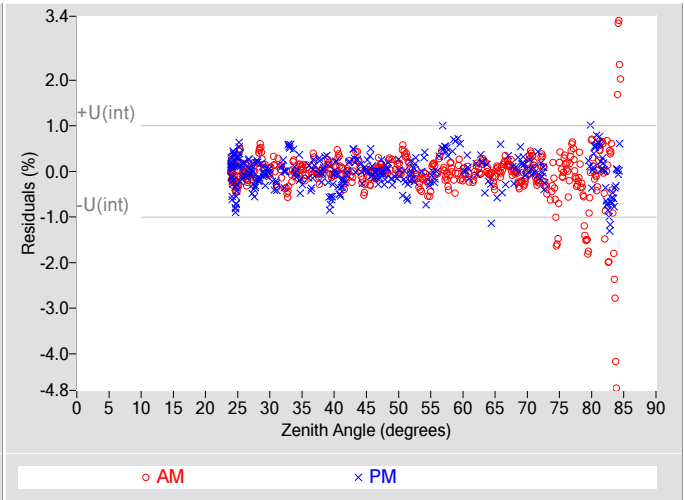


Table 3. Uncertainty using Spline Interpolation ‡

Type-B Standard Uncertainty, u(B) (%)	±0.74
Type-A Interpolating Function, u(int) (%)	±0.50
Combined Standard Uncertainty, u(c) (%)	±0.89
Effective degrees of freedom, DF(c)	6879
Coverage factor, k	1.96
Expanded Uncertainty, U95 (%)	±1.8
AM Valid zenith angle range	24° to 76°
PM Valid zenith angle range	24° to 64°

‡ An illustration for how to reduce the uncertainty in calculating the irradiance using a function rather than R@45°. Not accredited.

Table 4. Calibration Label Values

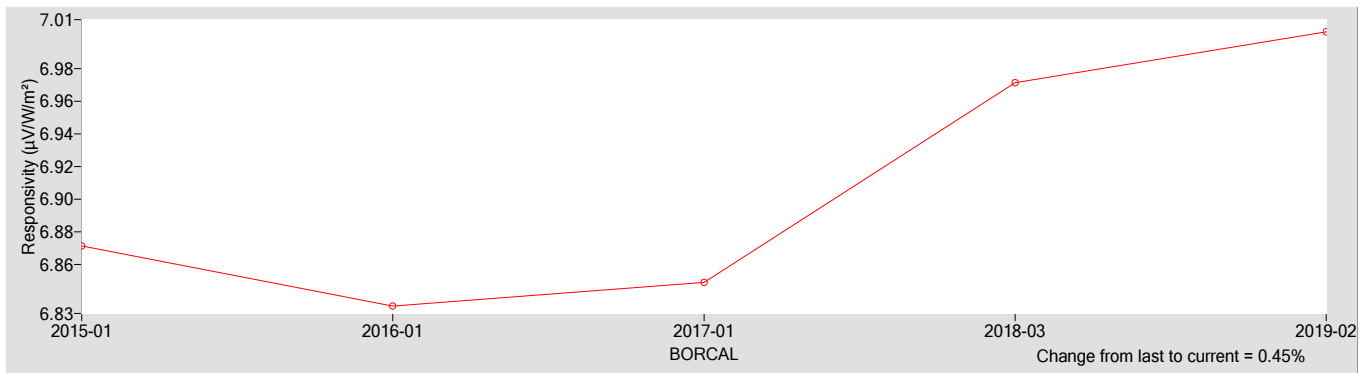
R @ 45° (μV/W/m²)	Rnet (μV/W/m²) †
7.0025	0.30000

† Rnet determination date: Estimated

Table 5. Uncertainty using R @ 45°

Type-B Expanded Uncertainty, U(B) (%)	±1.0
Offset Uncertainty, U(off) (%)	+0.96 / -3.0
Expanded Uncertainty, U (%)	+2.0 / -4.1
Effective degrees of freedom, DF	+Inf
Coverage factor, k	1.96
Valid zenith angle range	30.0° to 60.0°

Figure 5. History of instrument at Zenith Angle = 45°



References:

[1] Reda, I.; Hickey, J.; Long, C.; Myers, D.; Stoffel, T.; Wilcox, S.; Michalsky, J. J.; Dutton, E. G.; Nelson, D. (2005). "Using a Blackbody to Calculate Net Longwave Responsivity of Shortwave Solar Pyranometers to Correct for Their Thermal Offset Error During Outdoor Calibration Using the Component Sum Method." Journal of Atmospheric and Oceanic Technology. , 2005; pp. 1531-1540; NREL Report No. JA-560-36646. doi:10.1175/JTECH1782.1

[2] Reda, I.; Myers, D.; Stoffel, T. (2008). "Uncertainty Estimate for the Outdoor Calibration of Solar Pyranometers: A Metrologist Perspective." Measure. (NCSLI Journal of Measurement Science). Vol. 3(4), December 2008; pp. 58-66; NREL Report No. JA-581-4137

[3] Reda, I.; Andreas, A. (2004). "Solar Position Algorithm for Solar Radiation Applications." Solar Energy. Vol. 76(5), 2004; pp. 577-589; NREL Report No. JA-560-35518. doi:10.1016/j.solener.2003.12.003

[4] Stoffel, T.; Reda, I. (2009). "NREL Pyrheliometer Comparisons: 22 September - 3 October 2008 (NPC-2008)." 54 pp.; NREL Report No. TP-550-45016.

[5] Reda, I.; Stoffel, T.; Myers, D. (2003). "Method to Calibrate a Solar Pyranometer for Measuring Reference Diffuse Irradiance." Solar Energy. Vol. 74, 2003; pp. 103-112; NREL Report No. JA-560-35025. doi:10.1016/S0038-092X(03)00124-5

[6] Reda, I. (1996). Calibration of a Solar Absolute Cavity Radiometer with Traceability to the World Radiometric Reference. 79 pp.; NREL Report No. TP-463-20619.

[7] Reda, I.; Gröbner, J.; Stoffel, T.; Myers, D.; Forgan, B. (2008). Improvements in the Blackbody Calibration of Pyrgeometers. ARM 2008 Science Team Meeting (Poster).





# National Renewable Energy Laboratory

## Solar Radiation Research Laboratory

### Metrology Laboratory

### Calibration Certificate



<b>Test Instrument:</b>	Silicon Pyranometer	<b>Manufacturer:</b>	EKO
<b>Model:</b>	ML-01	<b>Serial Number:</b>	S13135063
<b>Calibration Date:</b>	5/3/2019	<b>Due Date:</b>	5/3/2020
<b>Customer:</b>	NREL-SRRL-BMS	<b>Environmental Conditions:</b>	see page 4
<b>Test Dates:</b>	5/3		

This certifies that the above product was calibrated in compliance with ISO/IEC 17025:2005. Measurement uncertainties at the time of calibration are consistent with the Guide to the Expression of Uncertainty in Measurement (GUM) using Reda et al., 2008. All nominal values are traceable to the International System (SI) Units of Measurement.

No statement of compliance with specifications is made or implied on this certificate. However, the estimated uncertainties are the uncertainties of the calibration process; users must add other uncertainties that are relevant to their measuring system, environmental and sky conditions, outdoor set-up, and site location.

The Type-B Standard Uncertainty of using the responsivity at each even zenith angle is reported, and the Expanded Uncertainty of the calibration is reported using two methods:

1. The Expanded Uncertainty of using the responsivity at zenith angle = 45°, within the zenith angle range from 30.0° to 60.0°
2. The Expanded Uncertainty of using Spline Interpolating Functions for the responsivity versus zenith angle.

This certificate applies only to the item identified above and shall not be reproduced other than in full, without specific written approval from the calibration facility. Certificate without signature is not valid.

**Table 1. Traceability**

Measurement Type	Instrument	Calibration Date	Calibration Due Date
Beam Irradiance †	Eppley Absolute Cavity Radiometer Model HF, S/N 29219	09/24/2018	09/24/2019
Diffuse Irradiance †	Hukseflux Pyranometer Model SR25, S/N 2541	04/19/2019	04/19/2020
Diffuse Irradiance †	Hukseflux Pyranometer Model SR25, S/N 2542	04/19/2019	04/19/2020
Data Acquisition	NREL Data Acquisition System Model RAP-DAQ, S/N 2005-998	02/14/2019	02/14/2021
Data Acquisition	NREL Data Acquisition System Model RAP-DAQ, S/N 2005-999	02/14/2019	02/14/2021

† Through the World Radiometric Reference (WRR)

**Number of pages of certificate:** 4

**Calibration Procedure:** BORCAL-P00-Calibration and QA Procedure; available upon request.

**Setup:** Radiometers are calibrated outdoors, using the sun as the source. Pyranometers and pyrgeometers are installed for horizontal measurements, with their signal connectors oriented north, if their design permits.

The shading disk for the reference diffuse subtends a solid angle of 5°. Pyrheliometers are installed on solar trackers.

**Calibrated by:** RCC

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Ibrahim Reda, Technical Manager

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Date

For questions or comments, please contact the technical manager at:

ibrahim.reda@nrel.gov; 303-384-6385; 15013 Denver West Parkway, Golden, CO 80401, USA

# Calibration Results

## S13135063 EKO ML-01

The responsivity (R,  $\mu\text{V}/\text{W}/\text{m}^2$ ) of the test instrument during calibration is calculated using this Measurement Equation:

$$R = (V - R_{net} * W_{net}) / I \tag{1}$$

where,

- $V$  = radiometer output voltage (microvolts),
  - $R_{net}$  = radiometer net infrared responsivity ( $\mu\text{V}/\text{W}/\text{m}^2$ ), see Table 4,
  - $W_{net}$  = effective net infrared measured by pyrgeometer ( $\text{W}/\text{m}^2$ ),
  - =  $W_{in} - W_{out} = W_{in} - \sigma * T_c^4$
  - where,  $W_{in}$  = incoming infrared ( $\text{W}/\text{m}^2$ ),  $\sigma = 5.6704\text{e-}8 \text{ W}\cdot\text{m}^{-2}\cdot\text{K}^{-4}$ ,
  - $T_c$  = case temperature of pyrgeometer (K).
- $I$  = reference irradiance ( $\text{W}/\text{m}^2$ ), beam (B) or global (G)
  - where,  $G = B * \text{COS}(Z) + D$ ,
  - $Z$  = zenith angle (degrees),
  - $D$  = reference diffuse irradiance ( $\text{W}/\text{m}^2$ ).

Figure 1. Responsivity vs Zenith Angle

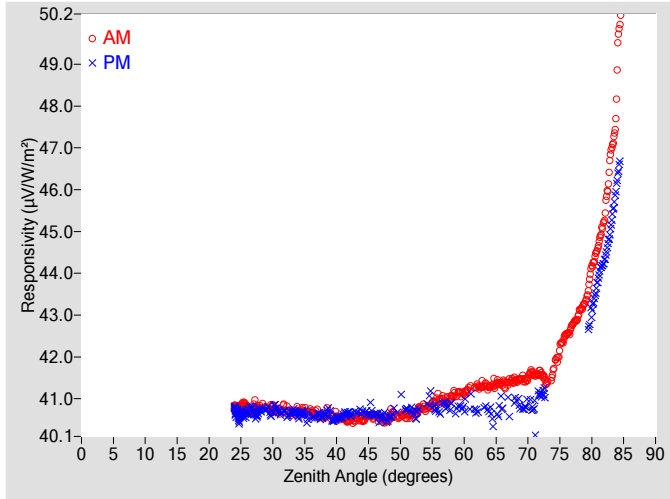


Figure 2. Responsivity vs Local Standard Time

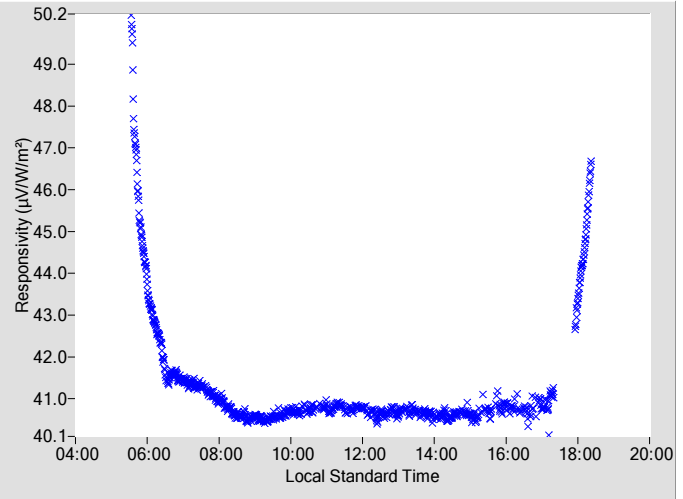


Table 2. Instrument Responsivity (R) and Calibration Type-B Standard Uncertainty, u(B)

Zenith Angle (deg.)	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle	Zenith Angle (deg.)	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	u(B) $\pm$ (%)	Azimuth Angle
0	N/A	N/A	N/A	N/A	N/A	N/A	46	40.560	0.34	108.40	40.629	0.38	251.84
2	N/A	N/A	N/A	N/A	N/A	N/A	48	40.491	0.35	105.92	40.494	0.39	254.15
4	N/A	N/A	N/A	N/A	N/A	N/A	50	40.591	0.36	103.70	41.101	0.44	256.54
6	N/A	N/A	N/A	N/A	N/A	N/A	52	40.647	0.36	101.67	40.715	0.44	258.43
8	N/A	N/A	N/A	N/A	N/A	N/A	54	40.768	0.37	99.74	40.880	N/A	260.63
10	N/A	N/A	N/A	N/A	N/A	N/A	56	40.999	0.38	97.76	40.700	0.49	262.33
12	N/A	N/A	N/A	N/A	N/A	N/A	58	41.039	0.39	95.97	40.839	0.50	264.06
14	N/A	N/A	N/A	N/A	N/A	N/A	60	41.143	0.40	94.23	40.814	N/A	265.90
16	N/A	N/A	N/A	N/A	N/A	N/A	62	41.297	0.41	92.45	40.695	0.51	267.64
18	N/A	N/A	N/A	N/A	N/A	N/A	64	41.287	0.43	90.81	40.707	0.55	269.43
20	N/A	N/A	N/A	N/A	N/A	N/A	66	41.389	0.45	89.12	40.865	N/A	270.95
22	N/A	N/A	N/A	N/A	N/A	N/A	68	41.430	0.48	87.47	40.960	N/A	272.69
24	40.768	0.32	173.97	40.724	0.31	185.43	70	41.506	0.51	85.87	40.895	N/A	274.11
26	40.797	0.32	154.18	40.673	0.32	205.90	72	41.625	0.56	84.25	41.094	N/A	275.93
28	40.794	0.33	144.79	40.720	0.32	215.49	74	41.685	0.62	82.66	N/A	N/A	N/A
30	40.779	0.34	137.35	40.741	0.33	222.86	76	42.530	0.68	81.06	N/A	N/A	N/A
32	40.847	0.33	131.76	40.672	0.34	228.29	78	43.044	N/A	79.41	N/A	N/A	N/A
34	40.725	0.33	126.98	40.609	0.34	233.05	80	44.139	N/A	77.80	43.162	N/A	282.45
36	40.698	0.33	122.86	40.547	0.35	237.37	82	45.378	N/A	76.15	44.347	N/A	284.07
38	40.573	0.33	119.46	40.604	0.35	240.72	84	48.968	N/A	74.44	46.294	N/A	285.74
40	40.581	0.33	116.28	40.536	0.36	243.92	86	N/A	N/A	N/A	N/A	N/A	N/A
42	40.466	0.33	113.47	40.638	0.39	246.72	88	N/A	N/A	N/A	N/A	N/A	N/A
44	40.512	0.34	110.70	40.671	0.40	249.39	90	N/A	N/A	N/A	N/A	N/A	N/A

N/A - Not Available

Figure 3. Type-B Standard Uncertainty vs Zenith Angle

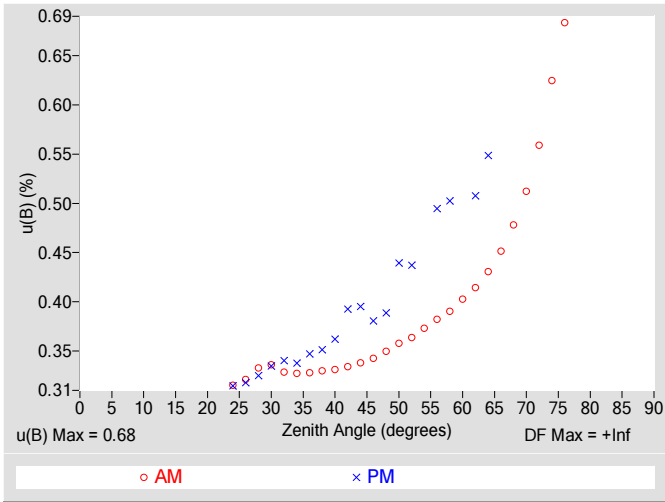


Figure 4. Residuals from Spline Interpolation

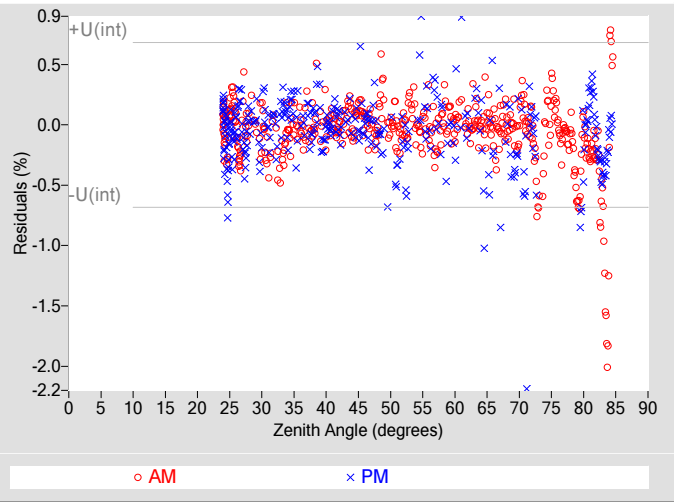


Table 3. Uncertainty using Spline Interpolation ‡

Type-B Standard Uncertainty, u(B) (%)	±0.68
Type-A Interpolating Function, u(int) (%)	±0.34
Combined Standard Uncertainty, u(c) (%)	±0.76
Effective degrees of freedom, DF(c)	17334
Coverage factor, k	1.96
Expanded Uncertainty, U95 (%)	±1.5
AM Valid zenith angle range	24° to 76°
PM Valid zenith angle range	24° to 64°

‡ An illustration for how to reduce the uncertainty in calculating the irradiance using a function rather than R@45°. Not accredited.

Table 4. Calibration Label Values

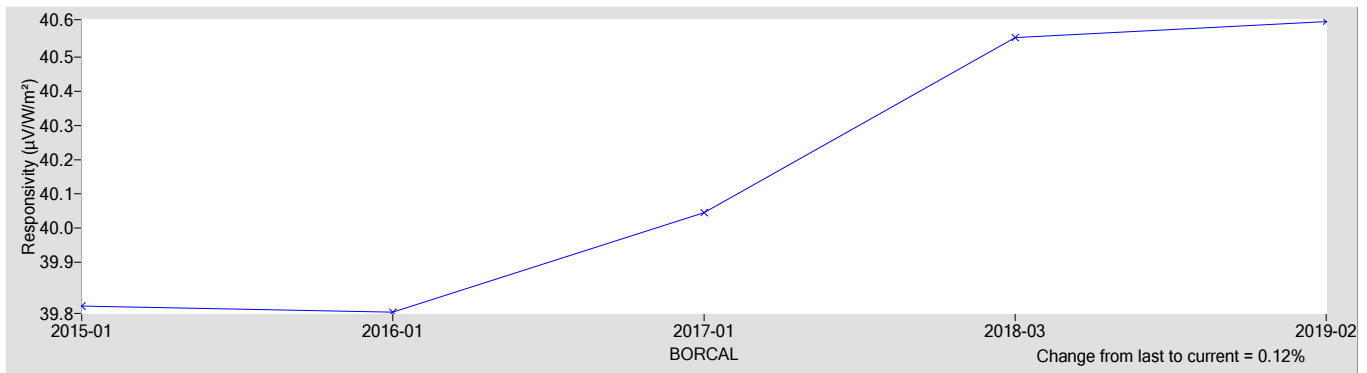
R @ 45° (μV/W/m²)	Rnet (μV/W/m²) †
40.604	0

† Rnet determination date: N/A

Table 5. Uncertainty using R @ 45°

Type-B Expanded Uncertainty, U(B) (%)	±0.98
Offset Uncertainty, U(off) (%)	+1.3 / -0.34
Expanded Uncertainty, U (%)	+2.3 / -1.3
Effective degrees of freedom, DF	+Inf
Coverage factor, k	1.96
Valid zenith angle range	30.0° to 60.0°

Figure 5. History of instrument at Zenith Angle = 45°



References:

[1] Reda, I.; Hickey, J.; Long, C.; Myers, D.; Stoffel, T.; Wilcox, S.; Michalsky, J. J.; Dutton, E. G.; Nelson, D. (2005). "Using a Blackbody to Calculate Net Longwave Responsivity of Shortwave Solar Pyranometers to Correct for Their Thermal Offset Error During Outdoor Calibration Using the Component Sum Method." Journal of Atmospheric and Oceanic Technology. , 2005; pp. 1531-1540; NREL Report No. JA-560-36646. doi:10.1175/JTECH1782.1

[2] Reda, I.; Myers, D.; Stoffel, T. (2008). "Uncertainty Estimate for the Outdoor Calibration of Solar Pyranometers: A Metrologist Perspective." Measure. (NCSLI Journal of Measurement Science). Vol. 3(4), December 2008; pp. 58-66; NREL Report No. JA-581-4137

[3] Reda, I.; Andreas, A. (2004). "Solar Position Algorithm for Solar Radiation Applications." Solar Energy. Vol. 76(5), 2004; pp. 577-589; NREL Report No. JA-560-35518. doi:10.1016/j.solener.2003.12.003

[4] Stoffel, T.; Reda, I. (2009). "NREL Pyrheliometer Comparisons: 22 September - 3 October 2008 (NPC-2008)." 54 pp.; NREL Report No. TP-550-45016.

[5] Reda, I.; Stoffel, T.; Myers, D. (2003). "Method to Calibrate a Solar Pyranometer for Measuring Reference Diffuse Irradiance." Solar Energy. Vol. 74, 2003; pp. 103-112; NREL Report No. JA-560-35025. doi:10.1016/S0038-092X(03)00124-5

[6] Reda, I. (1996). Calibration of a Solar Absolute Cavity Radiometer with Traceability to the World Radiometric Reference. 79 pp.; NREL Report No. TP-463-20619.

[7] Reda, I.; Gröbner, J.; Stoffel, T.; Myers, D.; Forgan, B. (2008). Improvements in the Blackbody Calibration of Pyrgeometers. ARM 2008 Science Team Meeting (Poster).



# National Renewable Energy Laboratory

## Solar Radiation Research Laboratory

### Metrology Laboratory

### Calibration Certificate



<b>Test Instrument:</b>	Pyranometer	<b>Manufacturer:</b>	EKO
<b>Model:</b>	MS-410	<b>Serial Number:</b>	S13144.085R
<b>Calibration Date:</b>	5/3/2019	<b>Due Date:</b>	5/3/2020
<b>Customer:</b>	NREL-SRRL-BMS	<b>Environmental Conditions:</b>	see page 4
<b>Test Dates:</b>	5/3		

This certifies that the above product was calibrated in compliance with ISO/IEC 17025:2005. Measurement uncertainties at the time of calibration are consistent with the Guide to the Expression of Uncertainty in Measurement (GUM) using Reda et al., 2008. All nominal values are traceable to the International System (SI) Units of Measurement.

No statement of compliance with specifications is made or implied on this certificate. However, the estimated uncertainties are the uncertainties of the calibration process; users must add other uncertainties that are relevant to their measuring system, environmental and sky conditions, outdoor set-up, and site location.

The Type-B Standard Uncertainty of using the responsivity at each even zenith angle is reported, and the Expanded Uncertainty of the calibration is reported using two methods:

1. The Expanded Uncertainty of using the responsivity at zenith angle = 45°, within the zenith angle range from 30.0° to 60.0°
2. The Expanded Uncertainty of using Spline Interpolating Functions for the responsivity versus zenith angle.

This certificate applies only to the item identified above and shall not be reproduced other than in full, without specific written approval from the calibration facility. Certificate without signature is not valid.

**Table 1. Traceability**

Measurement Type	Instrument	Calibration Date	Calibration Due Date
Beam Irradiance †	Eppley Absolute Cavity Radiometer Model HF, S/N 29219	09/24/2018	09/24/2019
Diffuse Irradiance †	Hukseflux Pyranometer Model SR25, S/N 2541	04/19/2019	04/19/2020
Diffuse Irradiance †	Hukseflux Pyranometer Model SR25, S/N 2542	04/19/2019	04/19/2020
Data Acquisition	NREL Data Acquisition System Model RAP-DAQ, S/N 2005-998	02/14/2019	02/14/2021
Data Acquisition	NREL Data Acquisition System Model RAP-DAQ, S/N 2005-999	02/14/2019	02/14/2021
Infrared Irradiance ‡	Kipp & Zonen Pyrgeometer Model CG4, S/N FT002	04/16/2018	04/16/2022

† Through the World Radiometric Reference (WRR)

‡ Through the World Infrared Standard Group (WISG)

**Number of pages of certificate:** 4

**Calibration Procedure:** BORCAL-P00-Calibration and QA Procedure; available upon request.

**Setup:** Radiometers are calibrated outdoors, using the sun as the source. Pyranometers and pyrgeometers are installed for horizontal measurements, with their signal connectors oriented north, if their design permits.

The shading disk for the reference diffuse subtends a solid angle of 5°. Pyrheliometers are installed on solar trackers.

**Calibrated by:** RCC

-----  
Ibrahim Reda, Technical Manager

-----  
Date

For questions or comments, please contact the technical manager at:

ibrahim.reda@nrel.gov; 303-384-6385; 15013 Denver West Parkway, Golden, CO 80401, USA

# Calibration Results

## S13144.085R EKO MS-410

The responsivity ( $R$ ,  $\mu\text{V}/\text{W}/\text{m}^2$ ) of the test instrument during calibration is calculated using this Measurement Equation:

$$R = (V - R_{net} * W_{net}) / I \tag{1}$$

where,

- $V$  = radiometer output voltage (microvolts),
  - $R_{net}$  = radiometer net infrared responsivity ( $\mu\text{V}/\text{W}/\text{m}^2$ ), see Table 4,
  - $W_{net}$  = effective net infrared measured by pyrgeometer ( $\text{W}/\text{m}^2$ ),
  - =  $W_{in} - W_{out} = W_{in} - \sigma * T_c^4$
  - where,  $W_{in}$  = incoming infrared ( $\text{W}/\text{m}^2$ ),  $\sigma = 5.6704\text{e-}8 \text{ W}\cdot\text{m}^{-2}\cdot\text{K}^{-4}$ ,
  - $T_c$  = case temperature of pyrgeometer (K).
- $I$  = reference irradiance ( $\text{W}/\text{m}^2$ ), beam (B) or global (G)
  - where,  $G = B * \text{COS}(Z) + D$ ,
  - $Z$  = zenith angle (degrees),
  - $D$  = reference diffuse irradiance ( $\text{W}/\text{m}^2$ ).

Figure 1. Responsivity vs Zenith Angle

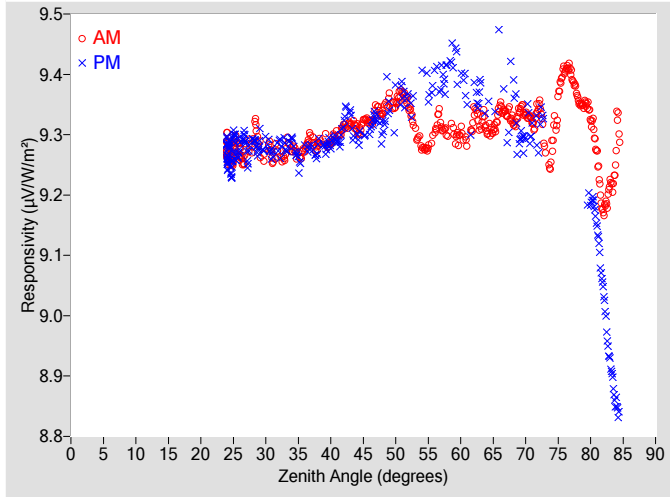


Figure 2. Responsivity vs Local Standard Time

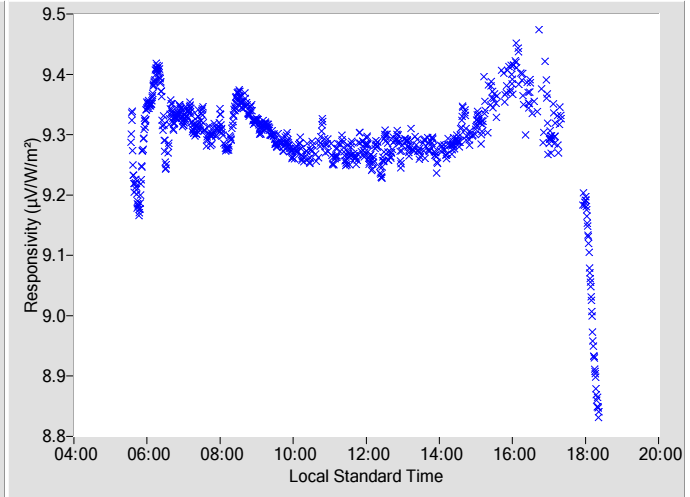
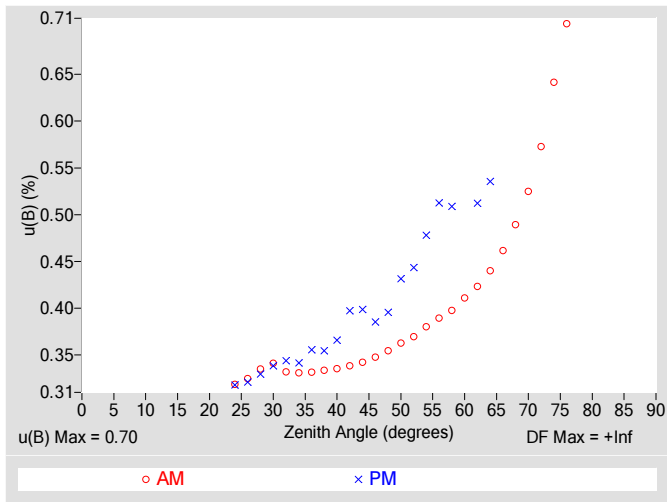


Table 2. Instrument Responsivity (R) and Calibration Type-B Standard Uncertainty, u(B)

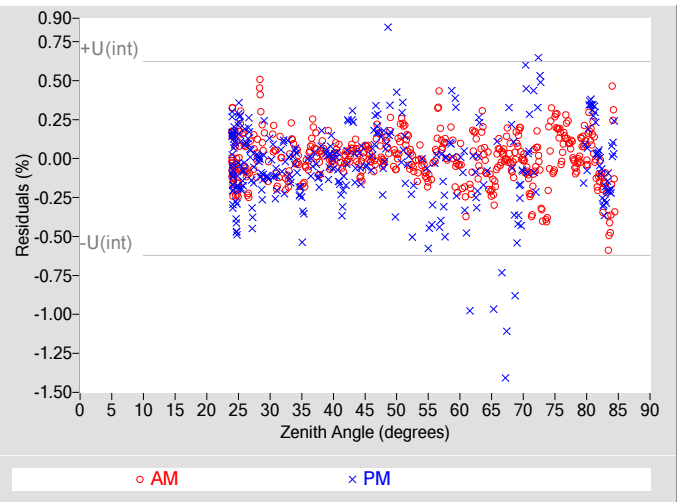
Zenith			AM			PM			Zenith			AM			PM		
Angle	R	u(B)	Azimuth	R	u(B)	Azimuth	Angle	R	u(B)	Azimuth	R	u(B)	Azimuth	R	u(B)	Azimuth	
(deg.)	( $\mu\text{V}/\text{W}/\text{m}^2$ )	$\pm$ (%)	Angle	( $\mu\text{V}/\text{W}/\text{m}^2$ )	$\pm$ (%)	Angle	(deg.)	( $\mu\text{V}/\text{W}/\text{m}^2$ )	$\pm$ (%)	Angle	( $\mu\text{V}/\text{W}/\text{m}^2$ )	$\pm$ (%)	Angle	( $\mu\text{V}/\text{W}/\text{m}^2$ )	$\pm$ (%)	Angle	
0	N/A	N/A	N/A	N/A	N/A	N/A	46	9.3222	0.35	108.28	9.3079	0.39	252.00				
2	N/A	N/A	N/A	N/A	N/A	N/A	48	9.3367	0.35	105.96	9.3061	0.40	254.20				
4	N/A	N/A	N/A	N/A	N/A	N/A	50	9.3518	0.36	103.77	9.3429	0.43	256.26				
6	N/A	N/A	N/A	N/A	N/A	N/A	52	9.3480	0.37	101.67	9.3674	0.44	258.36				
8	N/A	N/A	N/A	N/A	N/A	N/A	54	9.2781	0.38	99.71	9.4068	0.48	260.47				
10	N/A	N/A	N/A	N/A	N/A	N/A	56	9.3051	0.39	97.76	9.4098	0.51	262.47				
12	N/A	N/A	N/A	N/A	N/A	N/A	58	9.2983	0.40	96.07	9.4153	0.51	263.96				
14	N/A	N/A	N/A	N/A	N/A	N/A	60	9.3036	0.41	94.23	9.4018	N/A	266.04				
16	N/A	N/A	N/A	N/A	N/A	N/A	62	9.3293	0.42	92.48	9.3866	0.51	267.75				
18	N/A	N/A	N/A	N/A	N/A	N/A	64	9.3074	0.44	90.81	9.3451	0.54	269.37				
20	N/A	N/A	N/A	N/A	N/A	N/A	66	9.3439	0.46	89.12	9.4742	N/A	270.91				
22	N/A	N/A	N/A	N/A	N/A	N/A	68	9.3222	0.49	87.46	9.3756	N/A	272.84				
24	9.2733	0.32	174.58	9.2697	0.32	185.11	70	9.3338	0.52	85.87	9.2955	N/A	274.16				
26	9.2694	0.32	153.68	9.2786	0.32	205.56	72	9.3471	0.57	84.25	9.2898	N/A	275.91				
28	9.2820	0.34	144.62	9.2914	0.33	216.22	74	9.2701	0.64	82.63	N/A	N/A	N/A				
30	9.2676	0.34	138.04	9.2844	0.34	222.75	76	9.4074	0.70	81.02	N/A	N/A	N/A				
32	9.2730	0.33	132.18	9.2808	0.34	228.52	78	9.3638	N/A	79.45	N/A	N/A	N/A				
34	9.2750	0.33	126.67	9.2898	0.34	233.19	80	9.3276	N/A	77.80	9.1916	N/A	282.41				
36	9.2782	0.33	122.85	9.2832	0.36	237.12	82	9.1761	N/A	76.15	9.0380	N/A	284.02				
38	9.2827	0.33	119.46	9.2763	0.35	240.65	84	9.2925	N/A	74.49	8.8503	N/A	285.70				
40	9.2864	0.34	116.28	9.2827	0.37	243.89	86	N/A	N/A	N/A	N/A	N/A	N/A				
42	9.3130	0.34	113.35	9.3284	0.40	246.93	88	N/A	N/A	N/A	N/A	N/A	N/A				
44	9.3115	0.34	110.70	9.2958	0.40	249.65	90	N/A	N/A	N/A	N/A	N/A	N/A				

N/A - Not Available

**Figure 3. Type-B Standard Uncertainty vs Zenith Angle**



**Figure 4. Residuals from Spline Interpolation**



**Table 3. Uncertainty using Spline Interpolation ‡**

Type-B Standard Uncertainty, $u(B)$ (%)	$\pm 0.70$
Type-A Interpolating Function, $u(int)$ (%)	$\pm 0.31$
Combined Standard Uncertainty, $u(c)$ (%)	$\pm 0.77$
Effective degrees of freedom, $DF(c)$	24535
Coverage factor, $k$	1.96
Expanded Uncertainty, $U95$ (%)	$\pm 1.5$
AM Valid zenith angle range	24° to 76°
PM Valid zenith angle range	24° to 64°

‡ An illustration for how to reduce the uncertainty in calculating the irradiance using a function rather than  $R@45^\circ$ . Not accredited.

**Table 4. Calibration Label Values**

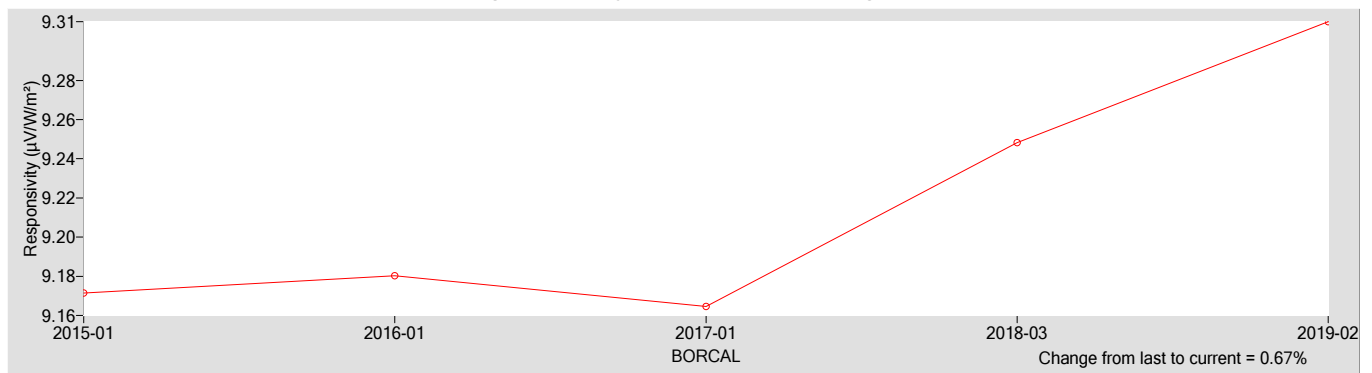
$R @ 45^\circ$ ( $\mu V/W/m^2$ )	$R_{net}$ ( $\mu V/W/m^2$ ) †
9.3100	0.20000

†  $R_{net}$  determination date: Estimated

**Table 5. Uncertainty using  $R @ 45^\circ$**

Type-B Expanded Uncertainty, $U(B)$ (%)	$\pm 1.0$
Offset Uncertainty, $U(off)$ (%)	+1.1 / -0.45
Expanded Uncertainty, $U$ (%)	+2.1 / -1.5
Effective degrees of freedom, $DF$	+Inf
Coverage factor, $k$	1.96
Valid zenith angle range	30.0° to 60.0°

**Figure 5. History of instrument at Zenith Angle = 45°**



**References:**

[1] Reda, I.; Hickey, J.; Long, C.; Myers, D.; Stoffel, T.; Wilcox, S.; Michalsky, J. J.; Dutton, E. G.; Nelson, D. (2005). "Using a Blackbody to Calculate Net Longwave Responsivity of Shortwave Solar Pyranometers to Correct for Their Thermal Offset Error During Outdoor Calibration Using the Component Sum Method." Journal of Atmospheric and Oceanic Technology. , 2005; pp. 1531-1540; NREL Report No. JA-560-36646. doi:10.1175/JTECH1782.1

[2] Reda, I.; Myers, D.; Stoffel, T. (2008). "Uncertainty Estimate for the Outdoor Calibration of Solar Pyranometers: A Metrologist Perspective." Measure. (NCSLI Journal of Measurement Science). Vol. 3(4), December 2008; pp. 58-66; NREL Report No. JA-581-4137

[3] Reda, I.; Andreas, A. (2004). "Solar Position Algorithm for Solar Radiation Applications." Solar Energy. Vol. 76(5), 2004; pp. 577-589; NREL Report No. JA-560-35518. doi:10.1016/j.solener.2003.12.003

[4] Stoffel, T.; Reda, I. (2009). "NREL Pyrheliometer Comparisons: 22 September - 3 October 2008 (NPC-2008)." 54 pp.; NREL Report No. TP-550-45016.

[5] Reda, I.; Stoffel, T.; Myers, D. (2003). "Method to Calibrate a Solar Pyranometer for Measuring Reference Diffuse Irradiance." Solar Energy. Vol. 74, 2003; pp. 103-112; NREL Report No. JA-560-35025. doi:10.1016/S0038-092X(03)00124-5

[6] Reda, I. (1996). Calibration of a Solar Absolute Cavity Radiometer with Traceability to the World Radiometric Reference. 79 pp.; NREL Report No. TP-463-20619.

[7] Reda, I.; Gröbner, J.; Stoffel, T.; Myers, D.; Forgan, B. (2008). Improvements in the Blackbody Calibration of Pyrgeometers. ARM 2008 Science Team Meeting (Poster).



# National Renewable Energy Laboratory

## Solar Radiation Research Laboratory

### Metrology Laboratory

### Calibration Certificate



<b>Test Instrument:</b>	Pyranometer	<b>Manufacturer:</b>	EKO
<b>Model:</b>	MS-80	<b>Serial Number:</b>	S17096005
<b>Calibration Date:</b>	5/3/2019	<b>Due Date:</b>	5/3/2020
<b>Customer:</b>	NREL-SRRL-BMS	<b>Environmental Conditions:</b>	see page 4
<b>Test Dates:</b>	5/3		

This certifies that the above product was calibrated in compliance with ISO/IEC 17025:2005. Measurement uncertainties at the time of calibration are consistent with the Guide to the Expression of Uncertainty in Measurement (GUM) using Reda et al., 2008. All nominal values are traceable to the International System (SI) Units of Measurement.

No statement of compliance with specifications is made or implied on this certificate. However, the estimated uncertainties are the uncertainties of the calibration process; users must add other uncertainties that are relevant to their measuring system, environmental and sky conditions, outdoor set-up, and site location.

The Type-B Standard Uncertainty of using the responsivity at each even zenith angle is reported, and the Expanded Uncertainty of the calibration is reported using two methods:

1. The Expanded Uncertainty of using the responsivity at zenith angle = 45°, within the zenith angle range from 30.0° to 60.0°
2. The Expanded Uncertainty of using Spline Interpolating Functions for the responsivity versus zenith angle.

This certificate applies only to the item identified above and shall not be reproduced other than in full, without specific written approval from the calibration facility. Certificate without signature is not valid.

**Table 1. Traceability**

Measurement Type	Instrument	Calibration Date	Calibration Due Date
Beam Irradiance †	Eppley Absolute Cavity Radiometer Model HF, S/N 29219	09/24/2018	09/24/2019
Diffuse Irradiance †	Hukseflux Pyranometer Model SR25, S/N 2541	04/19/2019	04/19/2020
Diffuse Irradiance †	Hukseflux Pyranometer Model SR25, S/N 2542	04/19/2019	04/19/2020
Data Acquisition	NREL Data Acquisition System Model RAP-DAQ, S/N 2005-998	02/14/2019	02/14/2021
Data Acquisition	NREL Data Acquisition System Model RAP-DAQ, S/N 2005-999	02/14/2019	02/14/2021
Infrared Irradiance ‡	Kipp & Zonen Pyrgeometer Model CG4, S/N FT002	04/16/2018	04/16/2022

† Through the World Radiometric Reference (WRR)

‡ Through the World Infrared Standard Group (WISG)

**Number of pages of certificate:** 4

**Calibration Procedure:** BORCAL-P00-Calibration and QA Procedure; available upon request.

**Setup:** Radiometers are calibrated outdoors, using the sun as the source. Pyranometers and pyrgeometers are installed for horizontal measurements, with their signal connectors oriented north, if their design permits.

The shading disk for the reference diffuse subtends a solid angle of 5°. Pyrheliometers are installed on solar trackers.

**Calibrated by:** RCC

-----  
Ibrahim Reda, Technical Manager

-----  
Date

For questions or comments, please contact the technical manager at:

ibrahim.reda@nrel.gov; 303-384-6385; 15013 Denver West Parkway, Golden, CO 80401, USA

# Calibration Results

## S17096005 EKO MS-80

The responsivity ( $R$ ,  $\mu\text{V}/\text{W}/\text{m}^2$ ) of the test instrument during calibration is calculated using this Measurement Equation:

$$R = (V - R_{net} * W_{net}) / I \tag{1}$$

where,

- $V$  = radiometer output voltage (microvolts),
  - $R_{net}$  = radiometer net infrared responsivity ( $\mu\text{V}/\text{W}/\text{m}^2$ ), see Table 4,
  - $W_{net}$  = effective net infrared measured by pyrgeometer ( $\text{W}/\text{m}^2$ ),
  - =  $W_{in} - W_{out} = W_{in} - \sigma * T_c^4$
  - where,  $W_{in}$  = incoming infrared ( $\text{W}/\text{m}^2$ ),  $\sigma = 5.6704\text{e-}8 \text{ W}\cdot\text{m}^{-2}\cdot\text{K}^{-4}$ ,
  - $T_c$  = case temperature of pyrgeometer (K).
- $I$  = reference irradiance ( $\text{W}/\text{m}^2$ ), beam (B) or global (G)
  - where,  $G = B * \text{COS}(Z) + D$ ,
  - $Z$  = zenith angle (degrees),
  - $D$  = reference diffuse irradiance ( $\text{W}/\text{m}^2$ ).

Figure 1. Responsivity vs Zenith Angle

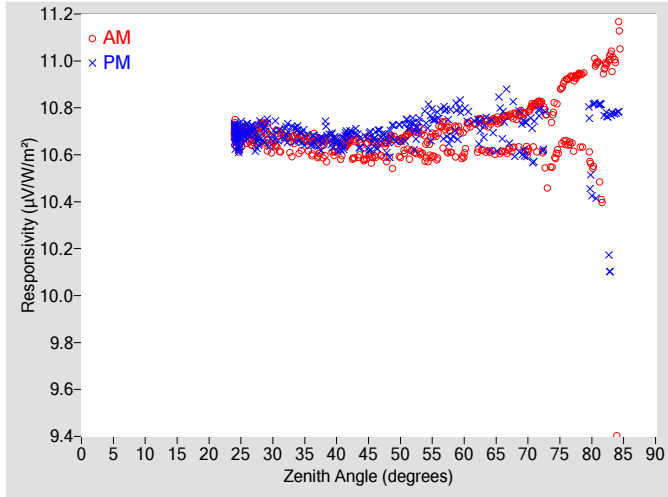


Figure 2. Responsivity vs Local Standard Time

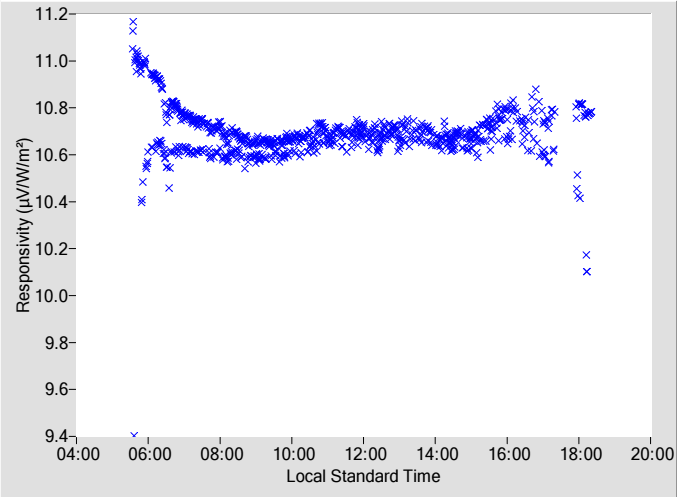


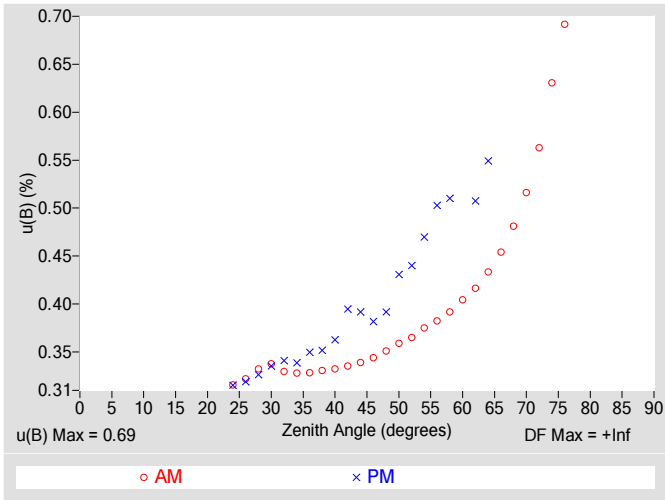
Table 2. Instrument Responsivity (R) and Calibration Type-B Standard Uncertainty, u(B)

Zenith Angle (deg.)	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	AM u(B) $\pm$ (%)	Azimuth Angle	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	PM u(B) $\pm$ (%)	Azimuth Angle	Zenith Angle (deg.)	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	AM u(B) $\pm$ (%)	Azimuth Angle	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	PM u(B) $\pm$ (%)	Azimuth Angle
0	N/A	N/A	N/A	N/A	N/A	N/A	46	10.628	0.34	108.29	10.668	0.38	251.88
2	N/A	N/A	N/A	N/A	N/A	N/A	48	10.625	0.35	105.97	10.630	0.39	254.24
4	N/A	N/A	N/A	N/A	N/A	N/A	50	10.639	0.36	103.78	10.705	0.43	256.30
6	N/A	N/A	N/A	N/A	N/A	N/A	52	10.636	0.36	101.76	10.705	0.44	258.47
8	N/A	N/A	N/A	N/A	N/A	N/A	54	10.628	0.38	99.71	10.745	0.47	260.48
10	N/A	N/A	N/A	N/A	N/A	N/A	56	10.645	0.38	97.91	10.768	0.50	262.22
12	N/A	N/A	N/A	N/A	N/A	N/A	58	10.642	0.39	96.07	10.713	0.51	264.18
14	N/A	N/A	N/A	N/A	N/A	N/A	60	10.622	0.40	94.23	10.798	N/A	266.05
16	N/A	N/A	N/A	N/A	N/A	N/A	62	10.674	0.42	92.48	10.743	0.51	267.80
18	N/A	N/A	N/A	N/A	N/A	N/A	64	10.684	0.43	90.76	10.683	0.55	269.52
20	N/A	N/A	N/A	N/A	N/A	N/A	66	10.708	0.45	89.13	10.731	N/A	271.12
22	N/A	N/A	N/A	N/A	N/A	N/A	68	10.742	0.48	87.47	10.709	N/A	272.53
24	10.696	0.32	174.94	10.687	0.32	185.25	70	10.652	0.52	85.88	10.592	N/A	274.12
26	10.689	0.32	153.75	10.699	0.32	205.92	72	10.787	0.56	84.25	10.725	N/A	275.92
28	10.695	0.33	144.29	10.702	0.33	215.85	74	10.702	0.63	82.64	N/A	N/A	N/A
30	10.648	0.34	137.42	10.686	0.34	222.76	76	10.784	0.69	81.03	N/A	N/A	N/A
32	10.676	0.33	131.81	10.685	0.34	228.46	78	10.881	N/A	79.42	N/A	N/A	N/A
34	10.662	0.33	126.97	10.697	0.34	233.01	80	10.557	N/A	77.81	10.553	N/A	282.35
36	10.643	0.33	123.05	10.655	0.35	237.36	82	10.971	N/A	76.11	10.775	N/A	284.12
38	10.635	0.33	119.39	10.688	0.35	240.62	84	10.521	N/A	74.51	10.781	N/A	285.78
40	10.639	0.33	116.26	10.650	0.36	243.93	86	N/A	N/A	N/A	N/A	N/A	N/A
42	10.657	0.34	113.41	10.693	0.39	246.80	88	N/A	N/A	N/A	N/A	N/A	N/A
44	10.612	0.34	110.61	10.630	0.39	249.07	90	N/A	N/A	N/A	N/A	N/A	N/A

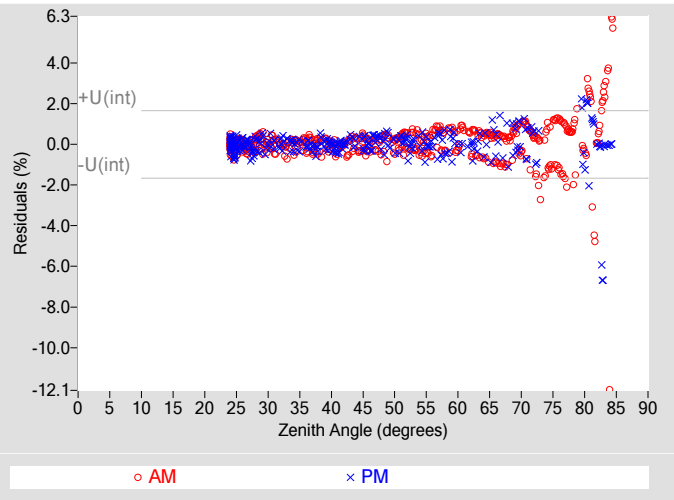
N/A - Not Available



**Figure 3. Type-B Standard Uncertainty vs Zenith Angle**



**Figure 4. Residuals from Spline Interpolation**



**Table 3. Uncertainty using Spline Interpolation ‡**

Type-B Standard Uncertainty, u(B) (%)	±0.69
Type-A Interpolating Function, u(int) (%)	±0.83
Combined Standard Uncertainty, u(c) (%)	±1.1
Effective degrees of freedom, DF(c)	2001
Coverage factor, k	1.96
Expanded Uncertainty, U95 (%)	±2.1
AM Valid zenith angle range	24° to 76°
PM Valid zenith angle range	24° to 64°

‡ An illustration for how to reduce the uncertainty in calculating the irradiance using a function rather than R@45°. Not accredited.

**Table 4. Calibration Label Values**

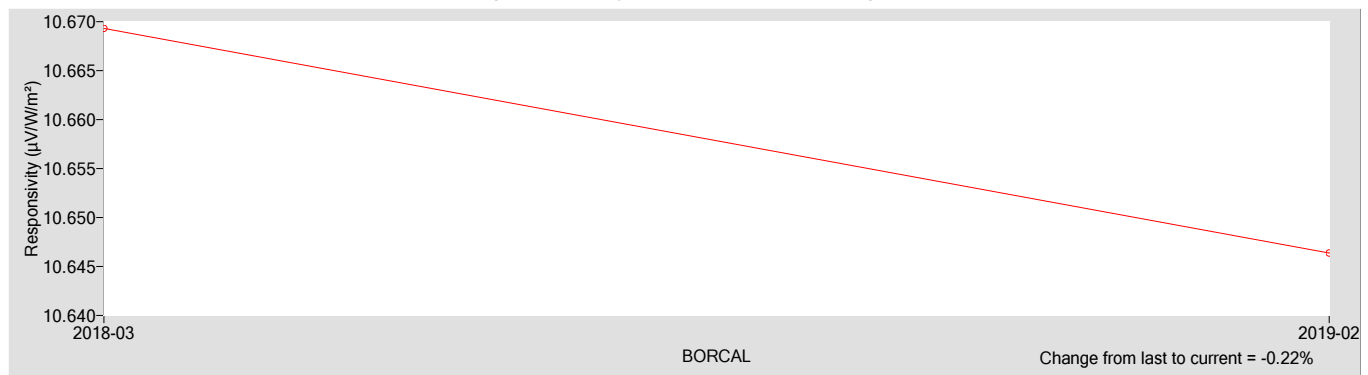
R @ 45° (μV/W/m²)	Rnet (μV/W/m²) †
10.646	0.043000

† Rnet determination date: Estimated

**Table 5. Uncertainty using R @ 45°**

Type-B Expanded Uncertainty, U(B) (%)	±1.00
Offset Uncertainty, U(off) (%)	+1.4 / -0.32
Expanded Uncertainty, U (%)	+2.4 / -1.3
Effective degrees of freedom, DF	+Inf
Coverage factor, k	1.96
Valid zenith angle range	30.0° to 60.0°

**Figure 5. History of instrument at Zenith Angle = 45°**



**References:**

[1] Reda, I.; Hickey, J.; Long, C.; Myers, D.; Stoffel, T.; Wilcox, S.; Michalsky, J. J.; Dutton, E. G.; Nelson, D. (2005). "Using a Blackbody to Calculate Net Longwave Responsivity of Shortwave Solar Pyranometers to Correct for Their Thermal Offset Error During Outdoor Calibration Using the Component Sum Method." *Journal of Atmospheric and Oceanic Technology.* , 2005; pp. 1531-1540; NREL Report No. JA-560-36646. doi:10.1175/JTECH1782.1

[2] Reda, I.; Myers, D.; Stoffel, T. (2008). "Uncertainty Estimate for the Outdoor Calibration of Solar Pyranometers: A Metrologist Perspective." *Measure.* (NCSLI Journal of Measurement Science). Vol. 3(4), December 2008; pp. 58-66; NREL Report No. JA-581-4137

[3] Reda, I.; Andreas, A. (2004). "Solar Position Algorithm for Solar Radiation Applications." *Solar Energy.* Vol. 76(5), 2004; pp. 577-589; NREL Report No. JA-560-35518. doi:10.1016/j.solener.2003.12.003

[4] Stoffel, T.; Reda, I. (2009). "NREL Pyrheliometer Comparisons: 22 September - 3 October 2008 (NPC-2008)." 54 pp.; NREL Report No. TP-550-45016.

[5] Reda, I.; Stoffel, T.; Myers, D. (2003). "Method to Calibrate a Solar Pyranometer for Measuring Reference Diffuse Irradiance." *Solar Energy.* Vol. 74, 2003; pp. 103-112; NREL Report No. JA-560-35025. doi:10.1016/S0038-092X(03)00124-5

[6] Reda, I. (1996). *Calibration of a Solar Absolute Cavity Radiometer with Traceability to the World Radiometric Reference.* 79 pp.; NREL Report No. TP-463-20619.

[7] Reda, I.; Gröbner, J.; Stoffel, T.; Myers, D.; Forgan, B. (2008). *Improvements in the Blackbody Calibration of Pyrgeometers.* ARM 2008 Science Team Meeting (Poster).



# National Renewable Energy Laboratory

## Solar Radiation Research Laboratory

### Metrology Laboratory

### Calibration Certificate



<b>Test Instrument:</b>	Pyrheliometer	<b>Manufacturer:</b>	EKO
<b>Model:</b>	MS-57	<b>Serial Number:</b>	S18015.22
<b>Calibration Date:</b>	5/3/2019	<b>Due Date:</b>	5/3/2020
<b>Customer:</b>	NREL-SRRL-BMS	<b>Environmental Conditions:</b>	see page 4
<b>Test Dates:</b>	5/3		

This certifies that the above product was calibrated in compliance with ISO/IEC 17025:2005. Measurement uncertainties at the time of calibration are consistent with the Guide to the Expression of Uncertainty in Measurement (GUM) using Reda et al., 2008. All nominal values are traceable to the International System (SI) Units of Measurement.

No statement of compliance with specifications is made or implied on this certificate. However, the estimated uncertainties are the uncertainties of the calibration process; users must add other uncertainties that are relevant to their measuring system, environmental and sky conditions, outdoor set-up, and site location.

The Type-B Standard Uncertainty of using the responsivity at each even zenith angle is reported, and the Expanded Uncertainty of the calibration is reported using two methods:

1. The Expanded Uncertainty of using the responsivity at zenith angle = 45°, within the zenith angle range from 30.0° to 60.0°
2. The Expanded Uncertainty of using Spline Interpolating Functions for the responsivity versus zenith angle.

This certificate applies only to the item identified above and shall not be reproduced other than in full, without specific written approval from the calibration facility. Certificate without signature is not valid.

**Table 1. Traceability**

Measurement Type	Instrument	Calibration Date	Calibration Due Date
Beam Irradiance †	Eppley Absolute Cavity Radiometer Model HF, S/N 29219	09/24/2018	09/24/2019
Diffuse Irradiance †	Hukseflux Pyranometer Model SR25, S/N 2541	04/19/2019	04/19/2020
Diffuse Irradiance †	Hukseflux Pyranometer Model SR25, S/N 2542	04/19/2019	04/19/2020
Data Acquisition	NREL Data Acquisition System Model RAP-DAQ, S/N 2005-998	02/14/2019	02/14/2021
Data Acquisition	NREL Data Acquisition System Model RAP-DAQ, S/N 2005-999	02/14/2019	02/14/2021

† Through the World Radiometric Reference (WRR)

**Number of pages of certificate:** 4

**Calibration Procedure:** BORCAL-P00-Calibration and QA Procedure; available upon request.

**Setup:** Radiometers are calibrated outdoors, using the sun as the source. Pyranometers and pyrgeometers are installed for horizontal measurements, with their signal connectors oriented north, if their design permits.

The shading disk for the reference diffuse subtends a solid angle of 5°. Pyrheliometers are installed on solar trackers.

**Calibrated by:** RCC

-----  
Ibrahim Reda, Technical Manager

-----  
Date

For questions or comments, please contact the technical manager at:

ibrahim.reda@nrel.gov; 303-384-6385; 15013 Denver West Parkway, Golden, CO 80401, USA

# Calibration Results

## S18015.22 EKO MS-57

The responsivity ( $R$ ,  $\mu\text{V}/\text{W}/\text{m}^2$ ) of the test instrument during calibration is calculated using this Measurement Equation:

$$R = (V - R_{net} * W_{net}) / I \tag{1}$$

where,

- $V$  = radiometer output voltage (microvolts),
  - $R_{net}$  = radiometer net infrared responsivity ( $\mu\text{V}/\text{W}/\text{m}^2$ ), see Table 4,
  - $W_{net}$  = effective net infrared measured by pyrgeometer ( $\text{W}/\text{m}^2$ ),
  - =  $W_{in} - W_{out} = W_{in} - \sigma * T_c^4$
  - where,  $W_{in}$  = incoming infrared ( $\text{W}/\text{m}^2$ ),  $\sigma = 5.6704\text{e-}8 \text{ W}\cdot\text{m}^{-2}\cdot\text{K}^{-4}$ ,
  - $T_c$  = case temperature of pyrgeometer (K).
- $I$  = reference irradiance ( $\text{W}/\text{m}^2$ ), beam (B) or global (G)
  - where,  $G = B * \text{COS}(Z) + D$ ,
  - $Z$  = zenith angle (degrees),
  - $D$  = reference diffuse irradiance ( $\text{W}/\text{m}^2$ ).

Figure 1. Responsivity vs Zenith Angle

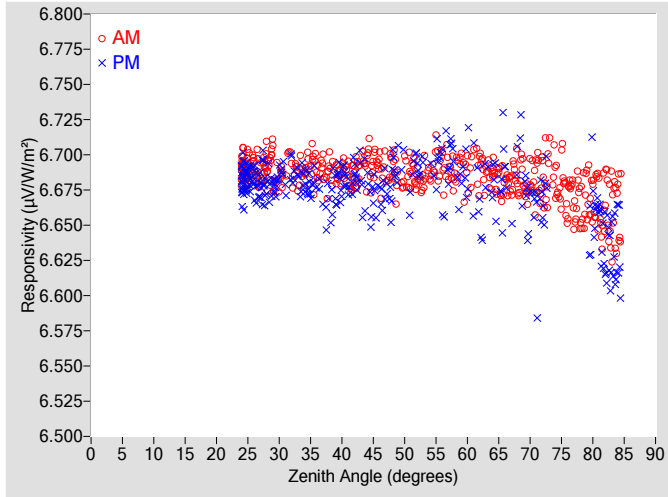


Figure 2. Responsivity vs Local Standard Time

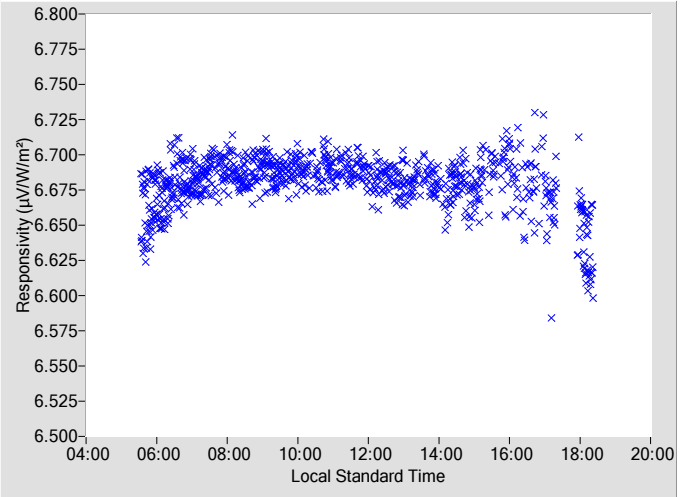
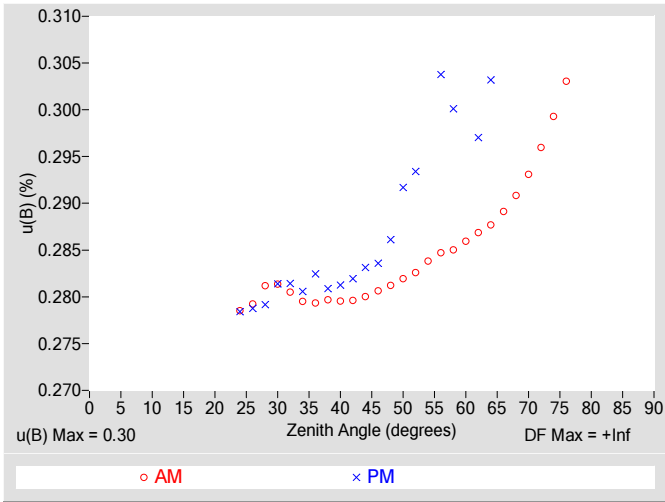


Table 2. Instrument Responsivity (R) and Calibration Type-B Standard Uncertainty, u(B)

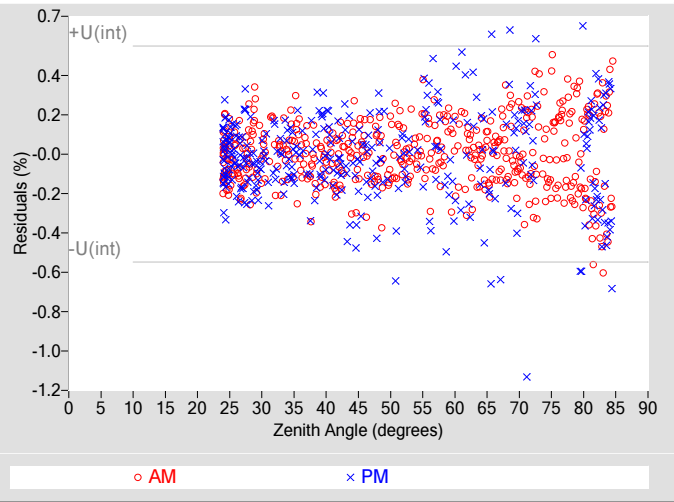
Zenith Angle (deg.)	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	AM u(B) $\pm$ (%)	Azimuth Angle	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	PM u(B) $\pm$ (%)	Azimuth Angle	Zenith Angle (deg.)	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	AM u(B) $\pm$ (%)	Azimuth Angle	R ( $\mu\text{V}/\text{W}/\text{m}^2$ )	PM u(B) $\pm$ (%)	Azimuth Angle
0	N/A	N/A	N/A	N/A	N/A	N/A	46	6.6904	0.28	108.32	6.6733	0.28	251.94
2	N/A	N/A	N/A	N/A	N/A	N/A	48	6.6917	0.28	105.93	6.6813	0.29	254.18
4	N/A	N/A	N/A	N/A	N/A	N/A	50	6.6860	0.28	103.73	6.7037	0.29	256.20
6	N/A	N/A	N/A	N/A	N/A	N/A	52	6.6819	0.28	101.73	6.6939	0.29	258.48
8	N/A	N/A	N/A	N/A	N/A	N/A	54	6.6859	0.28	99.70	6.6938	N/A	260.63
10	N/A	N/A	N/A	N/A	N/A	N/A	56	6.6914	0.28	97.76	6.6799	0.30	262.32
12	N/A	N/A	N/A	N/A	N/A	N/A	58	6.6845	0.29	95.98	6.6952	0.30	263.96
14	N/A	N/A	N/A	N/A	N/A	N/A	60	6.6865	0.29	94.18	6.6922	N/A	265.90
16	N/A	N/A	N/A	N/A	N/A	N/A	62	6.6921	0.29	92.48	6.6566	0.30	267.64
18	N/A	N/A	N/A	N/A	N/A	N/A	64	6.6863	0.29	90.76	6.6796	0.30	269.42
20	N/A	N/A	N/A	N/A	N/A	N/A	66	6.6794	0.29	89.13	6.6909	N/A	271.02
22	N/A	N/A	N/A	N/A	N/A	N/A	68	6.6809	0.29	87.47	6.6957	N/A	272.61
24	6.6913	0.28	174.17	6.6832	0.28	185.95	70	6.6794	0.29	85.87	6.6584	N/A	274.12
26	6.6925	0.28	154.51	6.6822	0.28	205.76	72	6.6834	0.30	84.25	6.6590	N/A	275.93
28	6.6924	0.28	144.27	6.6805	0.28	215.71	74	6.6859	0.30	82.63	N/A	N/A	N/A
30	6.6831	0.28	136.96	6.6880	0.28	223.03	76	6.6651	0.30	81.02	N/A	N/A	N/A
32	6.6807	0.28	131.84	6.6890	0.28	228.43	78	6.6623	N/A	79.41	N/A	N/A	N/A
34	6.6857	0.28	126.86	6.6814	0.28	233.13	80	6.6709	N/A	77.80	6.6689	N/A	282.48
36	6.6894	0.28	122.90	6.6765	0.28	236.86	82	6.6699	N/A	76.15	6.6299	N/A	284.07
38	6.6922	0.28	119.55	6.6667	0.28	240.58	84	6.6581	N/A	74.44	6.6411	N/A	285.75
40	6.6896	0.28	116.27	6.6761	0.28	243.83	86	N/A	N/A	N/A	N/A	N/A	N/A
42	6.6871	0.28	113.40	6.6881	0.28	246.73	88	N/A	N/A	N/A	N/A	N/A	N/A
44	6.6941	0.28	110.70	6.6832	0.28	249.58	90	N/A	N/A	N/A	N/A	N/A	N/A

N/A - Not Available

**Figure 3. Type-B Standard Uncertainty vs Zenith Angle**



**Figure 4. Residuals from Spline Interpolation**



**Table 3. Uncertainty using Spline Interpolation ‡**

Type-B Standard Uncertainty, u(B) (%)	±0.30
Type-A Interpolating Function, u(int) (%)	±0.27
Combined Standard Uncertainty, u(c) (%)	±0.41
Effective degrees of freedom, DF(c)	3382
Coverage factor, k	1.96
Expanded Uncertainty, U95 (%)	±0.80
AM Valid zenith angle range	24° to 76°
PM Valid zenith angle range	24° to 64°

‡ An illustration for how to reduce the uncertainty in calculating the irradiance using a function rather than R@45°. Not accredited.

**Table 4. Calibration Label Values**

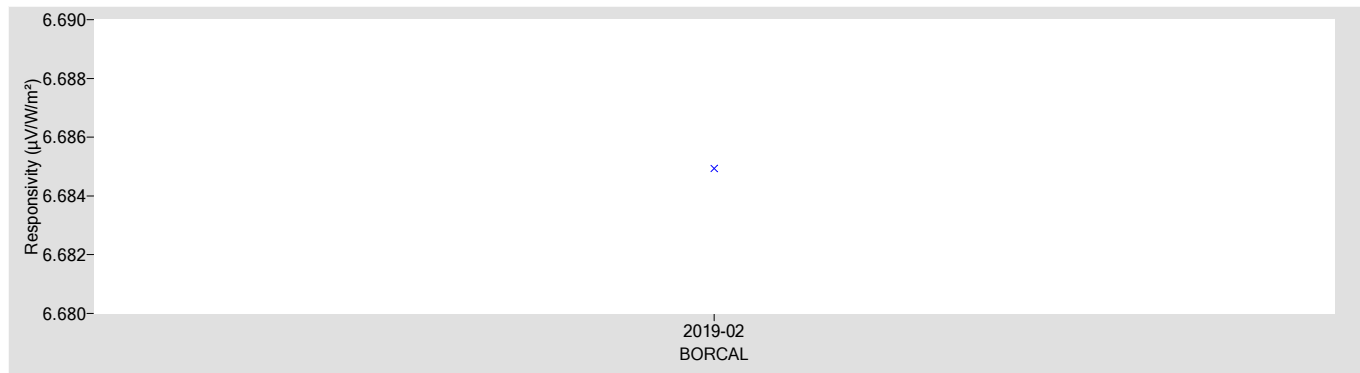
R @ 45° (μV/W/m²)	Rnet (μV/W/m²) †
6.6849	0

† Rnet determination date: N/A

**Table 5. Uncertainty using R @ 45°**

Type-B Expanded Uncertainty, U(B) (%)	±0.60
Offset Uncertainty, U(off) (%)	+0.28 / -0.27
Expanded Uncertainty, U (%)	+0.88 / -0.87
Effective degrees of freedom, DF	+Inf
Coverage factor, k	1.96
Valid zenith angle range	30.0° to 60.0°

**Figure 5. History of instrument at Zenith Angle = 45°**



**References:**

[1] Reda, I.; Hickey, J.; Long, C.; Myers, D.; Stoffel, T.; Wilcox, S.; Michalsky, J. J.; Dutton, E. G.; Nelson, D. (2005). "Using a Blackbody to Calculate Net Longwave Responsivity of Shortwave Solar Pyranometers to Correct for Their Thermal Offset Error During Outdoor Calibration Using the Component Sum Method." Journal of Atmospheric and Oceanic Technology. , 2005; pp. 1531-1540; NREL Report No. JA-560-36646. doi:10.1175/JTECH1782.1

[2] Reda, I.; Myers, D.; Stoffel, T. (2008). "Uncertainty Estimate for the Outdoor Calibration of Solar Pyranometers: A Metrologist Perspective." Measure. (NCSLI Journal of Measurement Science). Vol. 3(4), December 2008; pp. 58-66; NREL Report No. JA-581-4137

[3] Reda, I.; Andreas, A. (2004). "Solar Position Algorithm for Solar Radiation Applications." Solar Energy. Vol. 76(5), 2004; pp. 577-589; NREL Report No. JA-560-35518. doi:10.1016/j.solener.2003.12.003

[4] Stoffel, T.; Reda, I. (2009). "NREL Pyrheliometer Comparisons: 22 September - 3 October 2008 (NPC-2008)." 54 pp.; NREL Report No. TP-550-45016.

[5] Reda, I.; Stoffel, T.; Myers, D. (2003). "Method to Calibrate a Solar Pyranometer for Measuring Reference Diffuse Irradiance." Solar Energy. Vol. 74, 2003; pp. 103-112; NREL Report No. JA-560-35025. doi:10.1016/S0038-092X(03)00124-5

[6] Reda, I. (1996). Calibration of a Solar Absolute Cavity Radiometer with Traceability to the World Radiometric Reference. 79 pp.; NREL Report No. TP-463-20619.

[7] Reda, I.; Gröbner, J.; Stoffel, T.; Myers, D.; Forgan, B. (2008). Improvements in the Blackbody Calibration of Pyrgeometers. ARM 2008 Science Team Meeting (Poster).

# Environmental and Sky Conditions for BORCAL-SW 2019-02

Calibration Facility: Solar Radiation Research Laboratory

Latitude: 39.742°N

Longitude: 105.180°W

Elevation: 1828.8 meters AMSL

Time Zone: -7.0

## Reference Irradiance:

Figure 6. Reference Irradiance

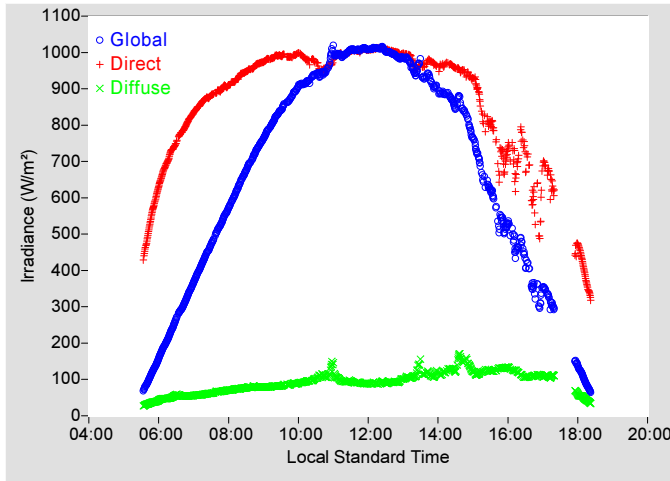
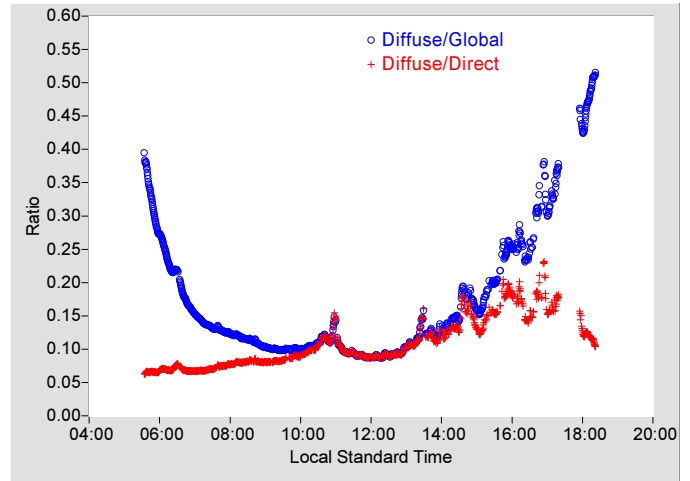


Figure 7. Diffuse Ratios



## Meteorological Observations:

Figure 8. Temperature

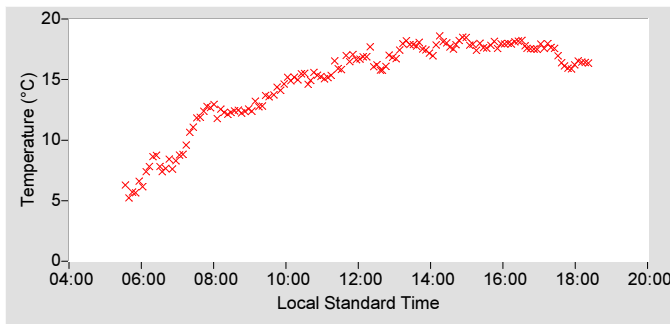


Figure 9. Humidity

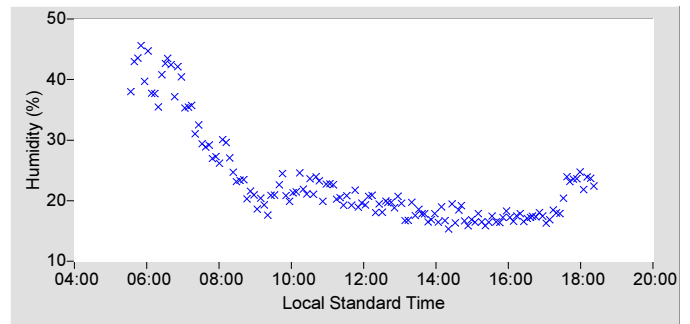


Figure 10. Pressure

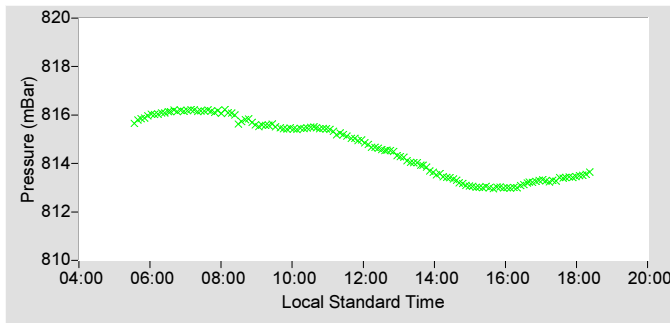


Figure 11. Effective Net Infrared

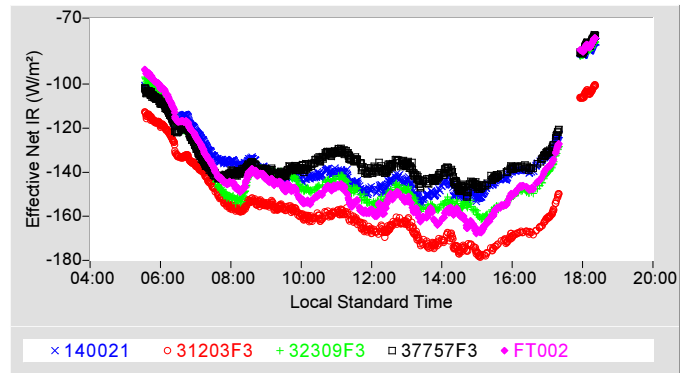


Figure 12. Estimated Broadband Aerosol Optical Depth

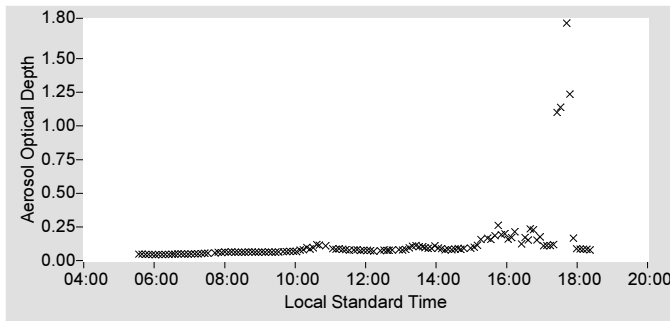


Table 6. Meteorological Observations

Observations	Mean	Min	Max
Temperature (°C)	14.78	5.23	18.60
Humidity (%)	23.16	15.36	45.59
Pressure (mBar)	814.6	813.0	816.2
Est. Aerosol Optical Depth (BB)	0.128	0.044	1.764

For other information about the calibration facility visit: <http://www.nrel.gov/esif/solar-radiation-research-laboratory.html>

# Appendix 2

## BORCAL Notes

Instrument, Configuration, and Session Notes for the BORCAL

# BORCAL Notes

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Facility: Solar Radiation Research Laboratory

Comments:

Avg. Station Pressure & Temperature is for Denver, CO, which is used for the Solar Position Algorithm (SPA).

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Session Config: 1171 Apogee SP-510; Number: 1

Comments:

30K case measured using co-located Apogee Pyrgeometer.